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AUTHORITY
WRDC/IST Notice, 25 Sep 1990

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## Volume II

### Bidirectional Reflectance: Graphic Data

Prepared by  
Target Signature Analysis Center  
Infrared and Optics Division  
Willow Run Laboratories  
The University of Michigan  
Ann Arbor, Michigan

October 1972

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Patterson Air Force Base, Ohio 45433

Air Force Avionics Laboratory  
Air Force Systems Command  
Wright-Patterson Air Force Base, Ohio

**TARGET SIGNATURE ANALYSIS CENTER: DATA COMPILATION  
ELEVENTH SUPPLEMENT**

**Volume II**

**Bidirectional Reflectance: Graphic Data**

Prepared by

Target Signature Analysis Center  
Infrared and Optics Division  
Willow Run Laboratories  
The University of Michigan  
Ann Arbor, Michigan

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Test and Evaluation: 11 Apr 1972. Other requests for  
this document must be submitted to AFAL R&A, Wright-  
Patterson Air Force Base, Ohio 45433

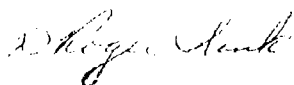
## FOREWORD

The work reported herein, covering the period from 1 November 1969 to 30 July 1972, was carried out by the Infrared and Optics Division of the Willow Run Laboratories, a unit of The University of Michigan's Institute of Science and Technology, Ann Arbor, Michigan. The work was performed under Contract F33615-70-C-1123, Project 6239, Task 10, for the Air Force Avionics Laboratory (AFAL), Air Force Systems Command, Wright-Patterson Air Force Base, Ohio. Volume I contains a definition of the parameters pertinent to the bidirectional reflectance, a discussion of the data, some equations for application of the data, and an index and cross reference of the data contained in Volume II. Bidirectional reflectance data in graphical form are presented in Volume II. The data were reduced and this supplement was prepared by (Mrs.) Sharon Ladd, Dwayne Carmer, Daniel Rice, Dennis Ladd, and John Ulrich under the direction of J. Robert Maxwell. The data reported in this supplement were obtained almost entirely from the laboratory measurements phase of the Target Signature Measurement Program conducted at The University of Michigan, sponsored by the Avionics Laboratory under U. S. Air Force Contracts AF33(615)-3924, F33(615)-66-C-1281 and F33(615)-70-C-1698, under the direction of Max Bair.

The Target Signature program is part of a comprehensive multispectral program at The University of Michigan devoted to the improvement of remote sensing capabilities; this comprehensive program is under the supervision of R. R. Legault, Associate Director of the Willow Run Laboratories. The Principal Investigator for this contract is J. R. Maxwell. The Willow Run Laboratories' number for this report is 32210-41-B (I and II).

This report was submitted by the authors on 10 August 1972.

This technical report has been reviewed and is approved.



D. ROGER SINK, ACTING CHIEF  
Reconnaissance Applications Branch  
Reconnaissance Division  
Air Force Avionics Laboratory



#### ABSTRACT

This report is the eleventh supplement to the Target Signature Analysis Center: Data Compilation and contains 2200 curves of bidirectional reflectance versus angle. The significance of this report to the Air Force is that these data provide the Air Force with essential optical properties-of-materials data to analyze the angular dependence of the reflected radiance from various targets. Volume I contains a definition of the parameters pertinent to the bidirectional reflectance, a discussion of the data, some equations for application of the data, and an index and cross reference of the data contained in Volume II. Bidirectional reflectance data are presented graphically in Volume II.

This supplement to the Target Signature Analysis Center: Data Compilation augments an ordered, indexed compilation of reflectance, radar cross sections, and apparent temperatures of target and background materials. The Data Compilation includes spectral reflectances and transmittances in the optical region from 0.3 to 15  $\mu\text{m}$ , normalized radar cross sections, and apparent temperatures at mm wavelengths. When available, the experimental parameters associated with each curve are listed to provide the user with a description of the important experimental conditions.

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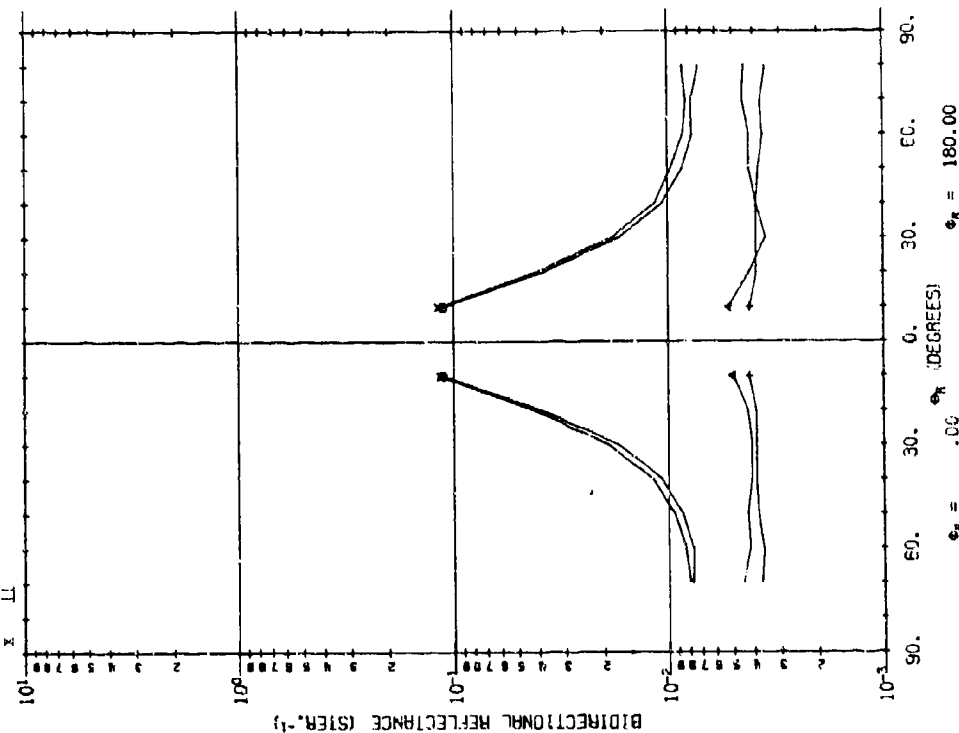
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**PAINT**

R01027 003

ONE COAT OLIVE DRAB PAINT ON TWO COATS  
ZINC CHROMATE (WET BECKED) ON ANODIZED  
ALUMINUM

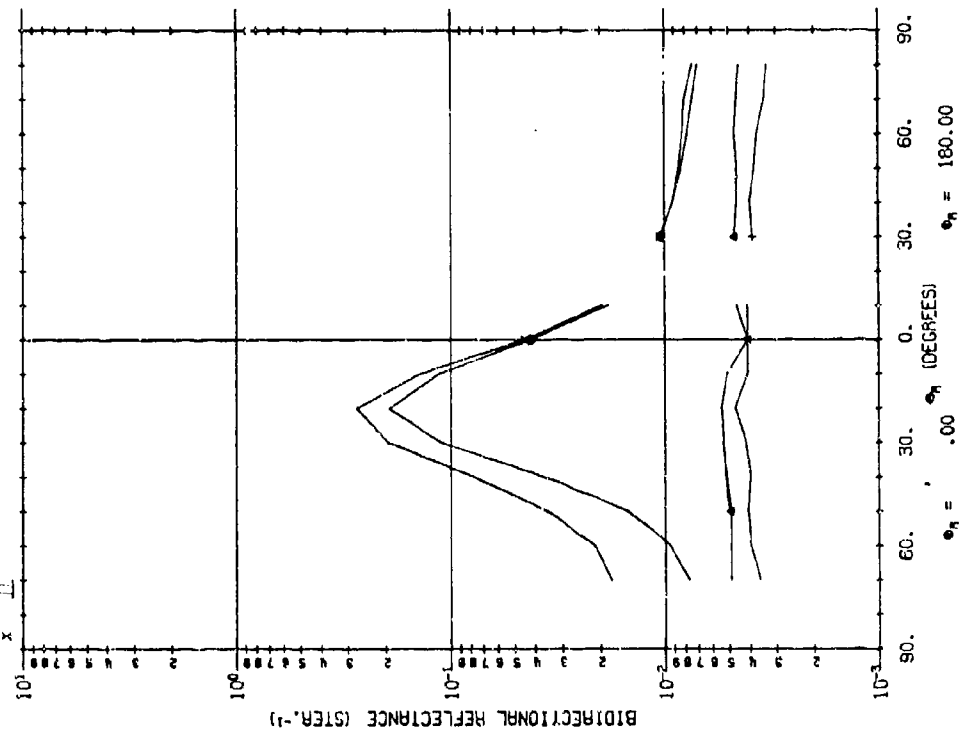
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 $\theta_r = 180.0$   
 $\lambda = 0.63$



R01027 003

ONE COAT OLIVE DRAB PAINT ON TWO COATS  
ZINC CHROMATE (WET BECKED) ON ANODIZED  
ALUMINUM

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 $\theta_r = 180.0$   
 $\lambda = 0.63$

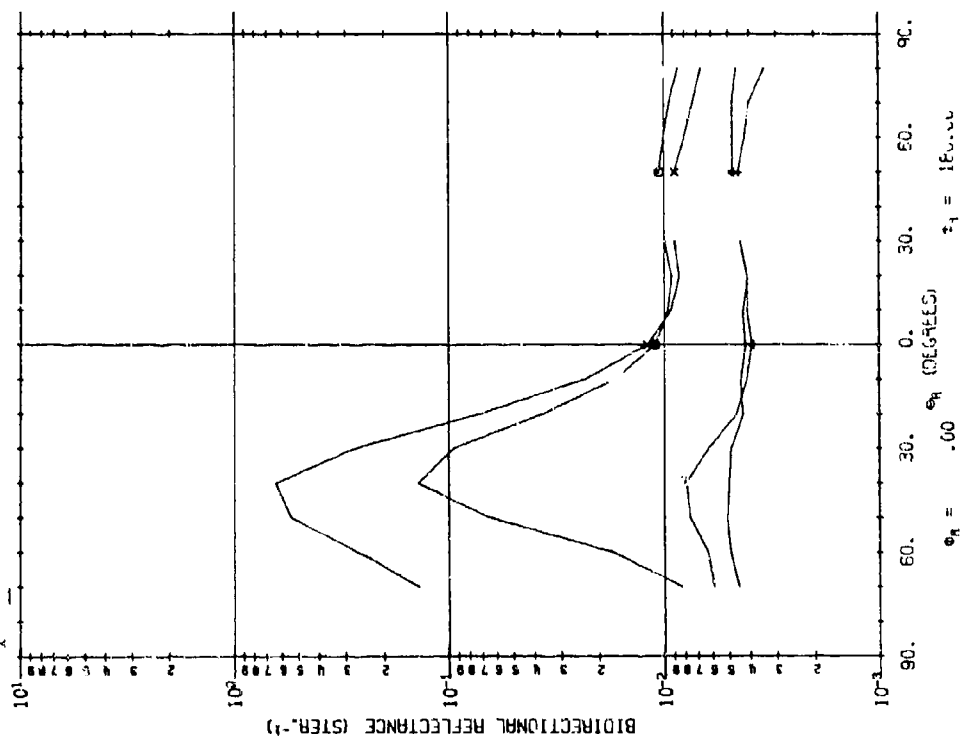


PAINT

A01027 003

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ZINC CHROMATE (NET DECKED) ON ANODIZED  
ALUMINUM

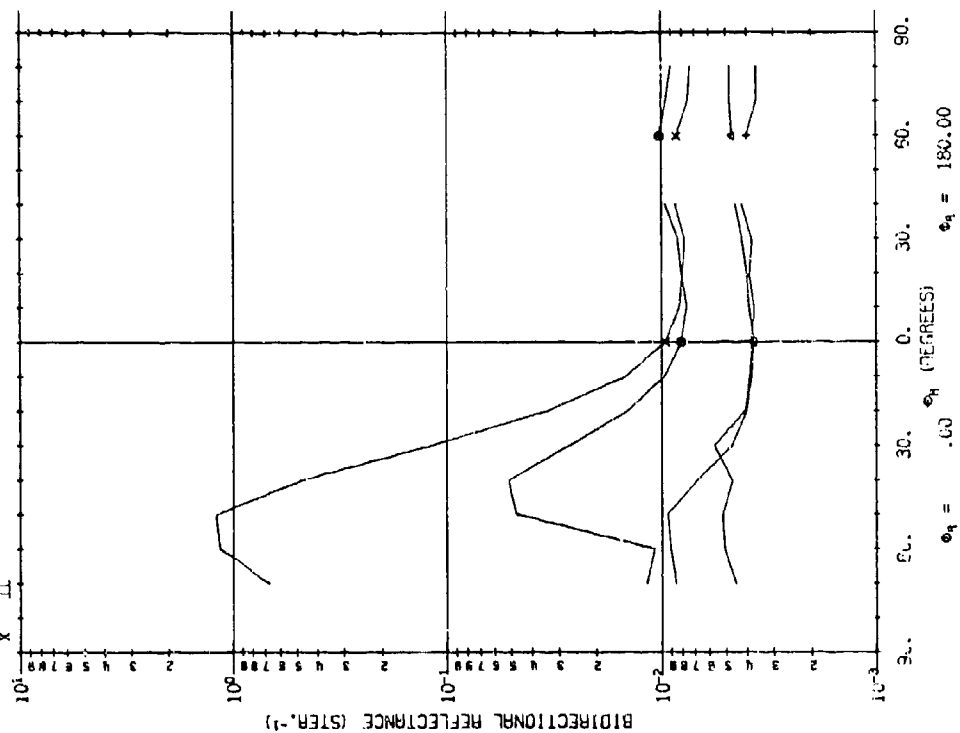
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ALUMINUM

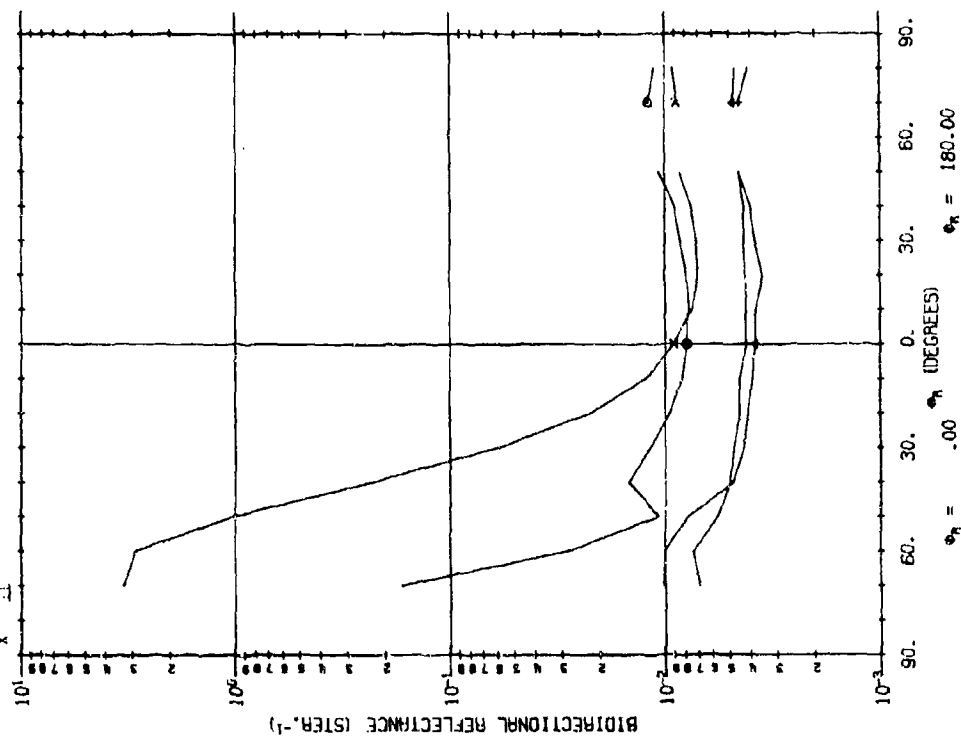
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ALUMINUM

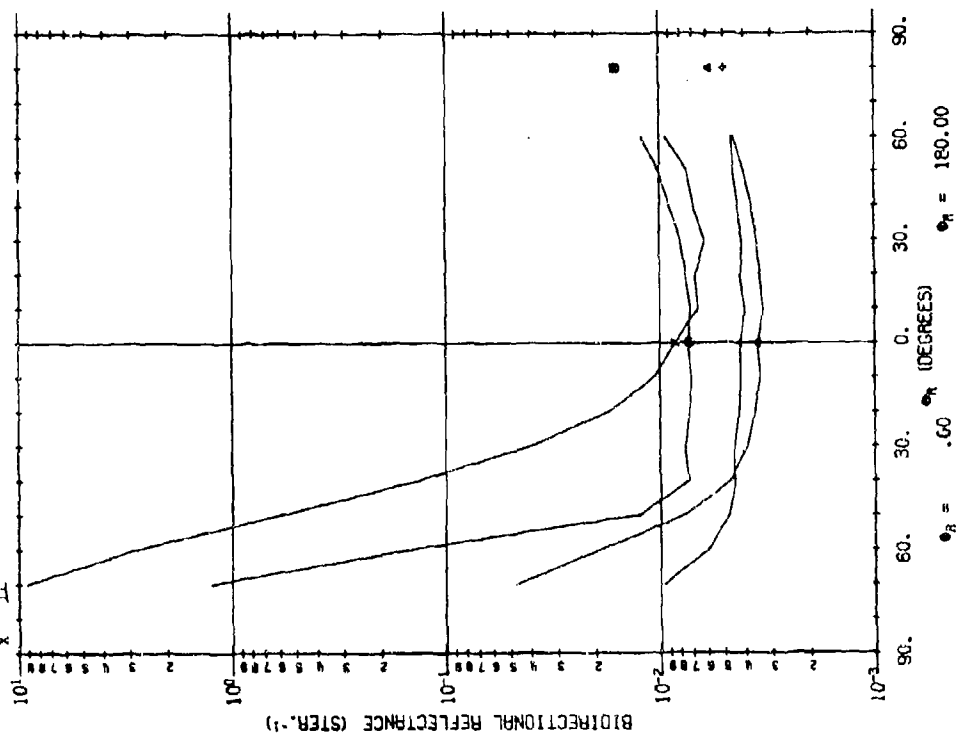
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-  $\theta_i = 0.63$



R01027 003

ONE COAT OLIVE DRAB PAINT ON TWO COATS  
ZINC CHROMATE (WET DECKED) ON ANODIZED  
ALUMINUM

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+  $\theta_i = 180.0$   
-  $\theta_i = 0.63$

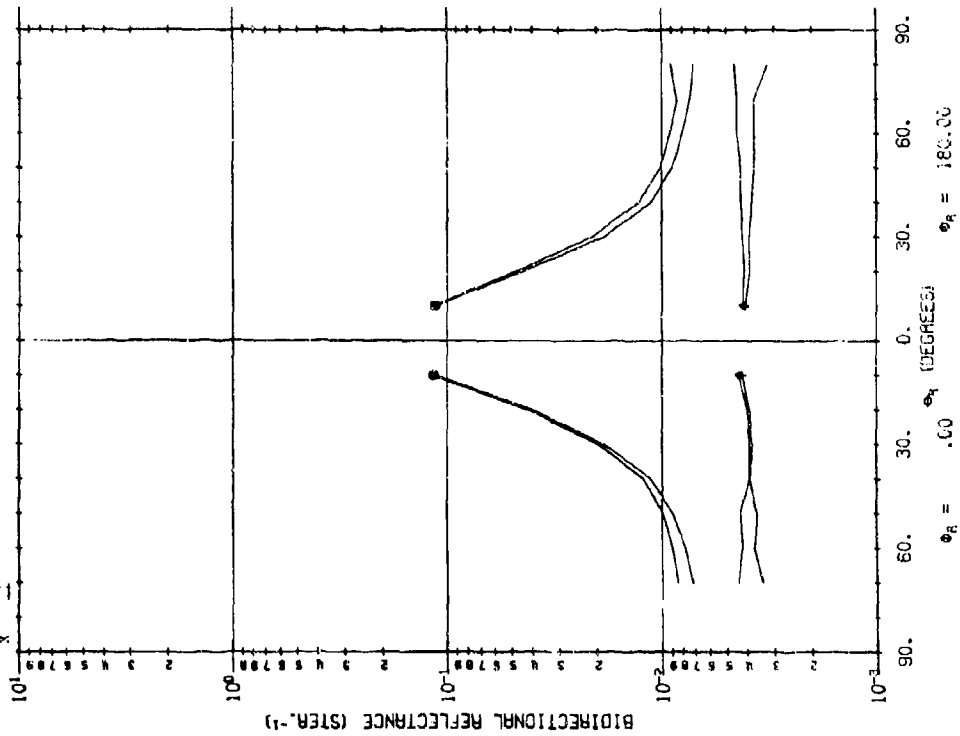


PAIN

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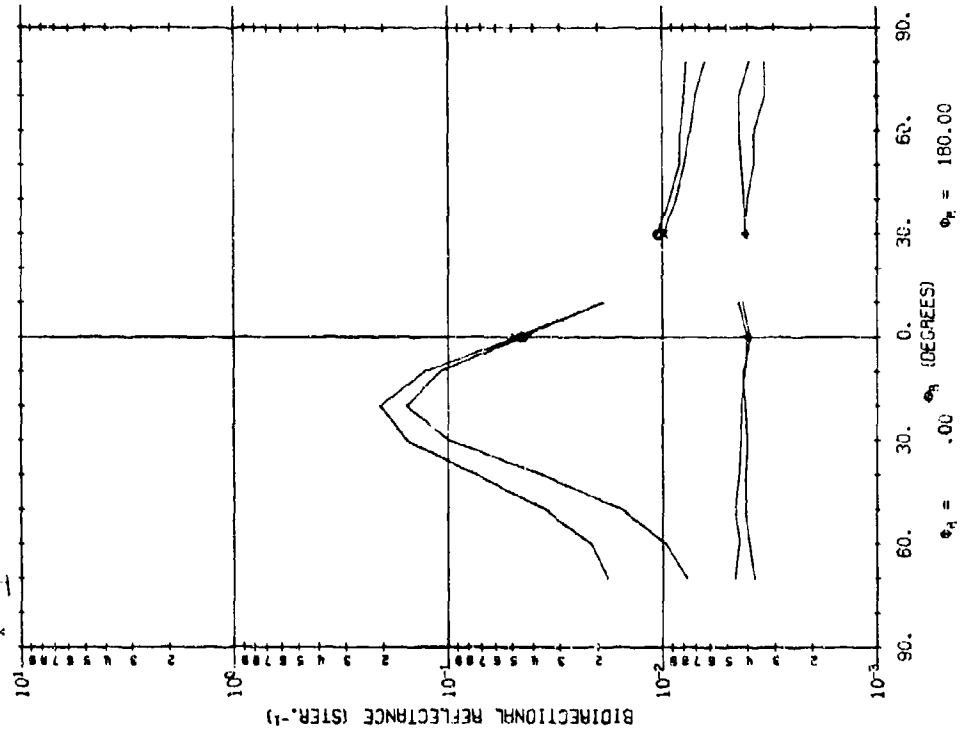
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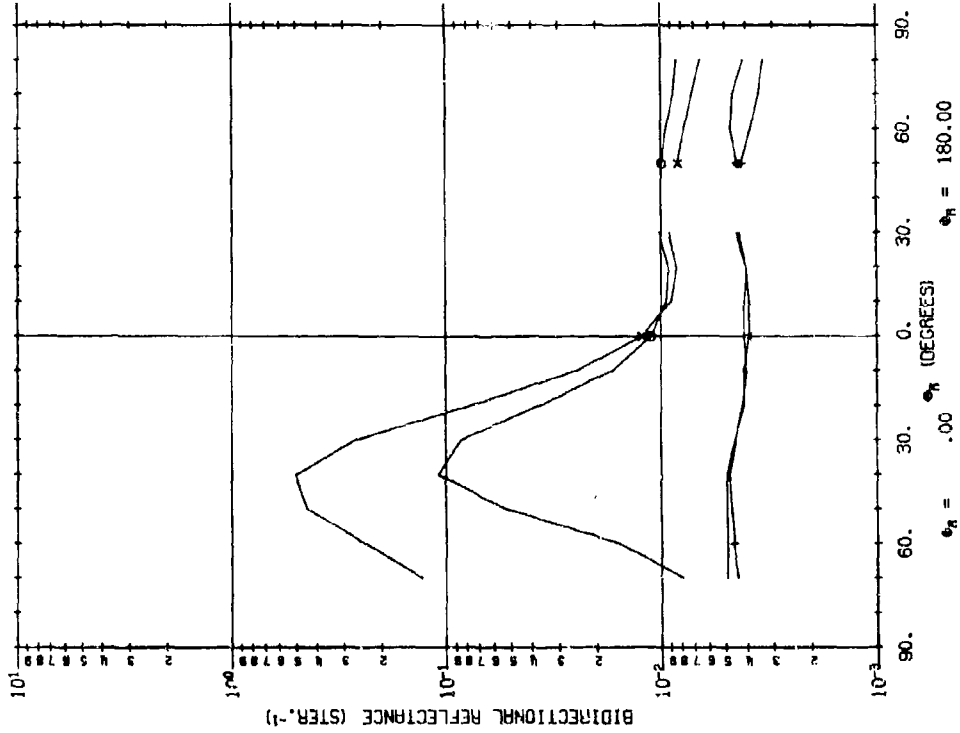
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COATS ZINC CHROMATE (WET DECKED) ON  
ANODIZED ALUMINUM

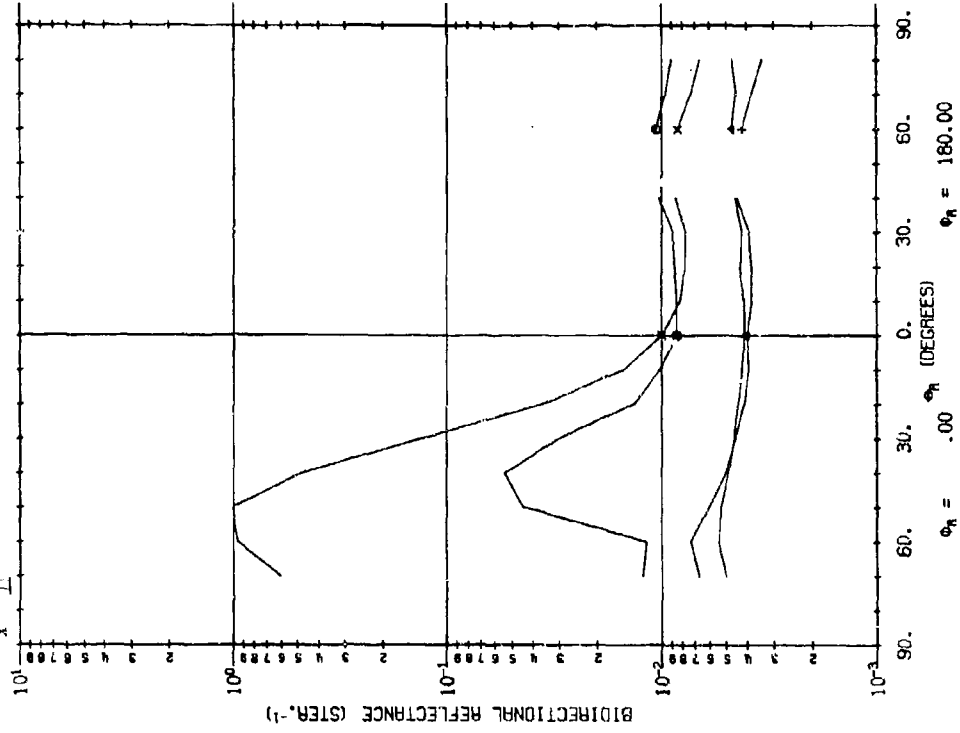
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 $\lambda = 0.63$



R01044 003

TWO COATS DEEP MOSS GREEN PAINT ON TWO  
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ANODIZED ALUMINUM

$\theta_i = 50.0$   
 $\phi_i = 180.0$   
 $\lambda = 0.63$



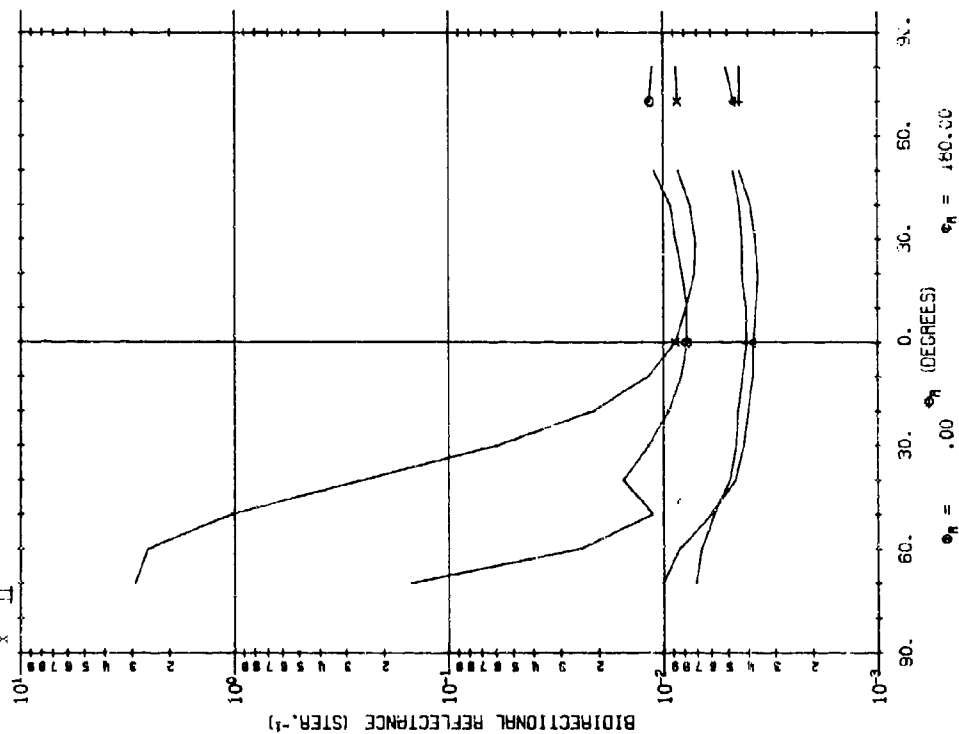
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R01044 003

TWO COATS DEEP MOSS GREEN PAINT ON TWO  
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ANODIZED ALUMINUM

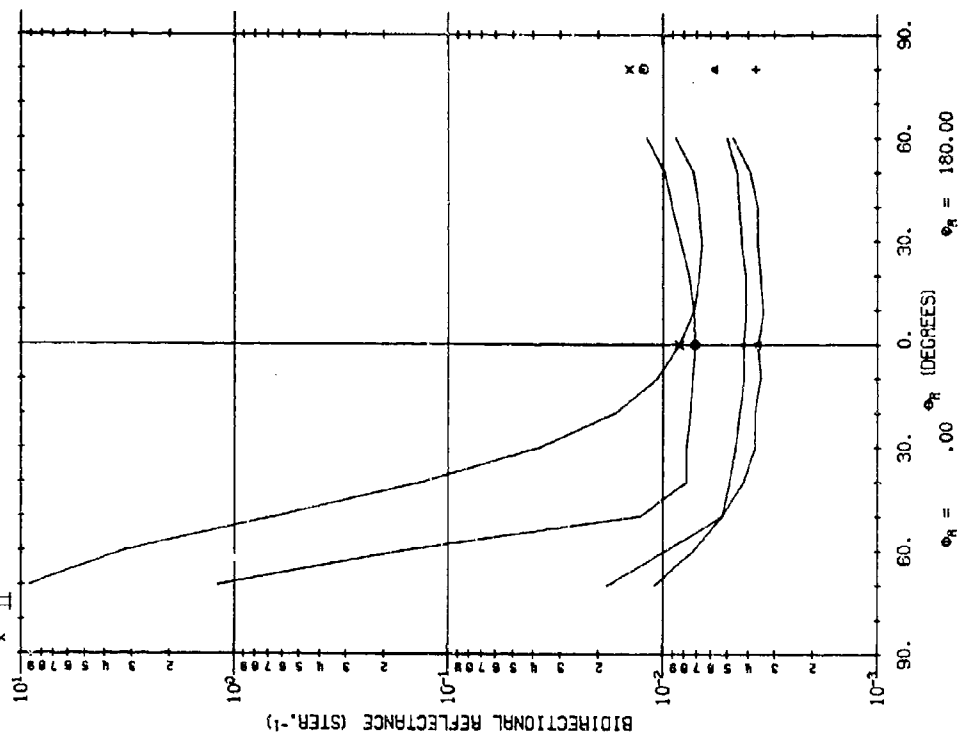
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- ||  $\lambda = 0.63$



R01044 003

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ON ANODIZED ALUMINUM

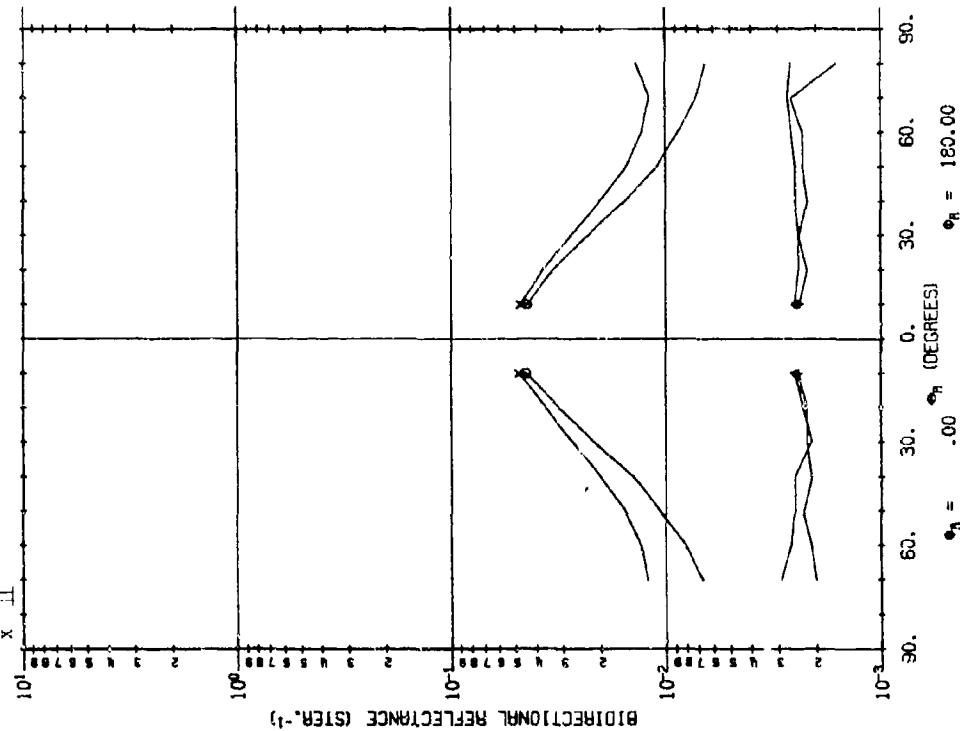
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A01047 003

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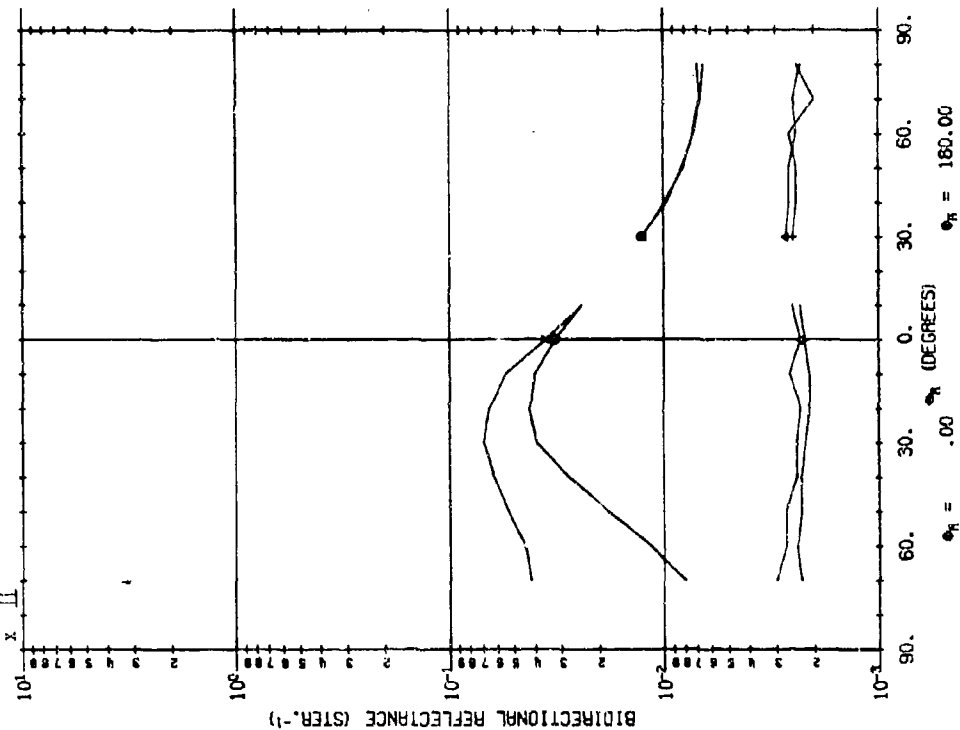
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A01047 003

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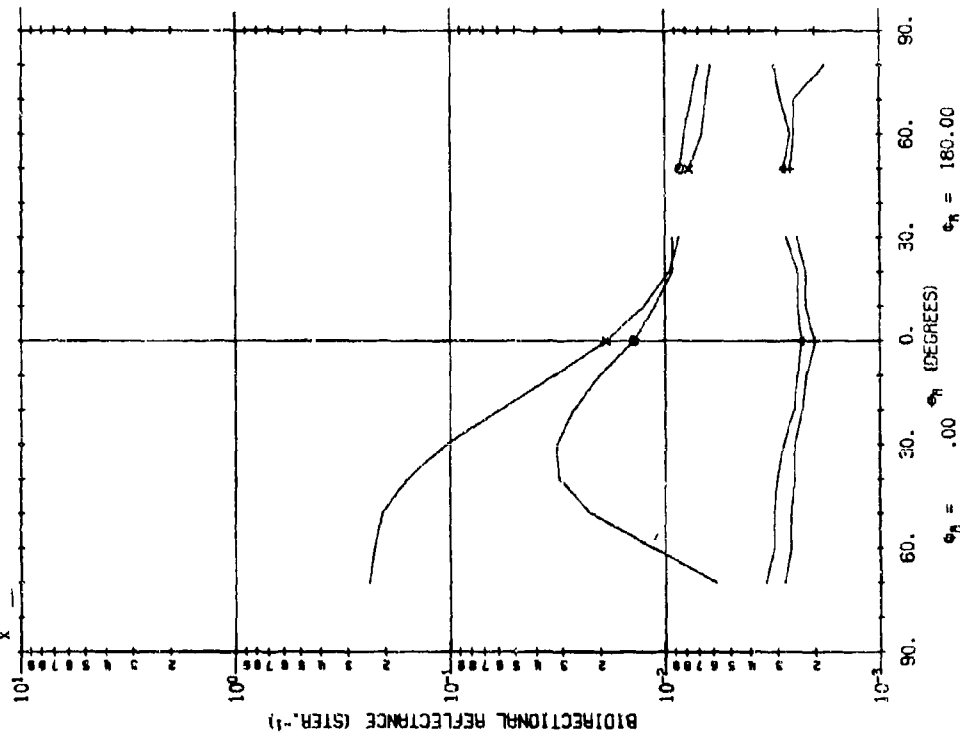


PAINT

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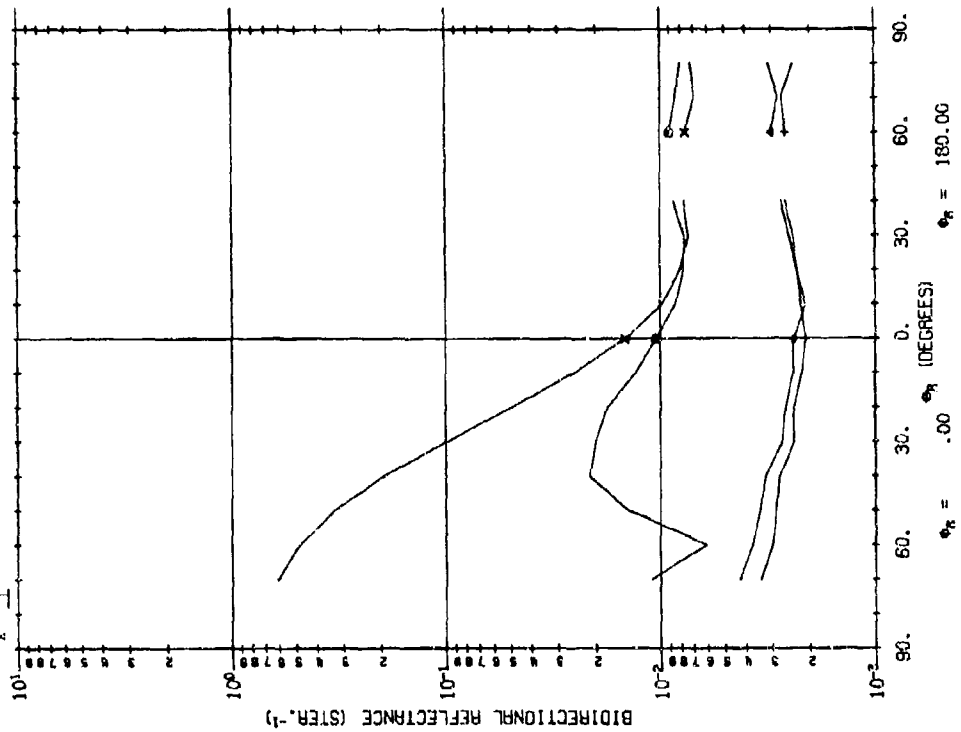
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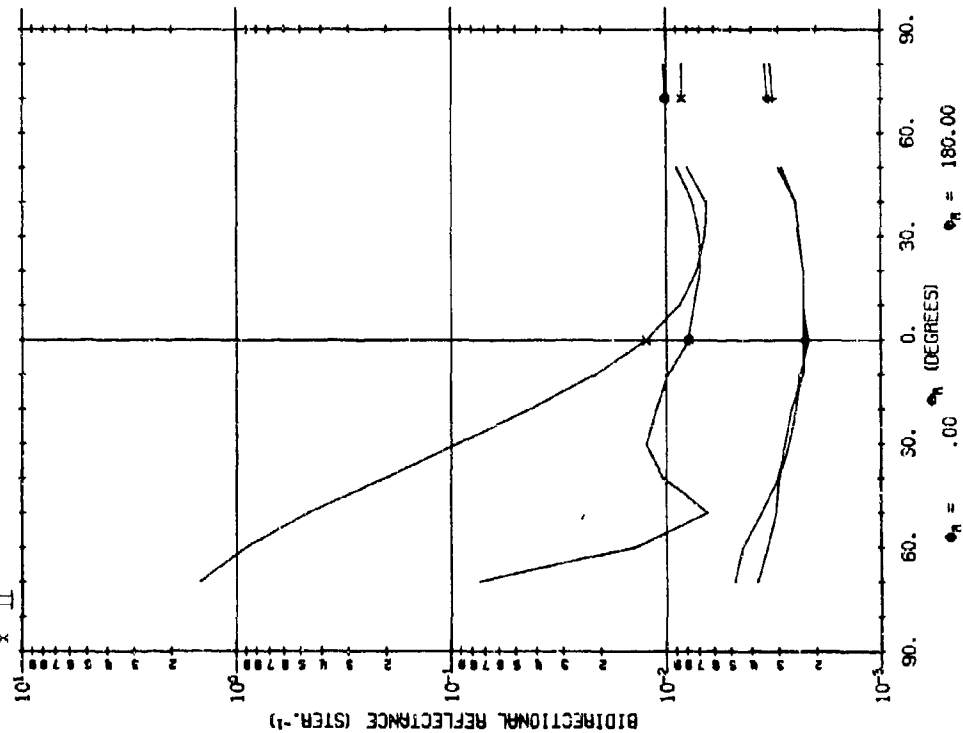
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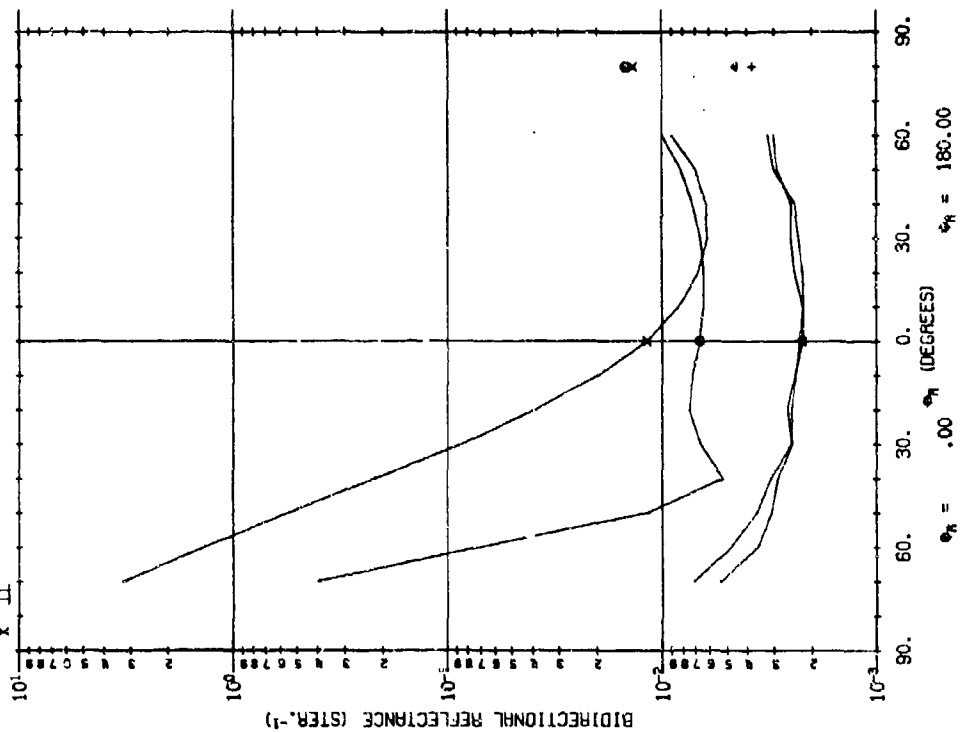
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A01047 003

TWO COATS OLIVE DRAB PAINT ON TWO  
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 $\phi_i = 180.0$   
 $\lambda = 0.63$

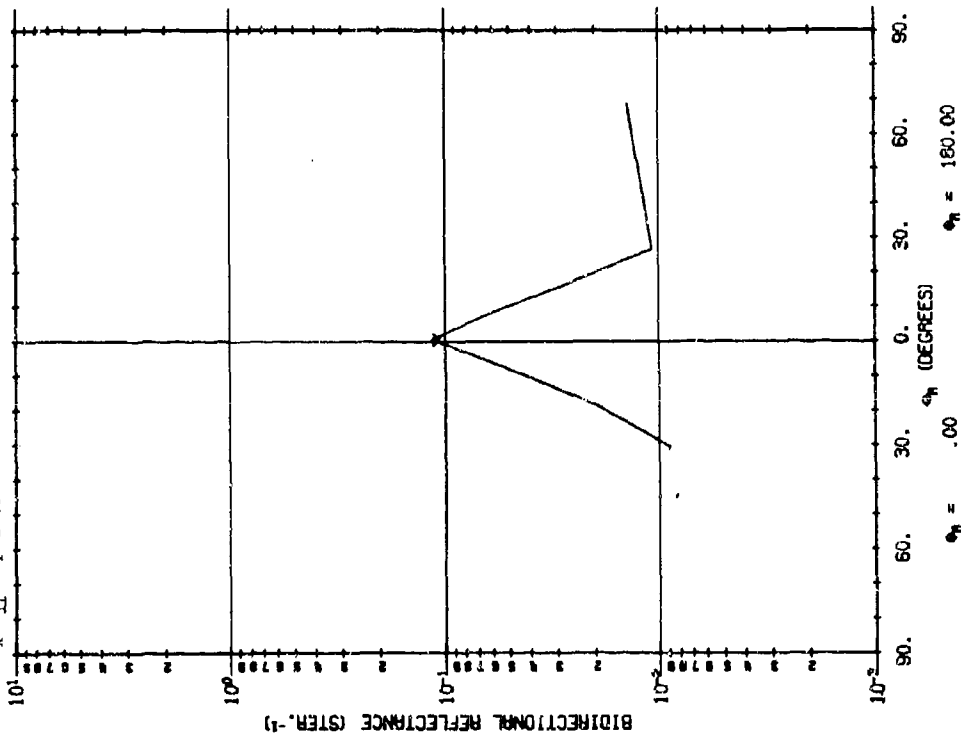


PAINT

R01049 001

Olive Drab Paint on Aluminum

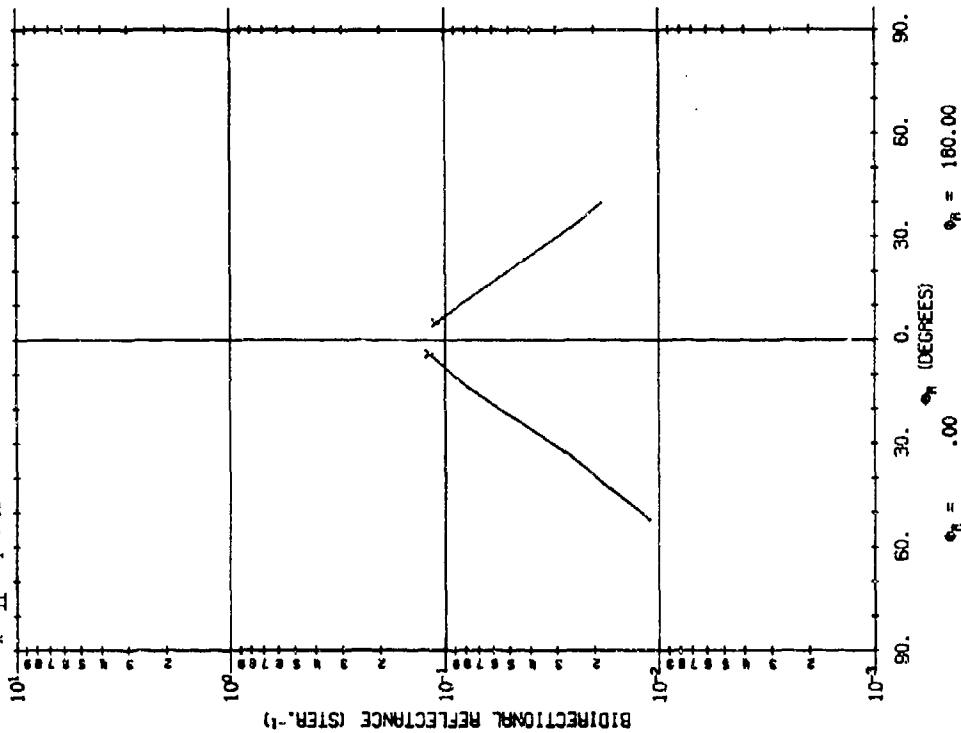
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 X || Y = UT

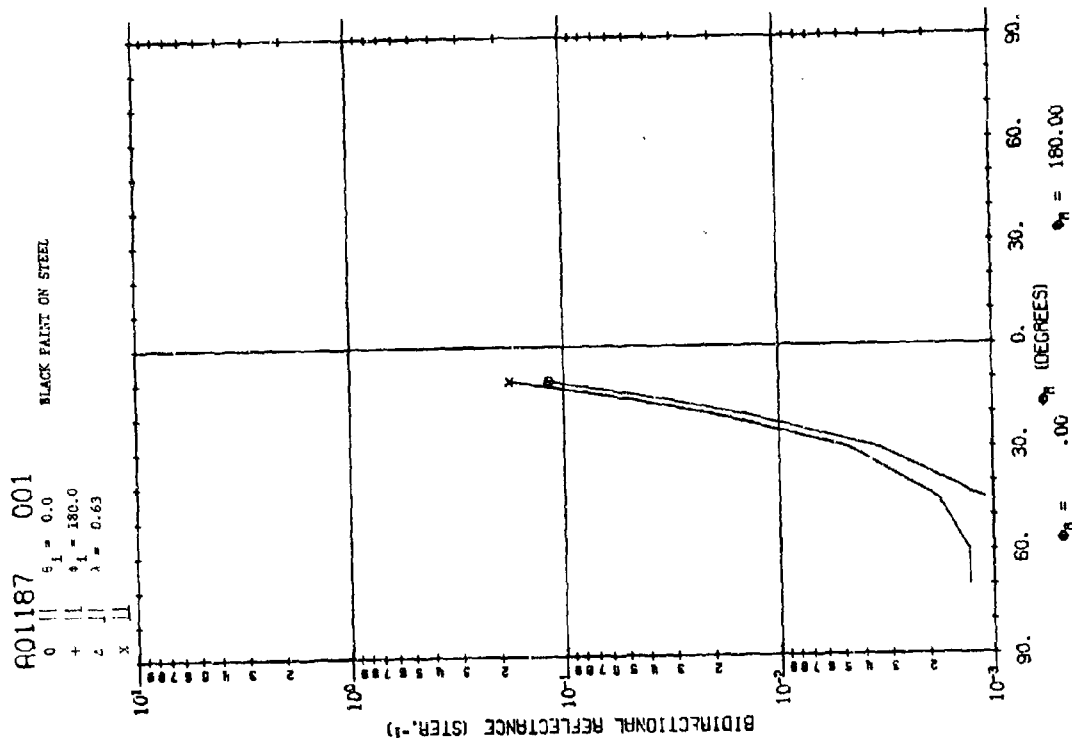
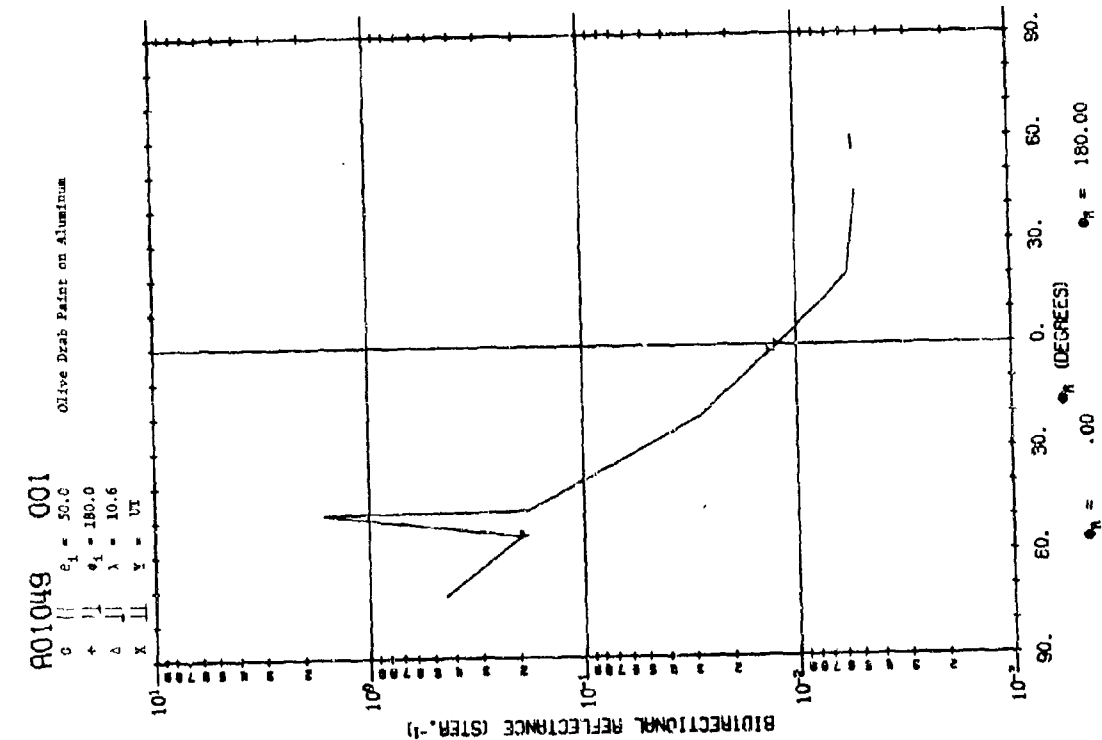


R01049 001

Olive Drab Paint on Aluminum

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 X || Y = UT



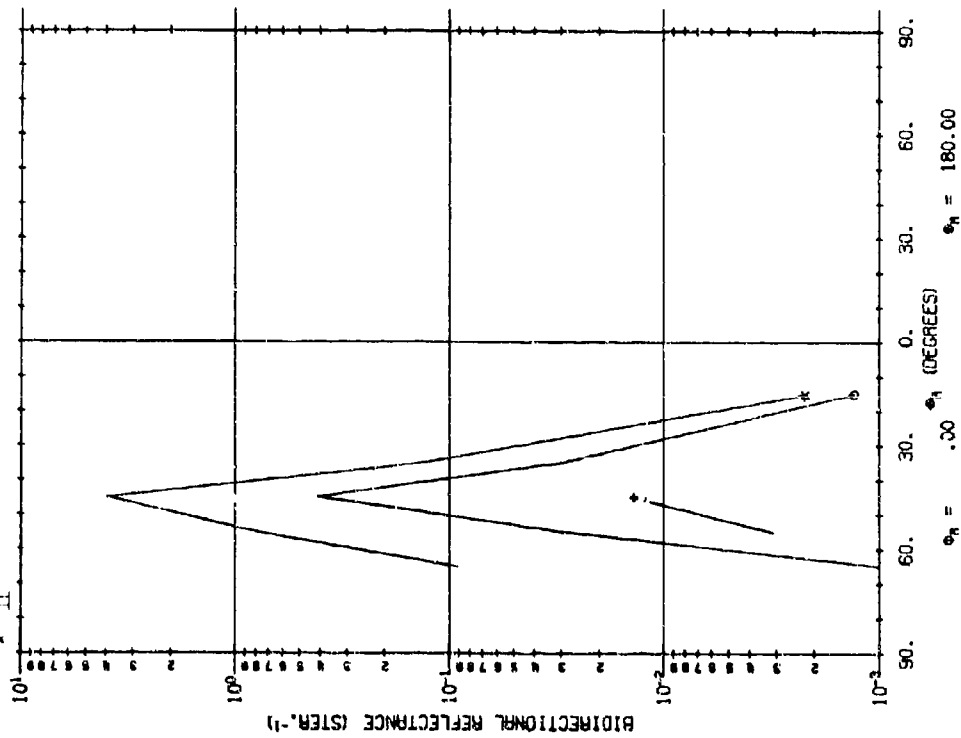


PAINT

A01187 001

BLACK PAINT ON STEEL

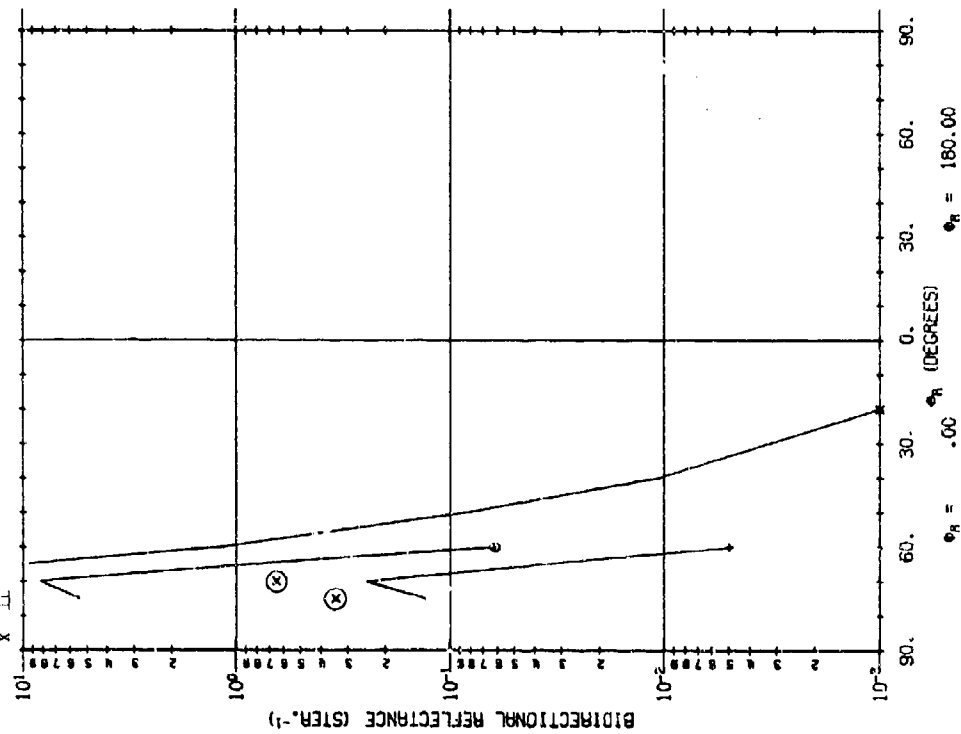
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 $\lambda = 0.63$



A01187 001

BLACK PAINT ON STEEL

$\theta_1 = 70.0$   
 $\theta_2 = 180.0$   
 $\lambda = 0.63$



A01224 004

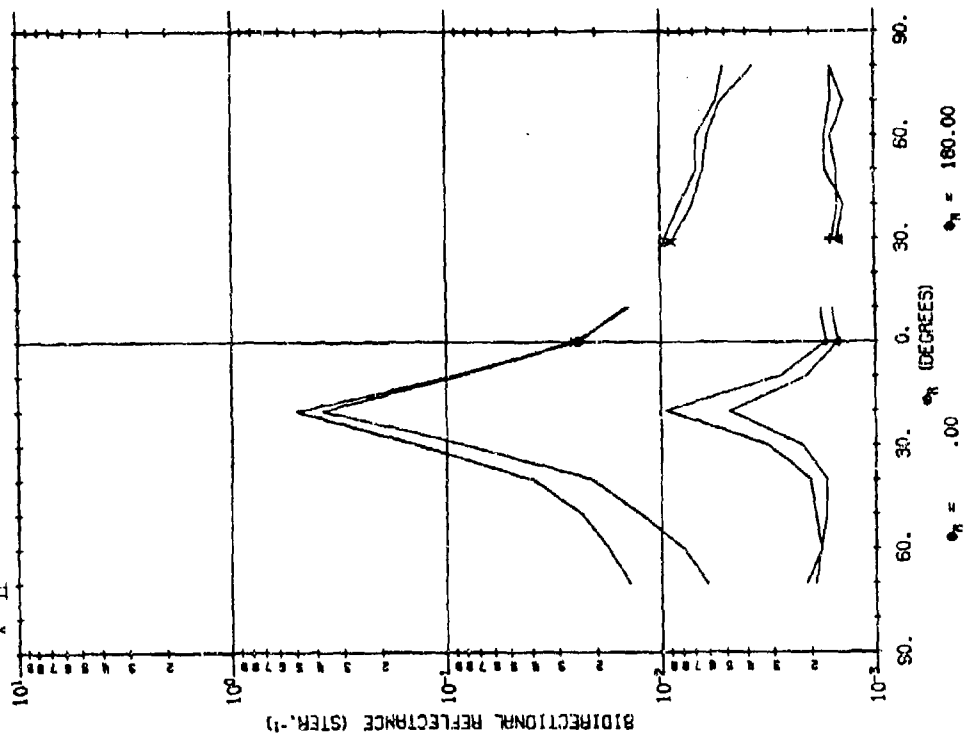
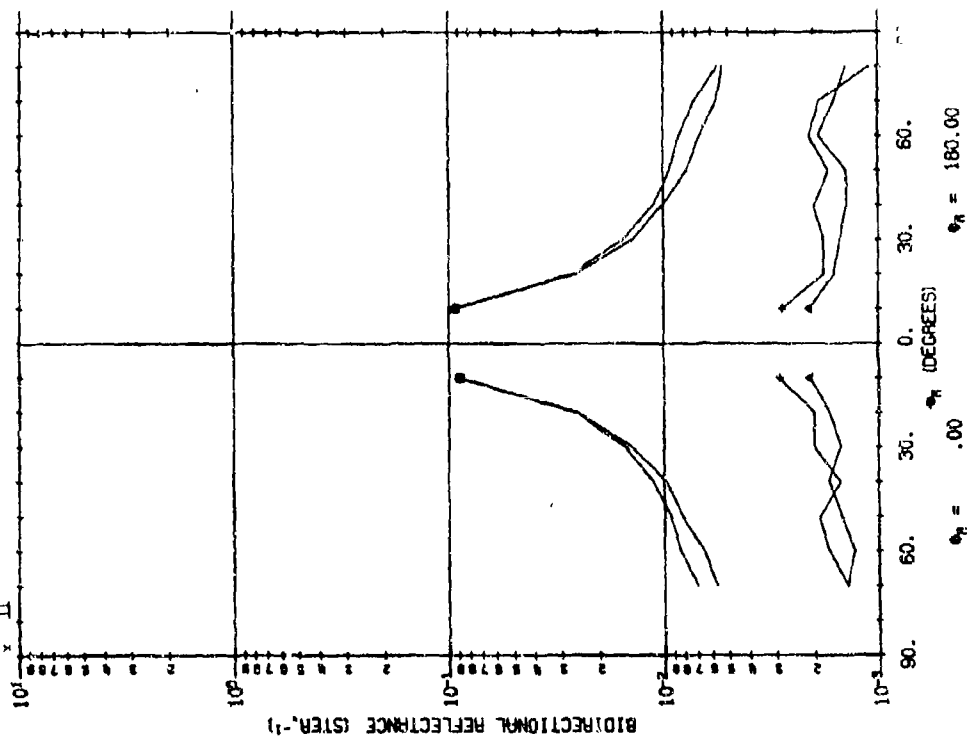
Olive Drab Paint on Metal

$\theta_1 = 0.0$   
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 $\lambda = 0.63$

A01224 004

Olive Drab Paint on Metal

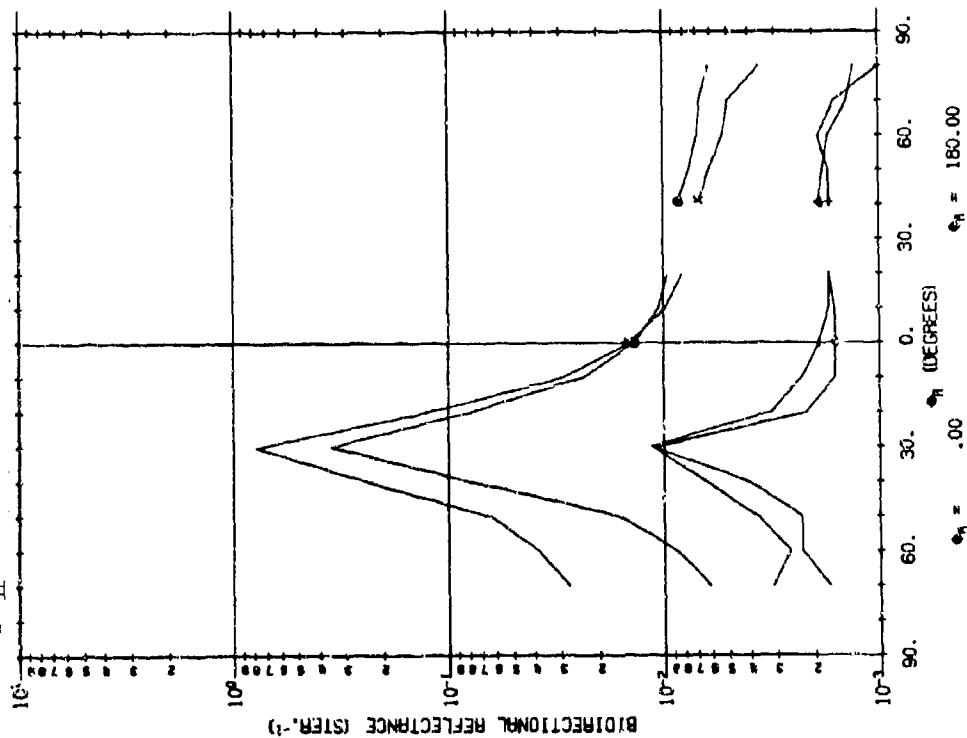
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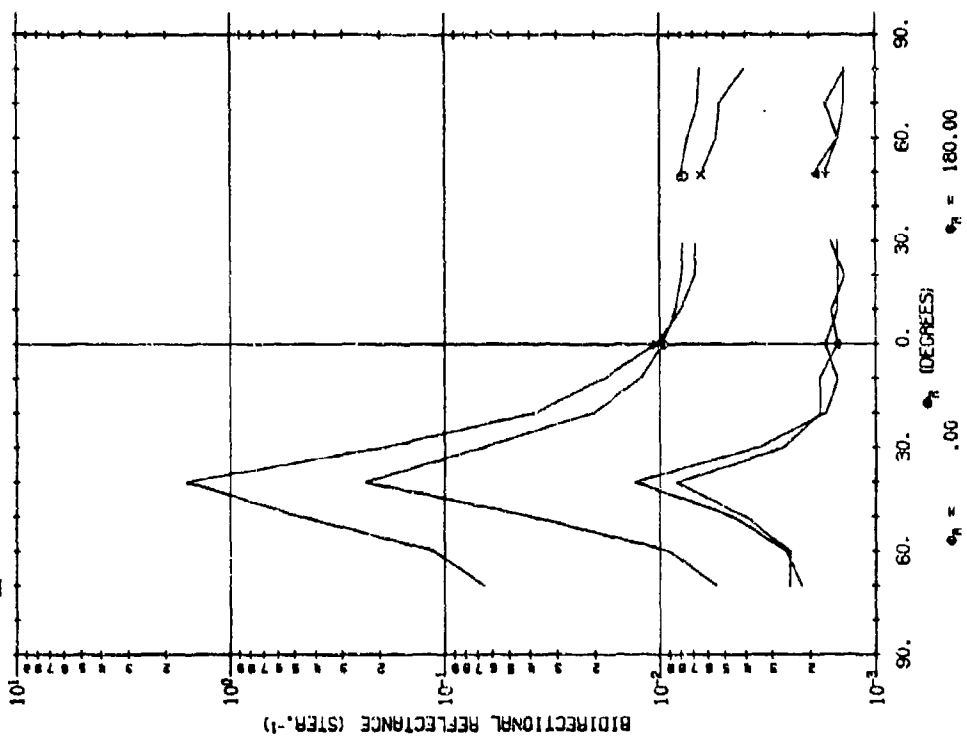
PAIN



AO1224 004  
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 $\lambda = 0.63$



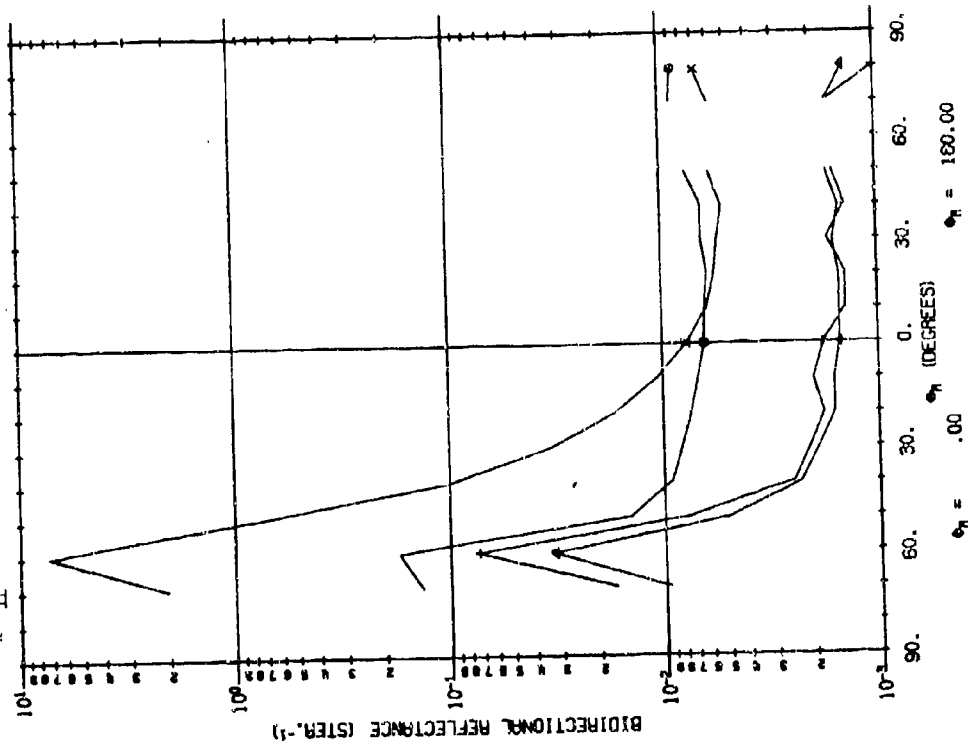
AO1224 004  
 Olive Drab Paint on Metal  
 $s_1 = 40.00$   
 $\phi_1 = 180.00$   
 $\lambda = 0.63$



A01224 004 Olive Drab Paint on Metal

$\phi_1 = 60.00$   
 $\phi_2 = 180.00$   
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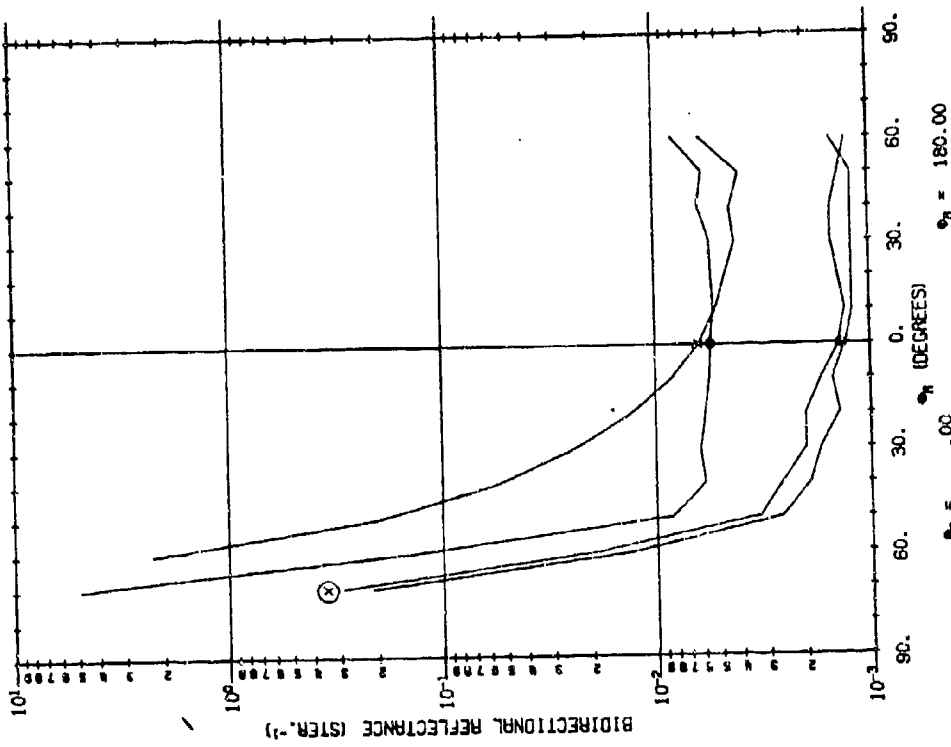
+ II  
 $\Delta$  II  
 $\times$  II



A01224 004 Olive Drab Paint on Metal

$\phi_1 = 60.00$   
 $\phi_2 = 180.00$   
 $\lambda = 0.63$

+ II  
 $\Delta$  II  
 $\times$  II

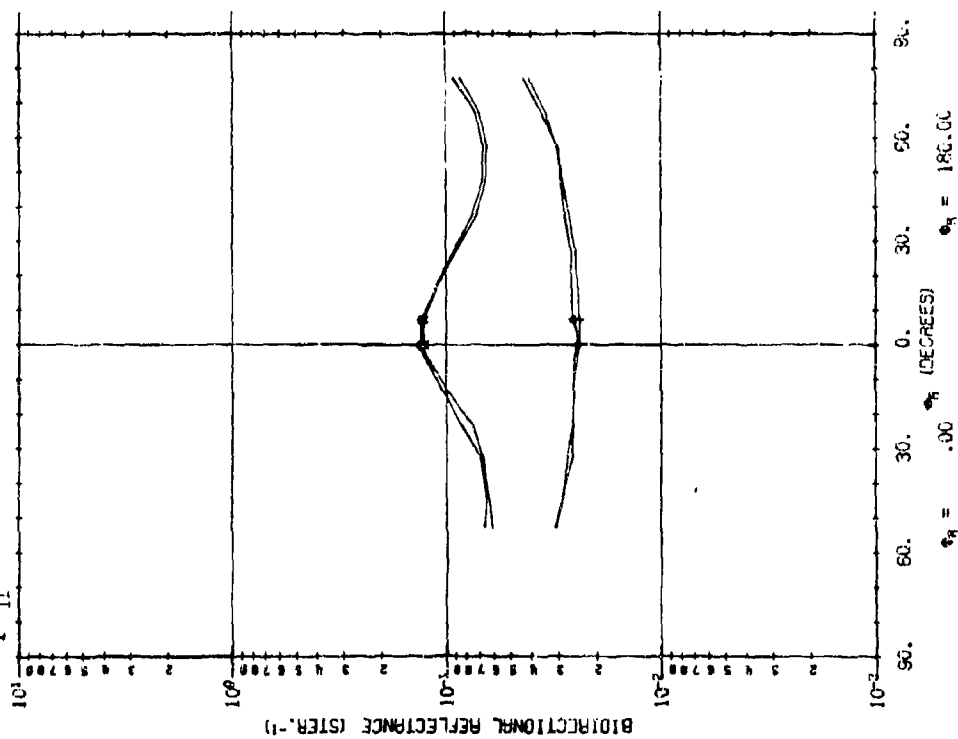


PAINT

A01295 004

Lt. Green Paint on Metal

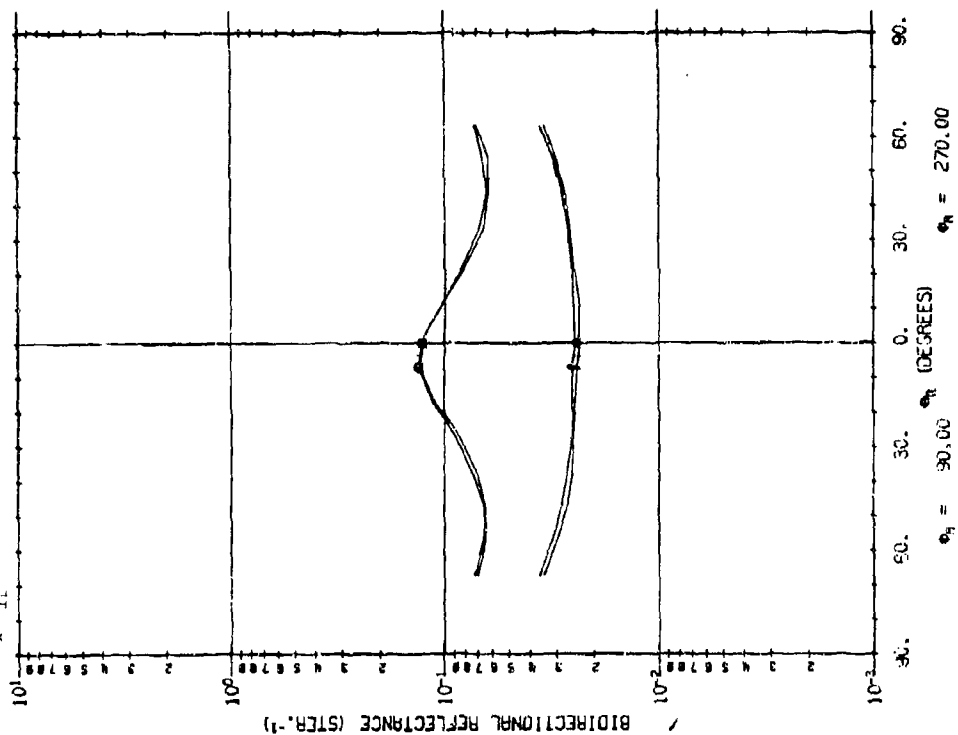
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 Δ II  $\lambda = 0.63$   
 x II



A01295 004

Lt. Green Paint on Metal

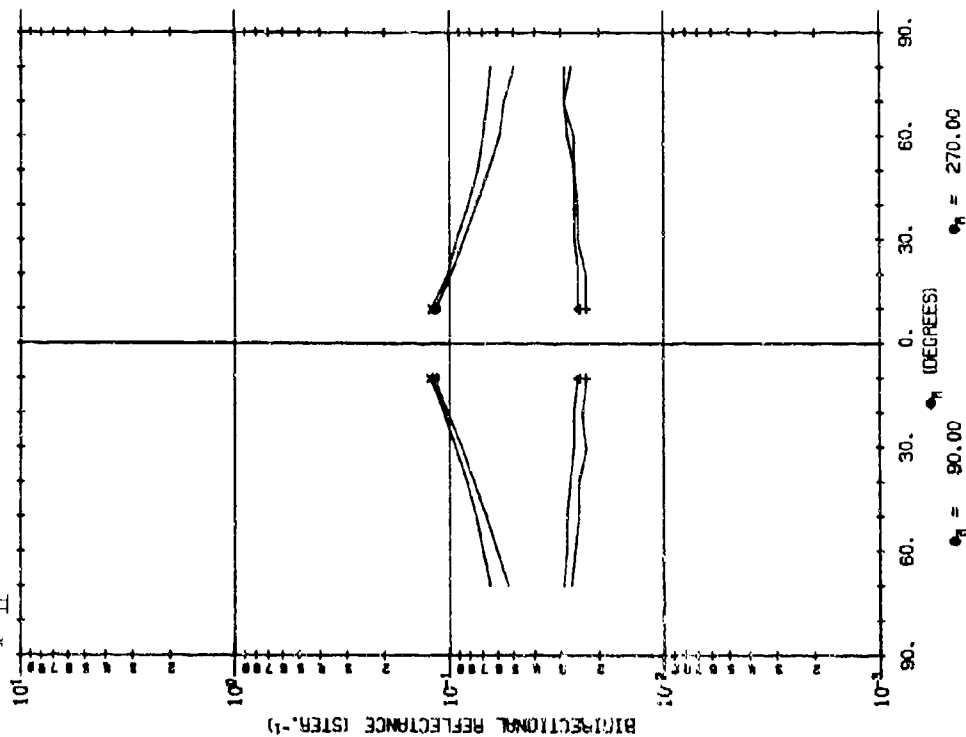
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 Δ II  $\lambda = 0.63$   
 x II



R01295 004

0 Lt. Green Paint on Metal

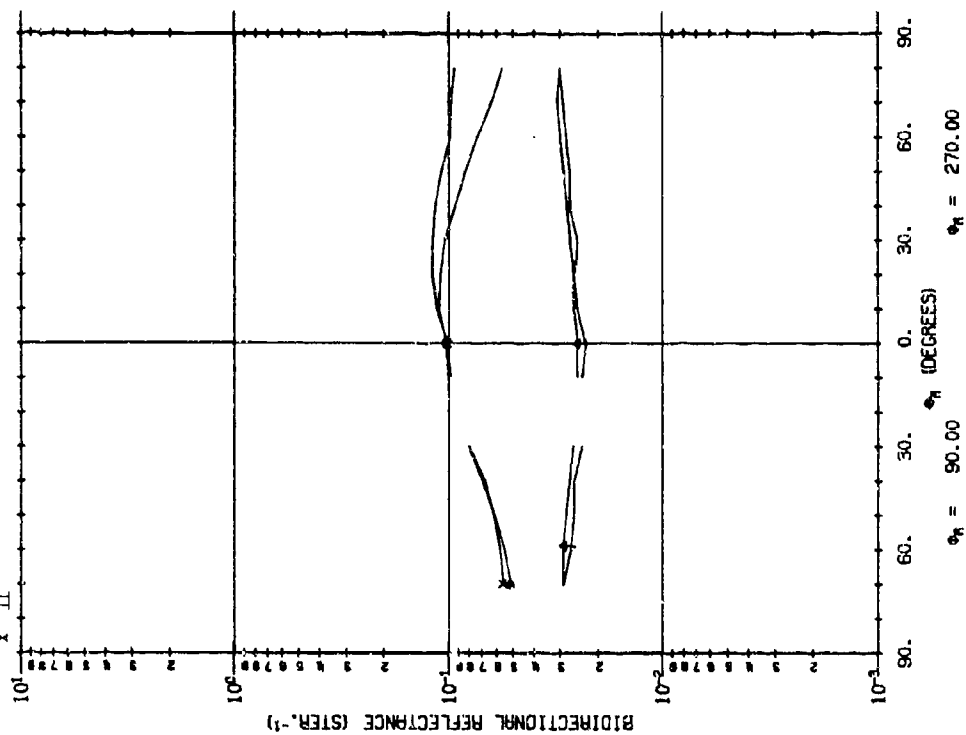
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+ 11 11 90.00  
Δ 11 11 0.63  
x 11



R01295 004

0 Lt. Green Paint on Metal

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+ 11 11 90.00  
Δ 11 11 0.63  
x 11

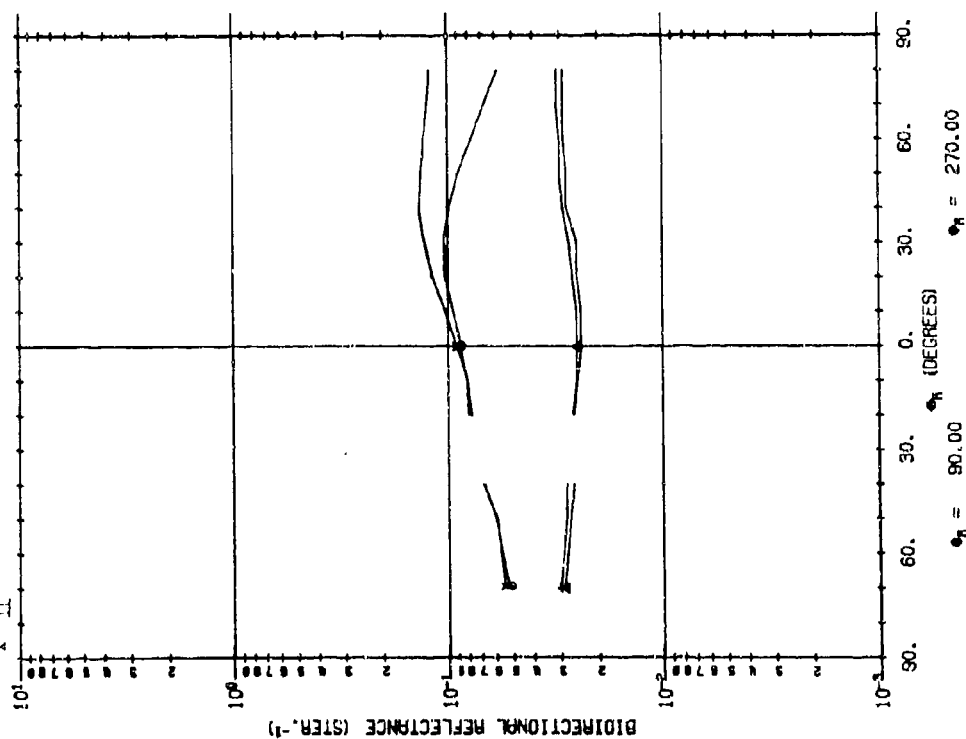


PAINT

A01295 004

Lt. Green Paint on Metal

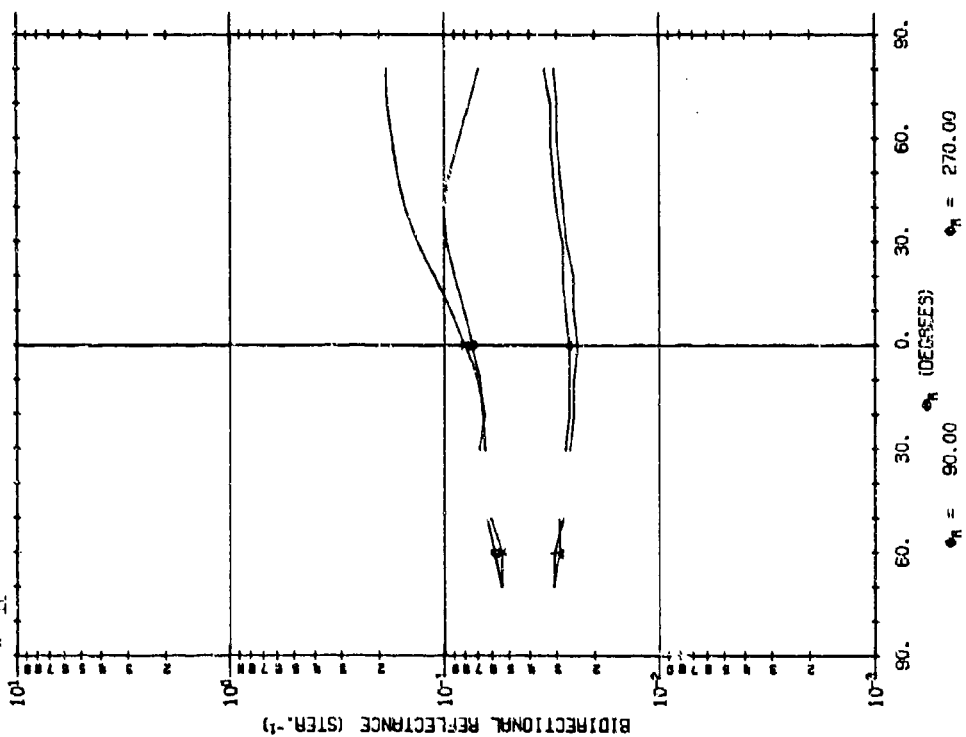
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A01295 004

Lt. Green Paint on Metal

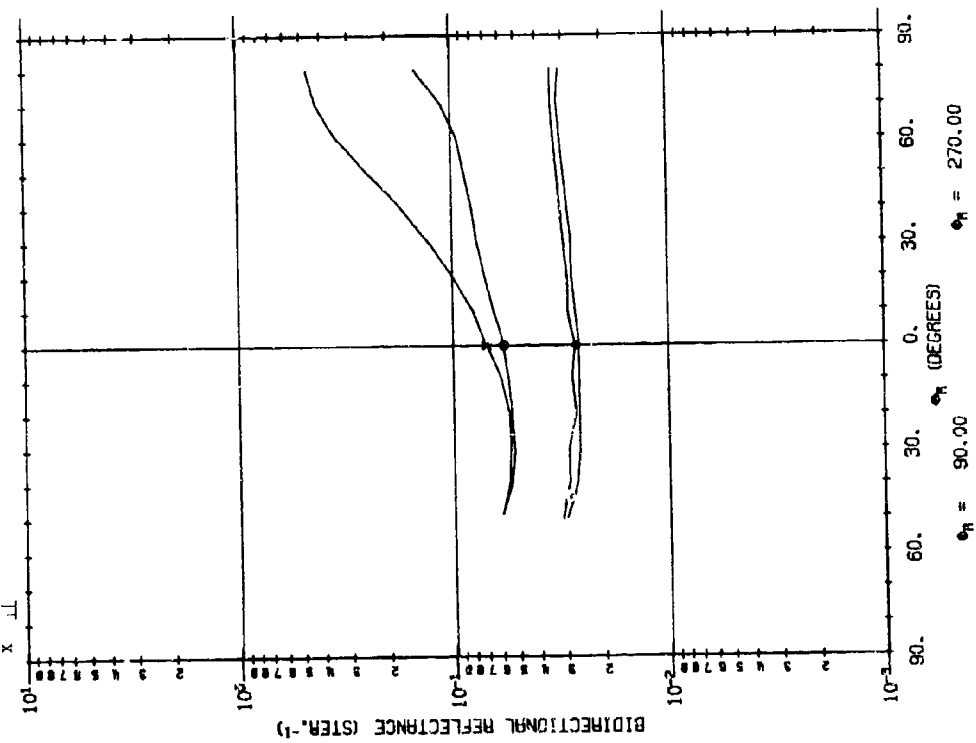
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A01295 004

Lt. Green Paint on Metal

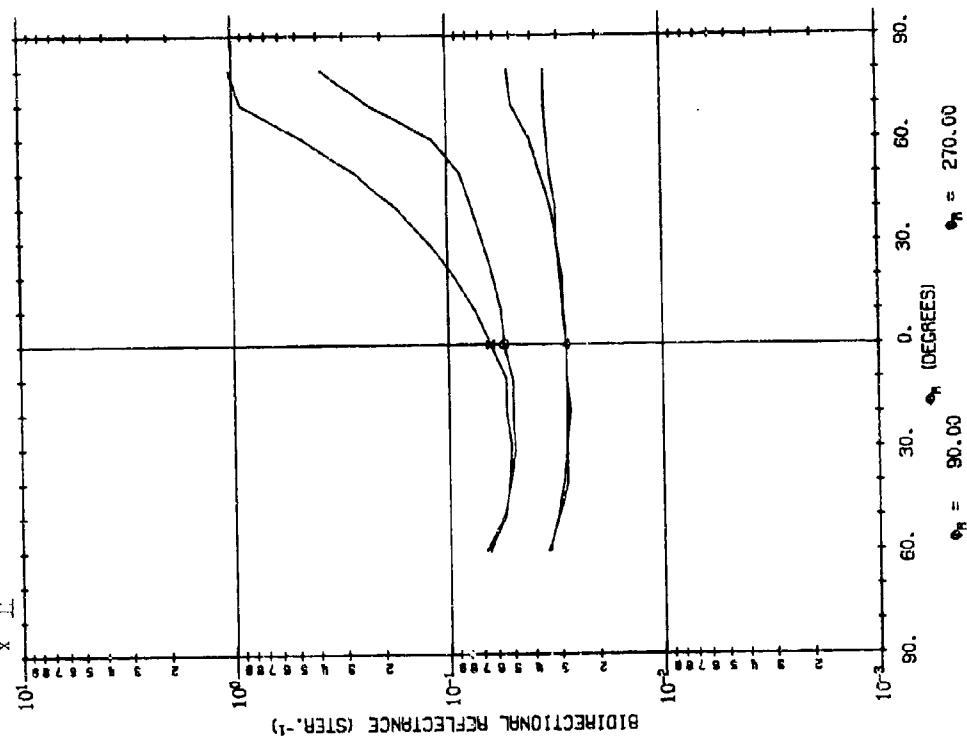
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A01295 004

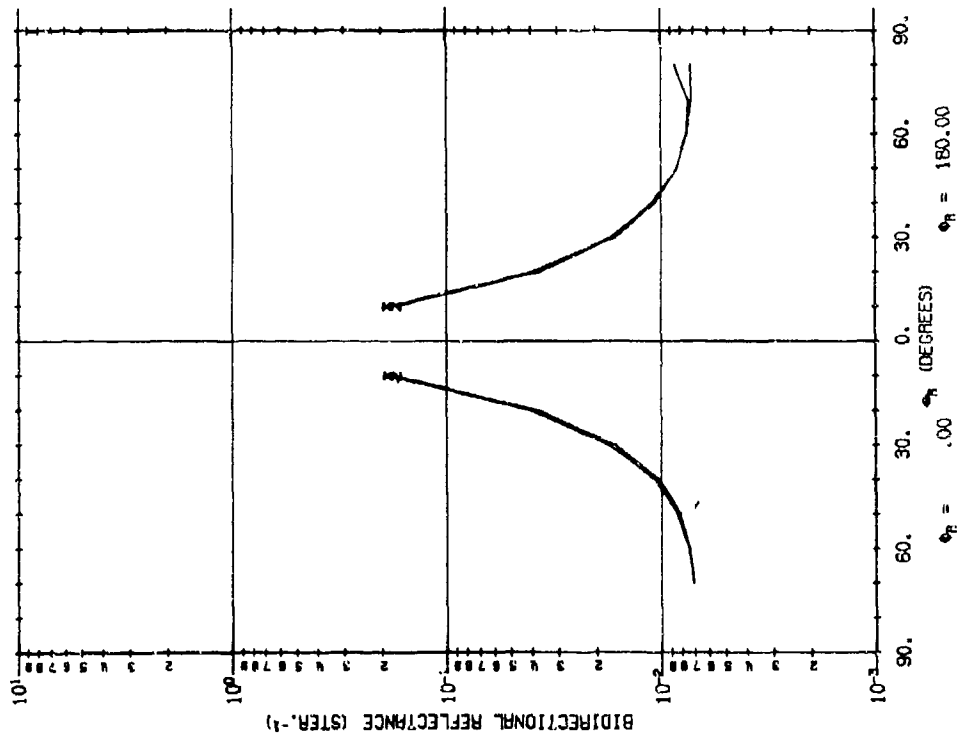
Lt. Green Paint on Metal

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 $\phi_2 = 90.00$   
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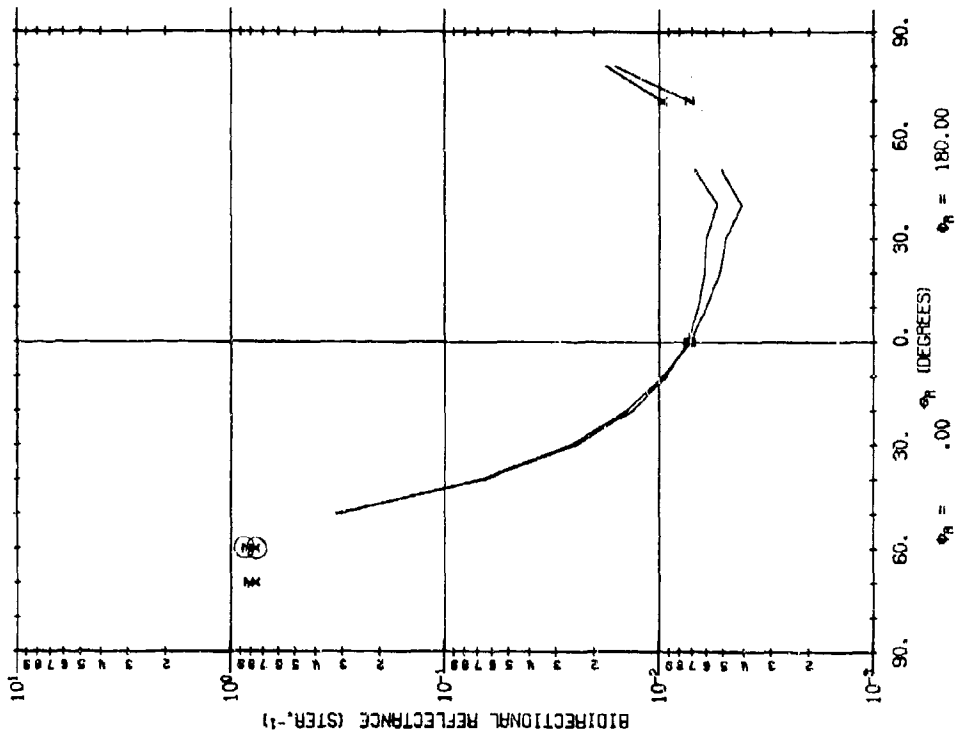
A01337 001

THREE COATS 3K BLACK VELVET PAINT  
COVERING 30% OF ALCLAD ALUMINUM  
PANEL  
X | T  $\theta_i = 0.0$   
Z | T  $\phi_i = 180.0$   
 $\lambda = 1.06$



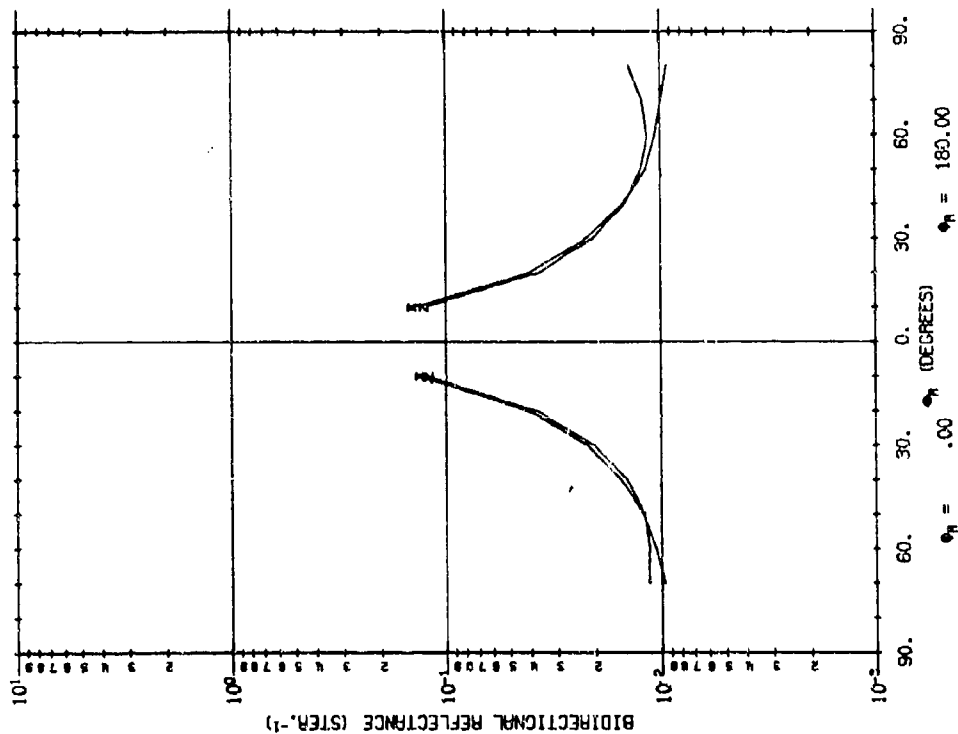
A01337 001

THREE COATS 3K BLACK VELVET PAINT  
COVERING 30% OF ALCLAD ALUMINUM  
PANEL  
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Z | T  $\phi_i = 180.0$   
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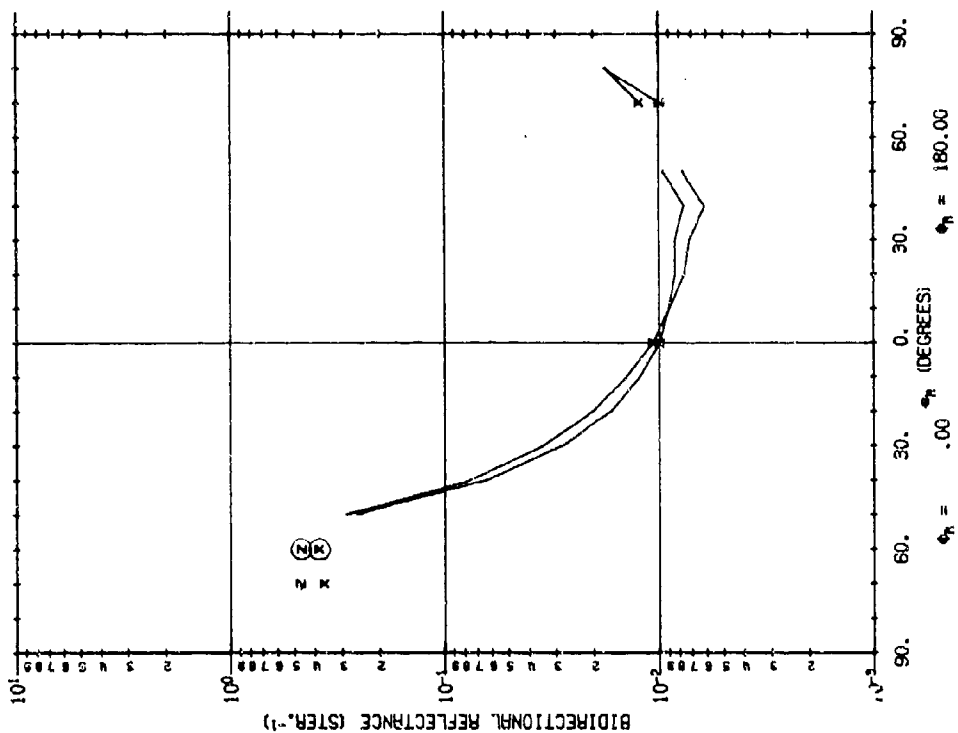
R01338 001

THREE COATS 3M BLACK VELVET PAINT  
COVERING 64.4% OF ALCLAD ALUMINUM  
PANEL  
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 $\lambda = 1.06$



R01338 001

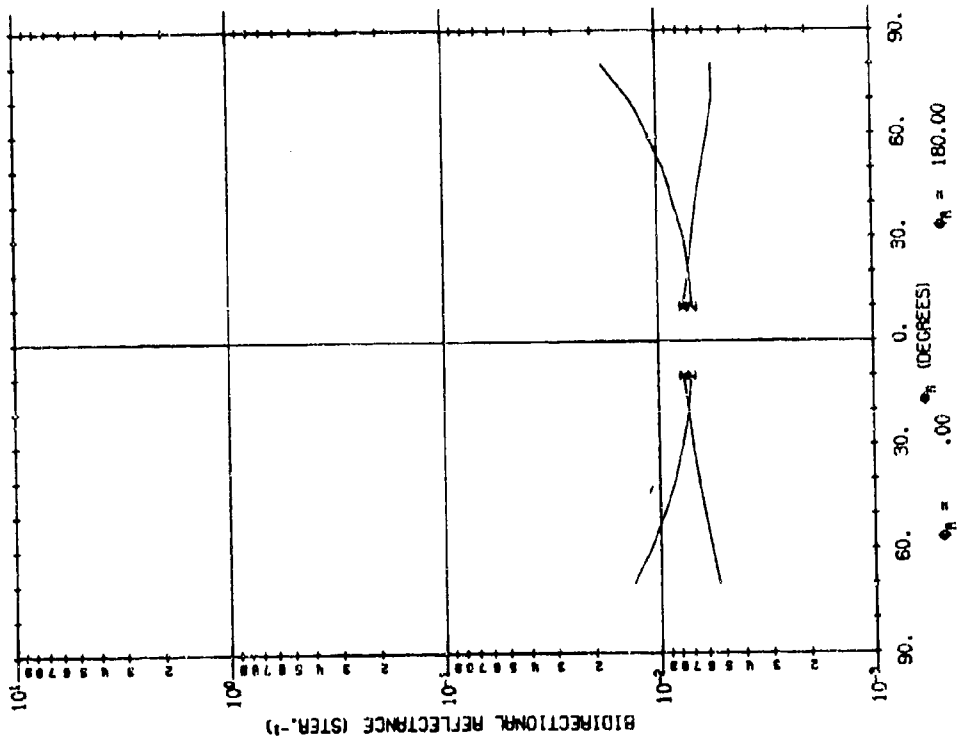
THREE COATS 3M BLACK VELVET PAINT  
COVERING 64.4% OF ALCLAD ALUMINUM  
PANEL  
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 $\lambda = 1.06$





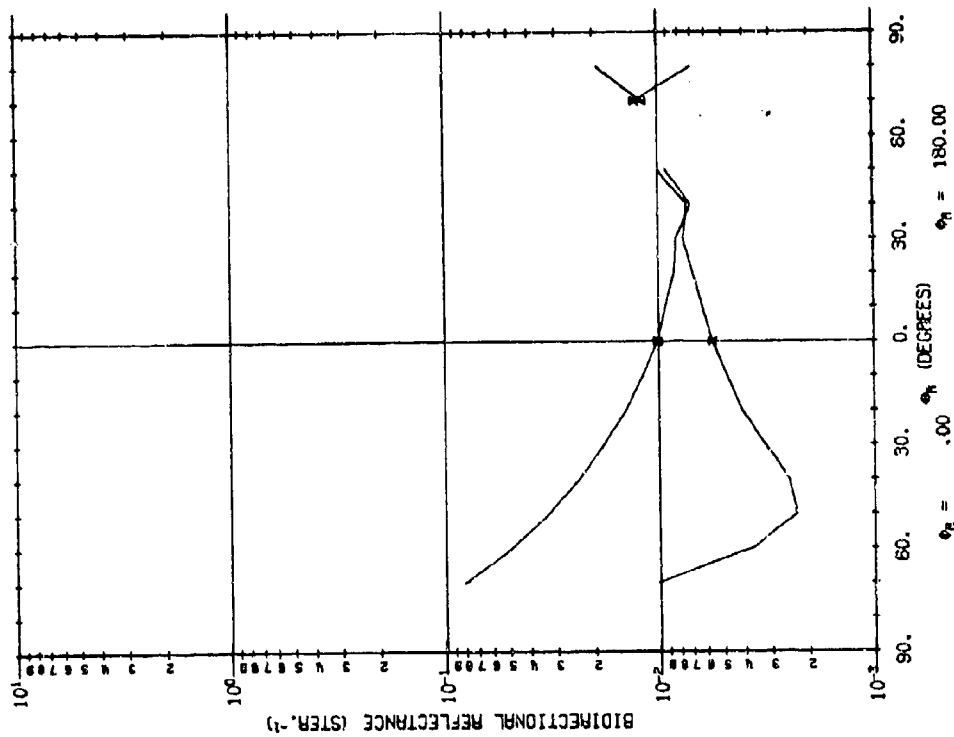
R01339 001

THREE COATS 3M BLACK VELVET PAINT  
ON ALCLAD ALUMINUM PANEL  
X  $\theta_i = 0.0$   
Z  $\theta_i = 180.0$   
 $\lambda = 1.06$



R01339 001

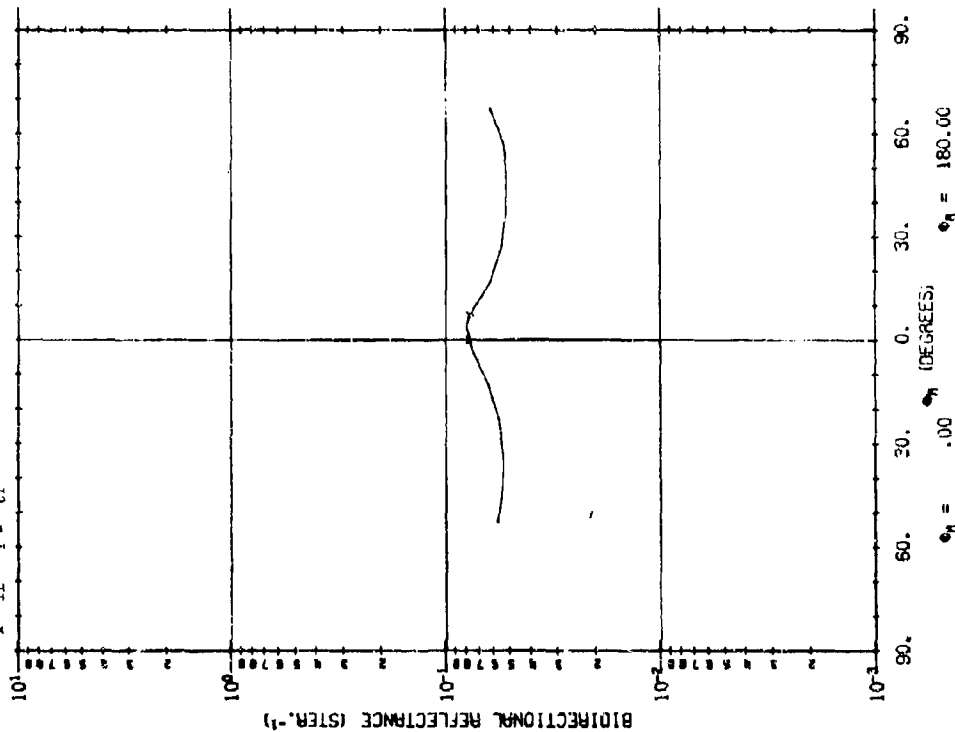
THREE COATS 3M BLACK VELVET PAINT  
ON ALCLAD ALUMINUM PANEL  
X  $\theta_i = 60.0$   
Z  $\theta_i = 180.0$   
 $\lambda = 1.06$



R01341 006

OLIVE DRAB PAINT ON METAL

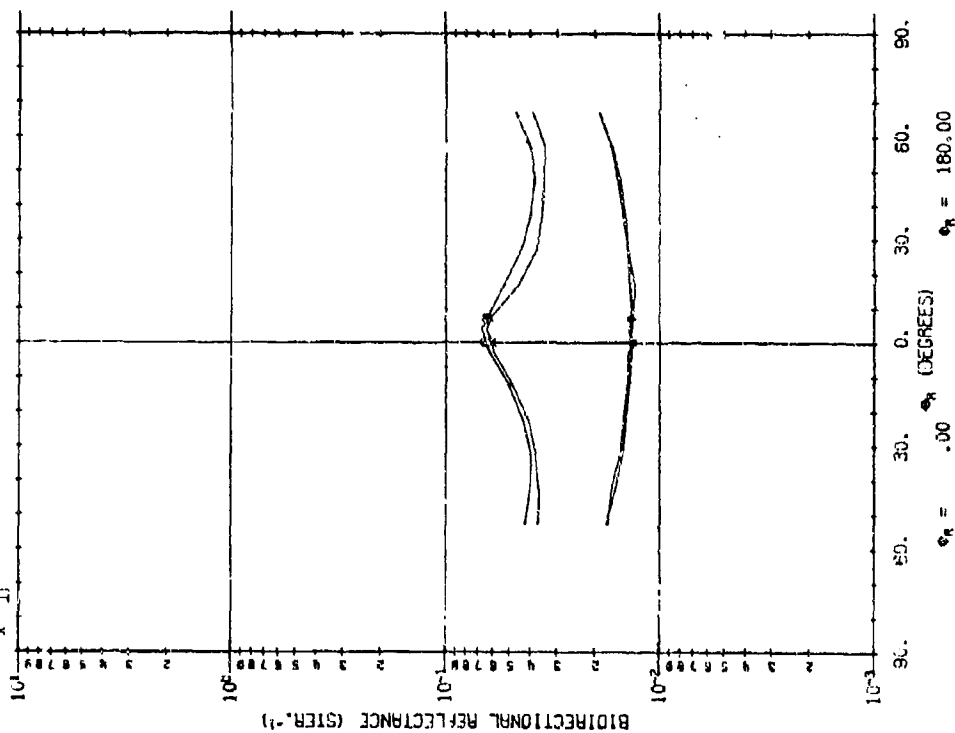
0 11 28 = 7.0  
+ 11  $\phi_1 = 42$   
Δ 11  $\lambda = 0.63$   
x 11 y = UT



R01341 006

OLIVE DRAB PAINT ON METAL

0 11 28 = 7.0  
+ 11  $\phi_1 = 42$   
Δ 11  $\lambda = 0.63$   
x 11 y = UT

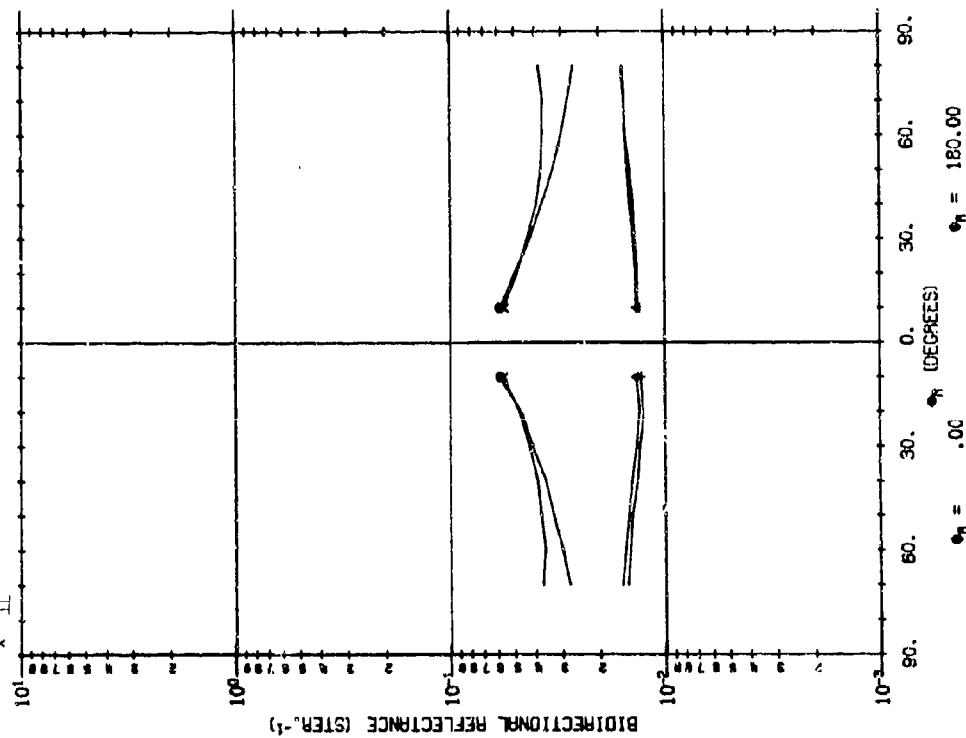


PAINT

A01341 006

Olive Drab Paint on Metal

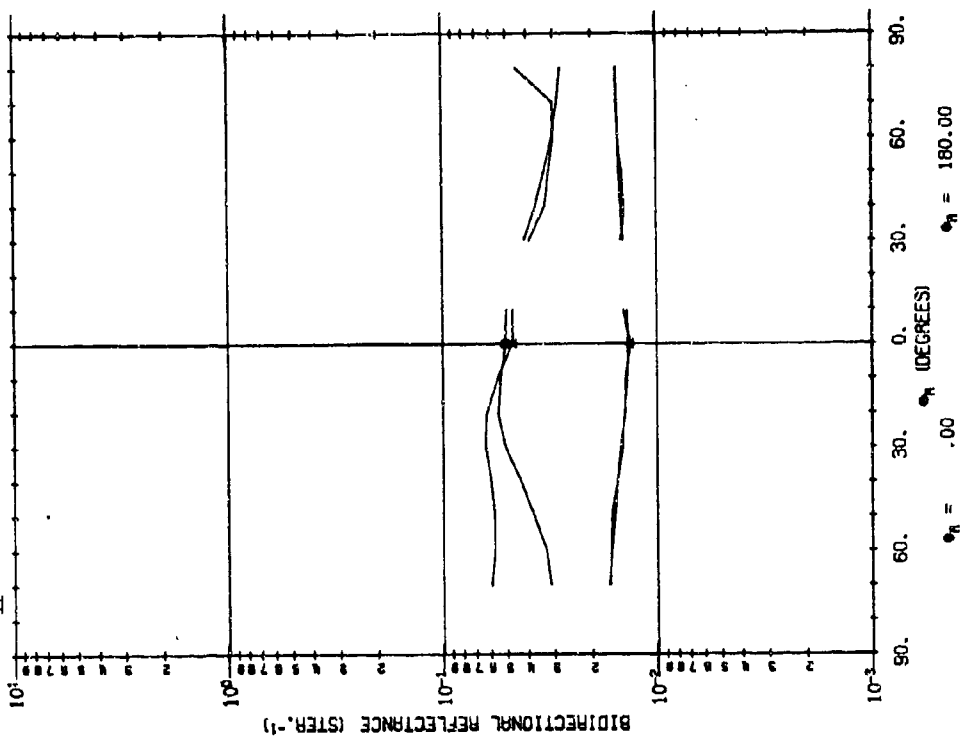
$\theta_i = 0.0$   
 $\theta_r = 180.00$   
 $\lambda = 0.63$



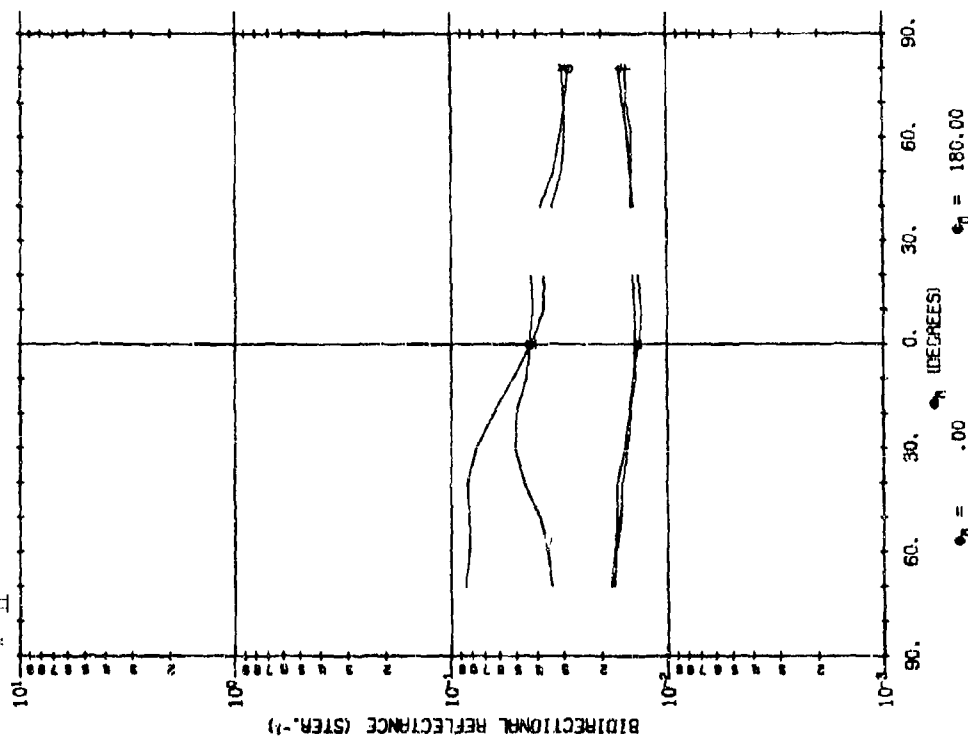
A01341 006

Olive Drab Paint on Metal

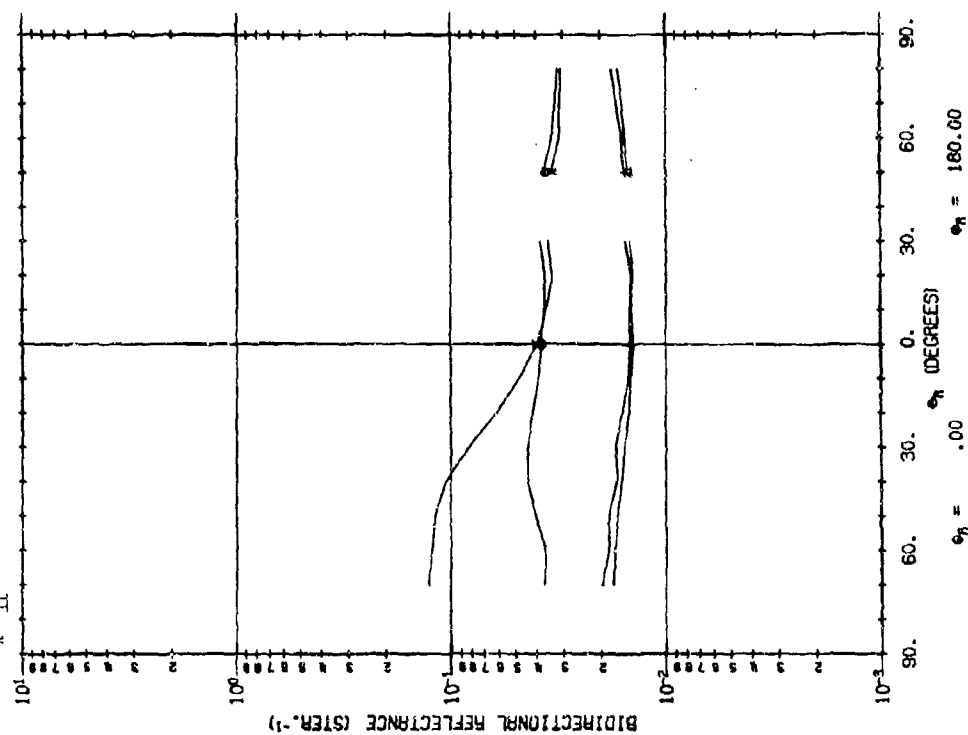
$\theta_i = 20.00$   
 $\theta_r = 180.00$   
 $\lambda = 0.63$



A01341 006  
 Olive Drab Paint on Metal  
 $\epsilon_1 = 30.00$   
 $\phi_1 = 180.00$   
 $\lambda = 0.63$   
 +  $\parallel$   
 A  $\parallel$   
 X  $\parallel$



A01341 006  
 Olive Drab Paint on Metal  
 $\epsilon_1 = 40.00$   
 $\phi_1 = 180.00$   
 $\lambda = 0.63$   
 +  $\parallel$   
 A  $\parallel$   
 X  $\parallel$

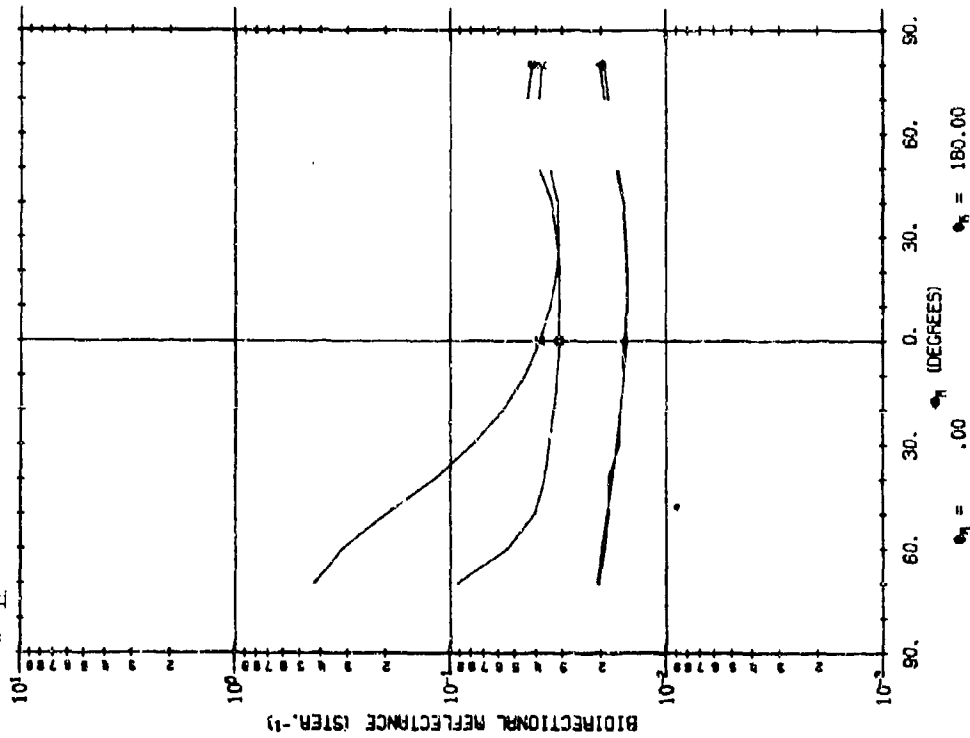


PAINT

A01341 006

Olive Drab Paint on Metal

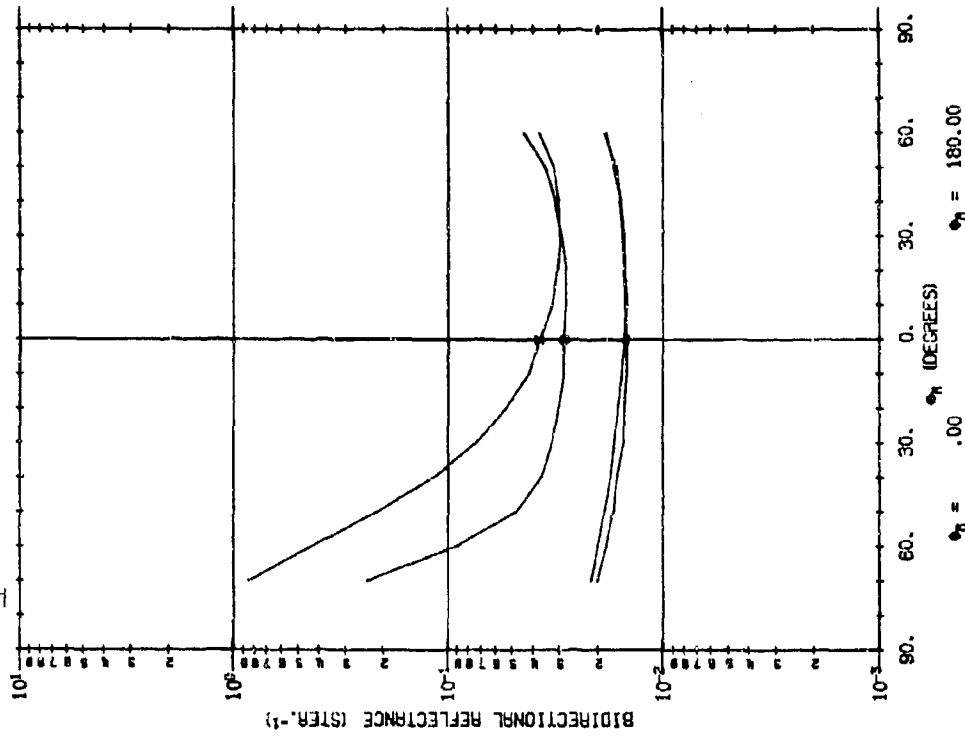
$\theta_1 = 50.00$   
 $\theta_2 = 180.00$   
 $\lambda = 0.63$



A01341 006

Olive Drab Paint on Metal

$\theta_1 = 70.00$   
 $\theta_2 = 180.00$   
 $\lambda = 0.63$



HC1341 006

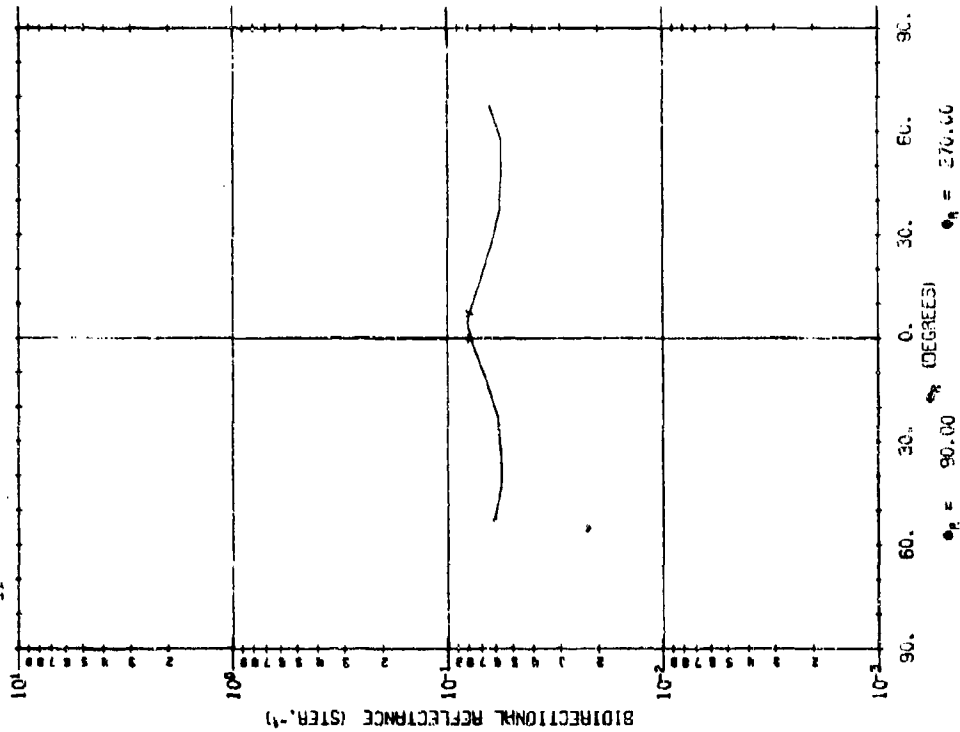
OLIVE DRAB PAINT ON METAL

$2\theta = 7.0$

$\phi_L = \phi_r$

$\lambda = 0.63$

$\gamma = 0^\circ$



HC1341 006

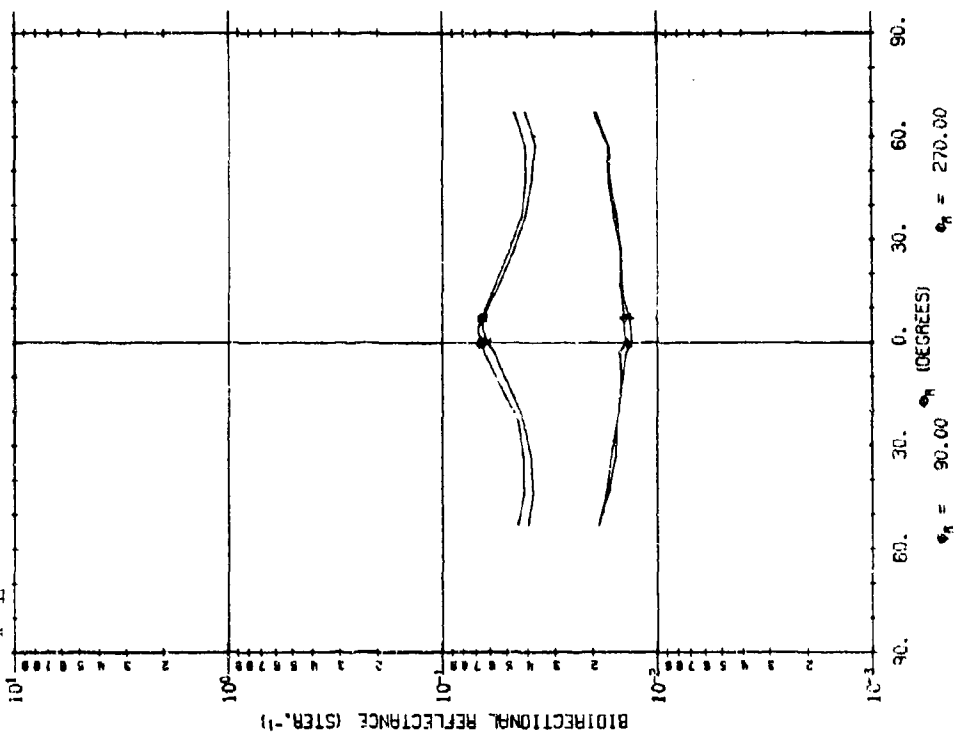
OLIVE DRAB PAINT ON METAL

$2\theta = 7.0$

$\phi_L = \phi_r$

$\lambda = 0.63$

$\gamma = 0^\circ$

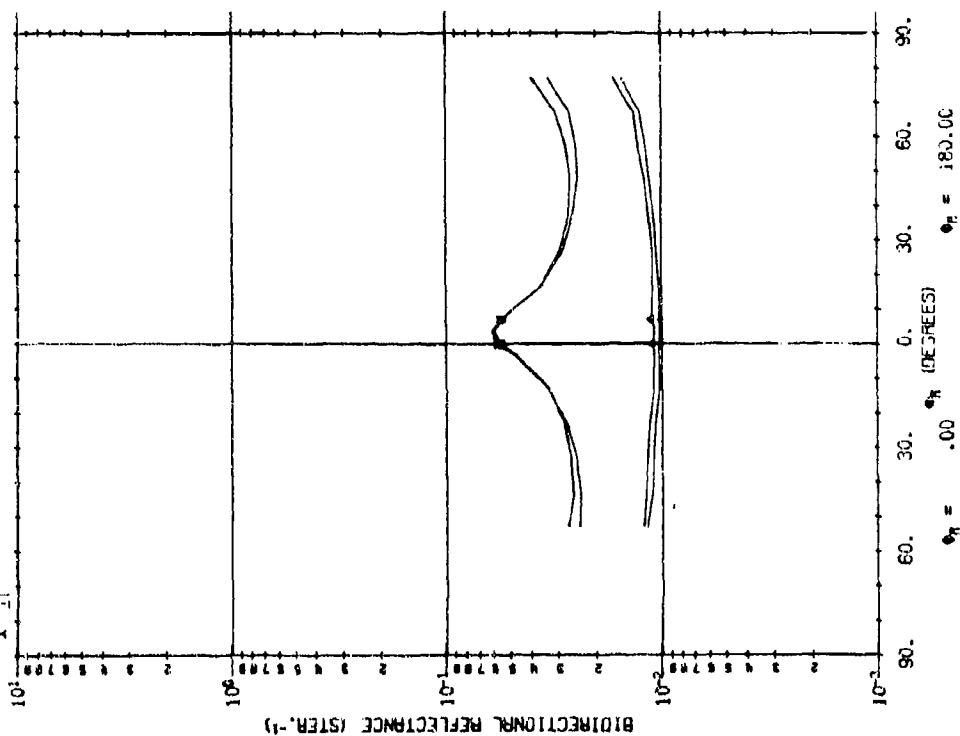


PAINT

R01342 005

OLIVE DRAB PAINT ON METAL

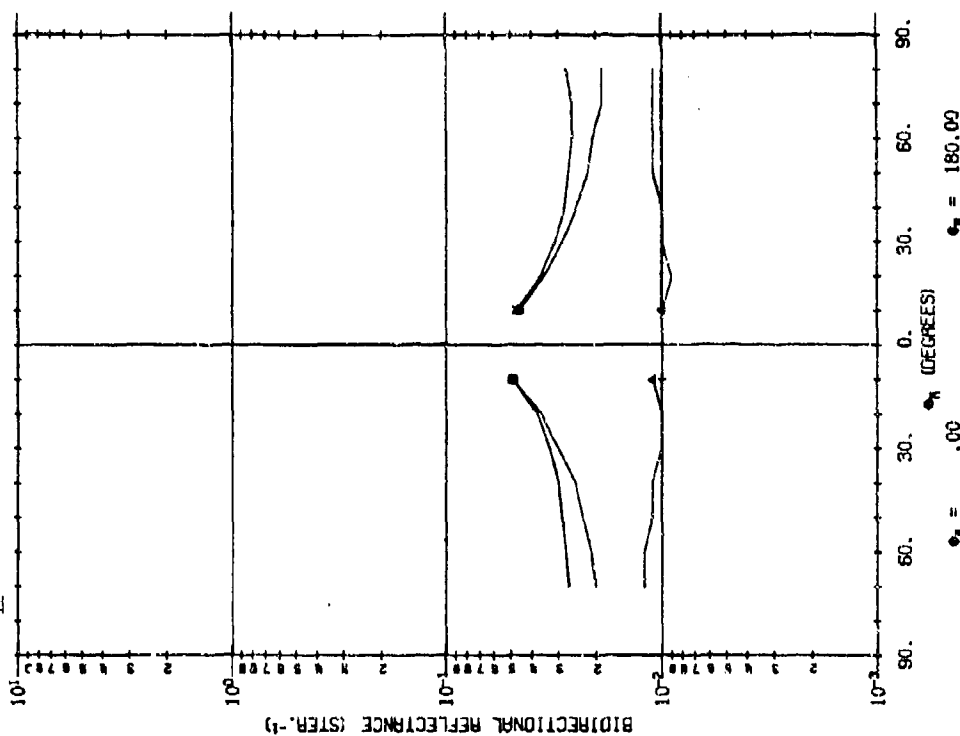
0 11 23 = 7.0  
+ 11  $\phi_1 = \phi_2$   
Δ 11  $\lambda = 0.63$   
X 11



R01342 005

OLIVE DRAB PAINT ON METAL

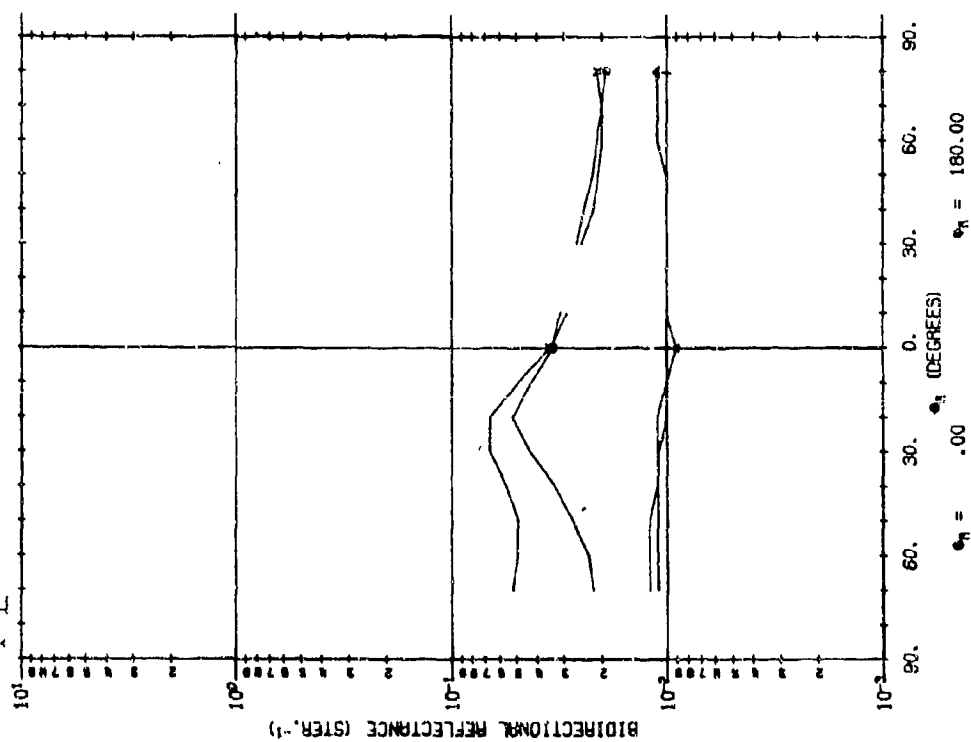
0 11  $\phi_1 = 0.0$   
+ 11  $\phi_1 = 180.00$   
Δ 11  $\lambda = 0.63$   
X 11



A01342 005

Olive Drab Paint on Metal

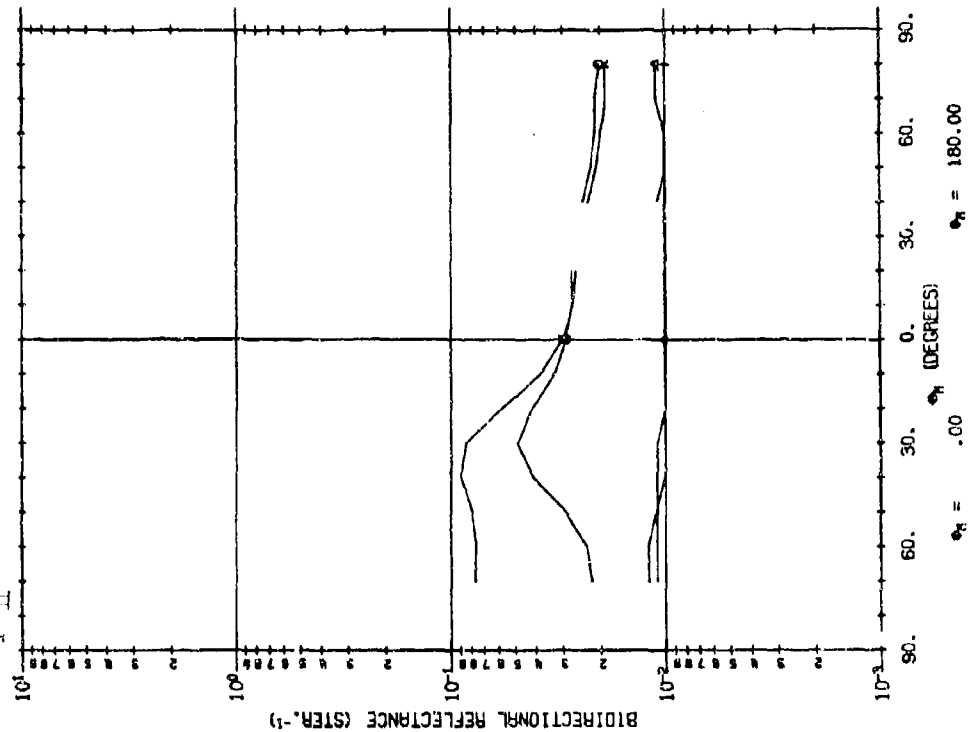
0 11 20.00  
+ 11 180.00  
Δ 11 0.63  
x 11



A01342 005

Olive Drab Paint on Metal

0 11 30.00  
+ 11 180.00  
Δ 11 0.63  
x 11



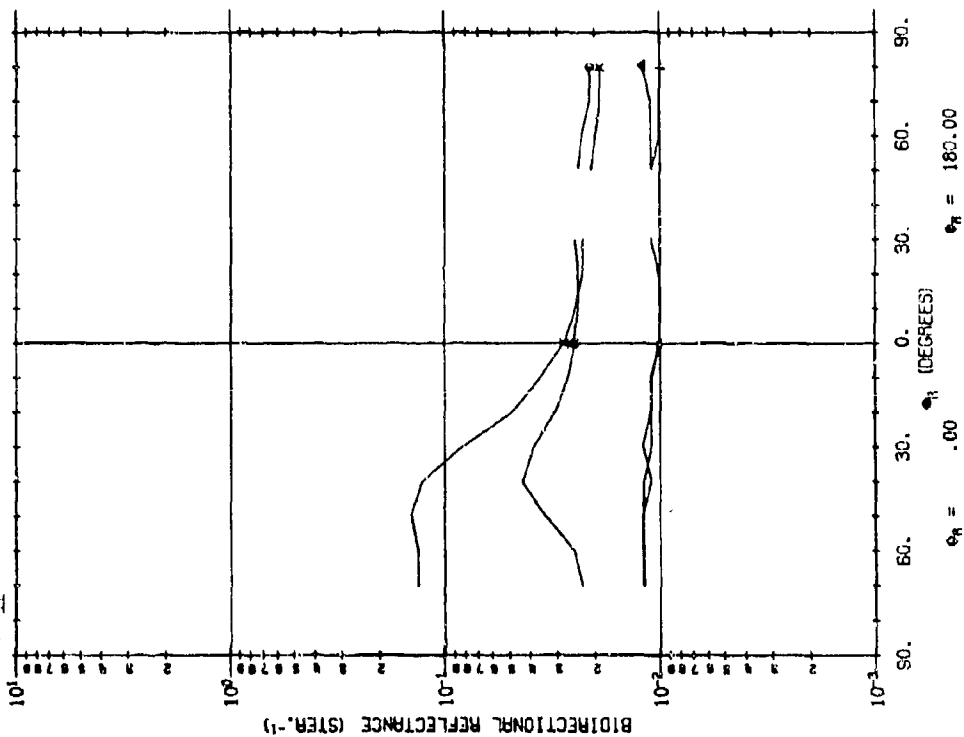
PAINT



A01342 005

Olive Drab Paint on Metal

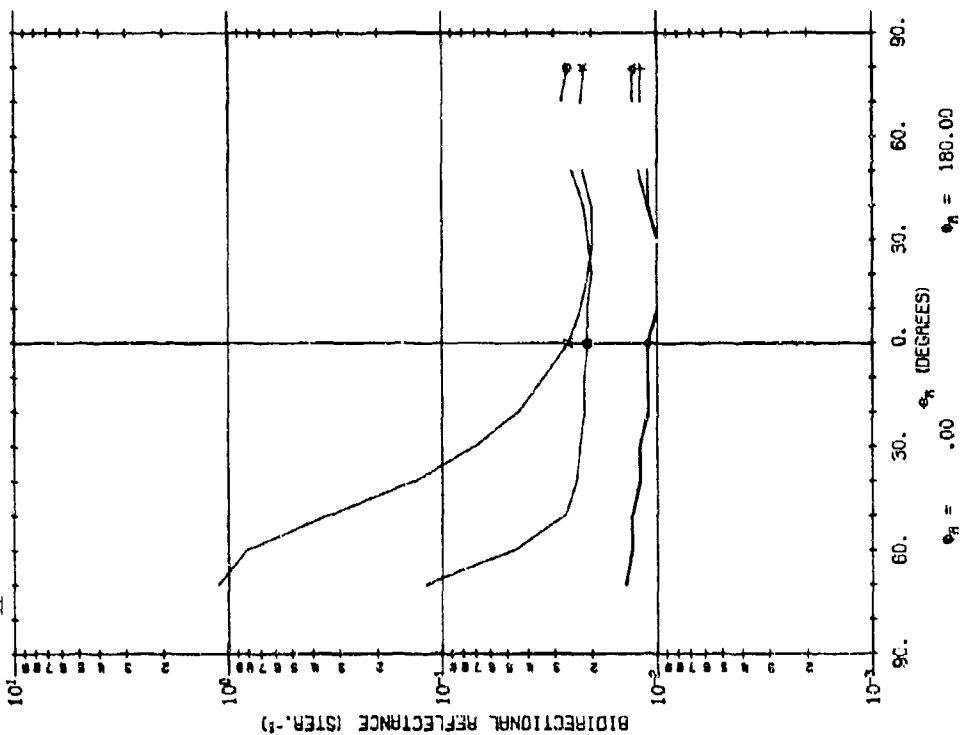
0 11 40.00  
+ 11 180.00  
Δ 11 0.63  
x 11



A01342 005

Olive Drab Paint on Metal

0 11 60.00  
+ 11 180.00  
Δ 11 0.63  
x 11

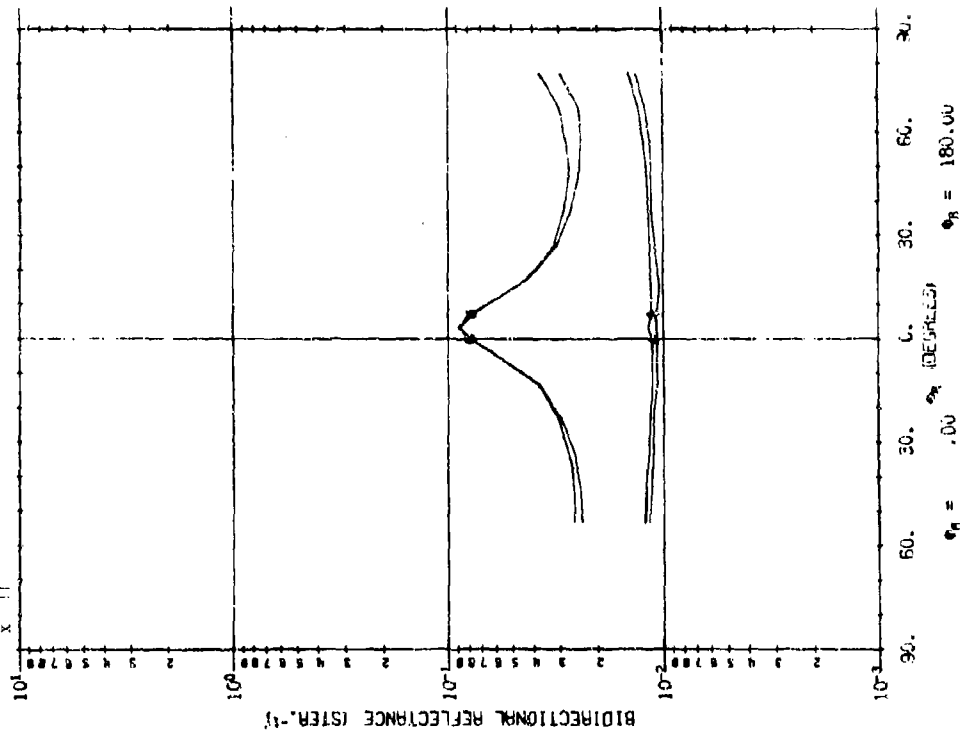




A01343 004

OLIVE DRAB PAINT ON METAL

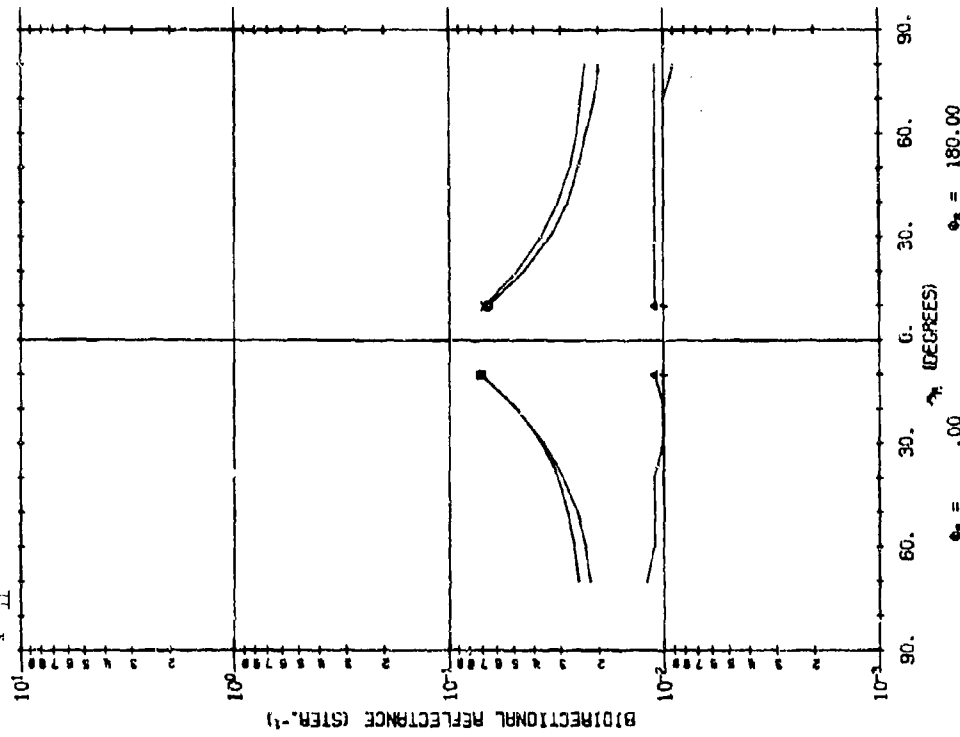
0 || 23 = 7.0  
+ ||  $\phi_1 = \phi_2$   
x ||  $\lambda_1 = 0.63$



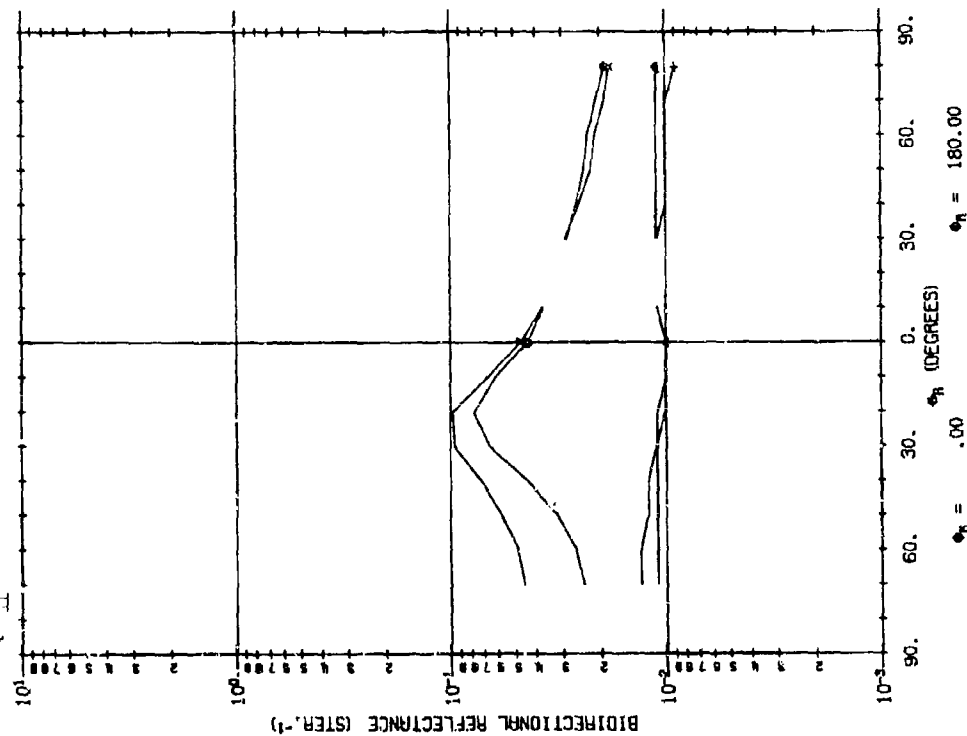
A01343 004

OLIVE DRAB PAINT ON METAL

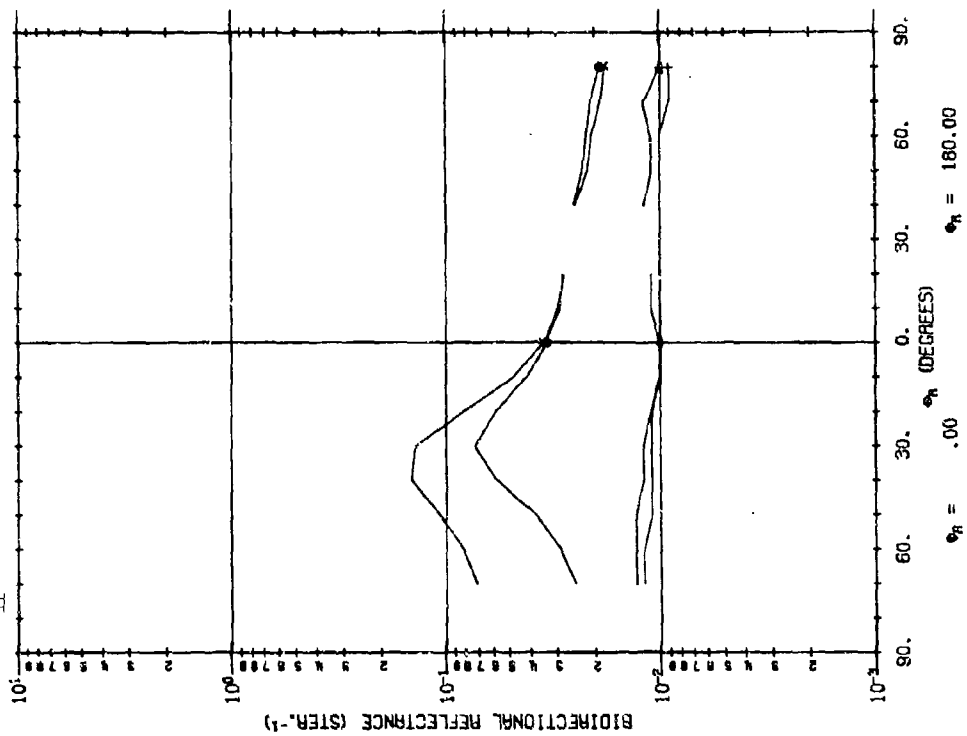
0 ||  $\phi_1 = 0.0$   
+ ||  $\phi_1 = 180.00$   
x ||  $\lambda_1 = 0.63$



A01343 004  
 Olive Drab Paint on Metal  
 $\phi_1 = 20.00$   
 $\phi_2 = 180.00$   
 $\lambda = 0.63$



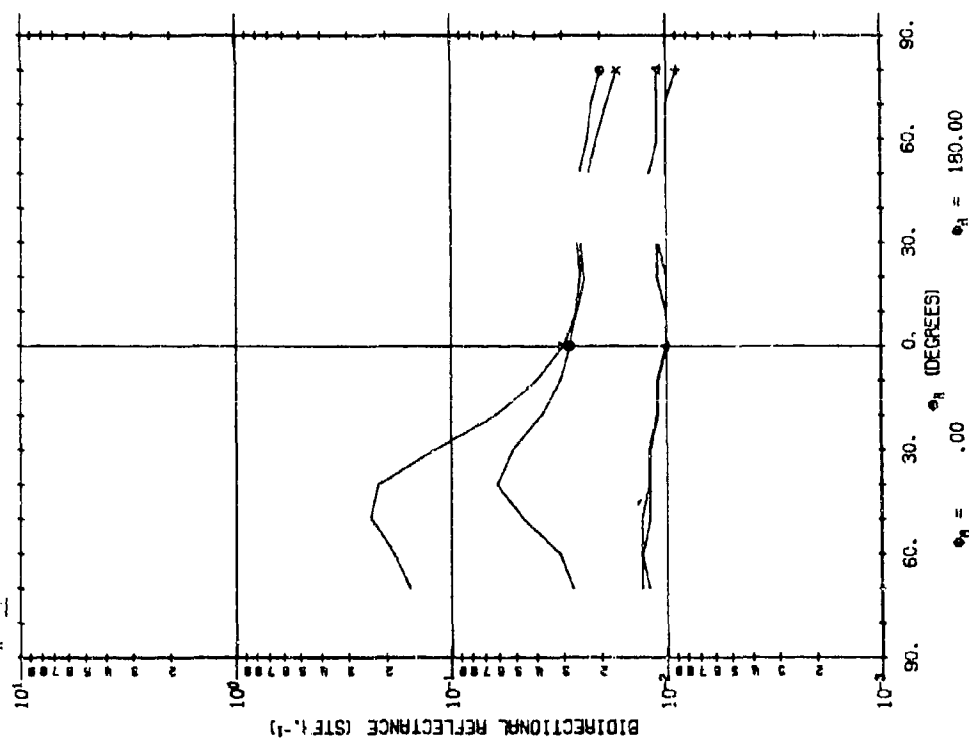
A01343 004  
 Olive Drab Paint on Metal  
 $\phi_1 = 30.00$   
 $\phi_2 = 180.00$   
 $\lambda = 0.63$



PAINT

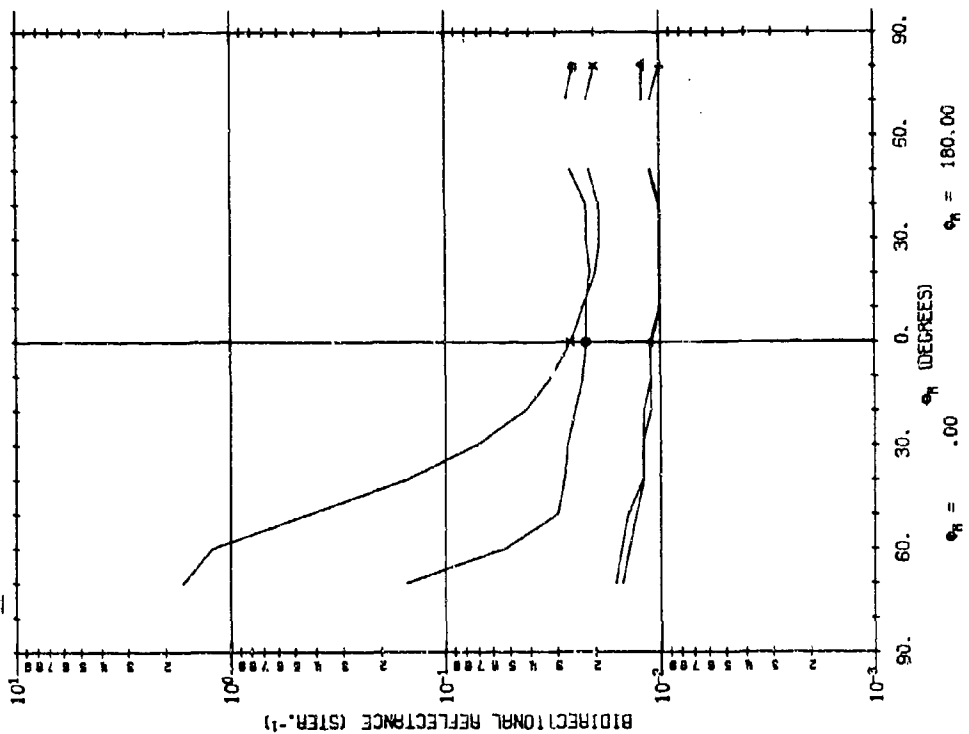
A01343 004  
 $\theta_0 = 0^\circ$   
 $\theta_1 = 40.00^\circ$   
 $\phi_1 = 180.00^\circ$   
 $\lambda = 0.63$

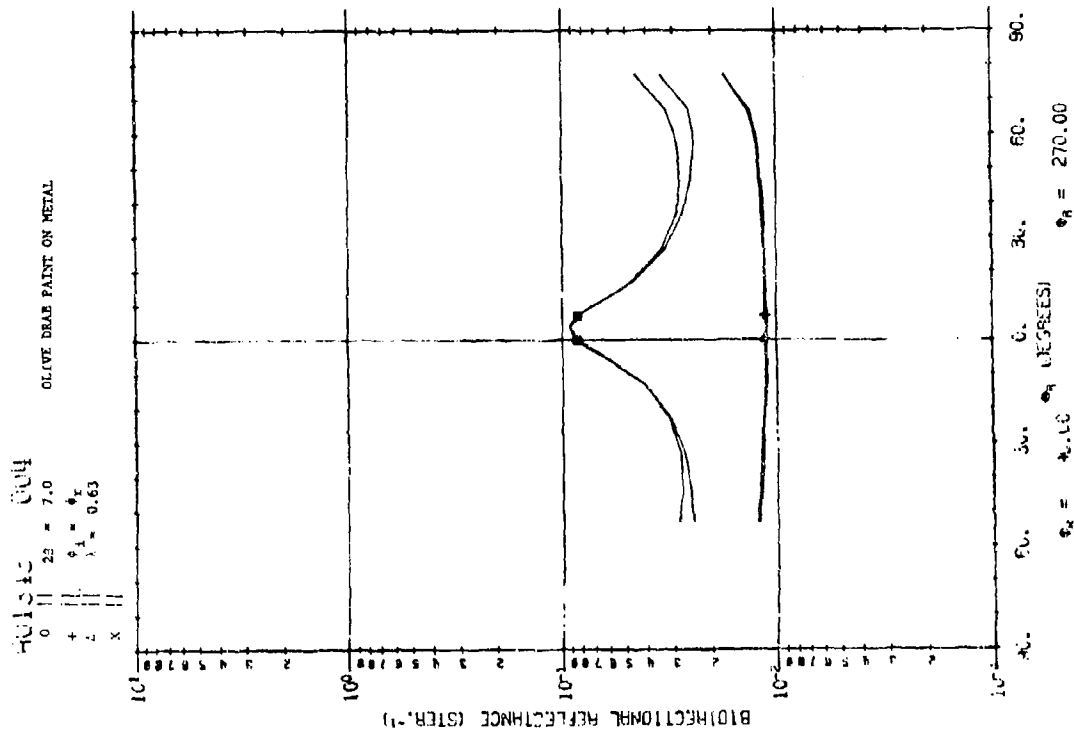
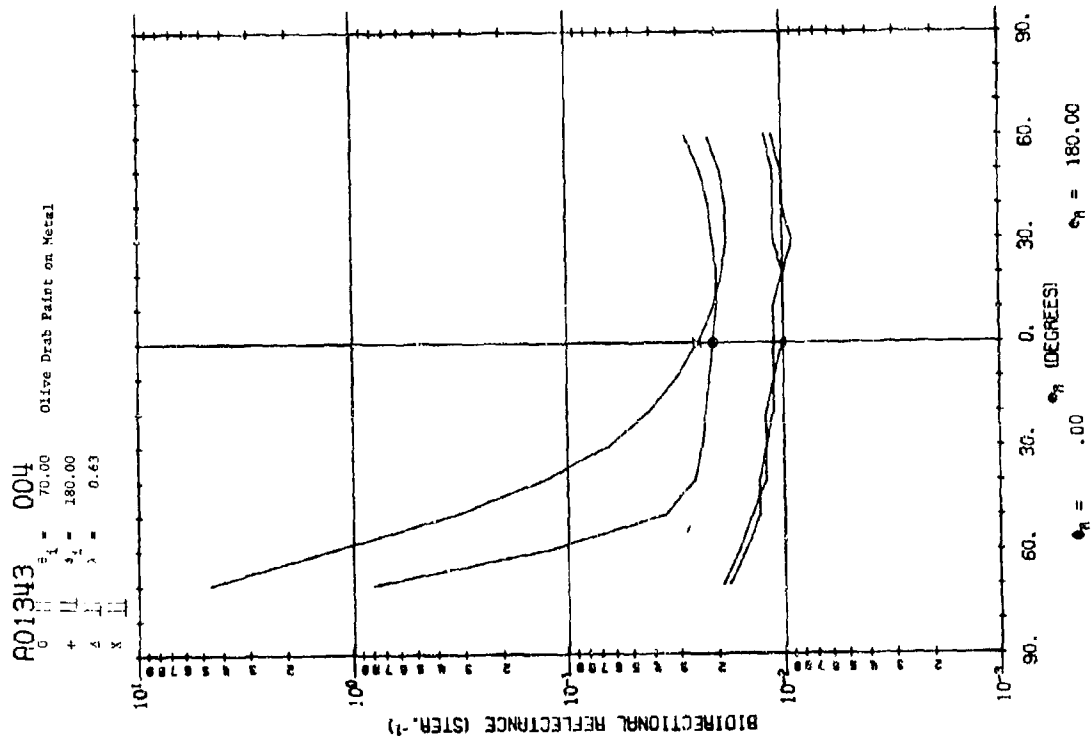
Olive Drab Paint on Metal



A01343 004  
 $\theta_0 = 0^\circ$   
 $\theta_1 = 60.00^\circ$   
 $\phi_1 = 180.00^\circ$   
 $\lambda = 0.63$

Olive Drab Paint on Metal



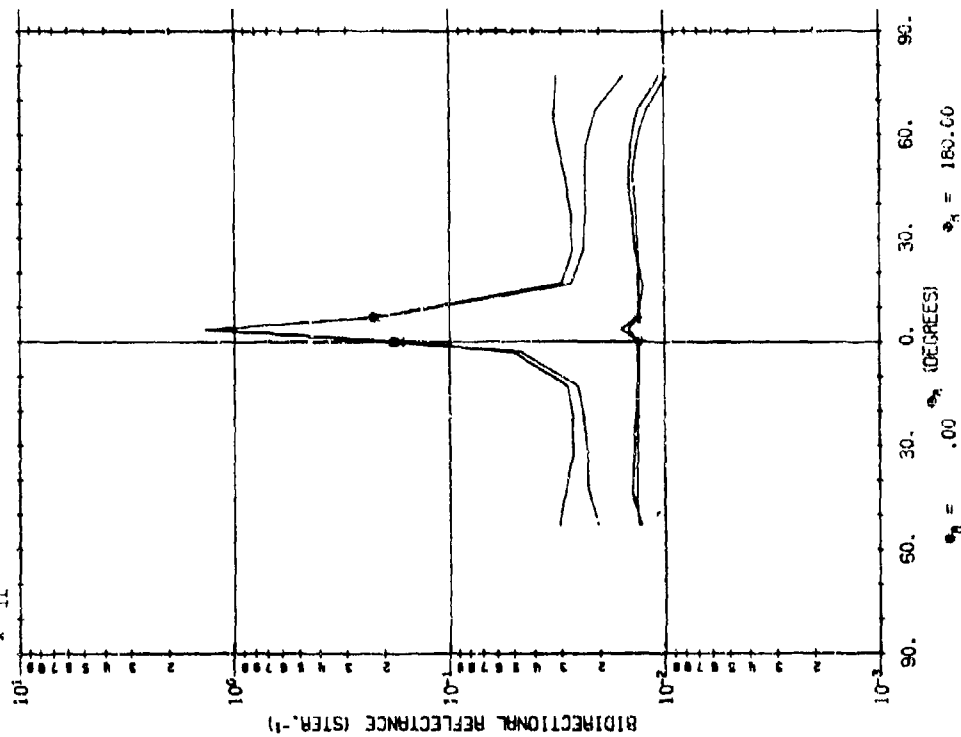


PAINT

001444 004

BLUE PAINT ON METAL

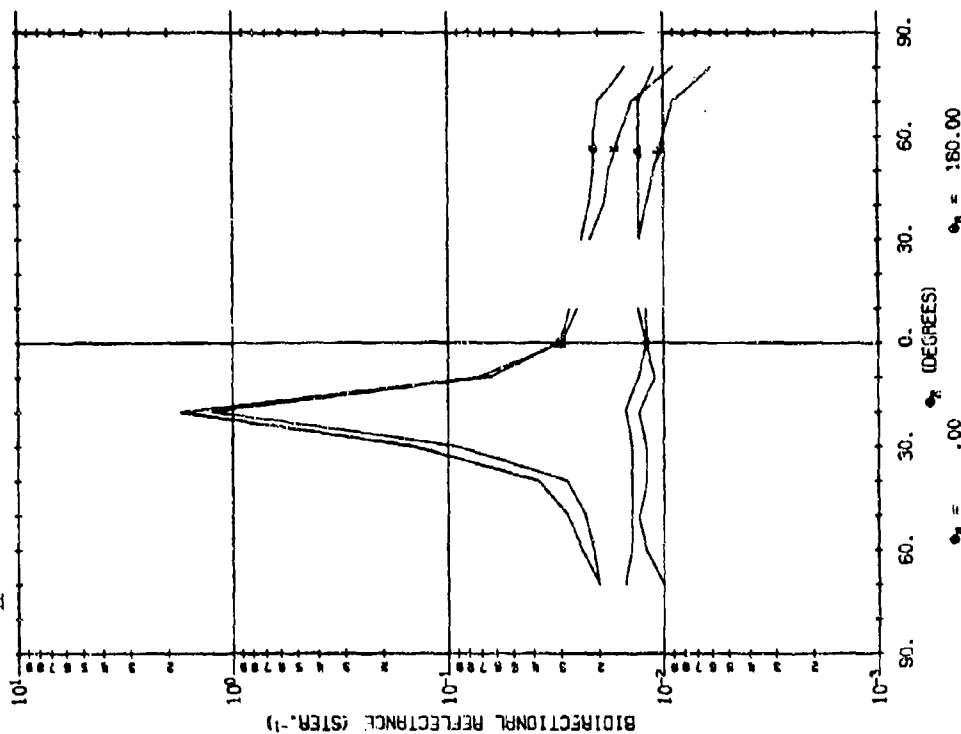
0 11 22 = 7.0  
+ 11 41 = 4x  
2 11 1 = 0.63  
x 11



001444 004

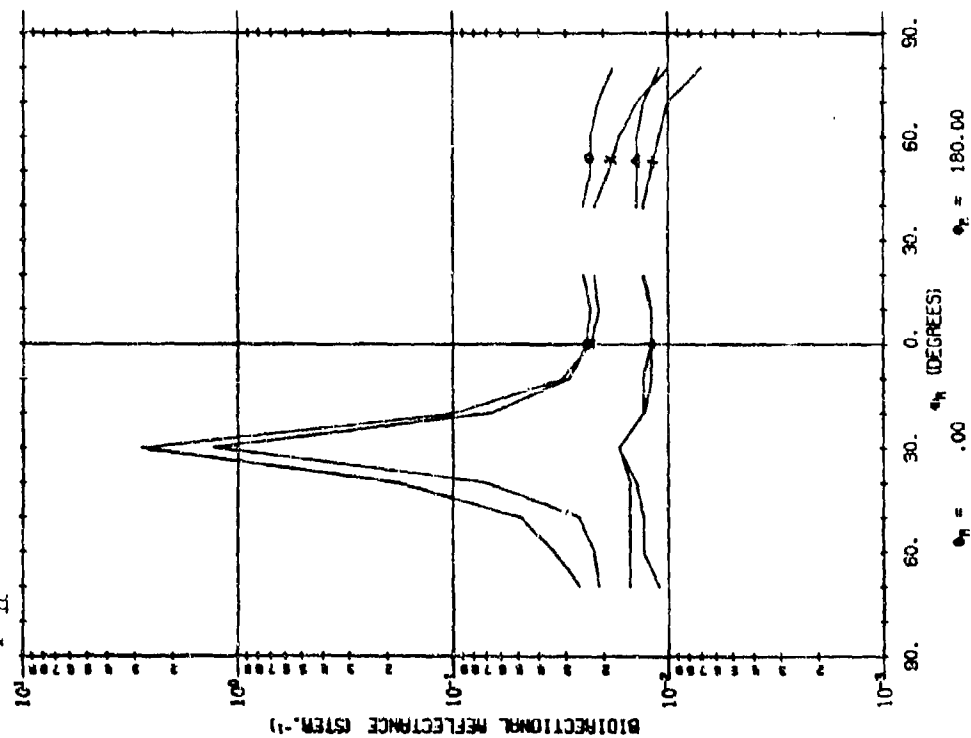
Blue Paint on Metal

0 11 22 = 25.00  
+ 11 41 = 180.0  
2 11 1 = .63  
x 11



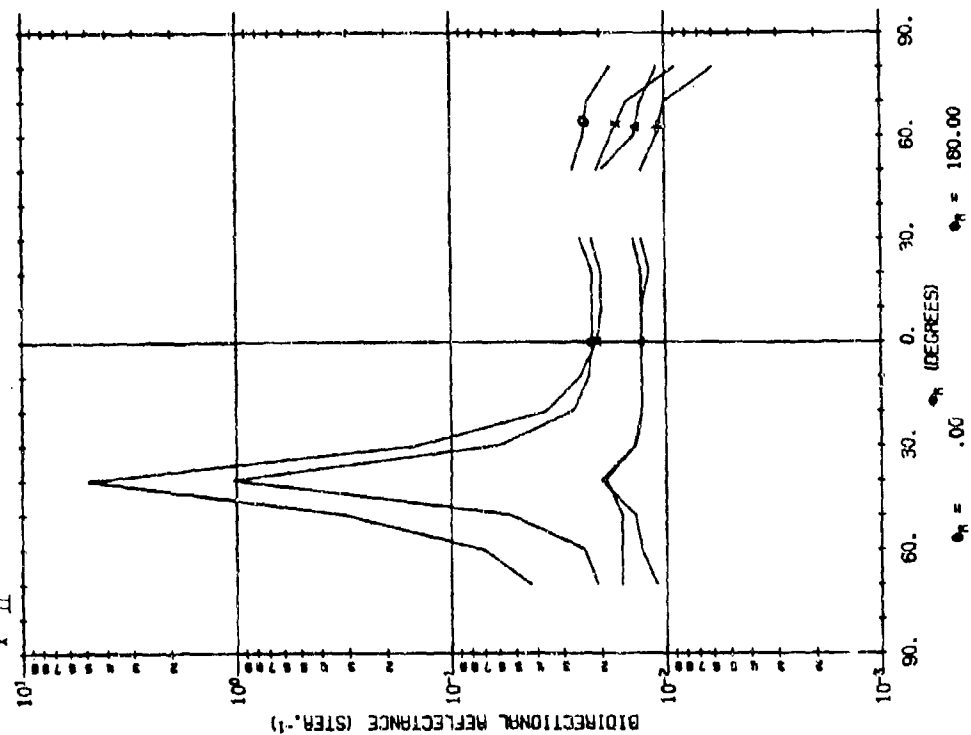
R01444 004  
 0 II  $\epsilon_1 = 30.0$   
 + II  $\epsilon_2 = 180.0$   
 4 II  $\lambda = .63$   
 X II

Blue Paint on Metal



R01444 004  
 0 II  $\epsilon_1 = 40.0$   
 + II  $\epsilon_2 = 180.0$   
 4 II  $\lambda = .63$   
 X II

Blue Paint on Metal



PAINT

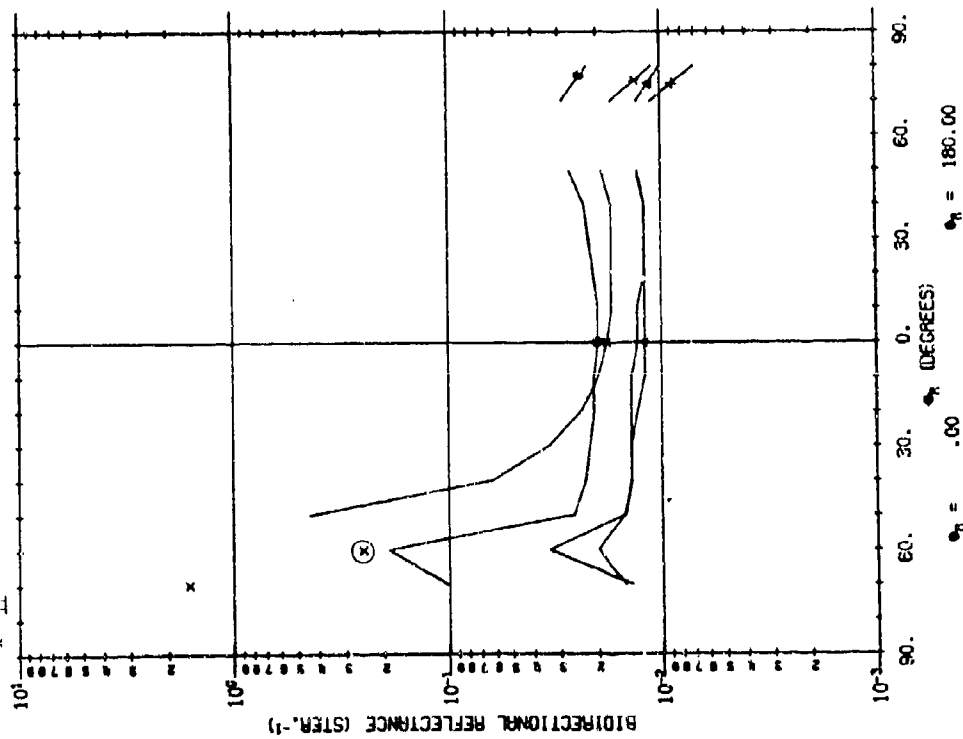


004

Blue Paint on Metal

0 11 11 11  
+ 11 11 11 11  
x 11 11 11 11  
x 11 11 11 11

$\epsilon_1 = 60.0$   
 $\phi_1 = 150.0$   
 $\lambda = .63$

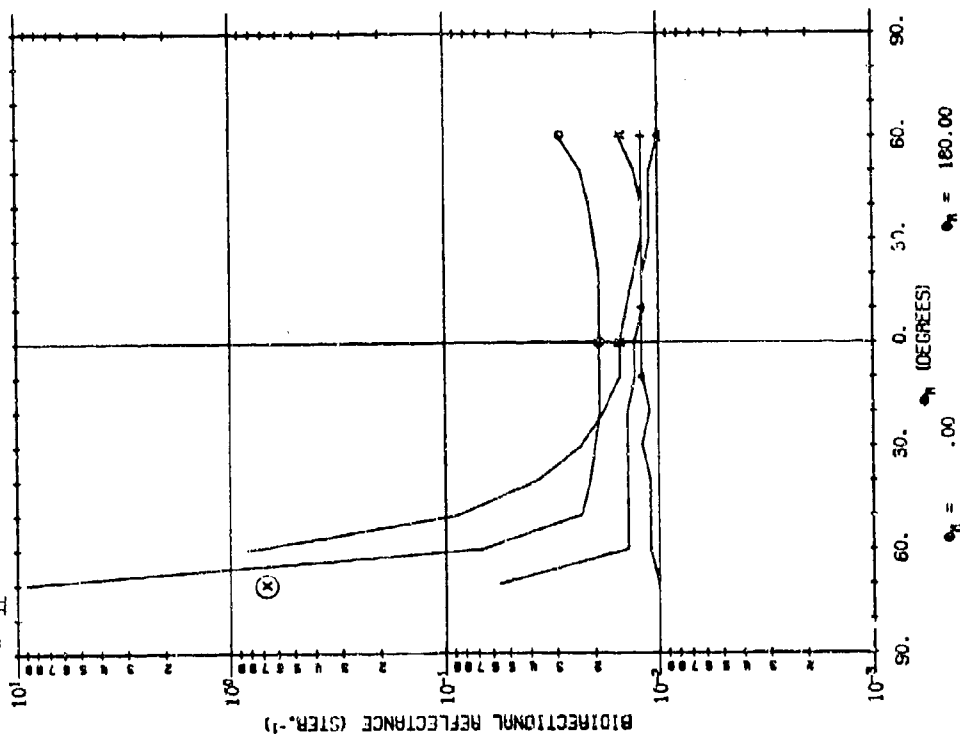


004

Blue Paint on Metal

0 11 11 11  
+ 11 11 11 11  
x 11 11 11 11  
x 11 11 11 11

$\epsilon_1 = 70.0$   
 $\phi_1 = 180.0$   
 $\lambda = .63$



801444 004

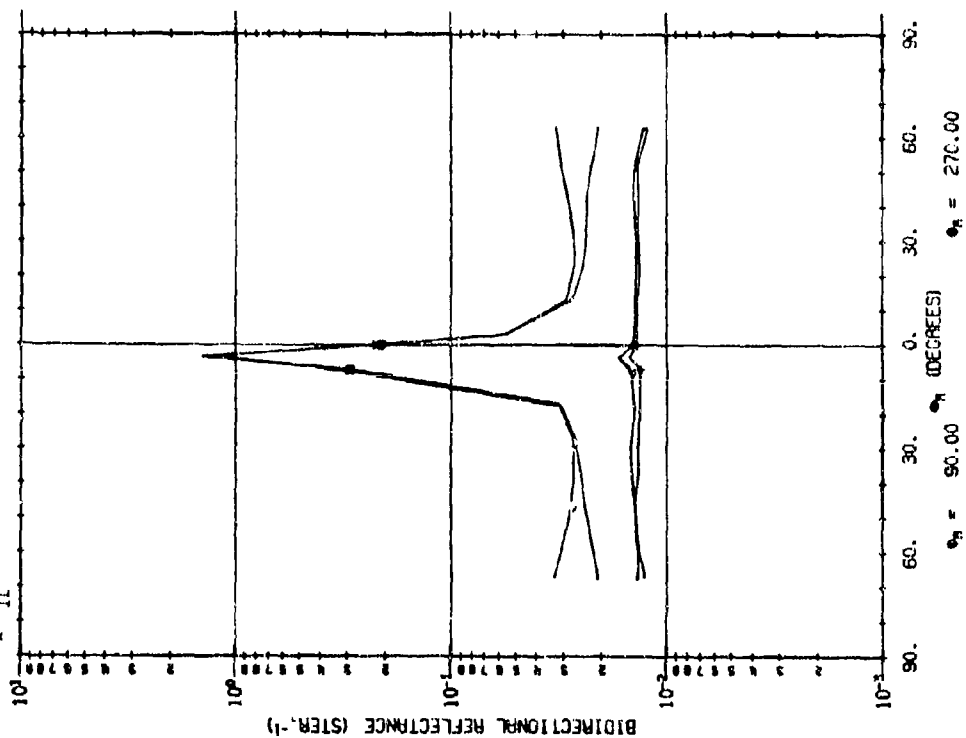
BLUE PAINT ON METAL

0 11 28 = 7.0

+ 11  $\phi_1 = \phi_r$

Δ 11  $\lambda = 0.63$

X 11



801444 005

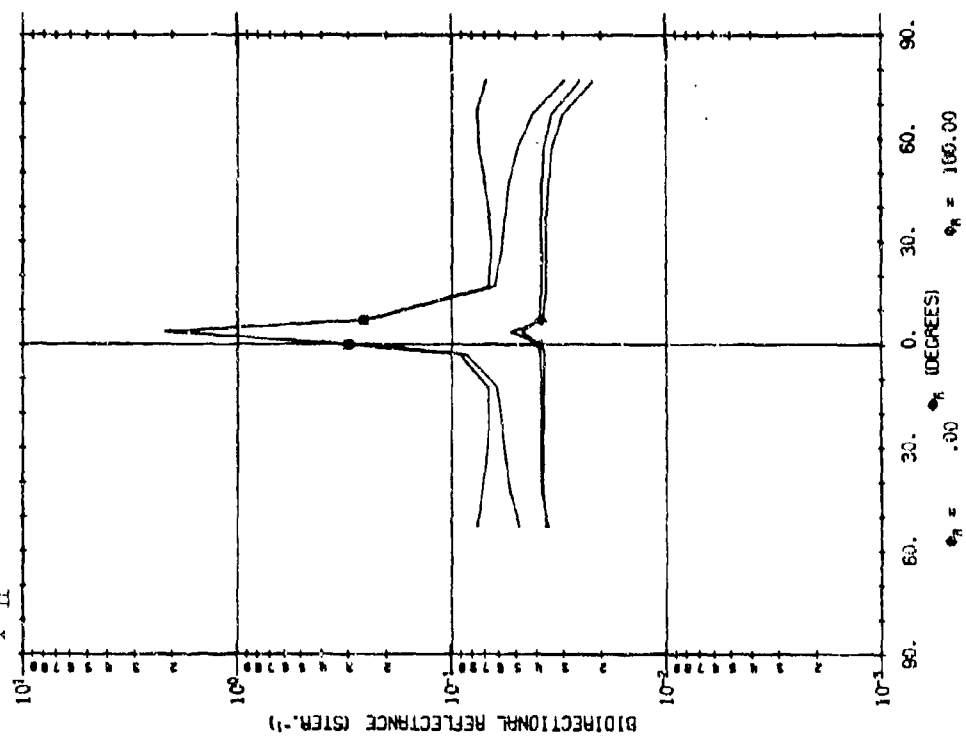
BLUE PAINT ON METAL

0 11 28 = 7.0

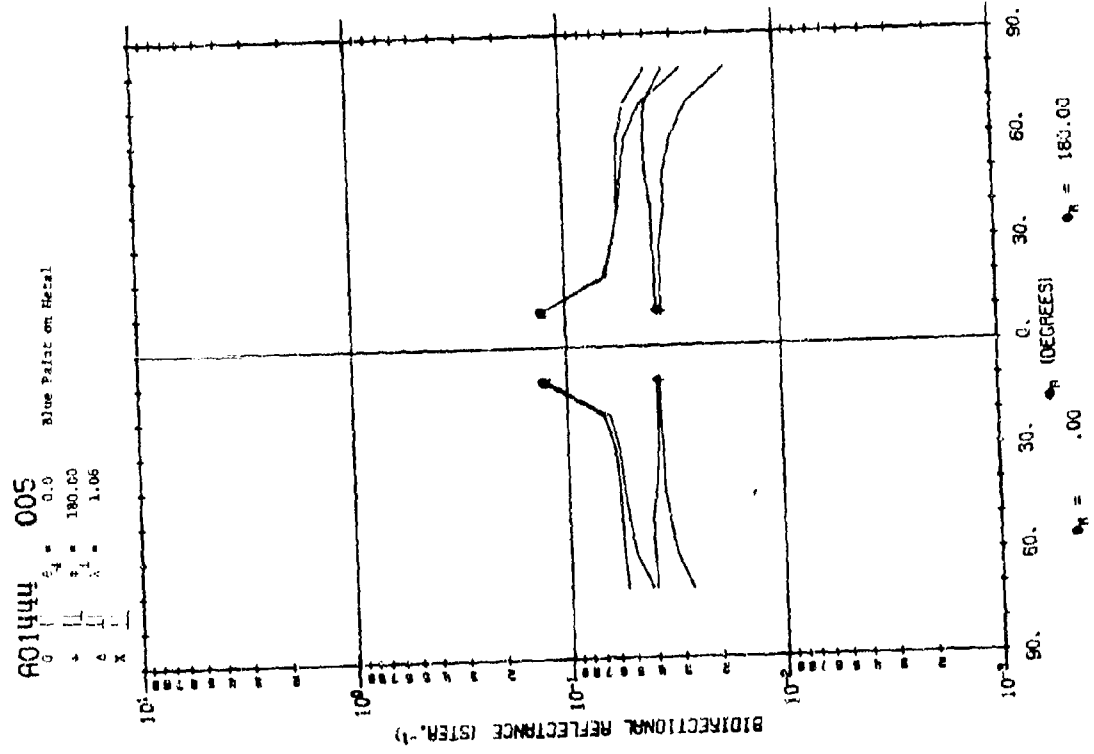
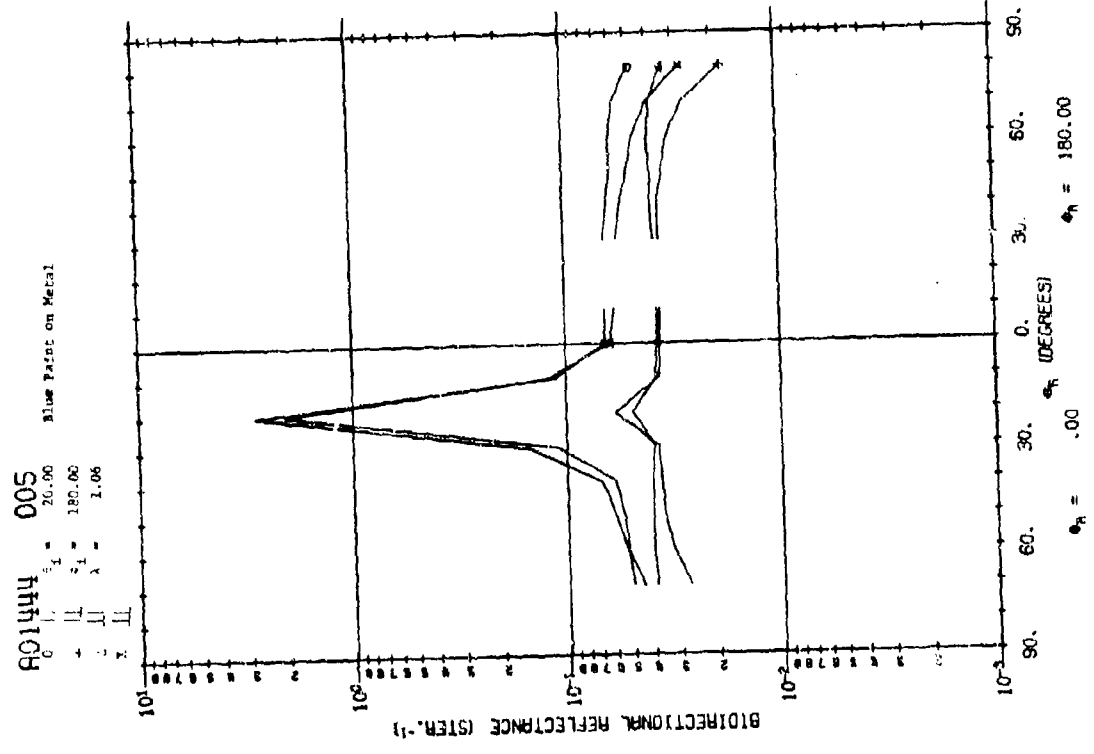
+ 11  $\phi_1 = \phi_r$

Δ 11  $\lambda = 1.06$

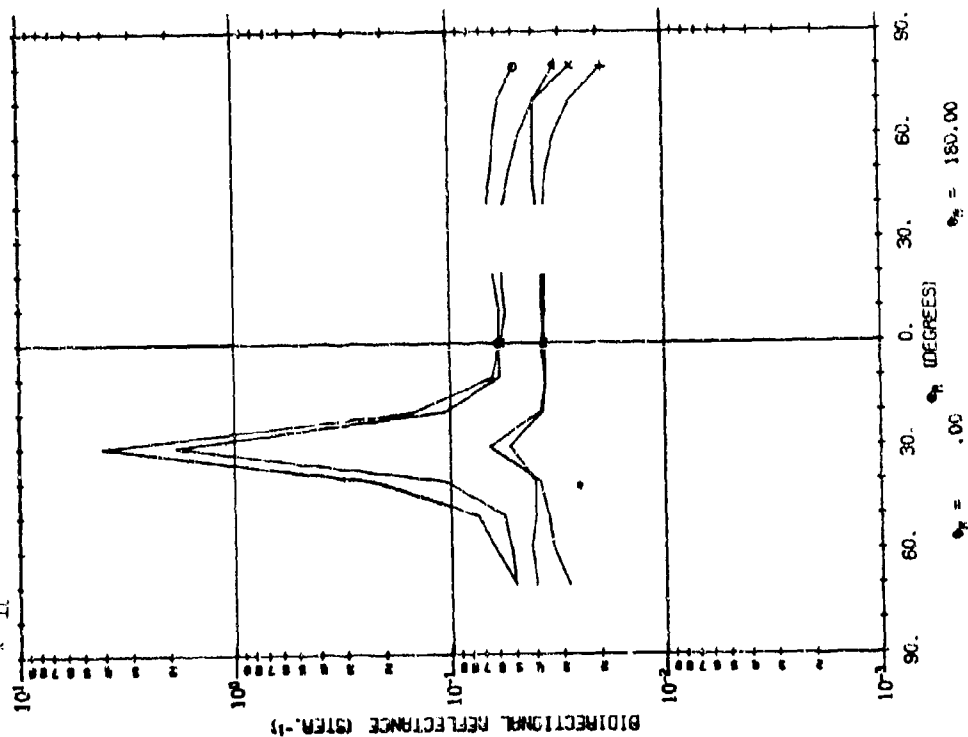
X 11



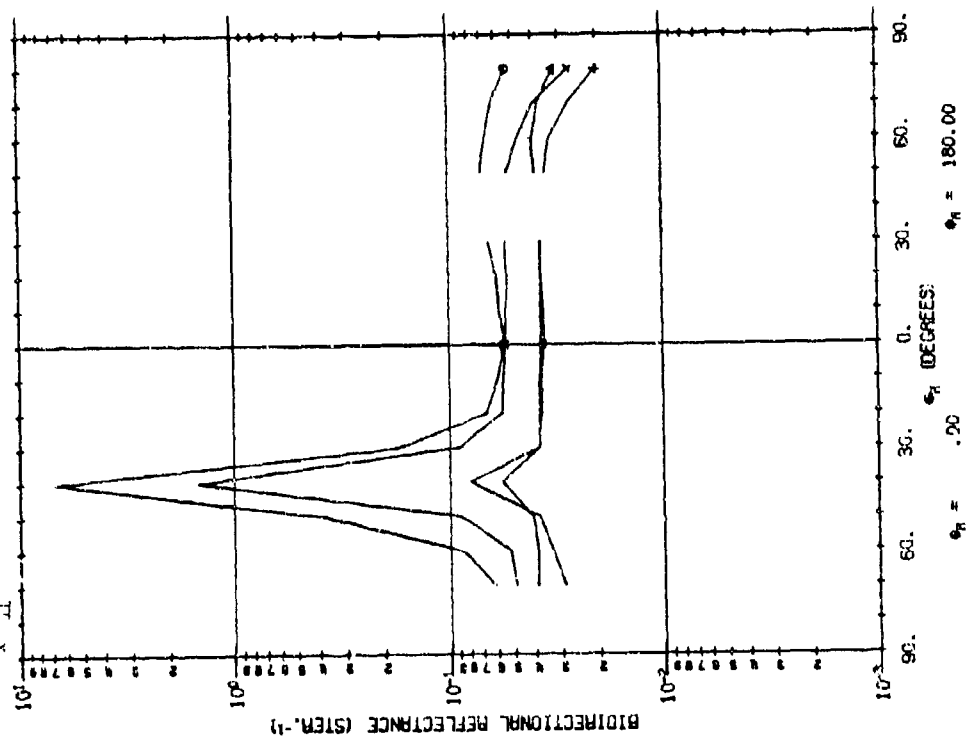
PAIN



RG1444 005  
Blue Paint on Metal  
 $\theta_i = 30.00$   
 $\theta_r = 180.00$   
 $\lambda = 1.06$



RG1444 005  
Blue Paint on Metal  
 $\theta_i = 40.00$   
 $\theta_r = 180.00$   
 $\lambda = 1.06$



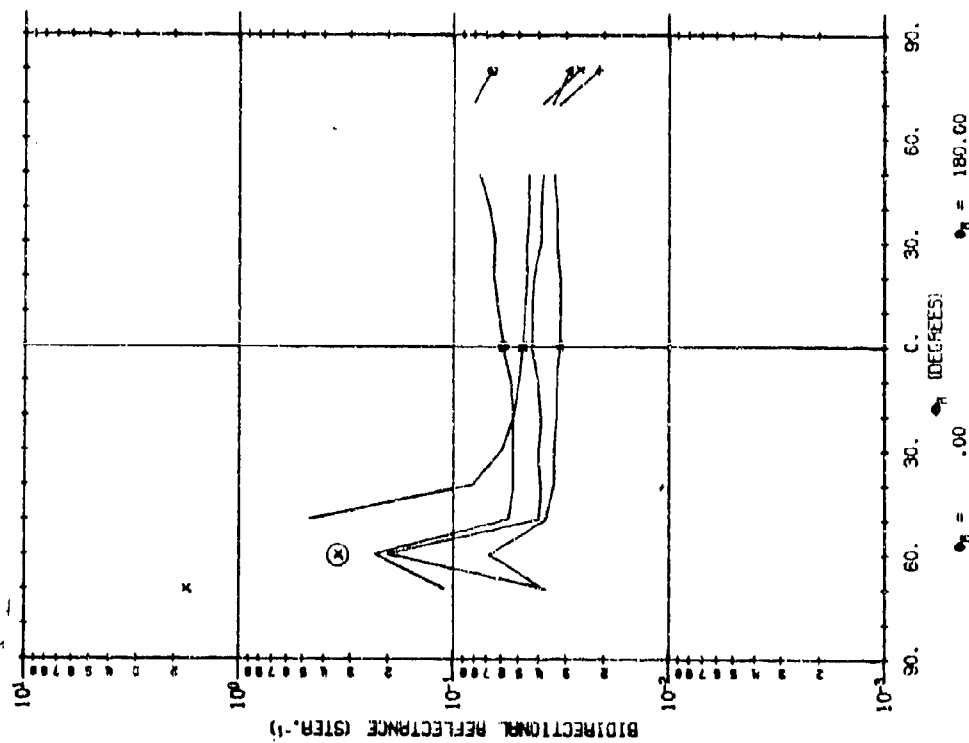
PAINT

R01444 005  
Blue Paint on Metal

$\theta_i = 50.00$

$\theta_r = 180.00$

$\theta_n = 1.06$



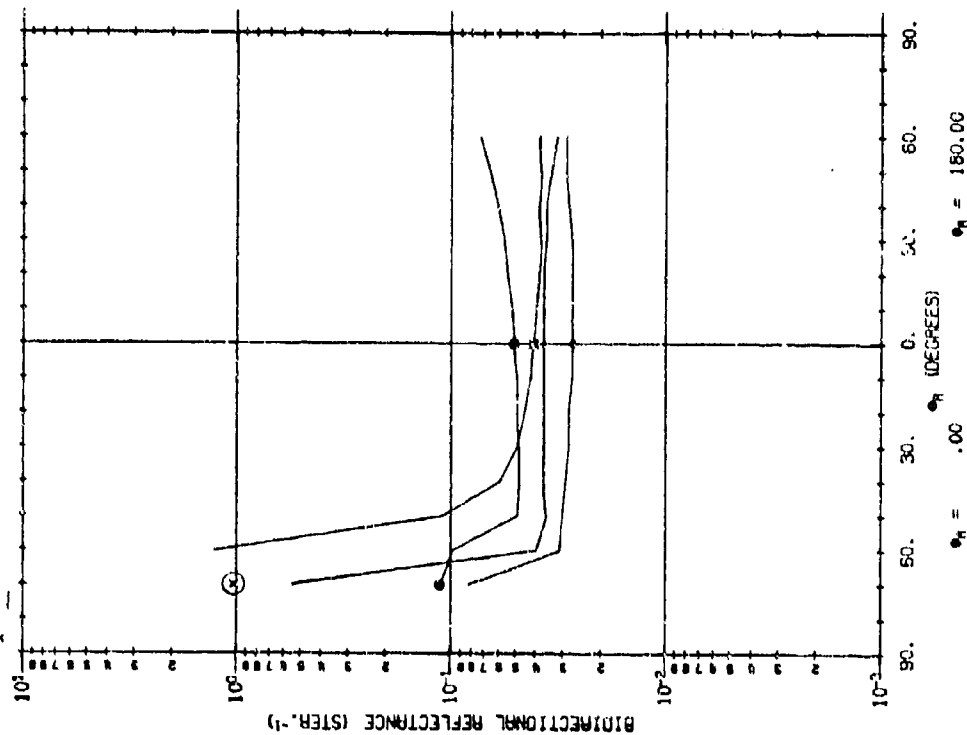
R01444 005

Blue Paint on Metal

$\theta_i = 70.00$

$\theta_r = 180.00$

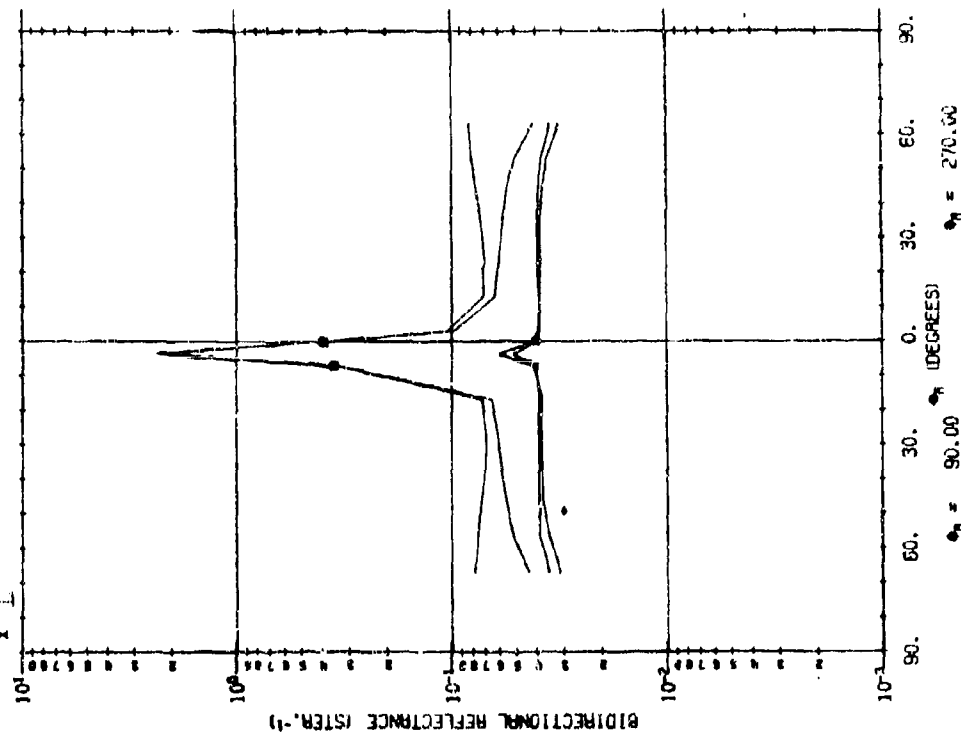
$\theta_n = 1.06$



AO1444 005

BLUISH PAINT ON METAL

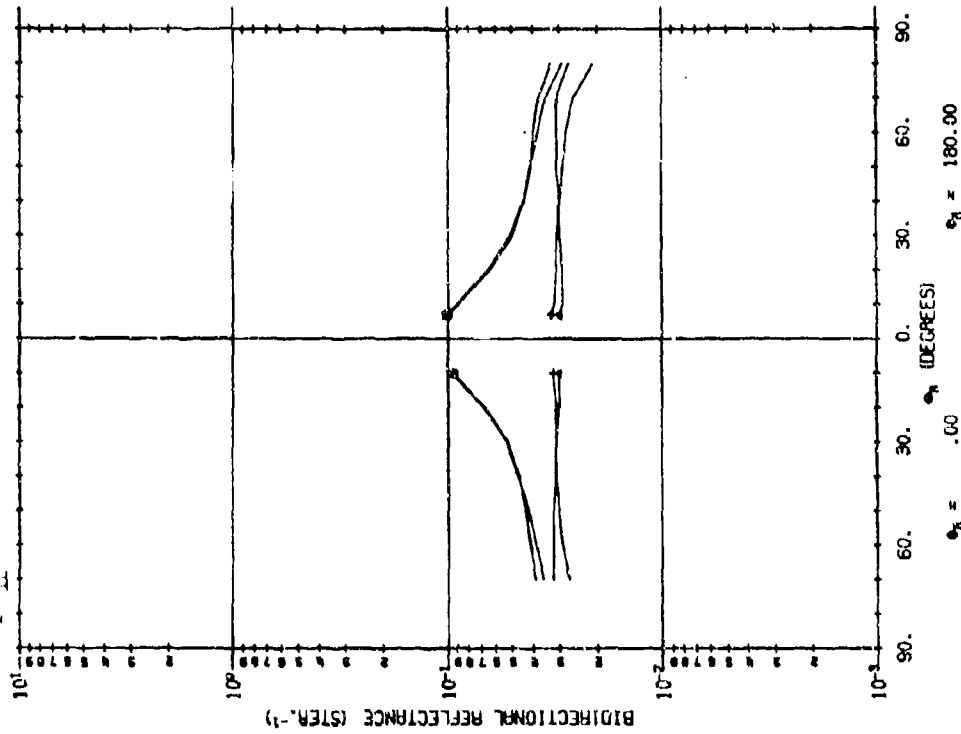
$2\theta = 7.0$   
 $\phi_1 = \phi_r$   
 $\lambda = 1.06$



AO1453 005

Light Brown Paint on Metal

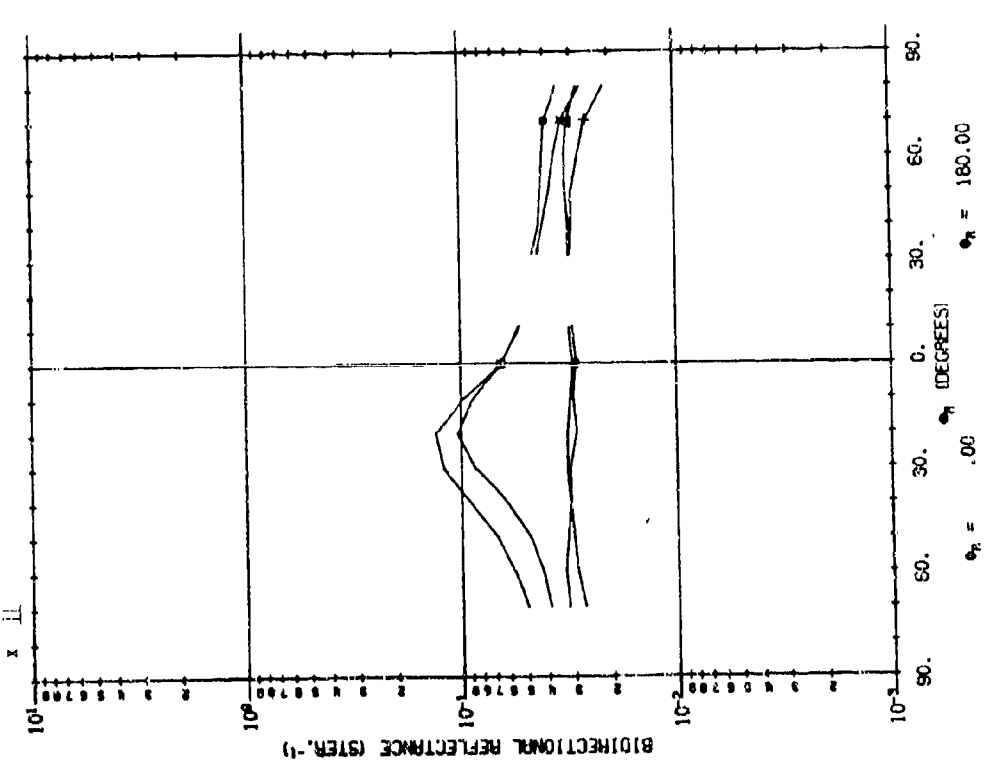
$\phi_1 = 0.0$   
 $\phi_2 = 180.0$   
 $\lambda = 0.63$



PAINT

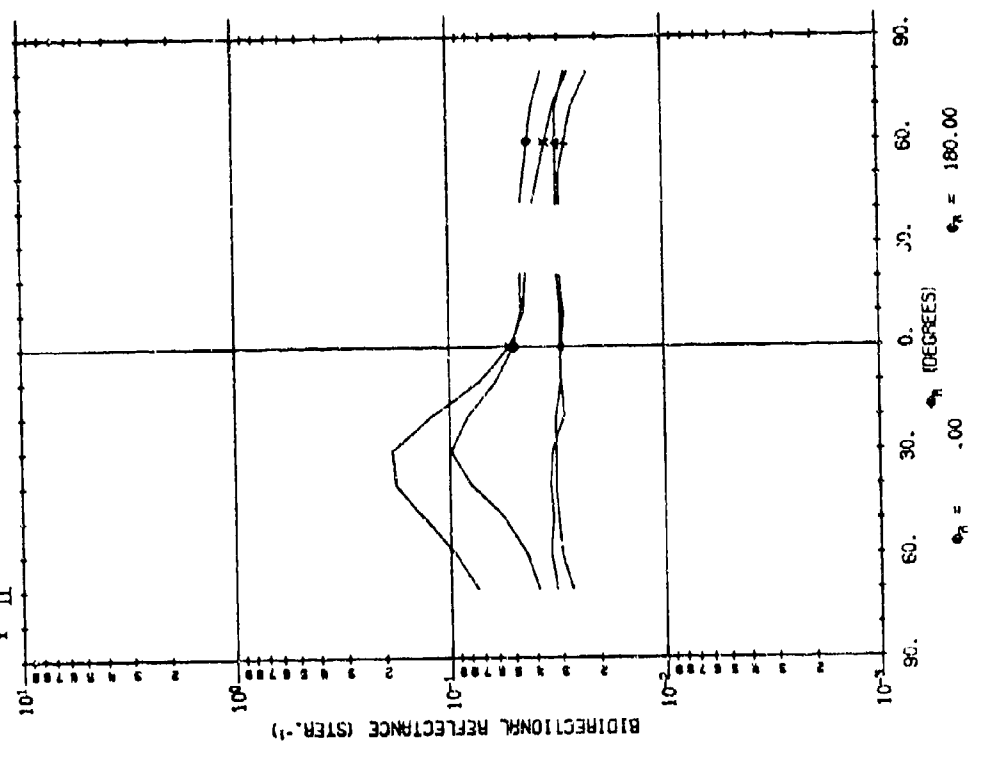
R01453 005  
 $\theta_i = 20.00$   
 $\phi_i = 180.00$   
 $\lambda = 0.63$

Light Brown Paint on Metal



R01453 005  
 $\theta_i = 30.00$   
 $\phi_i = 180.00$   
 $\lambda = 0.63$

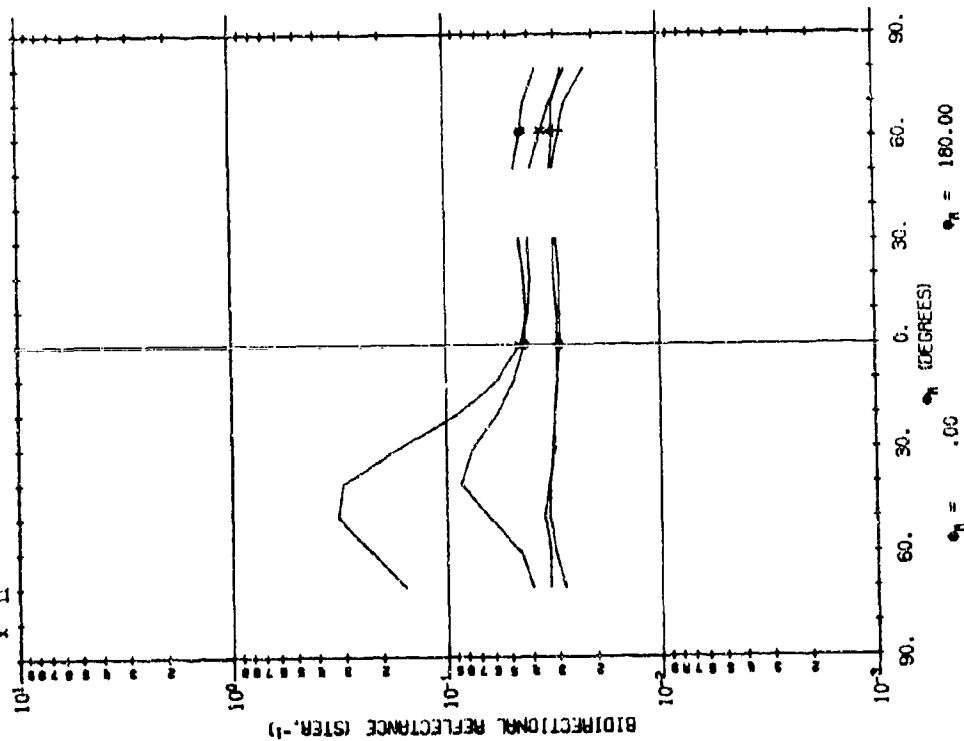
Light Brown Paint on Metal



A01453 005

Light Brown Paint on Metal

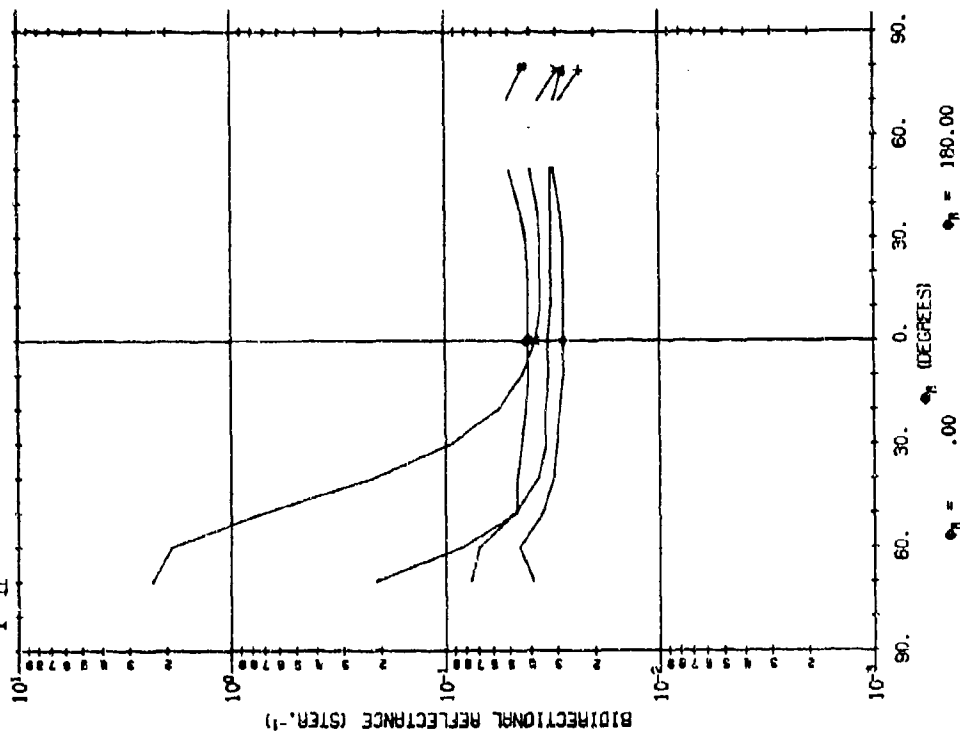
$\theta_1 = 40.00$   
 $\phi_1 = 180.00$   
 $\lambda = 0.63$



A01453 005

Light Brown Paint on Metal

$\theta_1 = 60.00$   
 $\phi_1 = 180.00$   
 $\lambda = 0.63$



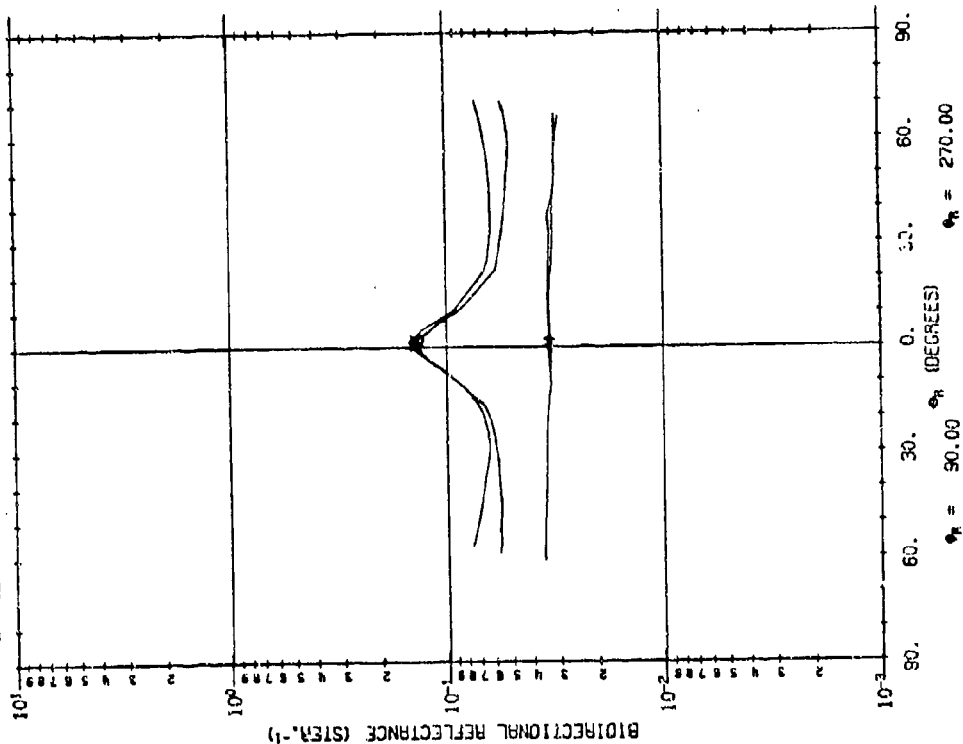
PAINT



A01453 005

LIGHT BROWN PAINT ON METAL

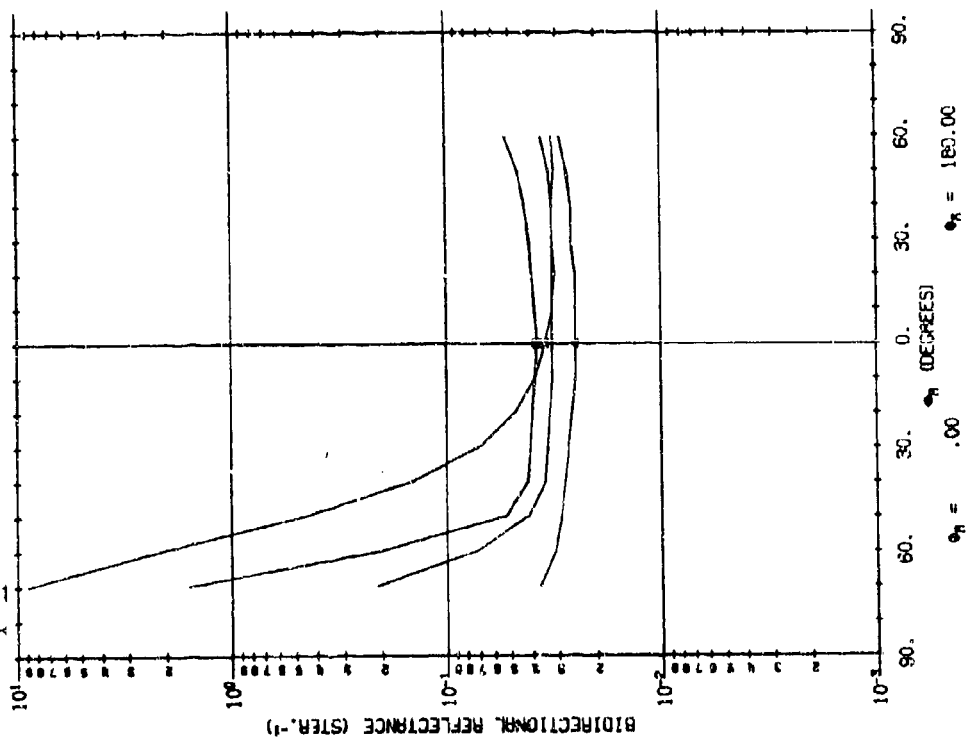
0 11 23 - 2.0  
+ 11  $\phi_1 = \phi_2$   
0 11  $\lambda = 0.63$   
X 11



A01453 005

Light Brown Paint on Metal

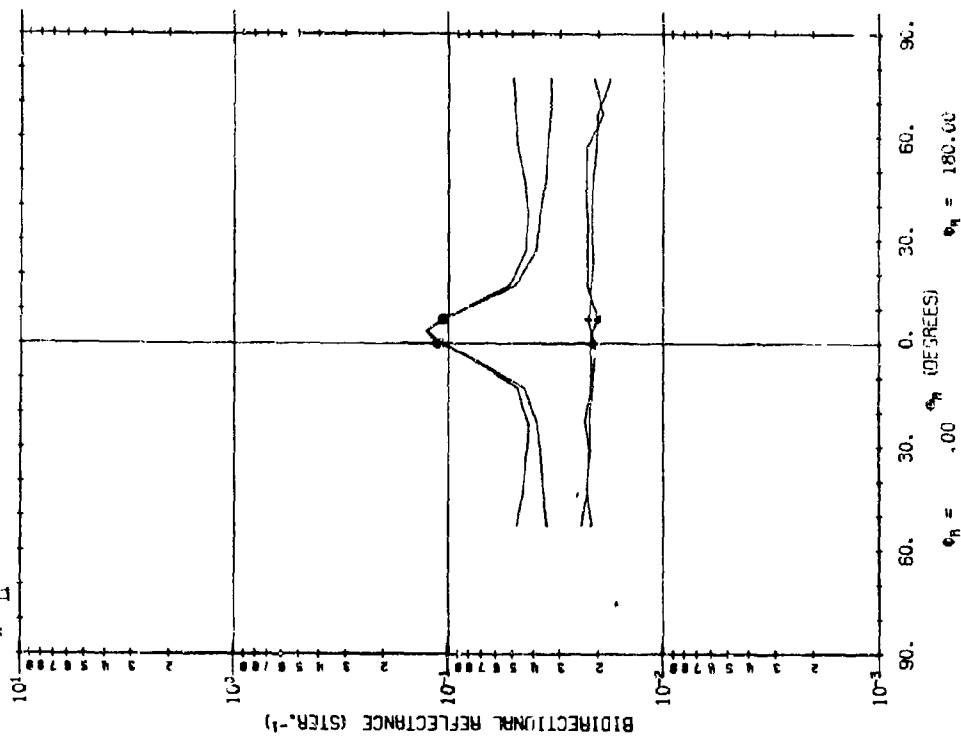
$\phi_1 = 70.00$   
 $\phi_2 = 180.00$   
 $\lambda = 0.63$



A01453 006

LIGHT BROWN PAINT ON METAL

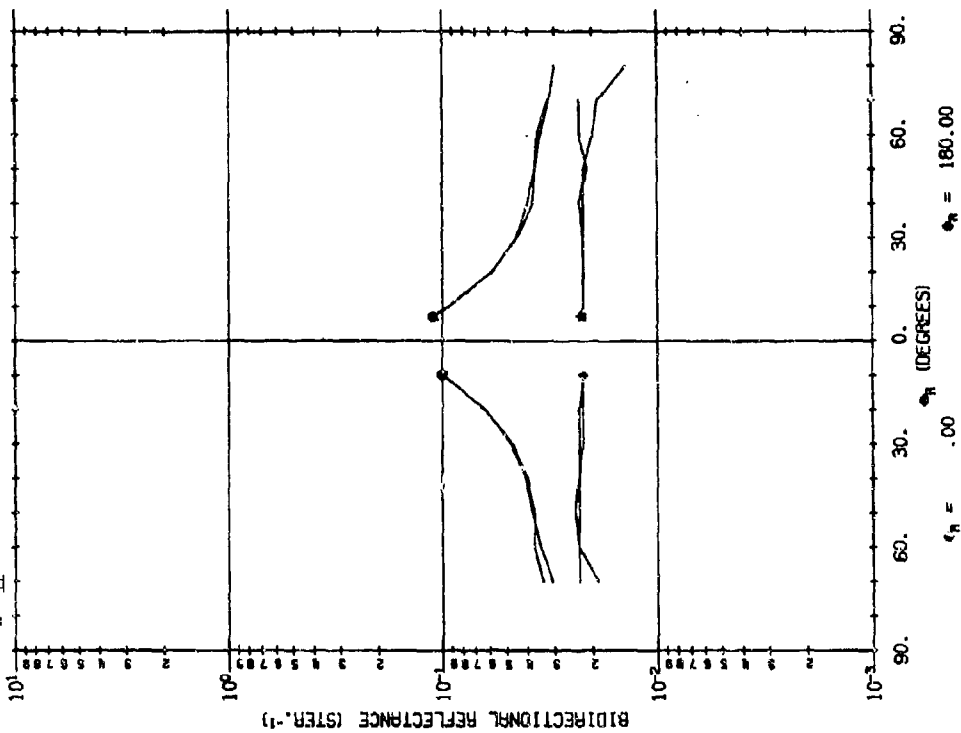
$\phi_i = 0.0$   
 $\phi_f = 180.00$   
 $\lambda = 1.06$



A01453 006

Light Brown Paint on Metal

$\phi_i = 0.0$   
 $\phi_f = 180.00$   
 $\lambda = 1.06$



PAINT

AO1453 006

Light Brown Paint on Metal

$\rho_1 = 20.00$   
 $\phi_1 = 180.00$   
 $\lambda = 1.06$

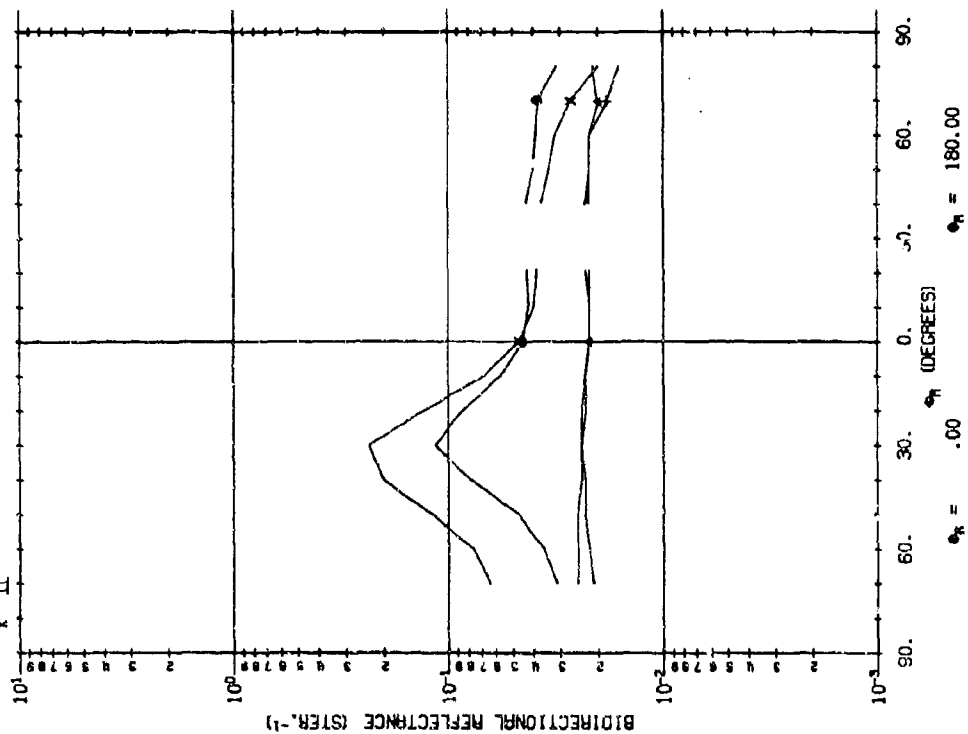
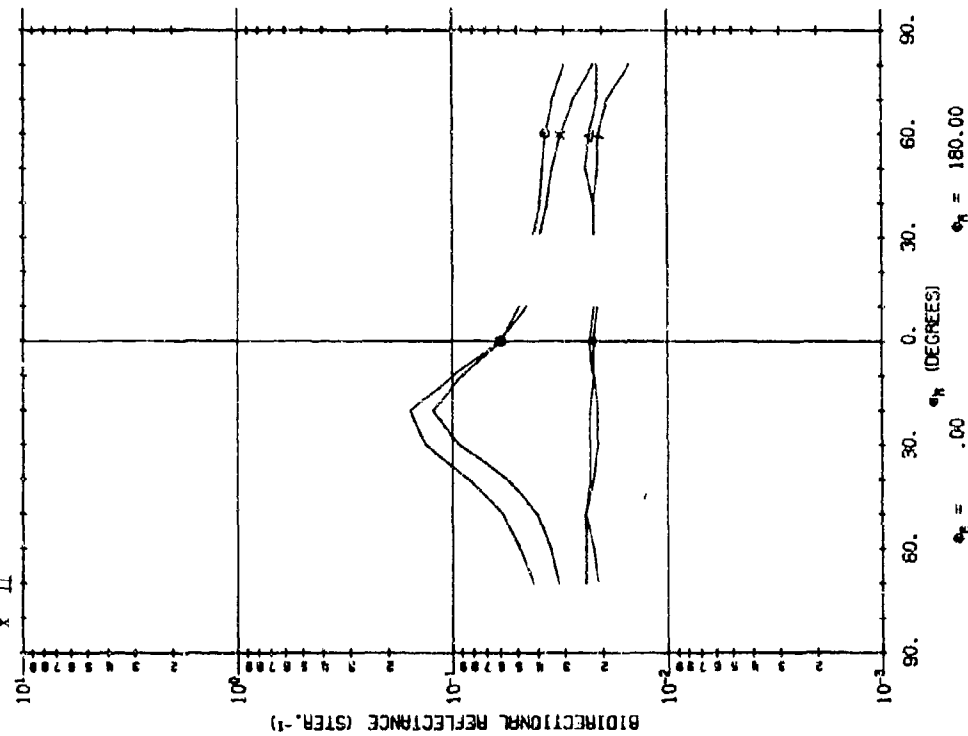
0 11

$\rho_1 = 30.00$   
 $\phi_1 = 180.00$   
 $\lambda = 1.06$

Light Brown Paint on Metal

AO1453 006

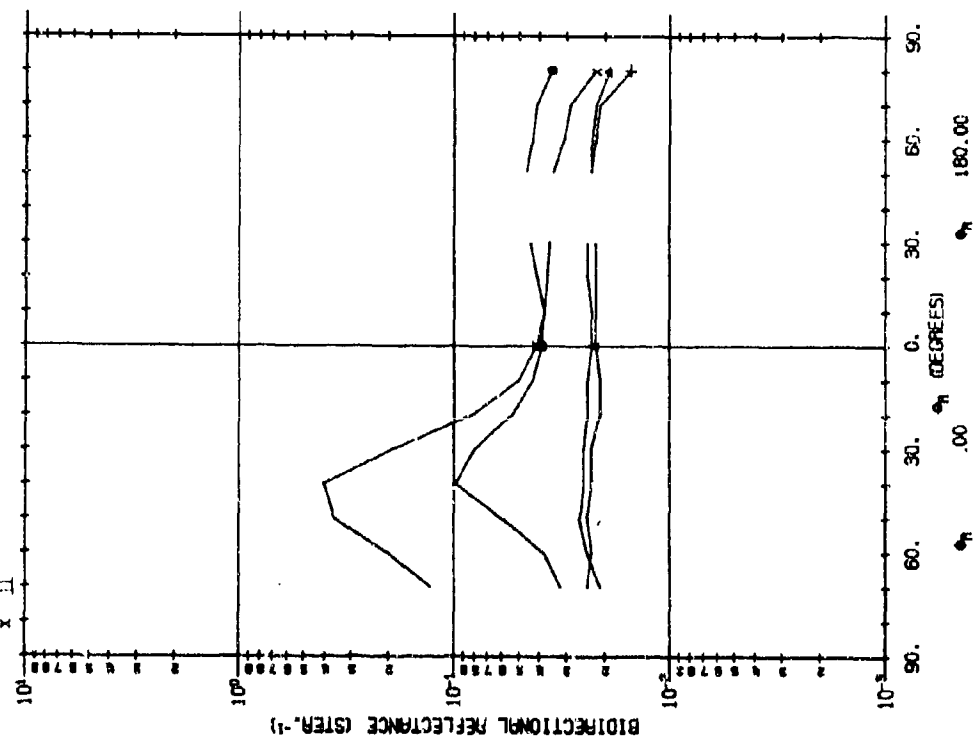
$\rho_1 = 30.00$   
 $\phi_1 = 180.00$   
 $\lambda = 1.06$



R01453 006  
 0 II  
 + II  
 Δ II  
 x II

$\theta_1 = 40.00$   
 $\phi_1 = 180.00$   
 $\lambda = 1.06$

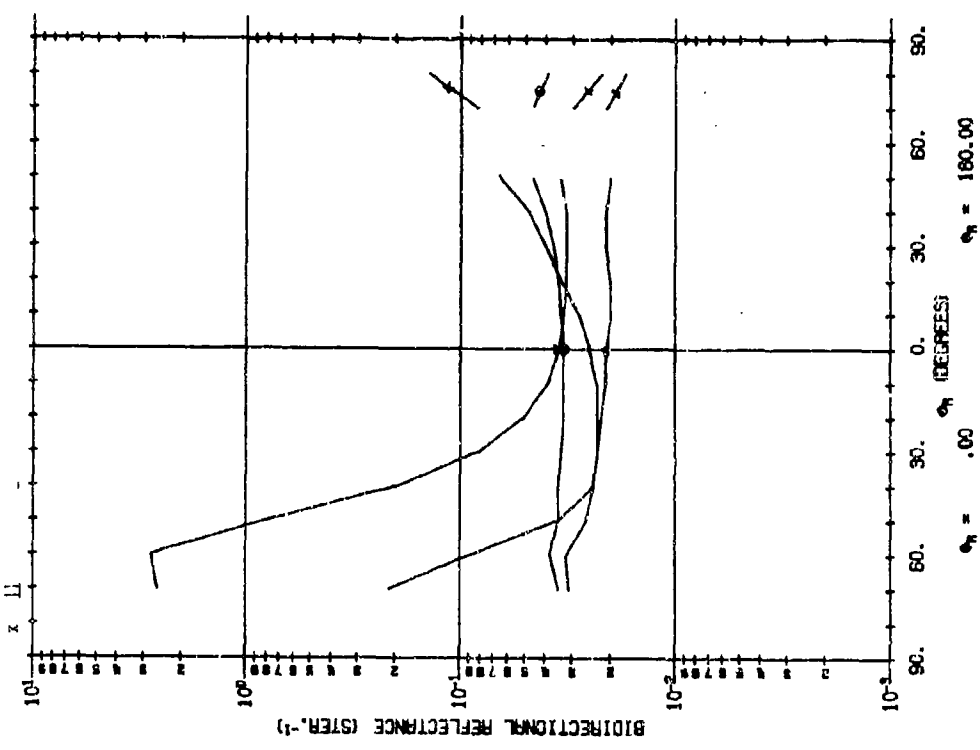
Light Brown Paint on Metal



R01453 006  
 0 II  
 + II  
 Δ II  
 x II

$\theta_1 = 60.00$   
 $\phi_1 = 180.00$   
 $\lambda = 1.06$

Light Brown Paint on Metal

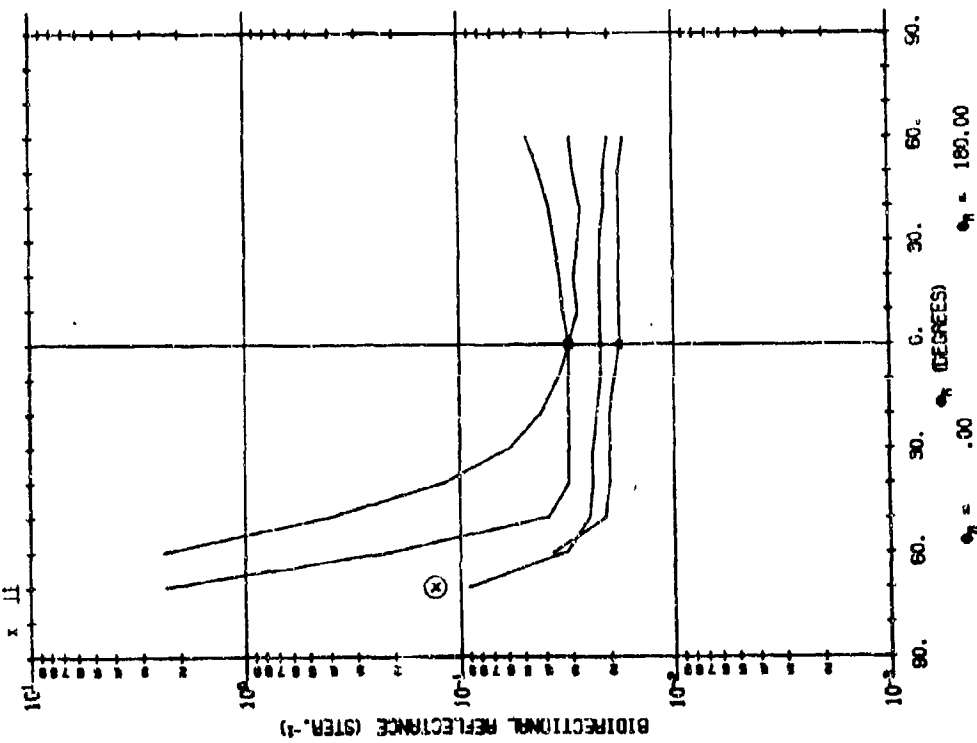


PAINT

A01453 006

Light Brown Paint on Metal

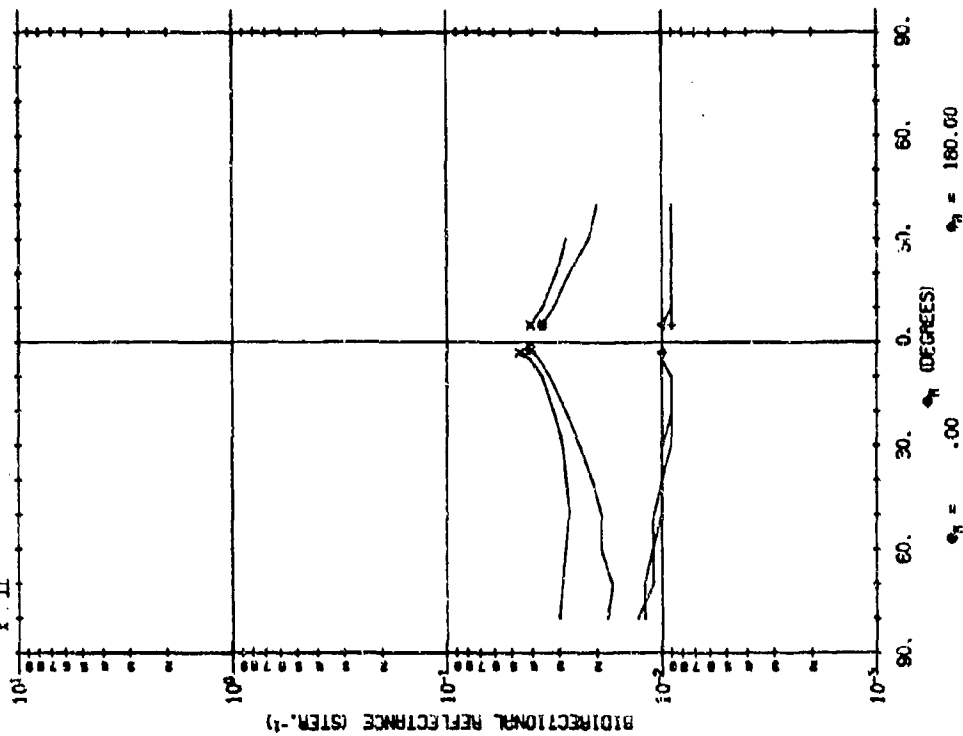
$\theta_i = 70.00$   
 $\theta_r = 180.00$   
 $\lambda = 1.06$



A01454 005

Field Drab Paint on Metal

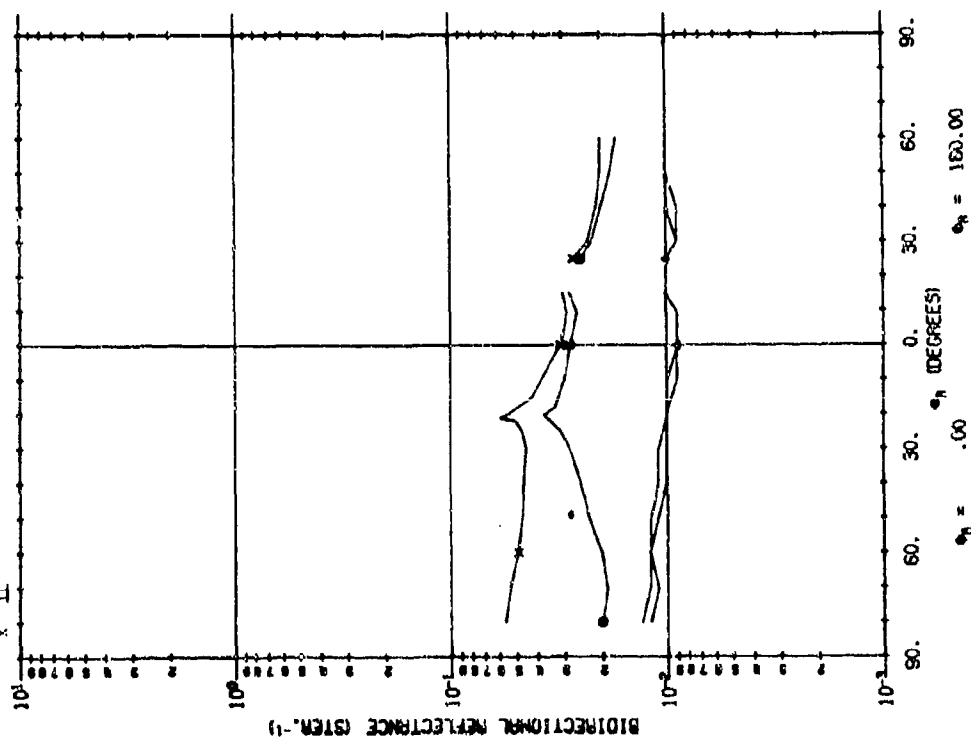
$\theta_i = 0.0$   
 $\theta_r = 180.00$   
 $\lambda = 0.63$



A01454 005  
 0 11  
 + 11  
 A 11  
 X 11

Field Draft Paint on Metal

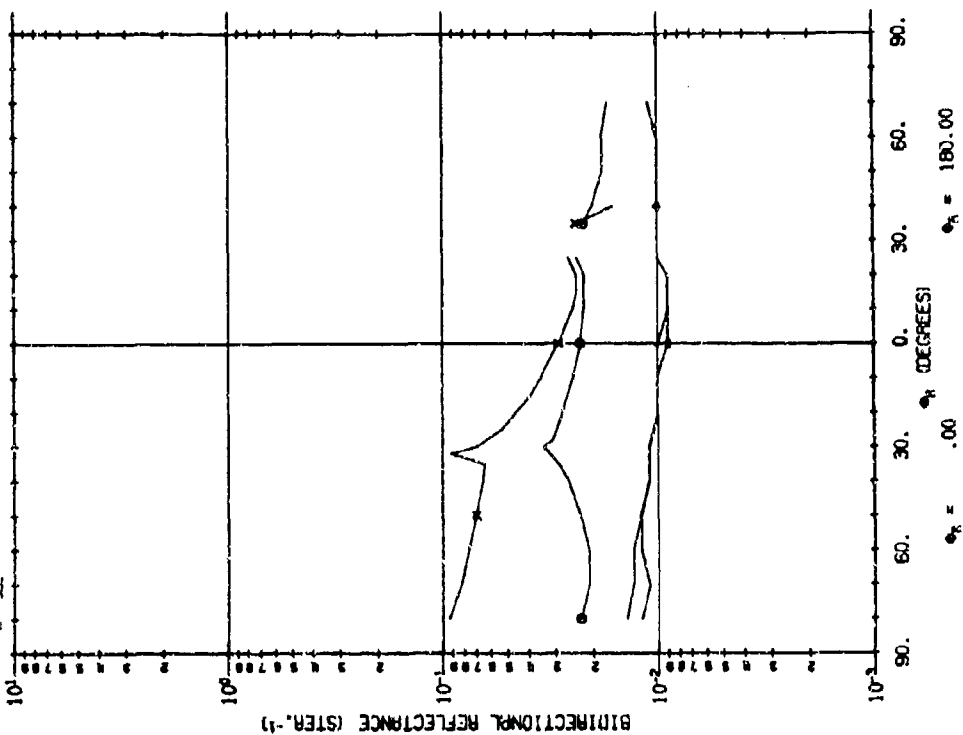
$\theta_i = 20.00$   
 $\phi_i = 180.00$   
 $\lambda = 0.63$



A01454 005  
 0 11  
 + 11  
 A 11  
 X 11

Field Draft Paint on Metal

$\theta_i = 30.00$   
 $\phi_i = 180.00$   
 $\lambda = 0.63$

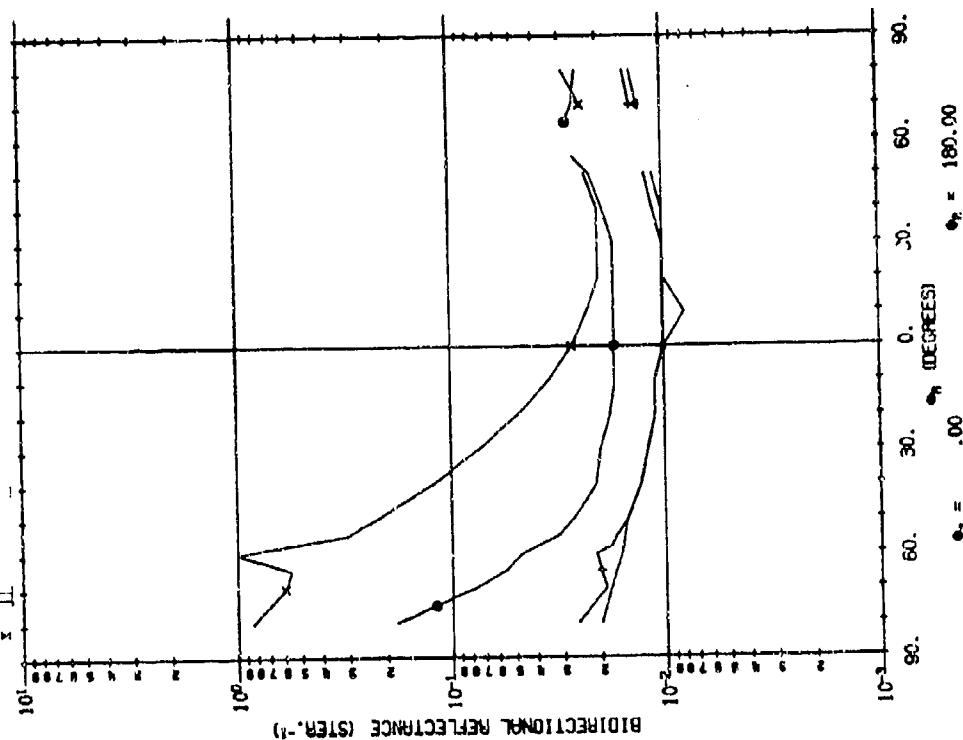


PAINT

R01454 005

Field Drab Paint on Metal

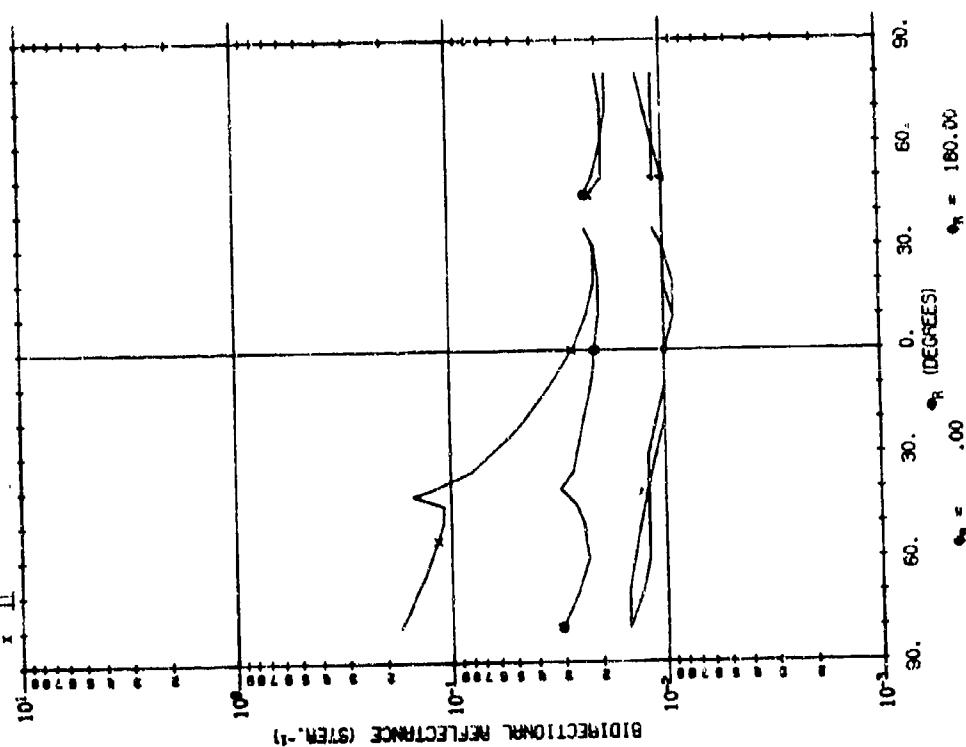
$\theta_1 = 60.00$   
 $\theta_2 = 180.00$   
 $\lambda = 0.63$



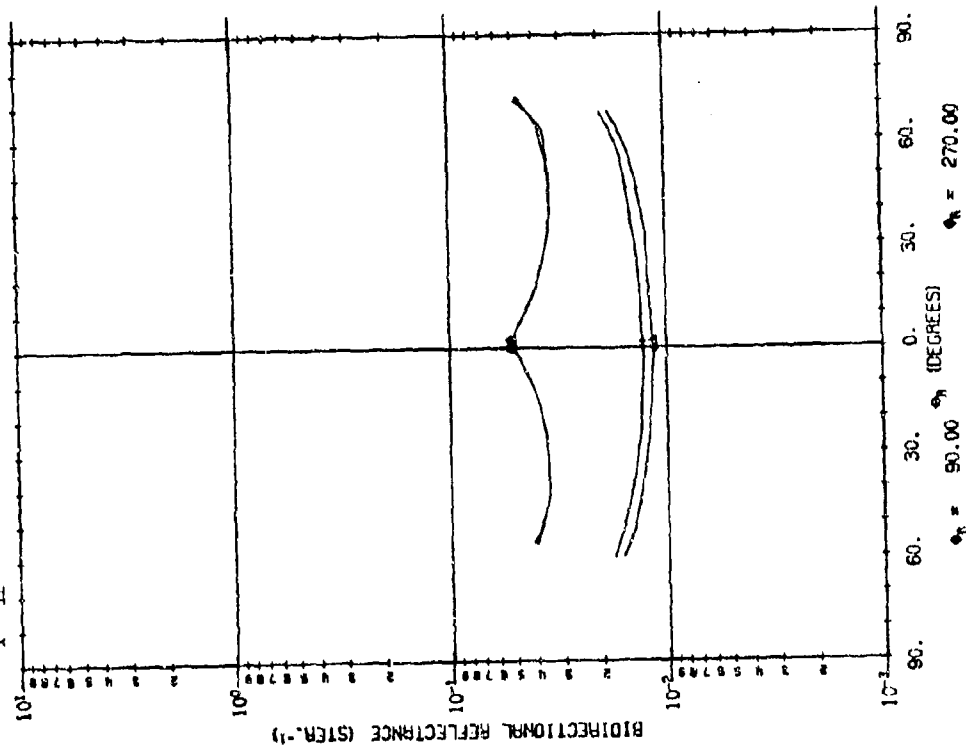
R01454 005

Field Drab Paint on Metal

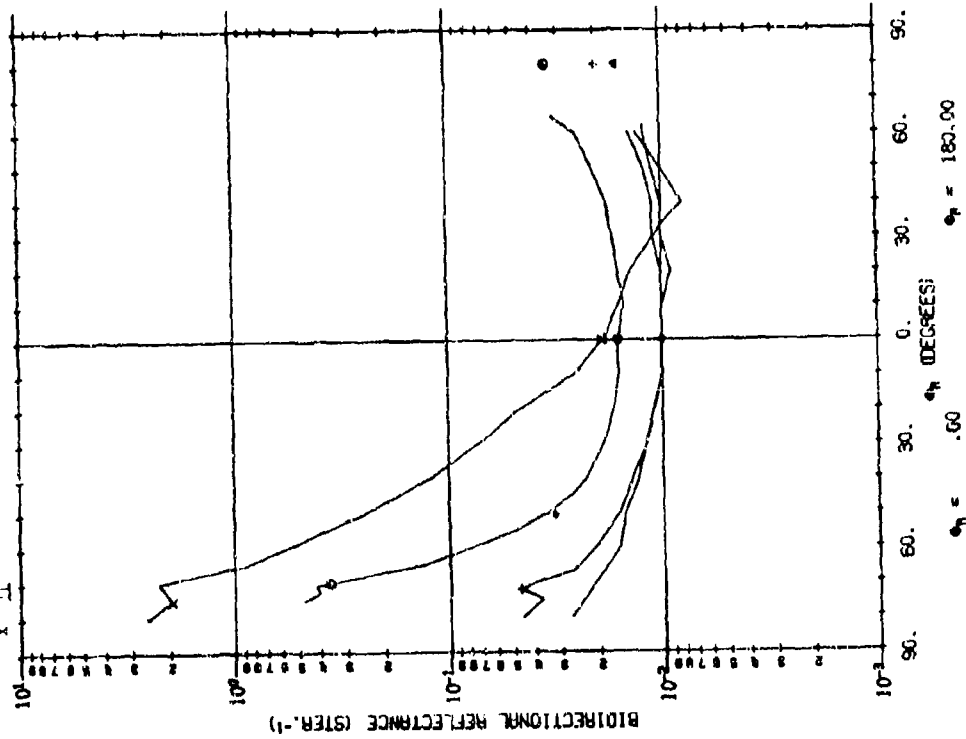
$\theta_1 = 40.00$   
 $\theta_2 = 180.00$   
 $\lambda = 0.63$



A01454 005  
 LIGHT BROWN PAINT ON METAL  
 $\theta_1 = 23^\circ$   
 $\theta_2 = 0^\circ$   
 $\theta_3 = 0.63$



A01454 005  
 Field Test Paint on Metal  
 $\theta_1 = 70.00$   
 $\theta_2 = 180.00$   
 $\theta_3 = 0.63$



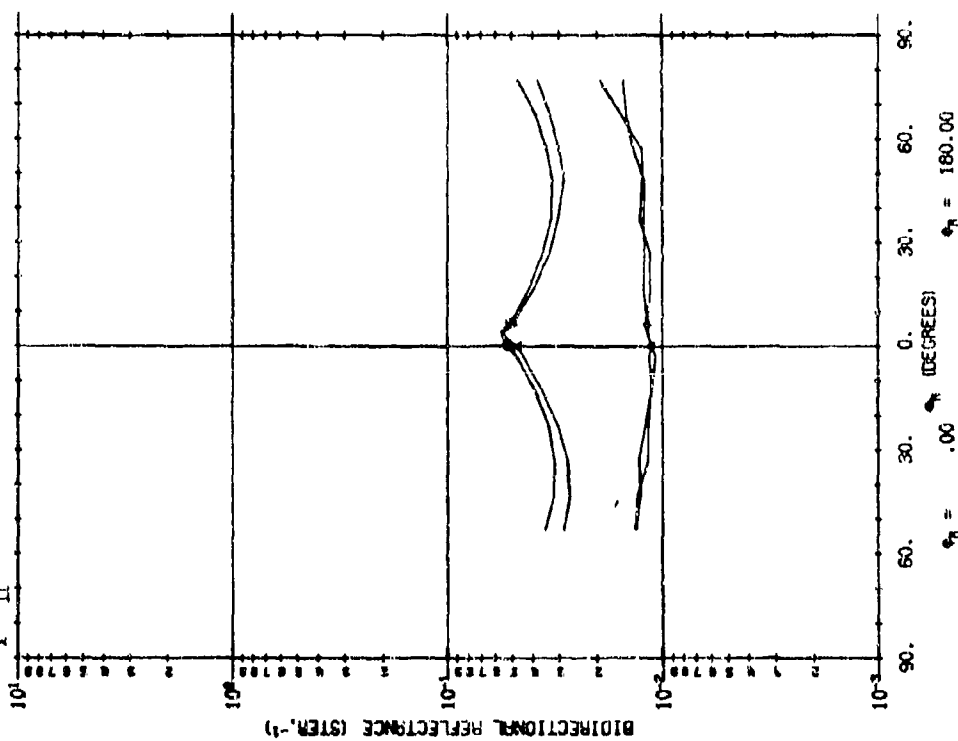
PAINT



A01454 004

FIELD DRAB PAINT ON METAL

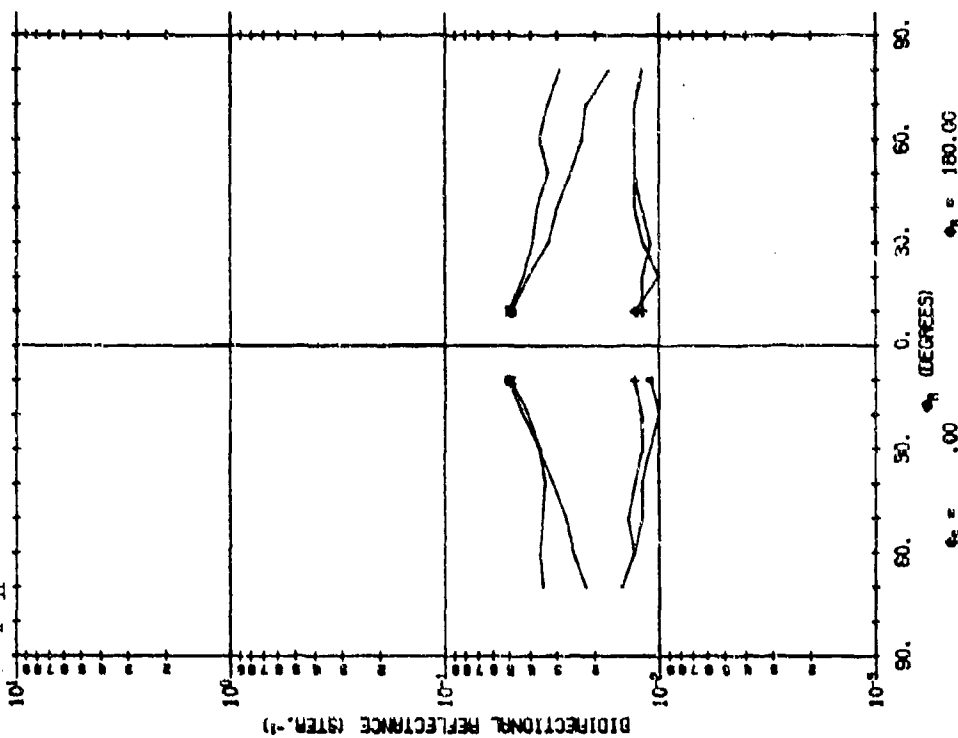
0 11 25 = 7.0  
+ 11 1 = 1.06  
X 11 1 = 1.06



A01454 004

FIELD DRAB PAINT ON METAL

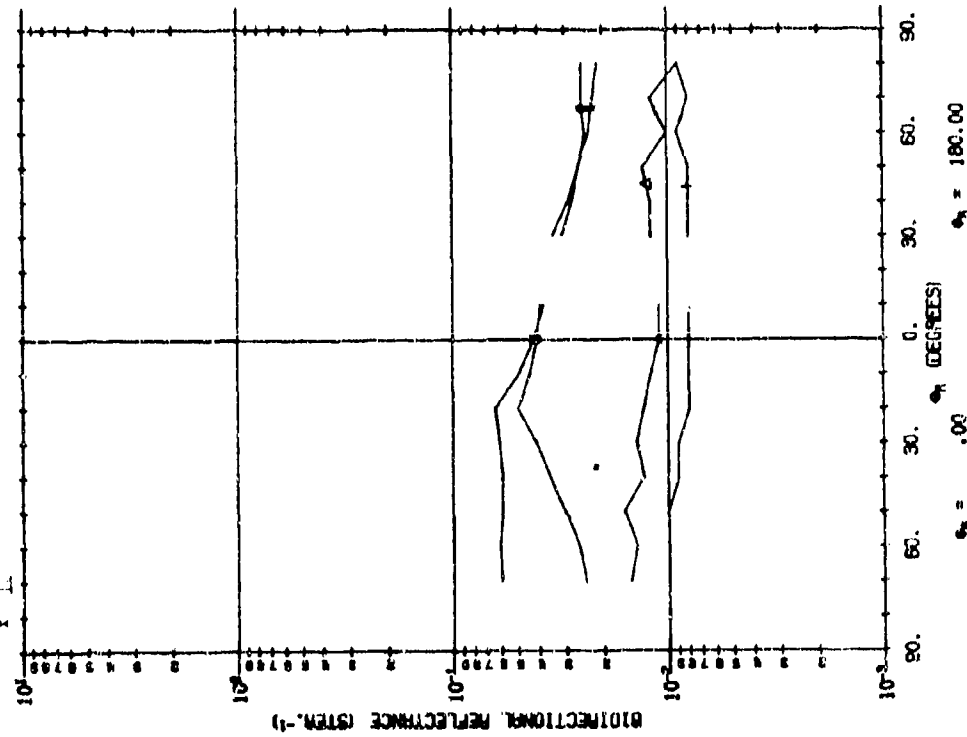
0 11 0 = 0.0  
+ 11 1 = 180.0  
X 11 1 = 1.06



R01454 004

Field Drab Paint on Metal

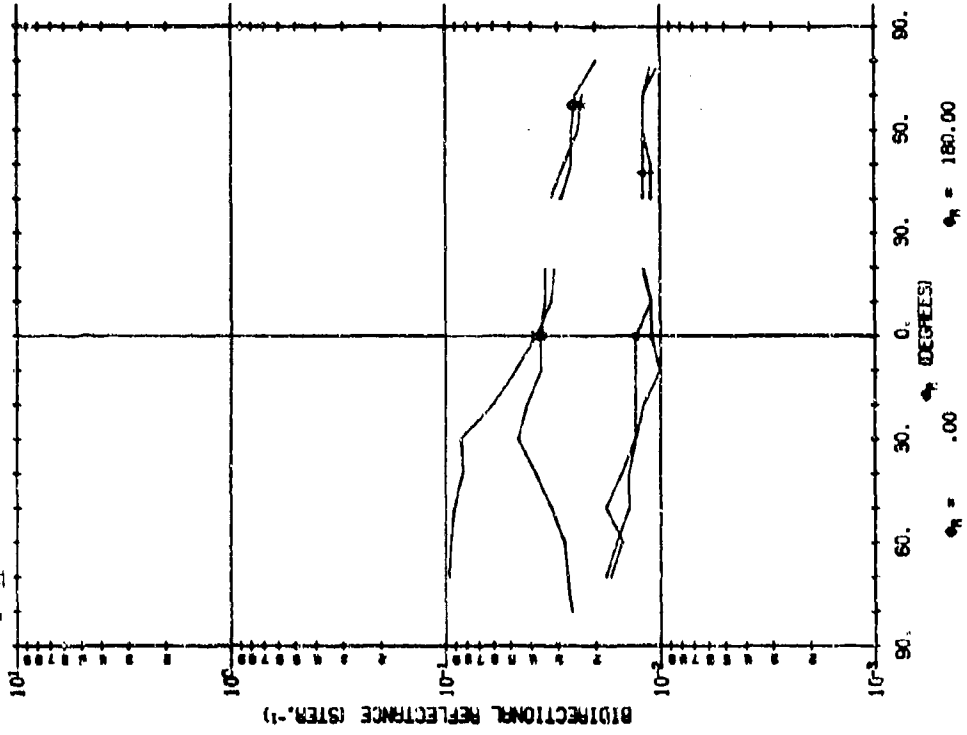
$\theta_1 = 20.00$   
 $\theta_2 = 180.00$   
 $\lambda = 1.06$



R01454 004

Field Drab Paint on Metal

$\theta_1 = 30.00$   
 $\theta_2 = 180.00$   
 $\lambda = 1.06$



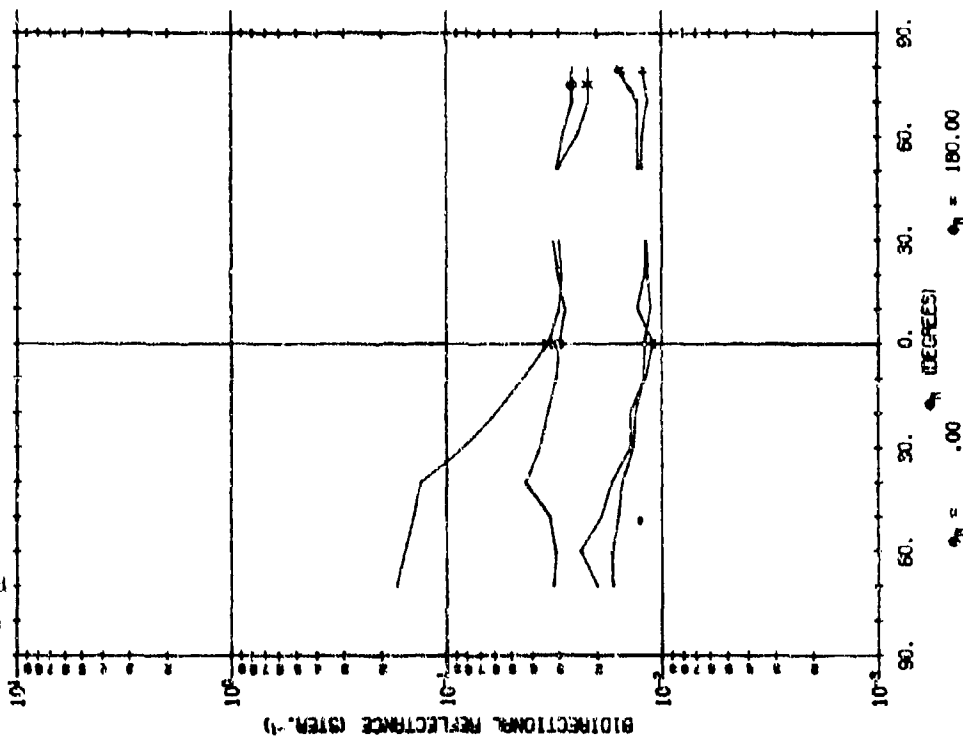
PAINT

A01454 004

Field Drab Paint on Metal

$\theta_1 = 45.00$   
 $\theta_2 = 180.00$   
 $\lambda = 1.06$

0 II  
 + II  
 x II

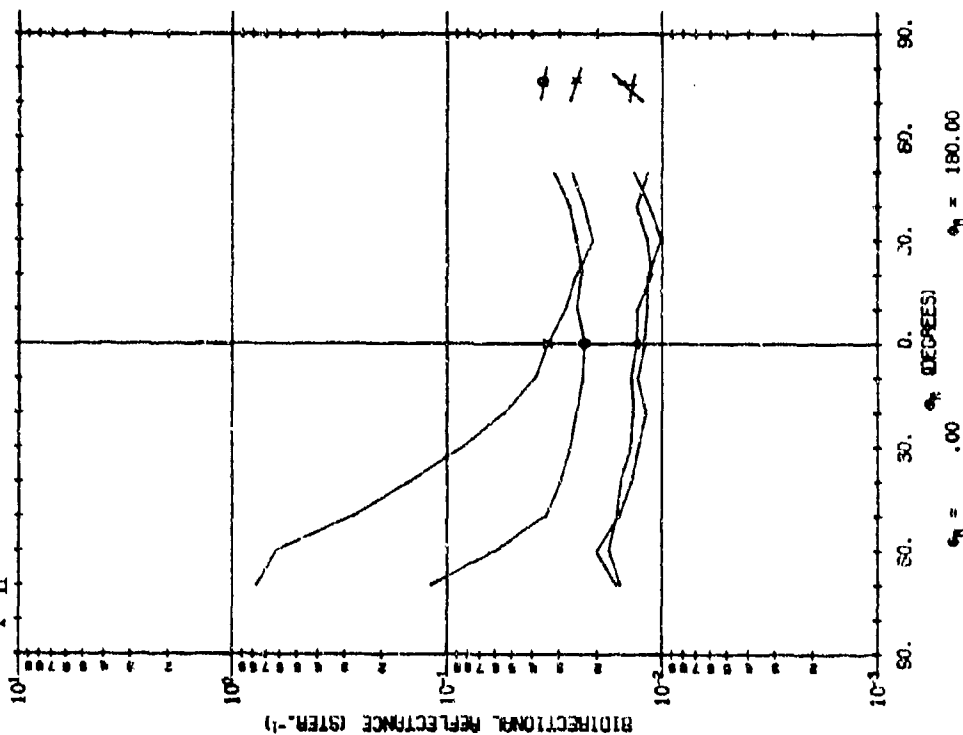


A01454 004

Field Drab Paint on Metal

$\theta_1 = 60.00$   
 $\theta_2 = 180.00$   
 $\lambda = 1.06$

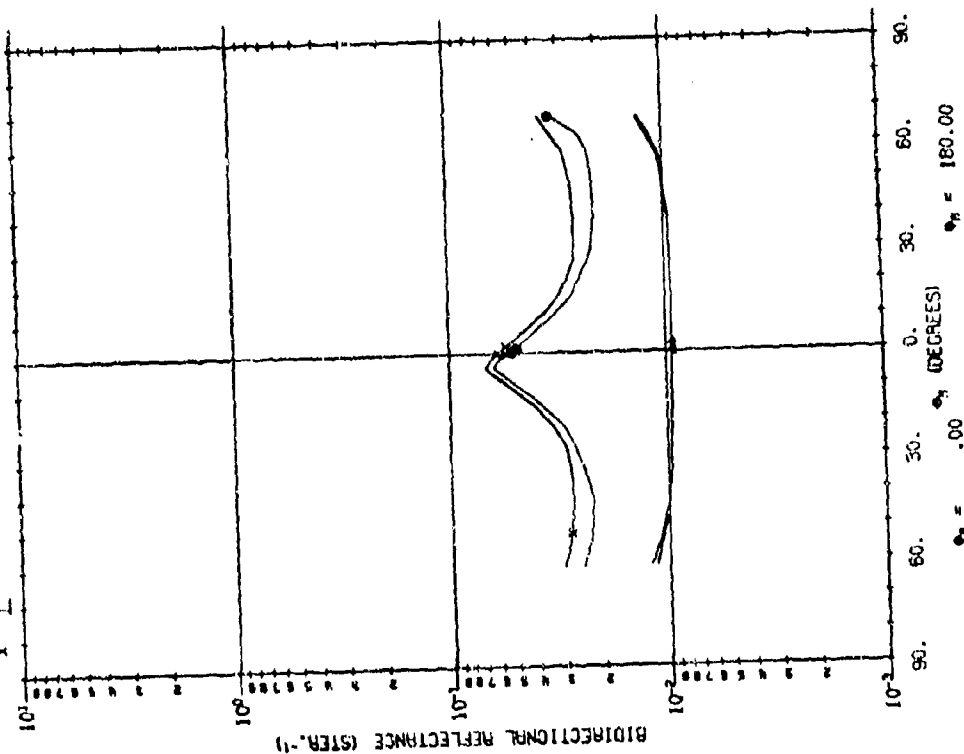
0 II  
 + II  
 x II



R01455 005

OLIVE DRAB PAINT ON METAL

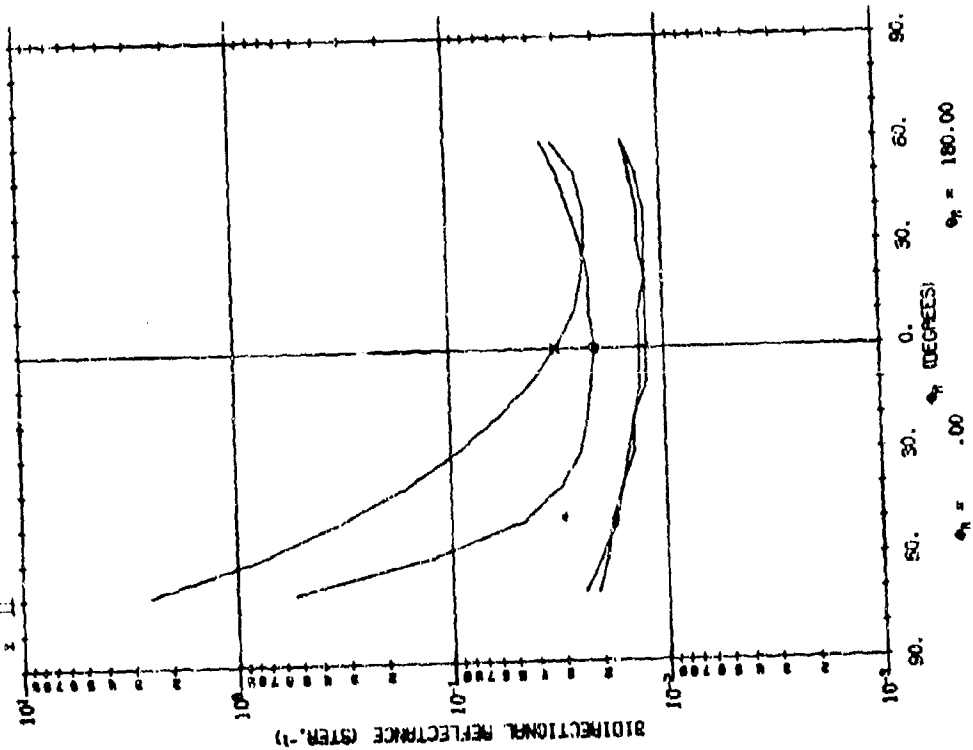
$\theta_1 = 2.0$   
 $\theta_2 = 0.53$   
 $\theta_3 = 0.53$



R01454 004

Field Drab Paint on Metal

$\theta_1 = 70.00$   
 $\theta_2 = 180.00$   
 $\theta_3 = 1.06$



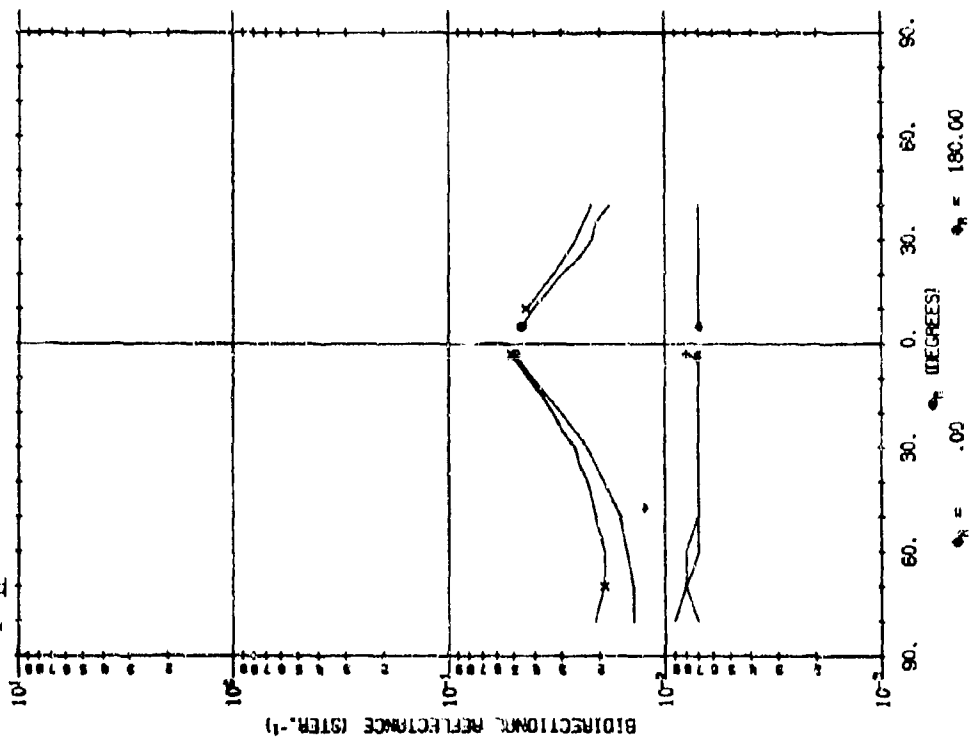
PAINT

R01455 005

Olive Drab Paint on Metal

$\theta_i = 0.0$   
 $\theta_r = 180.00$   
 $\lambda = 0.63$

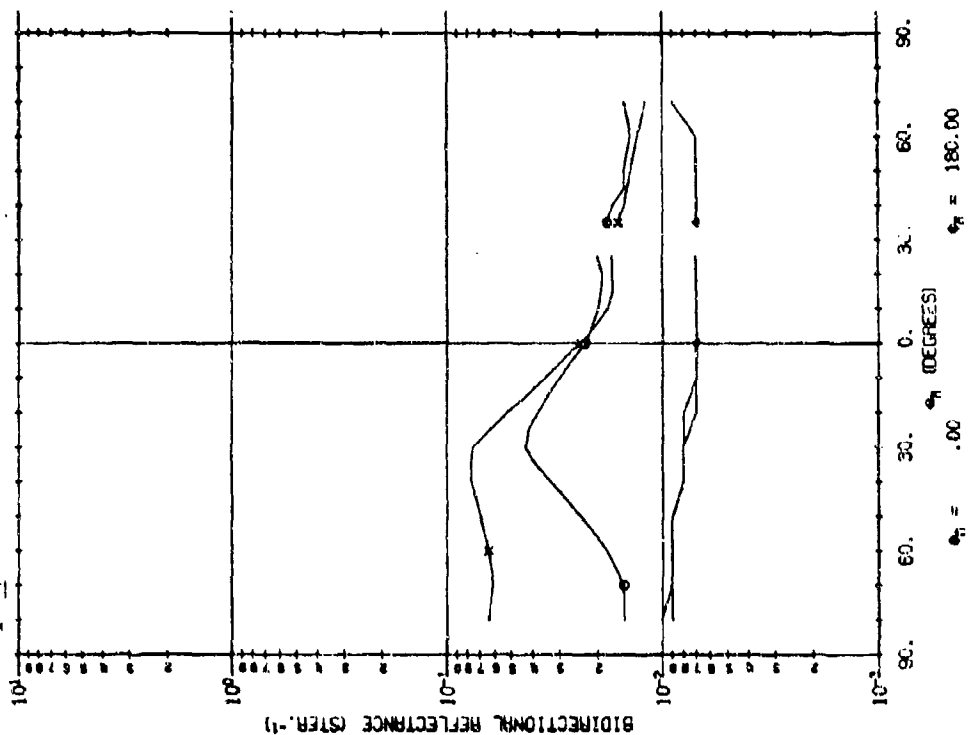
$\theta_i = 30.00$   
 $\theta_r = 180.00$   
 $\lambda = 0.63$



R01455 005

Olive Drab Paint on Metal

$\theta_i = 30.00$   
 $\theta_r = 180.00$   
 $\lambda = 0.63$

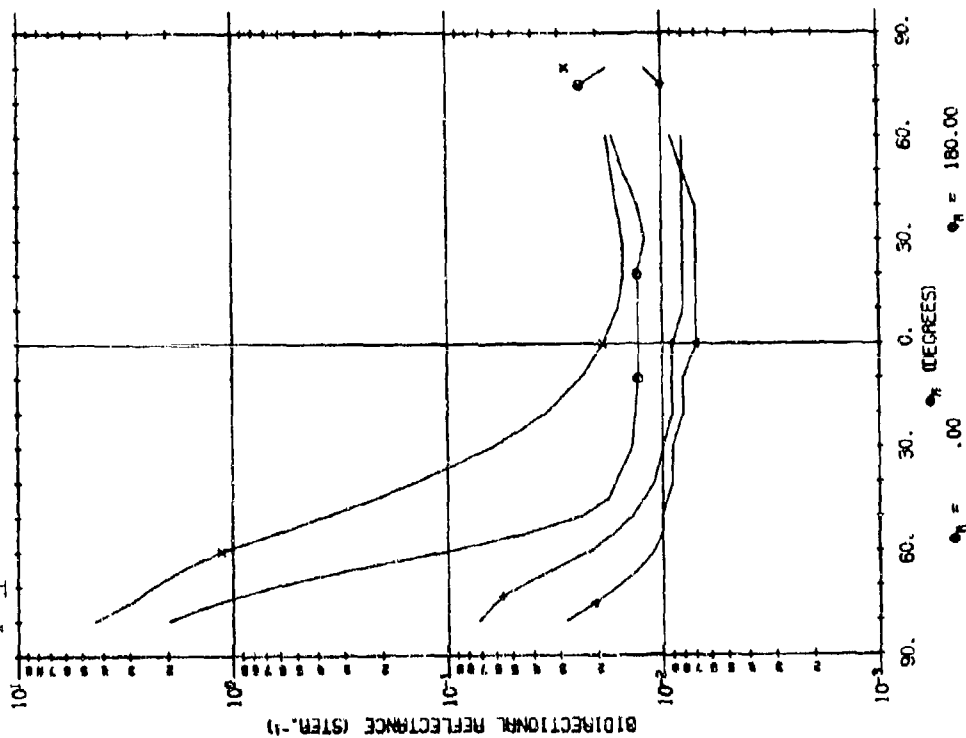


R01455 005

Olive Drab Paint on Metal

$\theta_1 = 70.00$   
 $\theta_2 = 180.00$   
 $\lambda = 0.63$

0  
 +  
 -  
 x

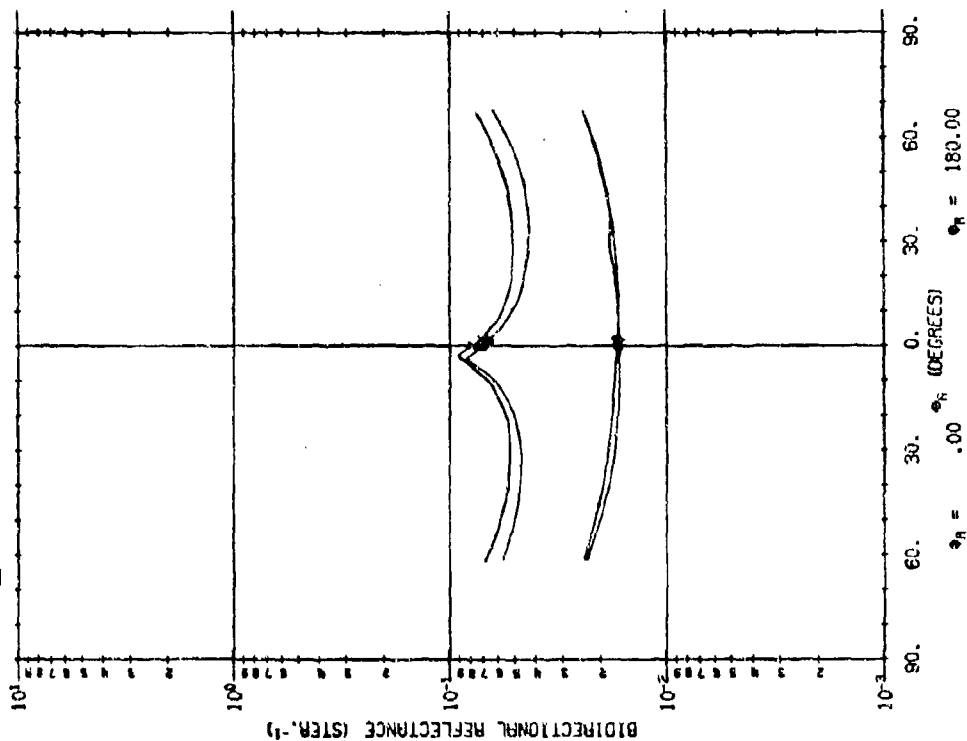


R01456 005

Olive Drab Paint on Metal

$\theta_1 = 2.0$   
 $\theta_2 = 180.00$   
 $\lambda = 0.63$

0  
 +  
 -  
 x

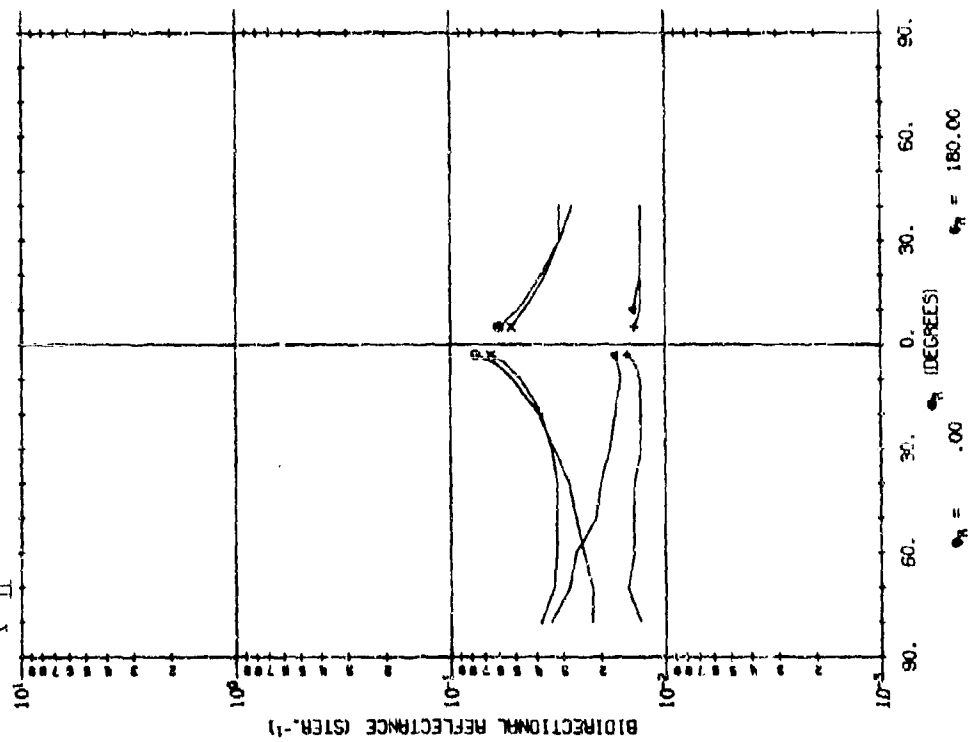


PAINT

R01456 005

Olive Drab Paint on Metal

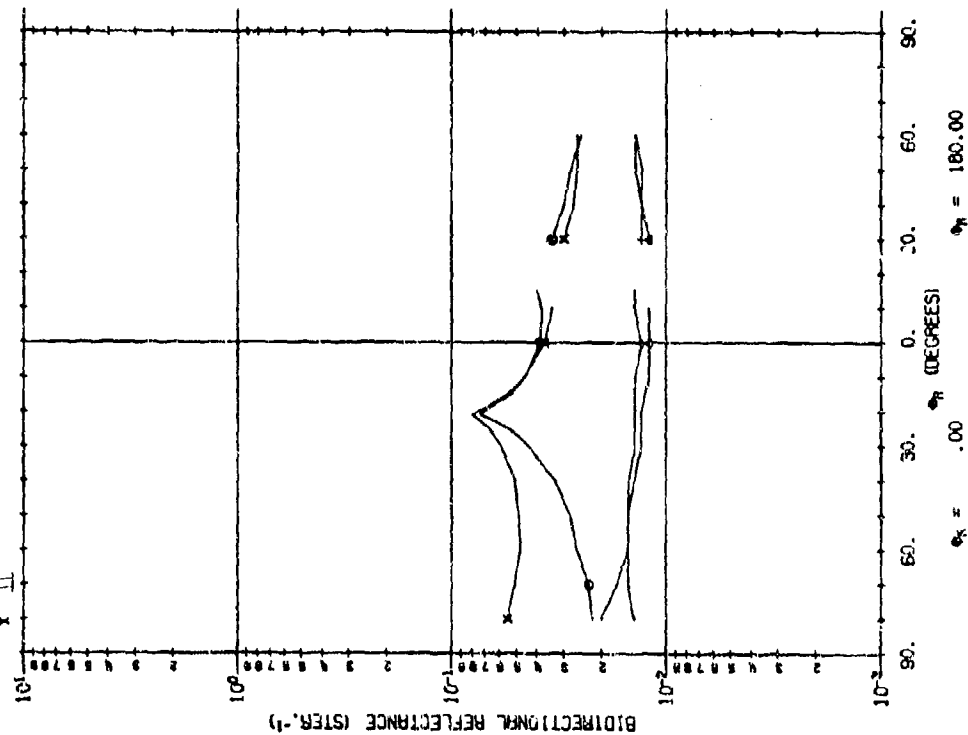
$\theta_1 = 0.0$   
 $\phi_1 = 180.00$   
 $\lambda = 0.63$



R01456 005

Olive Drab Paint on Metal

$\theta_1 = 20.00$   
 $\phi_1 = 180.00$   
 $\lambda = 0.63$

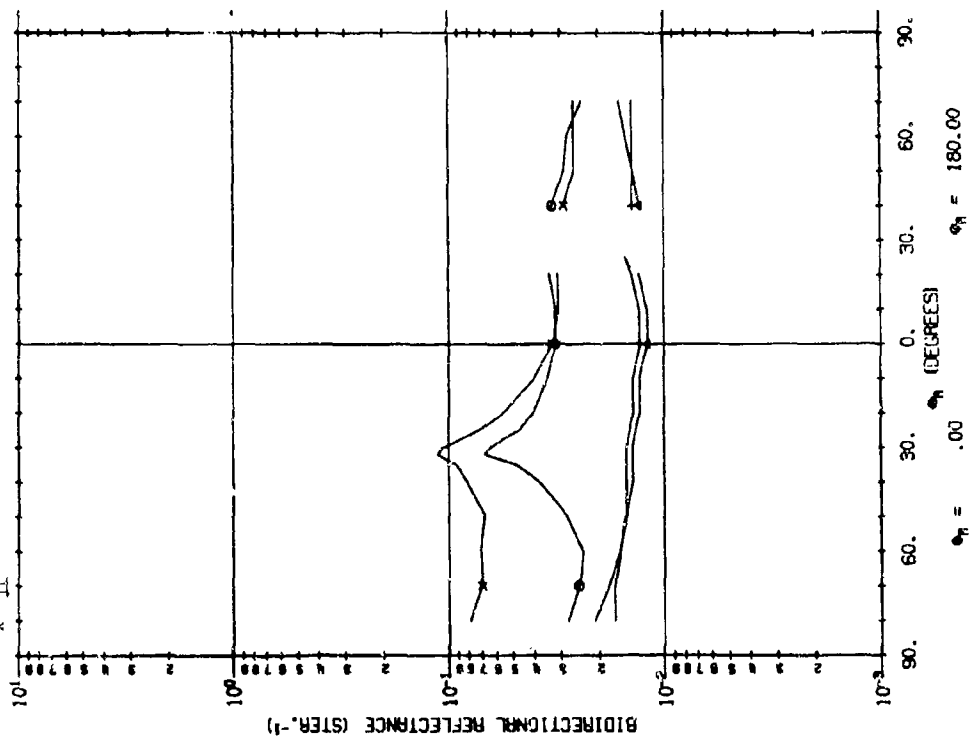


R01456 005

Olive Drab Paint on Metal

$\epsilon_1 = 30.00$   
 $\phi_1 = 180.00$   
 $\lambda = 0.63$

0 II  
 + II  
 Δ II  
 x II

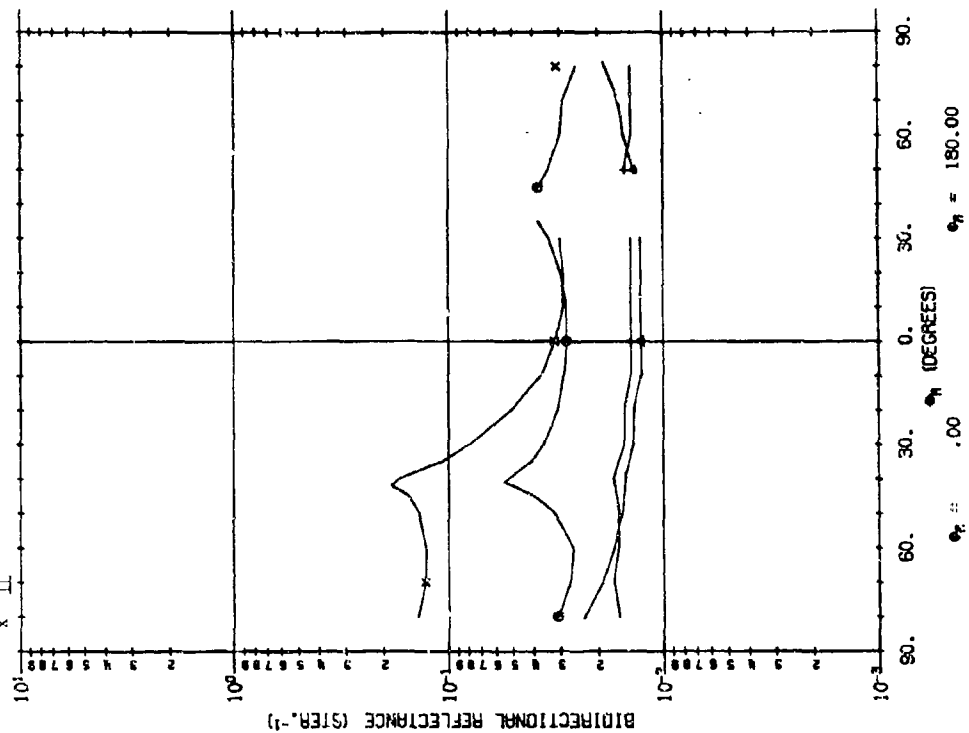


R01456 005

Olive Drab Paint on Metal

$\epsilon_1 = 40.00$   
 $\phi_1 = 180.00$   
 $\lambda = 0.63$

0 II  
 + II  
 Δ II  
 x II

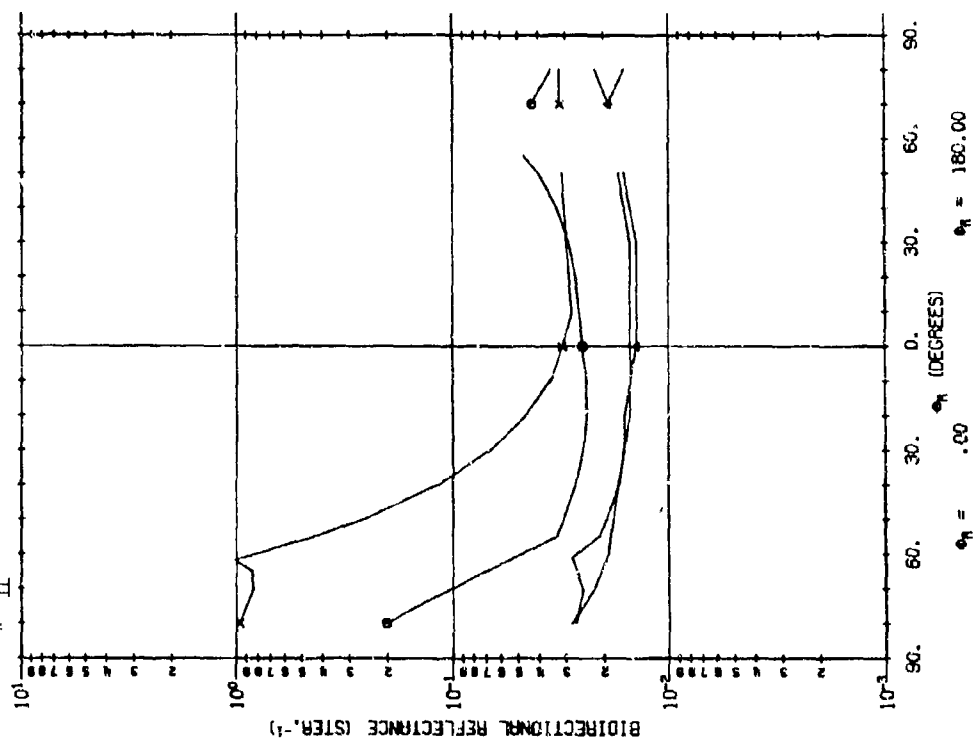




R01456 005

Olive Drab Paint on Metal

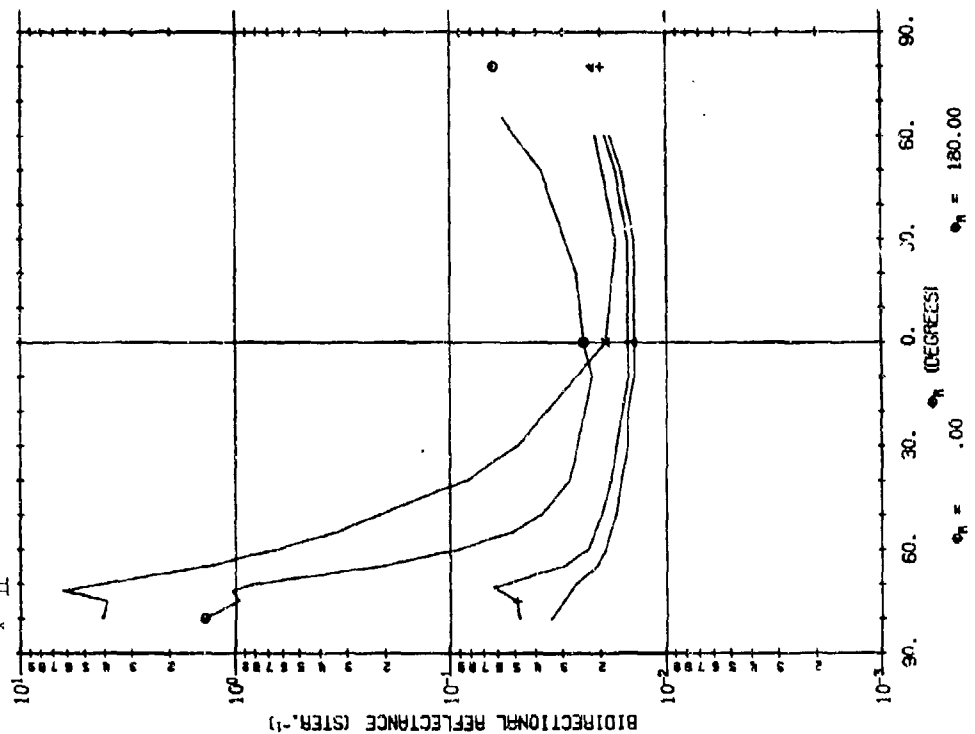
$\theta_i = 60.00$   
 $\phi_i = 180.00$   
 $\lambda = 0.63$



R01456 005

Olive Drab Paint on Metal

$\theta_i = 70.00$   
 $\phi_i = 180.00$   
 $\lambda = 0.63$



A01456 005

OLIVE DRAB PAINT ON METAL

28 = 2.0

$\rho_1 = \rho_2$

$\lambda = 0.63$

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A01456 004

OLIVE DRAB PAINT ON METAL

28 = 2.0

$\rho_1 = \rho_2$

$\lambda = 1.06$

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$\lambda = 1.06$

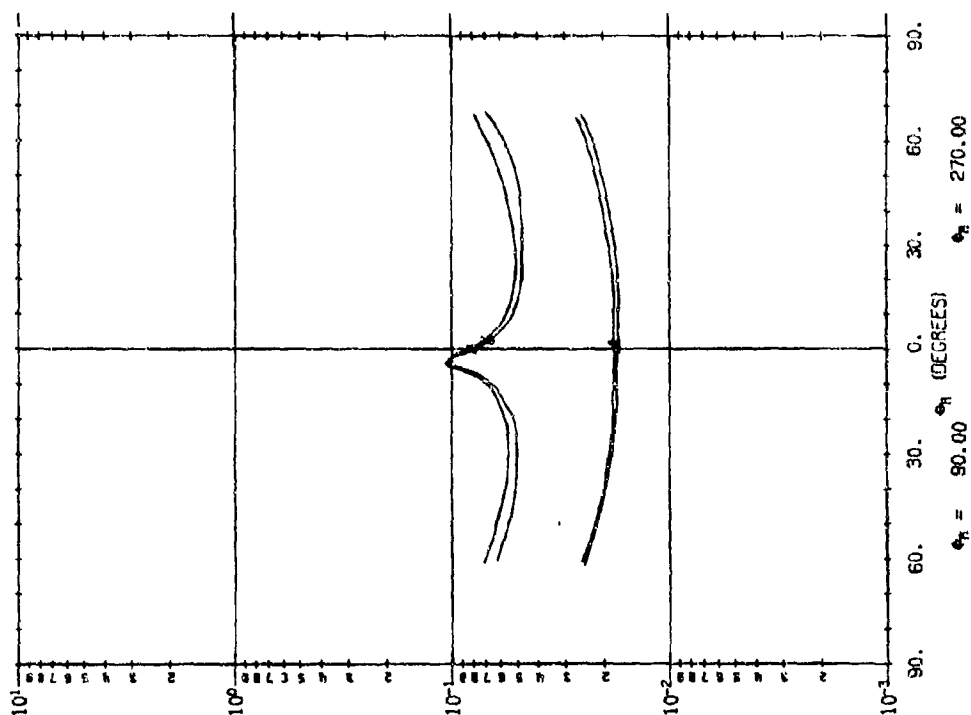
$\lambda = 1.06$

$\lambda = 1.06$

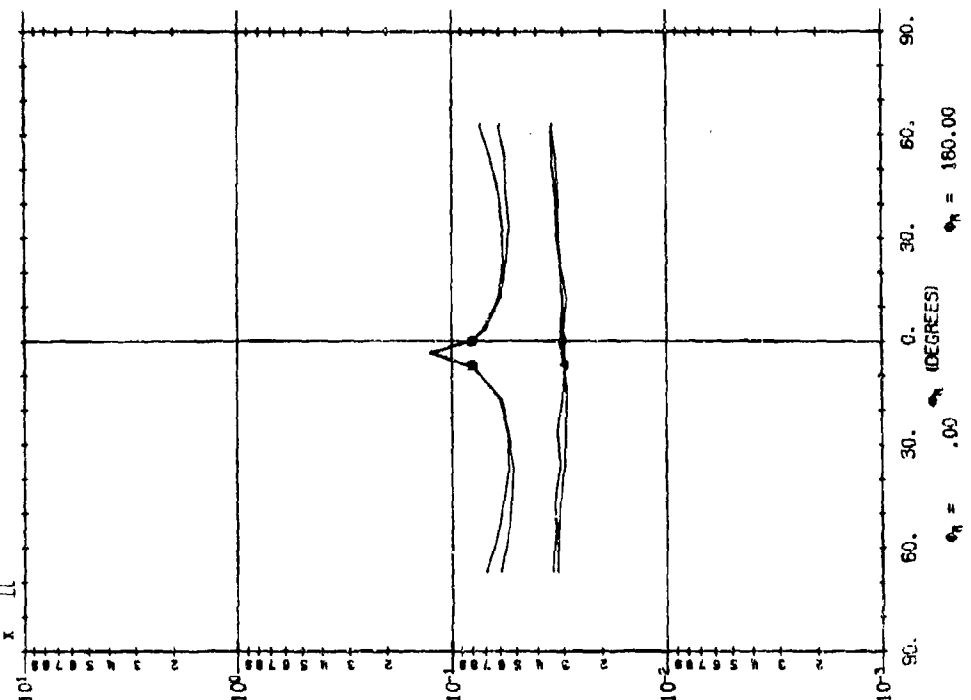
$\lambda = 1.06$

$\lambda = 1.06$

BIDIRECTIONAL REFLECTANCE (STER.-1)



BIDIRECTIONAL REFLECTANCE (STER.-1)



PAINT

A01456 004

Olive Drab Paint on Metal

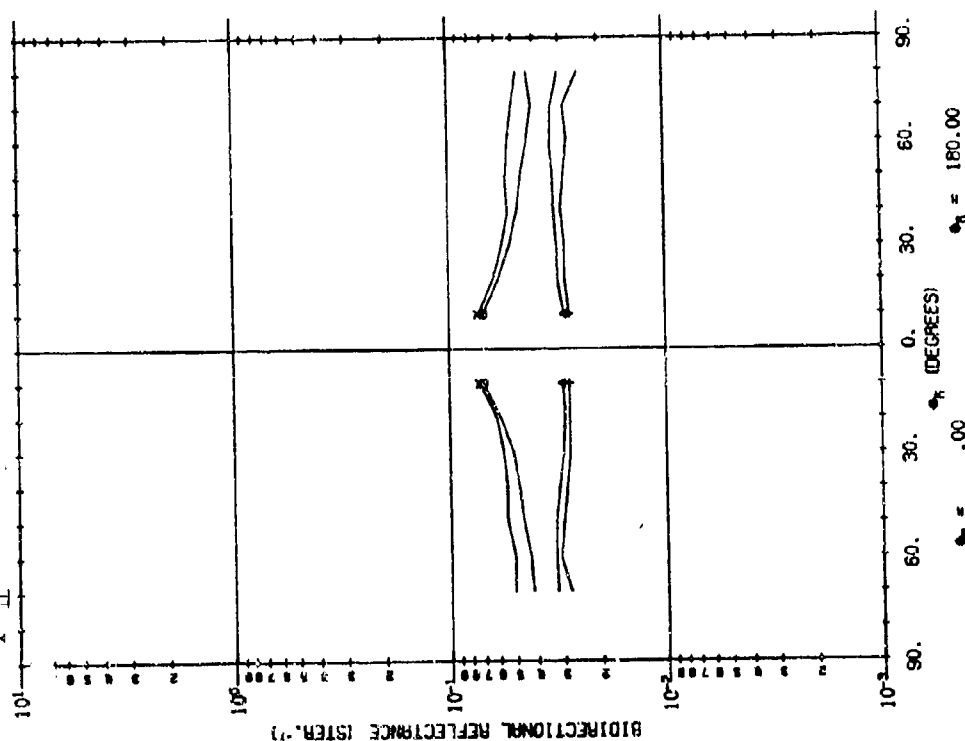
$\epsilon_1 = 0.6$   
 $\epsilon_2 = 180.00$   
 $\lambda = 1.06$

C II

+ II

A II

X II



A01456 004

Olive Drab Paint on Metal

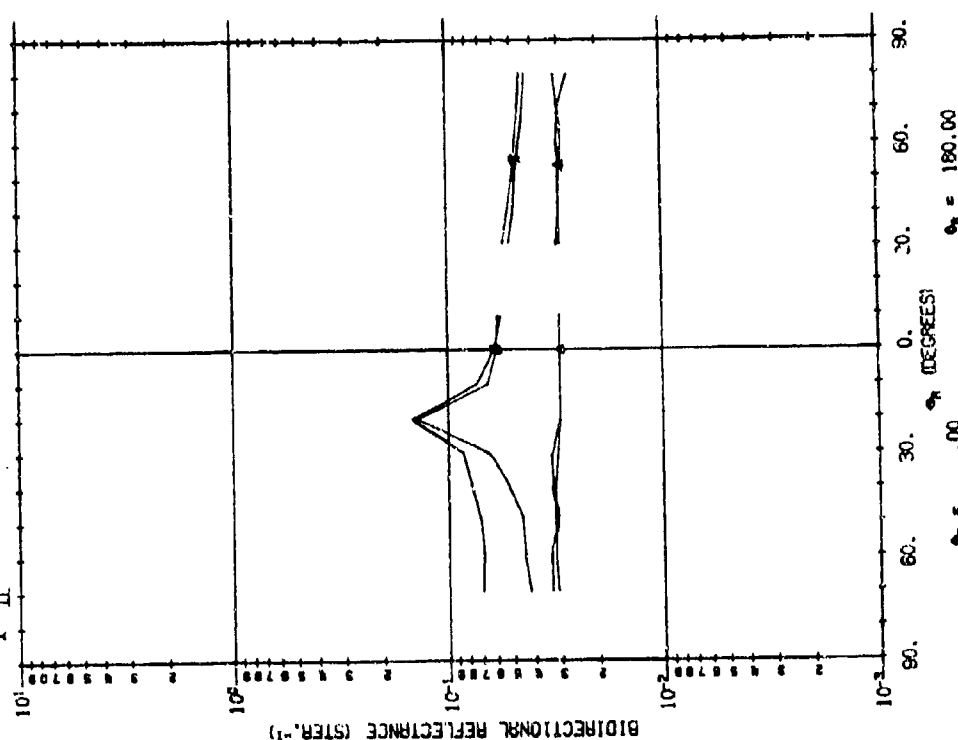
$\epsilon_1 = 20.00$   
 $\epsilon_2 = 180.00$   
 $\lambda = 1.06$

C II

+ II

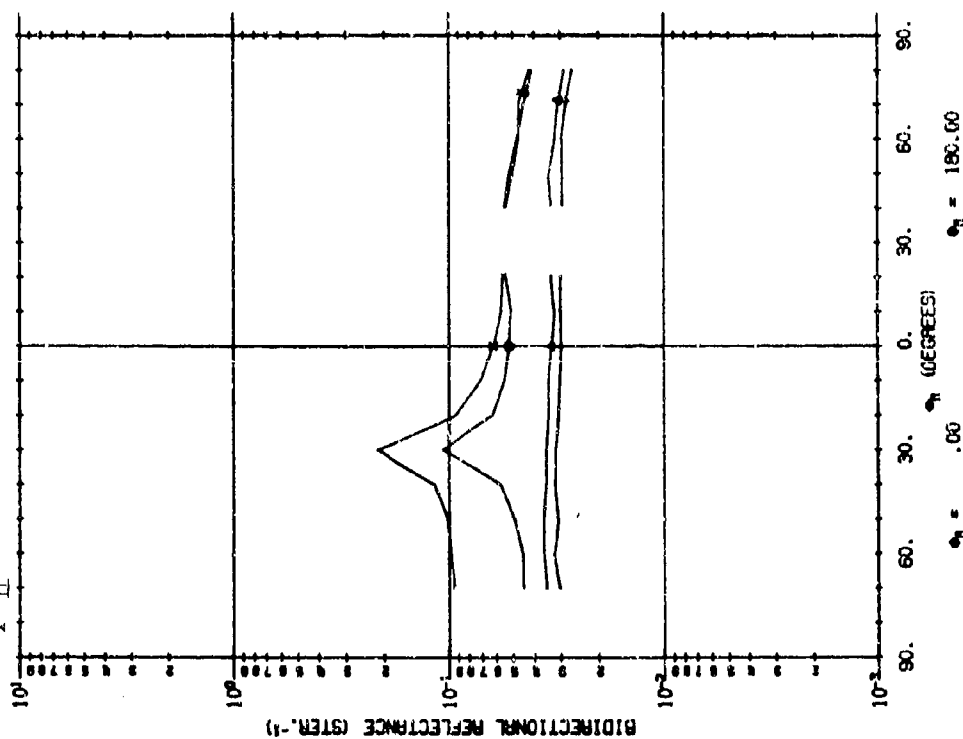
A II

X II



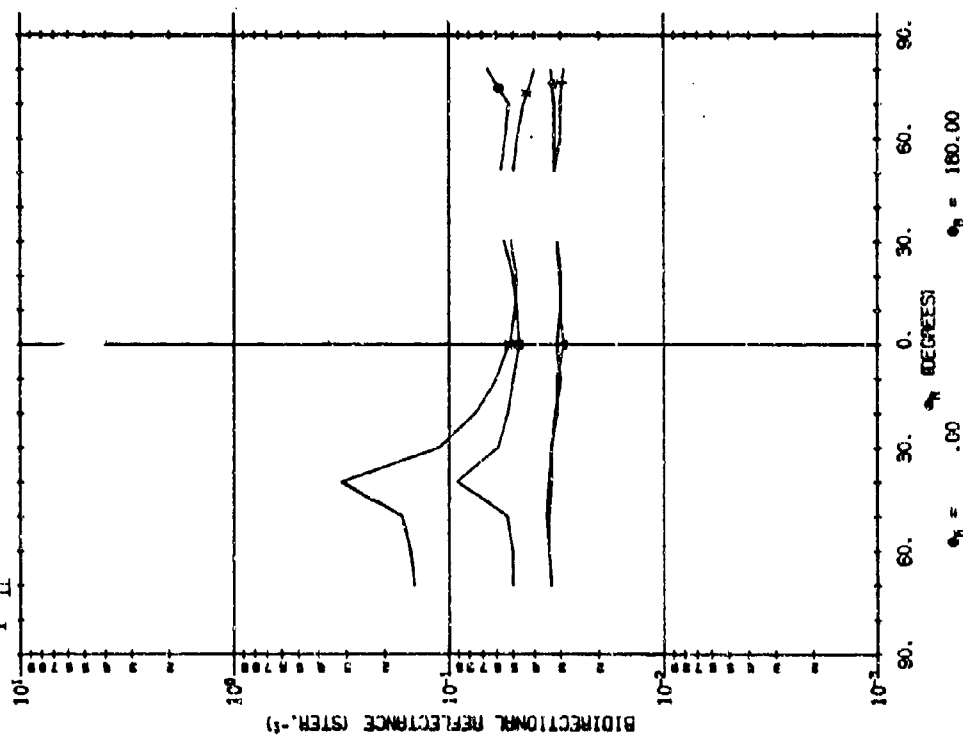
R01456 004  
 $\theta_1 = 30.00$   
 $\phi_1 = 180.00$   
 $\lambda = 1.06$

Olive Drab Paint on Metal



R01456 004  
 $\theta_1 = 40.00$   
 $\phi_1 = 180.00$   
 $\lambda = 1.06$

Olive Drab Paint on Metal

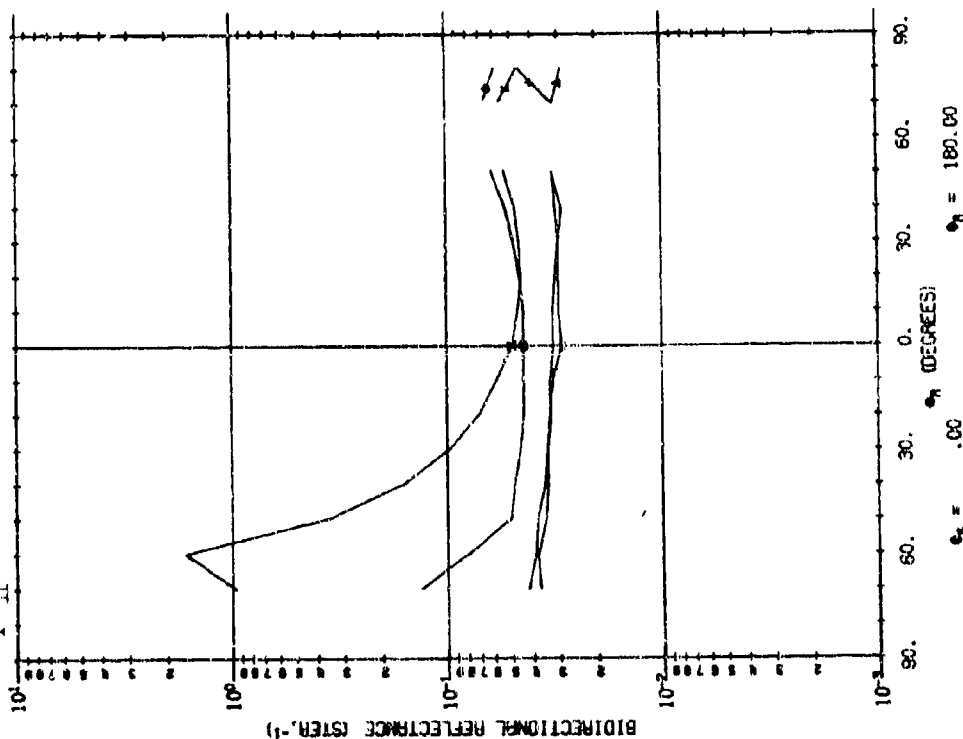


PAINT

A01456 004

Olive Drab Paint on Metal

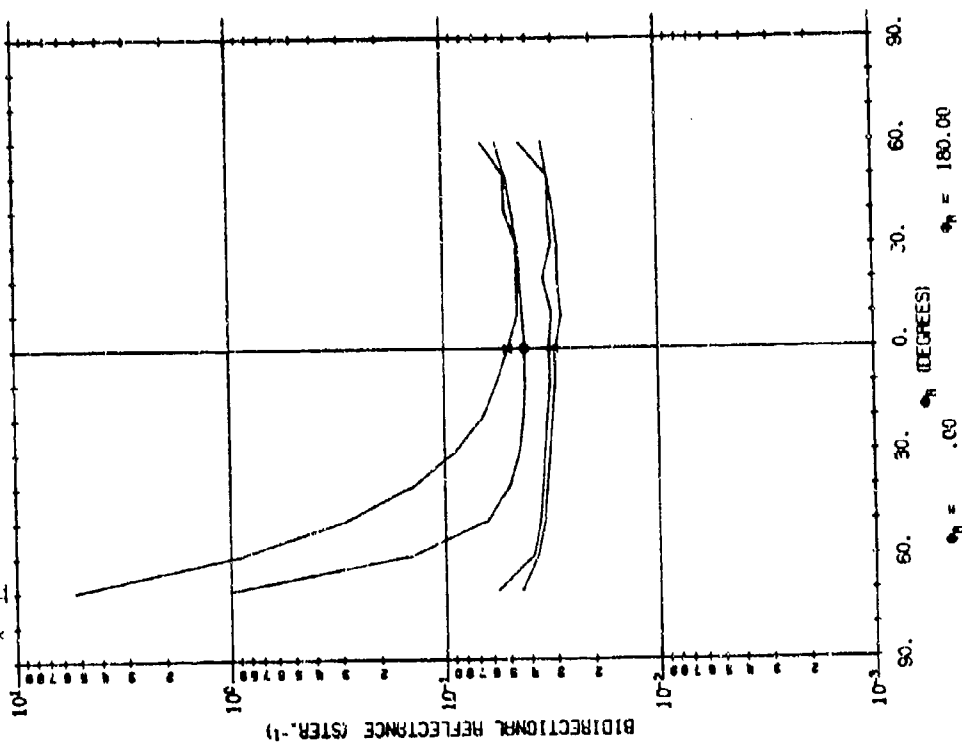
$\theta_i = 60.00$   
 $\theta_r = 180.00$   
 $\lambda = 1.06$



A01456 004

Olive Drab Paint on Metal

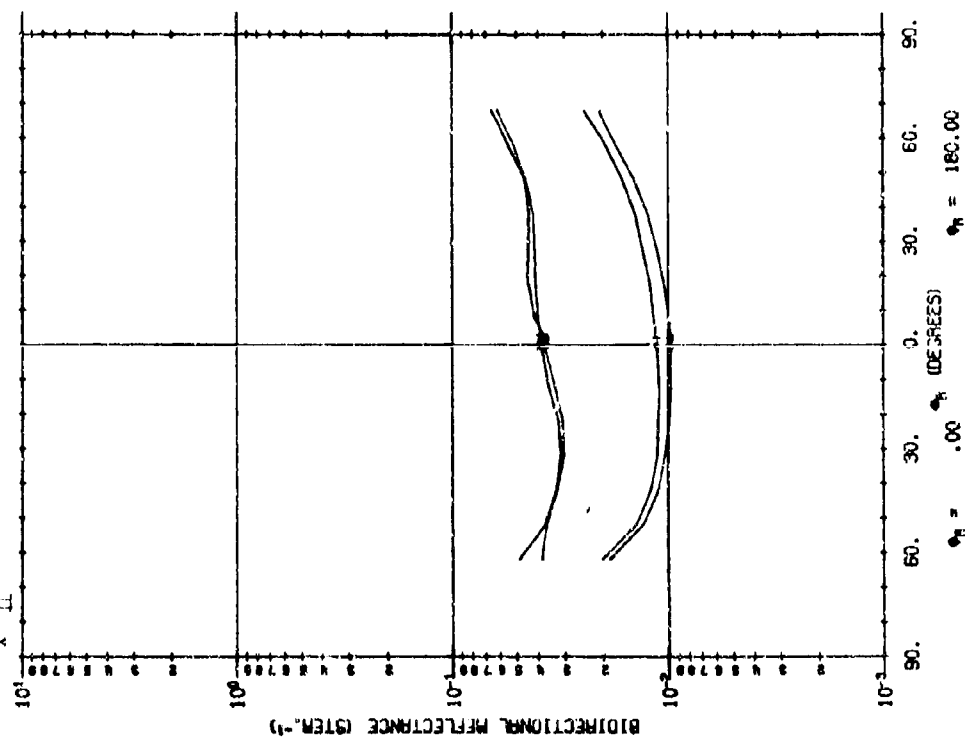
$\theta_i = 70.00$   
 $\theta_r = 180.00$   
 $\lambda = 1.06$



R01457 006

OLIVE DRAB PAINT ON LOWERED  
METAL PANEL

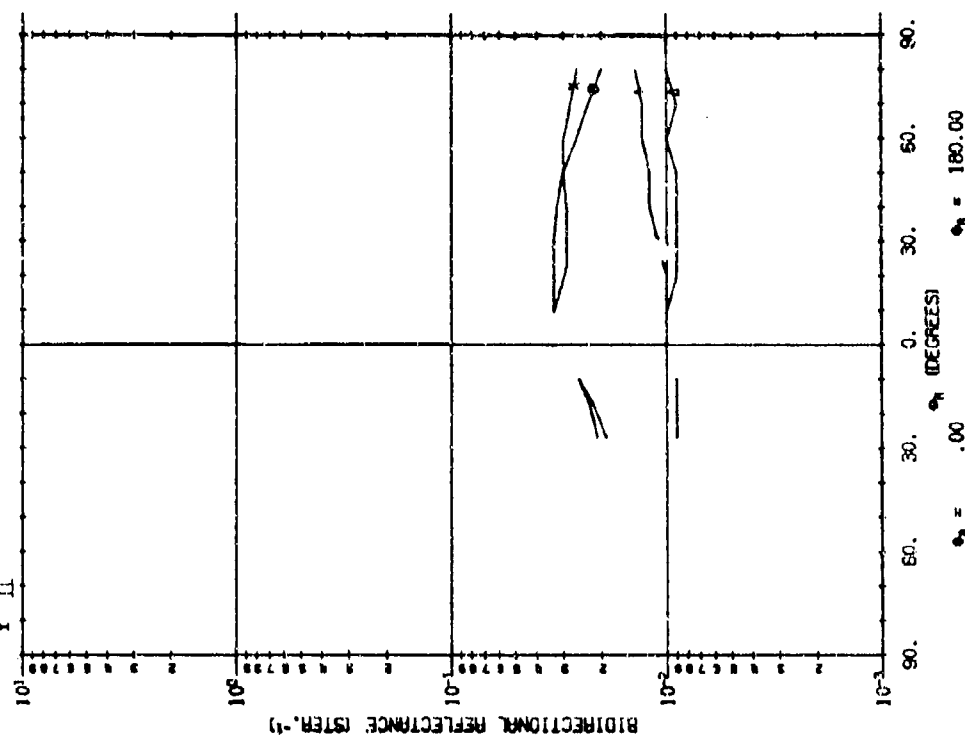
$\phi_1 = 2.0$   
 $\phi_2 = 0.0$   
 $\lambda = 0.63$



R01457 006

OLIVE DRAB PAINT ON LOWERED  
METAL PANEL

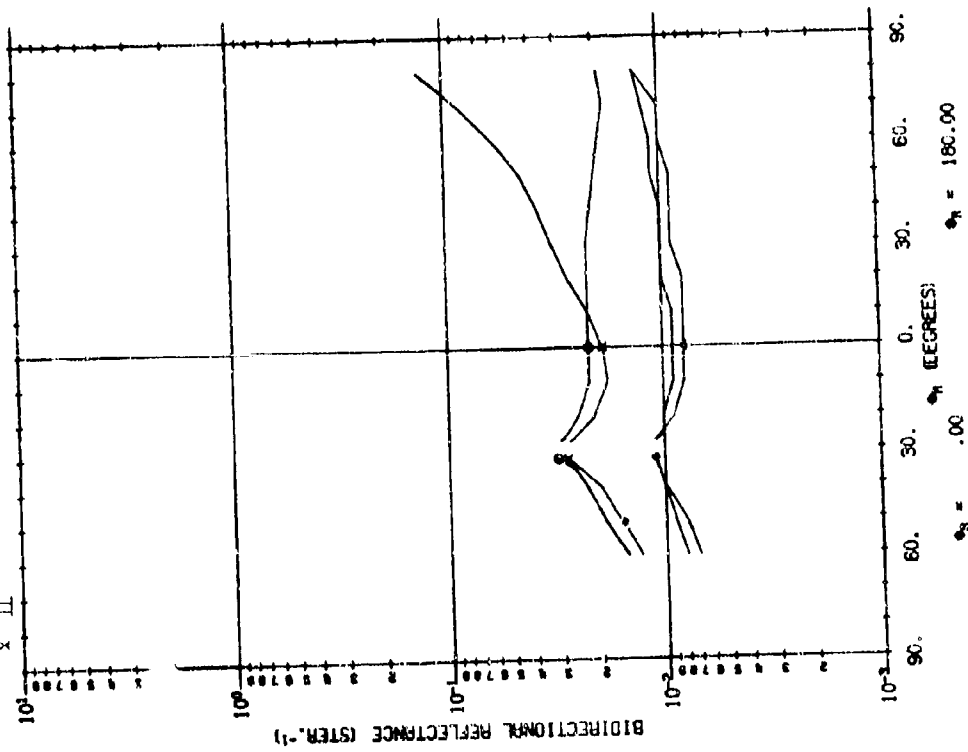
$\phi_1 = 0.0$   
 $\phi_2 = 0.0$   
 $\lambda = 0.63$



PAINT

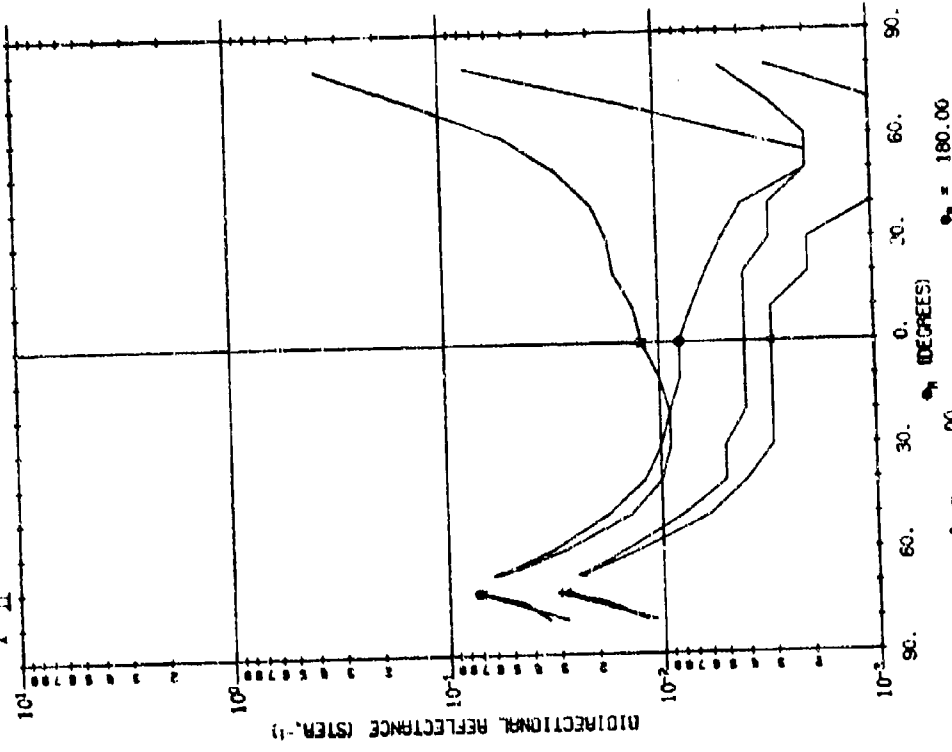
OLIVE DRAB PAINT ON LAMINATED  
METAL PANEL

R01457 008  
 $\theta_1 = 30.00$   
 $\theta_2 = 0.0$   
 $\lambda = 0.63$



OLIVE DRAB PAINT ON LAMINATED  
METAL PANEL

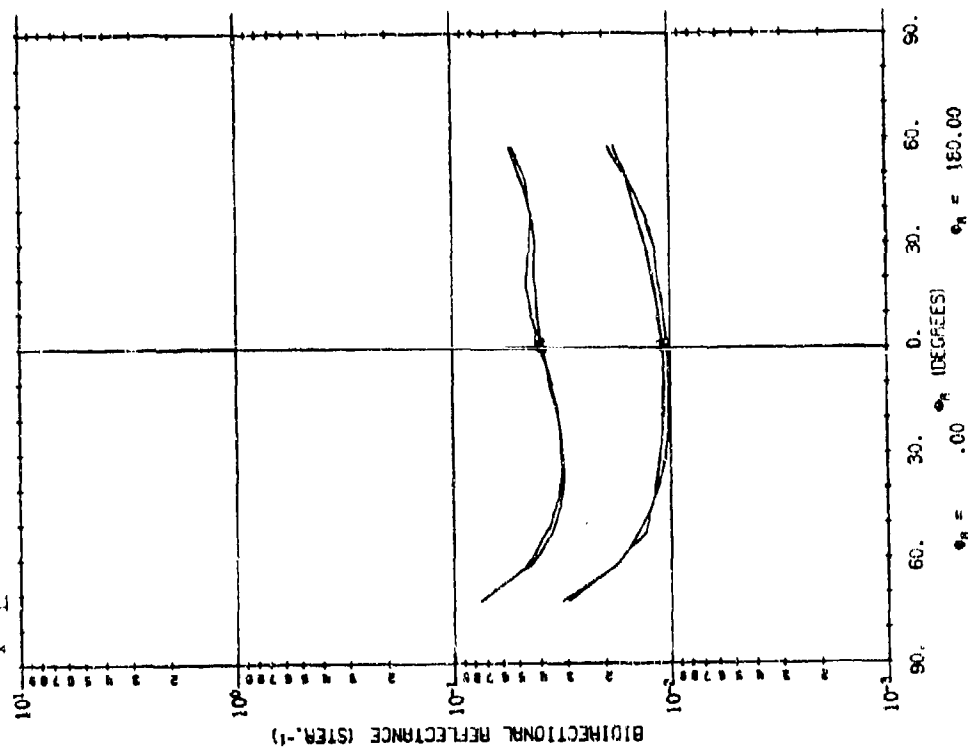
R01457 005  
 $\theta_1 = 30.00$   
 $\theta_2 = 0.0$   
 $\lambda = 0.63$



R01457 006

OLIVE DRAB PAINT ON LAMINATED  
METAL PANEL

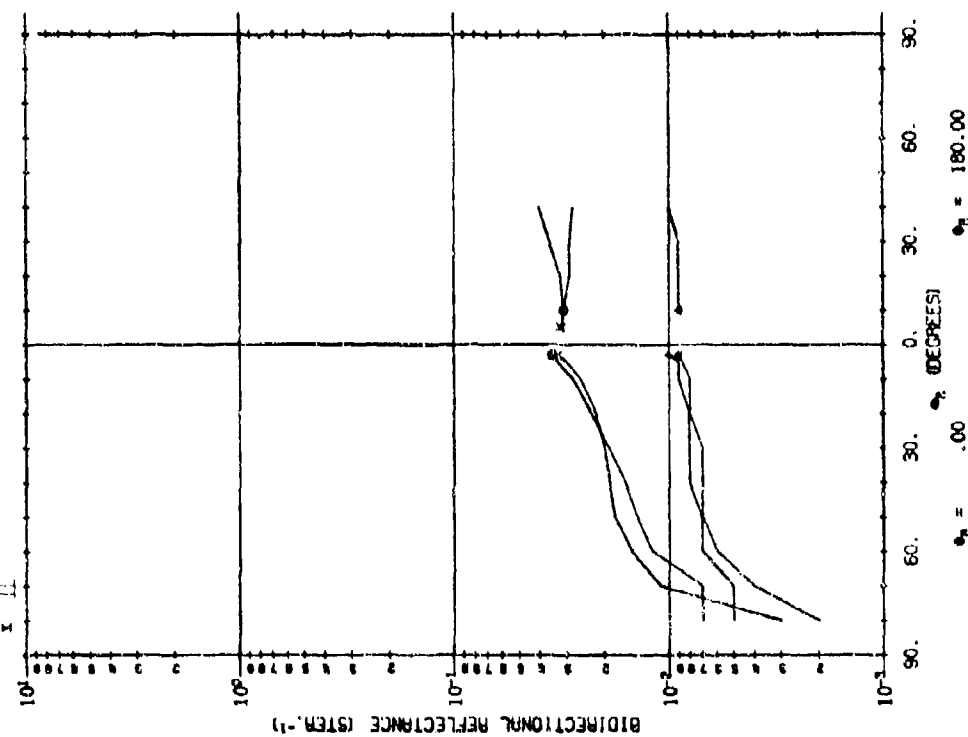
$\theta_1 = 2.0$   
 $\theta_2 = 1.0$   
 $\theta_3 = 0.63$



R01457 006

OLIVE DRAB PAINT ON LAMINATED  
METAL PANEL

$\theta_1 = 0.0$   
 $\theta_2 = 1.0$   
 $\theta_3 = 0.63$



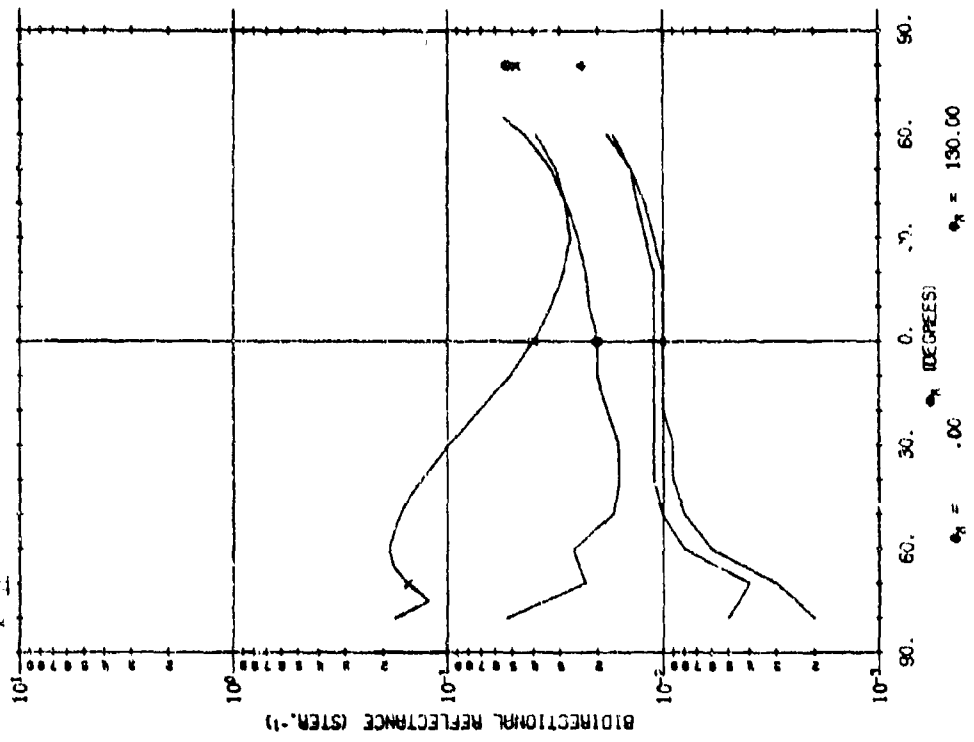
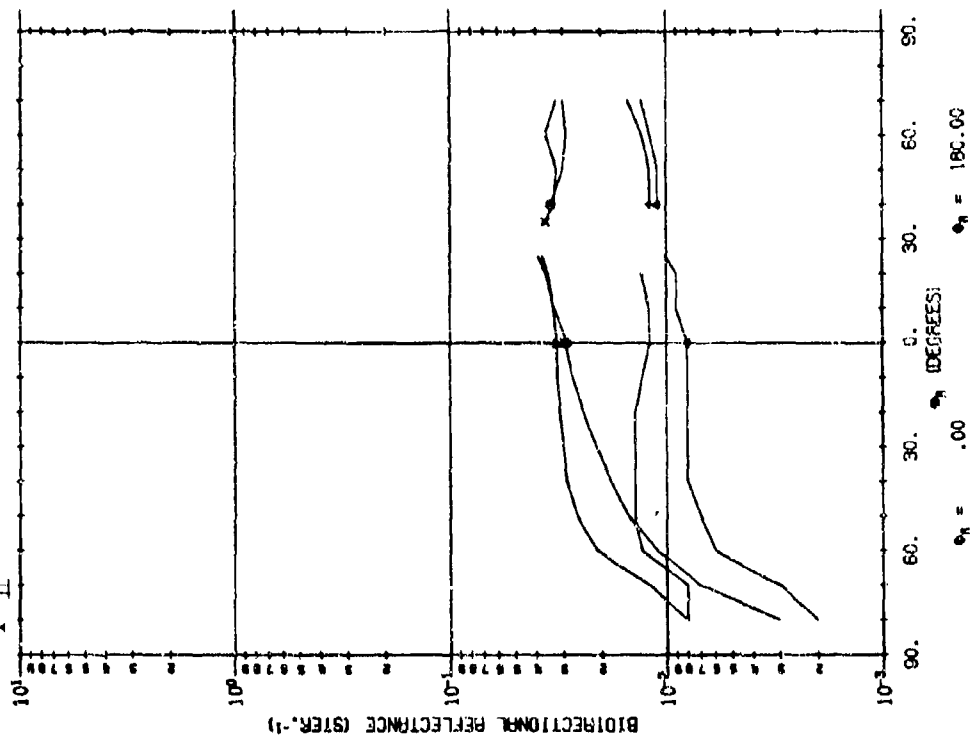
PAINT



R01457 006

OLIVE DRAB PAINT ON LOUVERED  
METAL PANEL  
 $\theta_1 = 30.00$   
 $\theta_2 = 150.00$   
 $\lambda = 0.63$

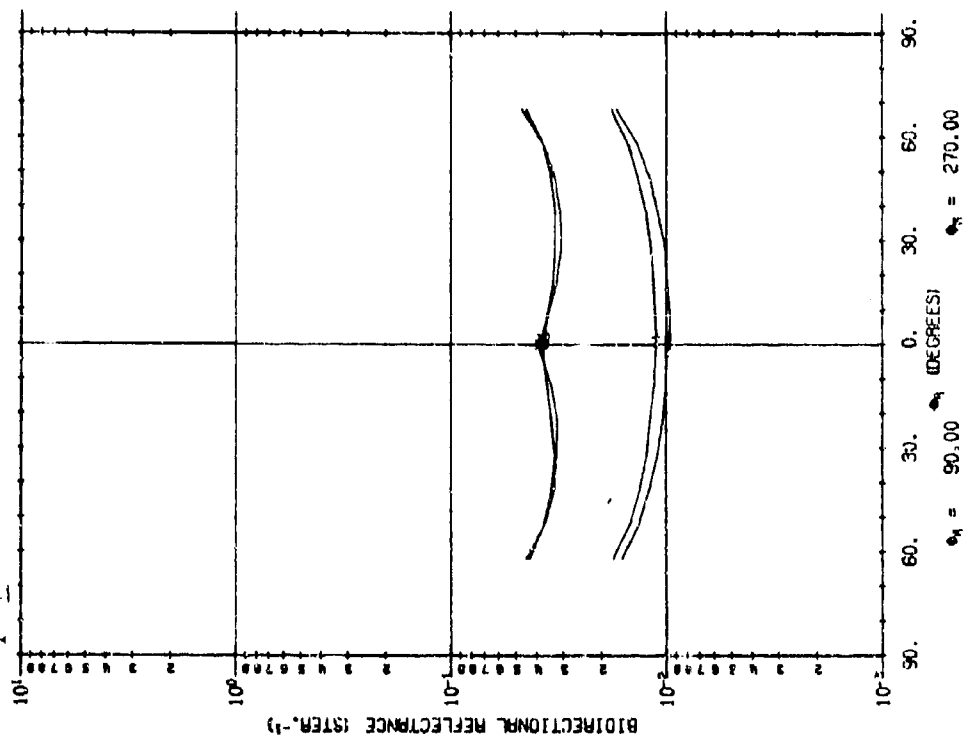
R01457 006  
 $\theta_1 = 70.00$   
 $\theta_2 = 180.00$   
 $\lambda = 0.63$



A01457 006

OLIVE DRAB PAINT ON LOUVERED  
METAL PANEL

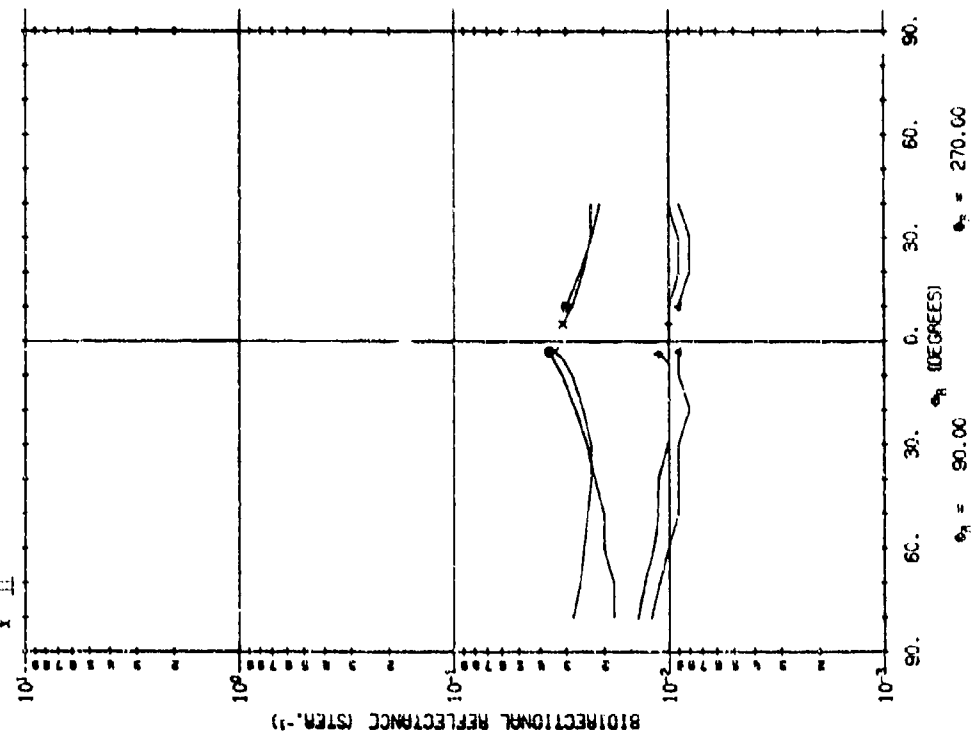
$\theta_1 = 2.0$   
 $\theta_2 = 4.0$   
 $\theta_3 = 0.63$



A01457 006

OLIVE DRAB PAINT ON LOUVERED  
METAL PANEL

$\theta_1 = 0.0$   
 $\theta_2 = 270.00$   
 $\theta_3 = 0.63$



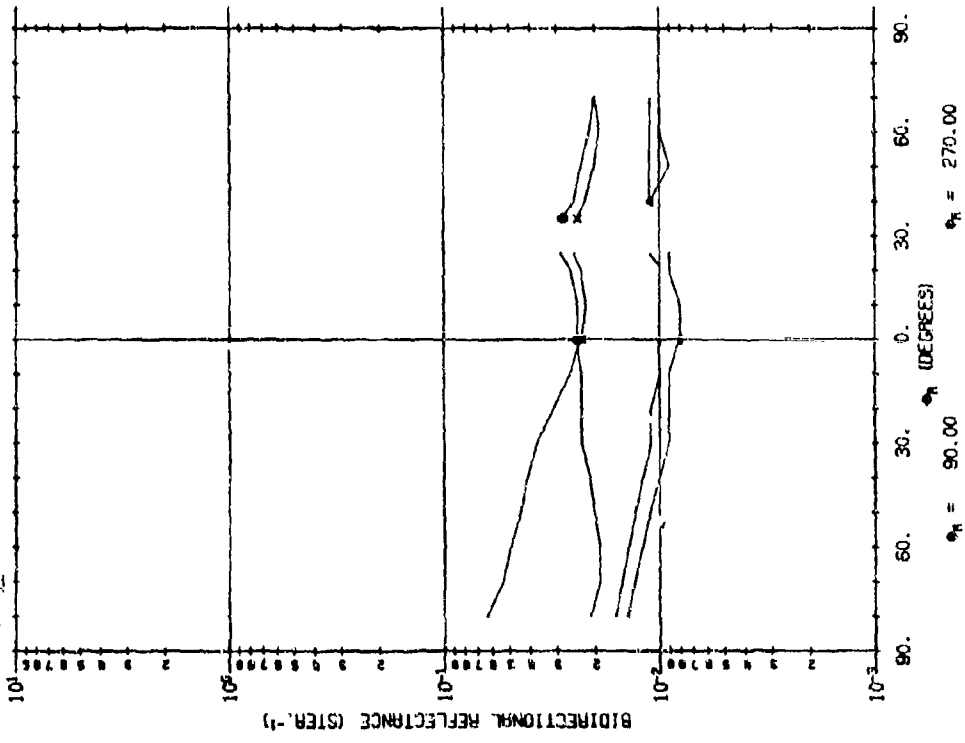
PAINT

R01457 006

OLIVE DRAB PAINT ON  
METAL PANEL

$\theta_i = 30.00$   
 $\theta_r = 270.00$   
 $\lambda = 0.63$

0 1 1  
+ 1 1  
x 1 1

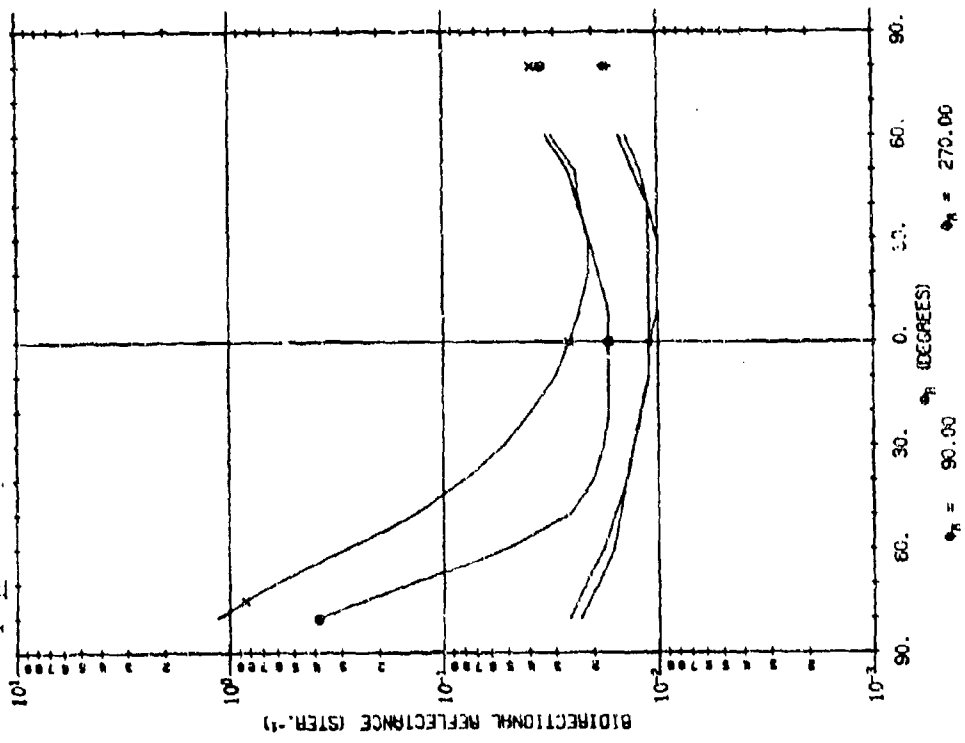


R01457 006

OLIVE DRAB PAINT ON LOUVERED  
METAL PANEL

$\theta_i = 70.00$   
 $\theta_r = 270.00$   
 $\lambda = 0.63$

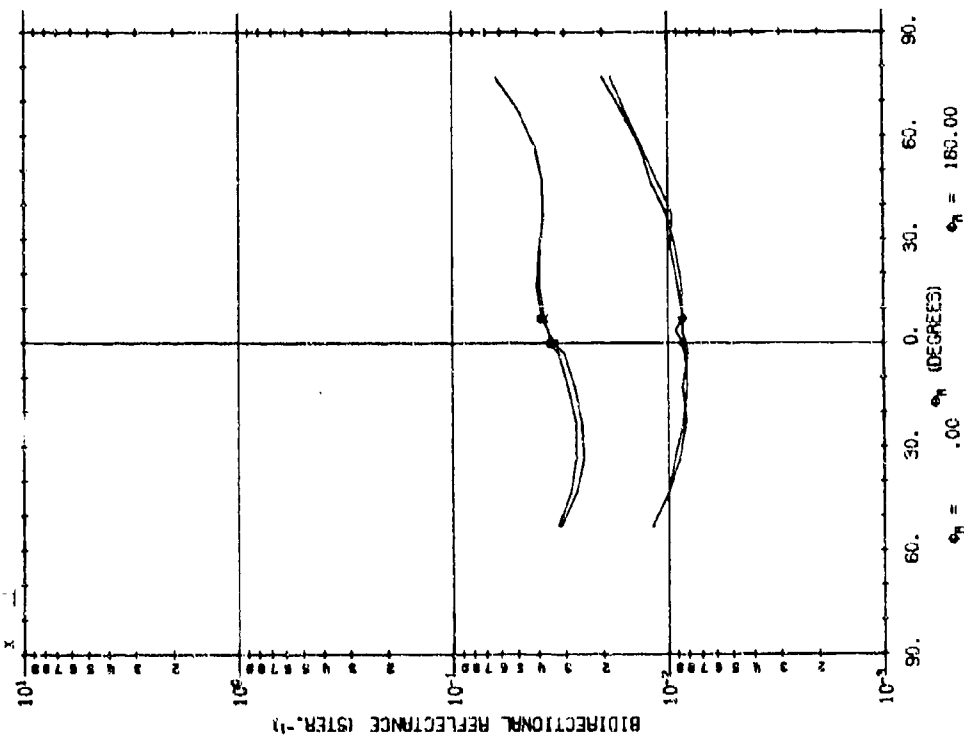
0 1 1  
+ 1 1  
x 1 1



R01457 005

OLIVE DRAB PAINT ON METAL

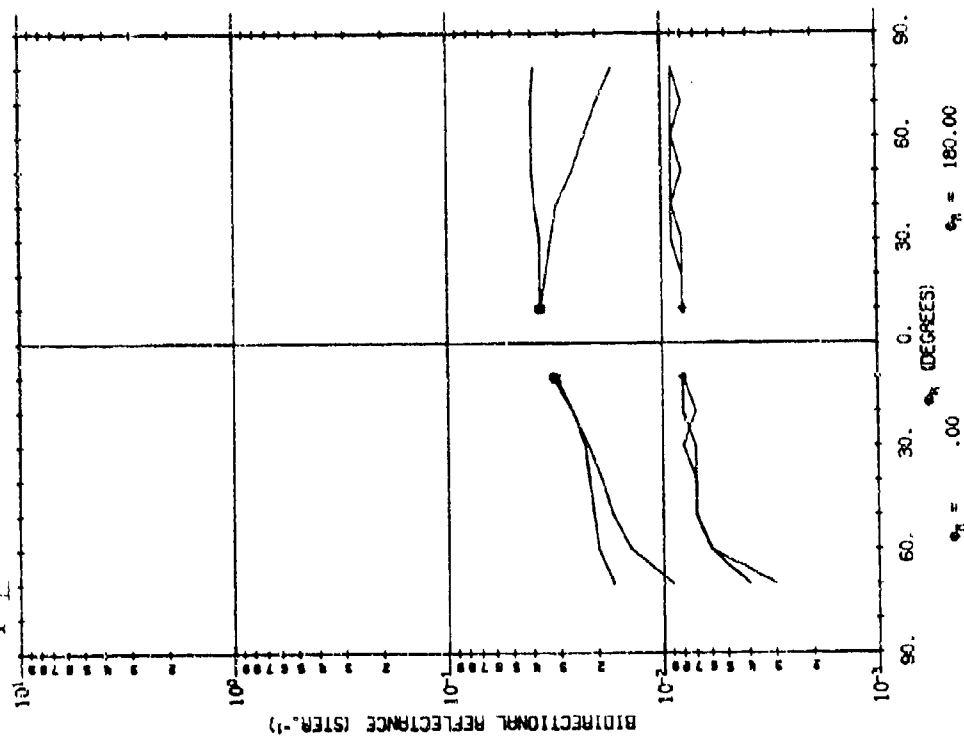
$\theta_i = 7.0$   
 $\phi_i = 0.0$   
 $\lambda = 1.06$



R01457 005

OLIVE DRAB PAINT ON LOUVERED METAL PANEL

$\theta_i = 0.0$   
 $\phi_i = 0.0$   
 $\lambda = 1.06$

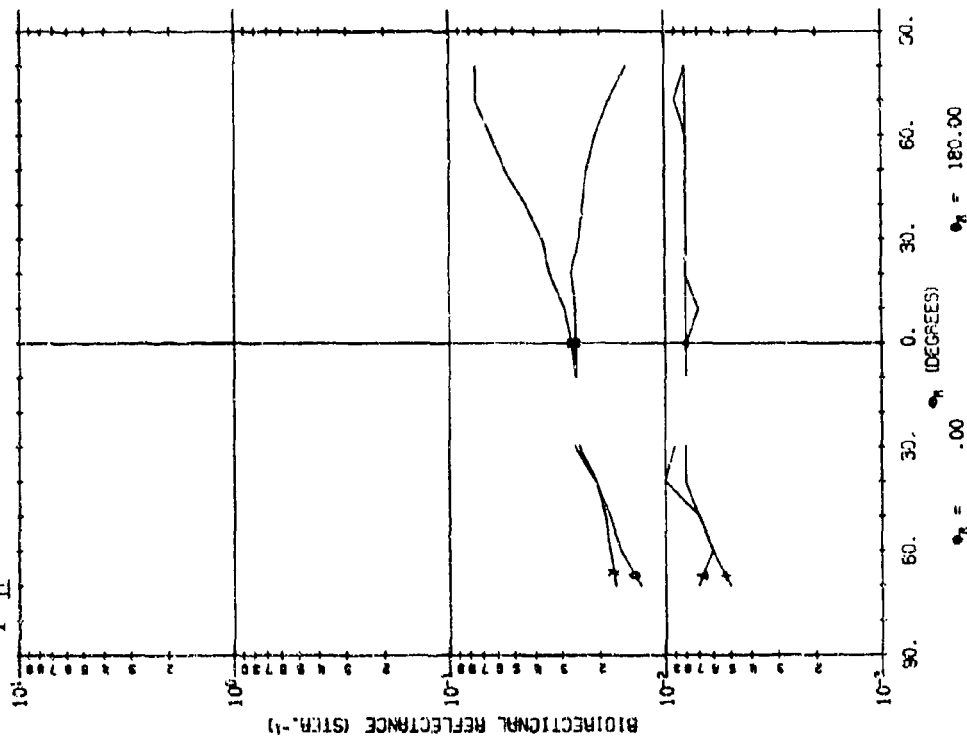


PAINT

R01457 005

Olive Drab Paint on Louvered Metal Panel

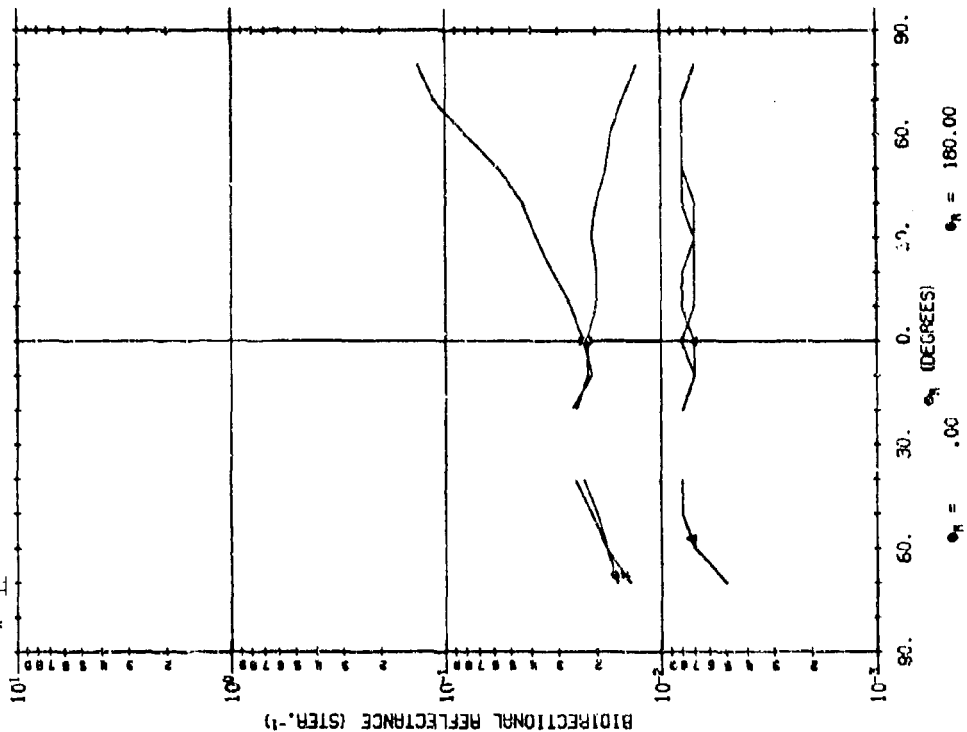
$\theta_i = 20.00$   
 $\phi_i = 0.0$   
 $\lambda = 1.06$



R01457 005

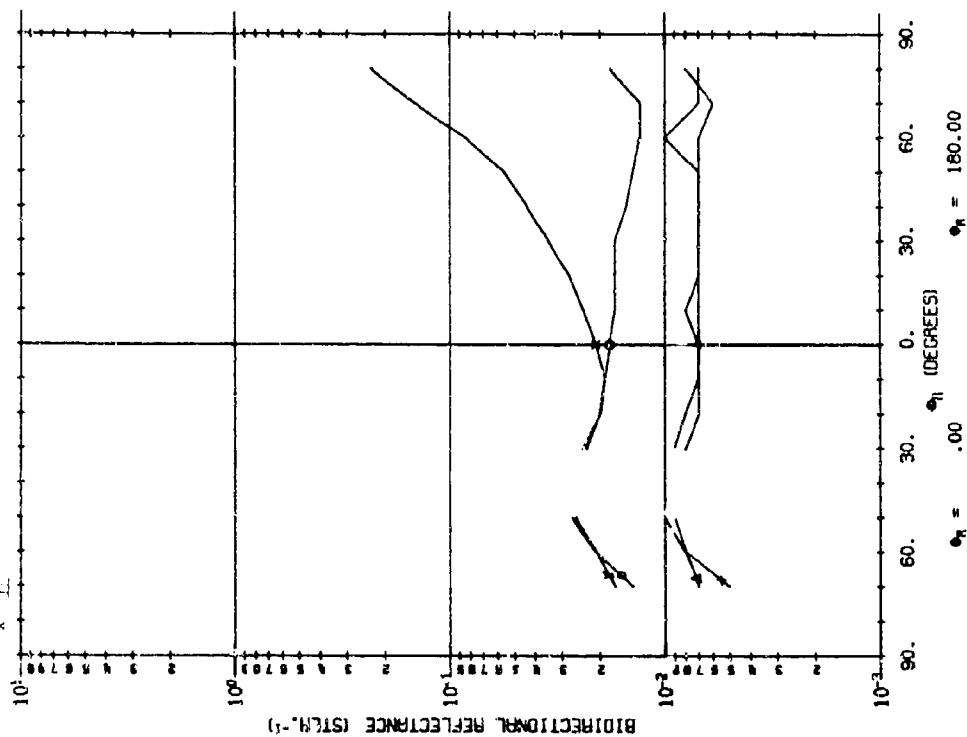
Olive Drab Paint on Louvered Metal Panel

$\theta_i = 30.00$   
 $\phi_i = 0.0$   
 $\lambda = 1.06$



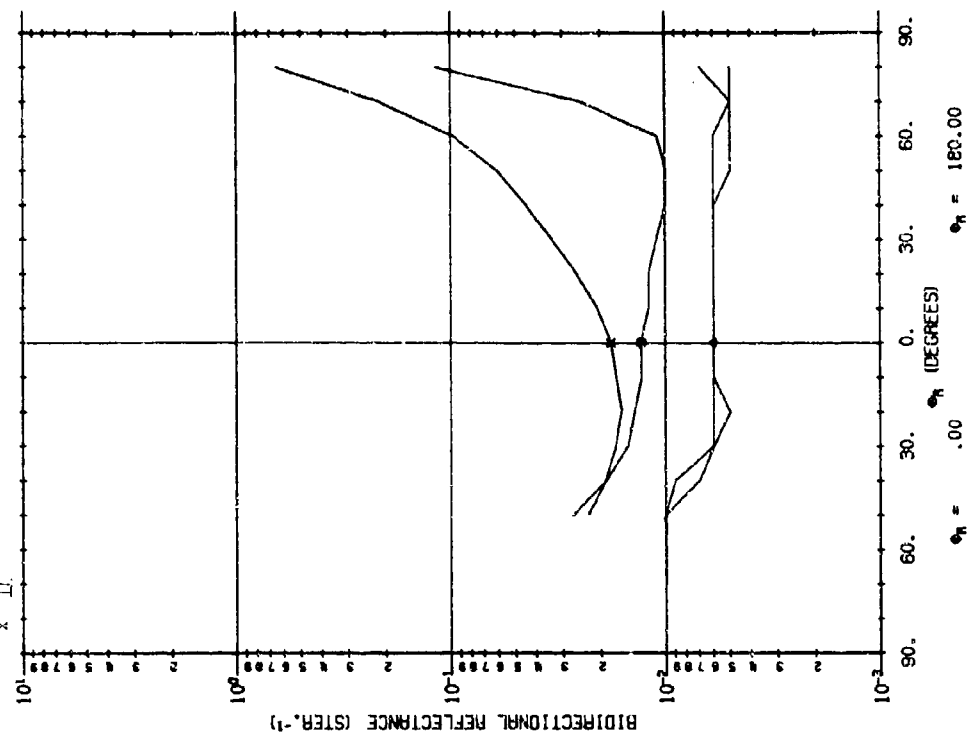
001457 005  
 0 11  $\theta_i = 40.00$   
 + 11  $\phi_i = 0.0$   
 Δ 11  $\lambda = 1.06$   
 x 11

Olive Drab Paint on Louvered Metal Panel



001457 005  
 0 11  $\theta_i = 60.00$   
 + 11  $\phi_i = 0.0$   
 Δ 11  $\lambda = 1.06$   
 x 11

Olive Drab Paint on Louvered Metal Panel



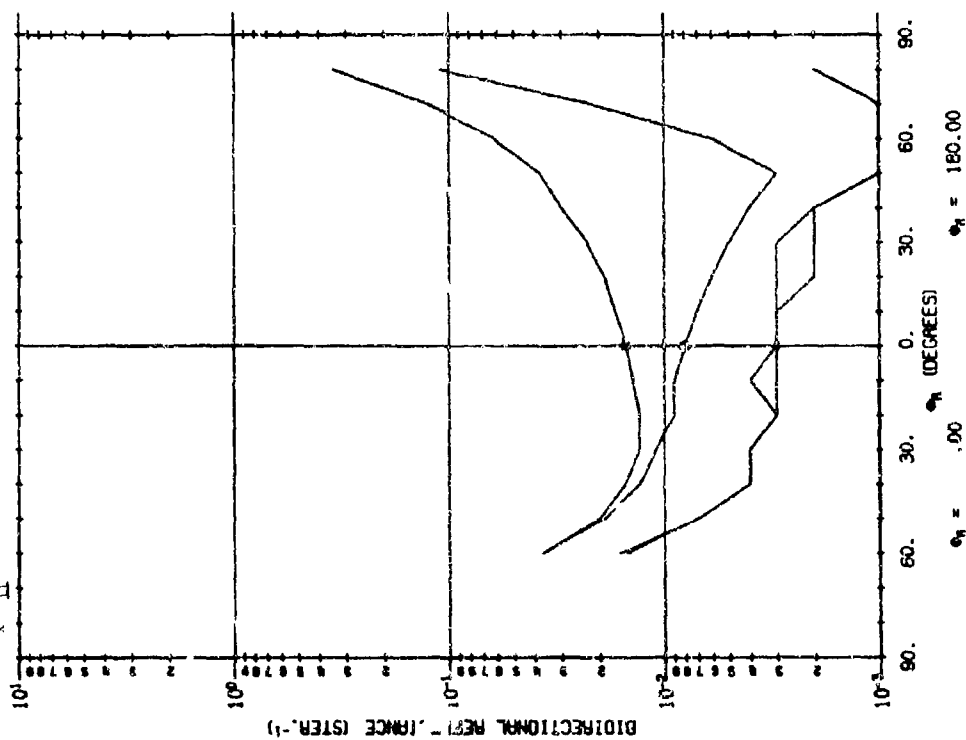
PAINT

R01457 005

Olive Drab Paint on Louvered Metal Panel

$\epsilon_1 = 70.00$   
 $\phi_1 = 0.0$   
 $\lambda = 1.06$

0 ||  
 + ||  
 x ||

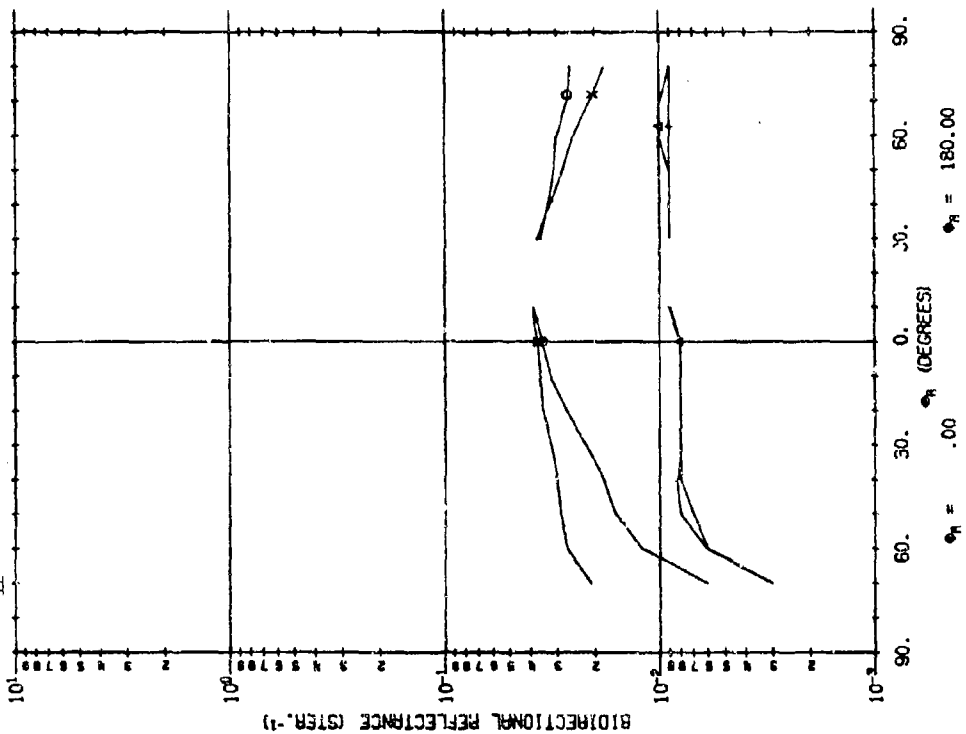


R01457 005

Olive Drab Paint on Louvered Metal Panel

$\epsilon_1 = 20.00$   
 $\phi_1 = 180.00$   
 $\lambda = 1.06$

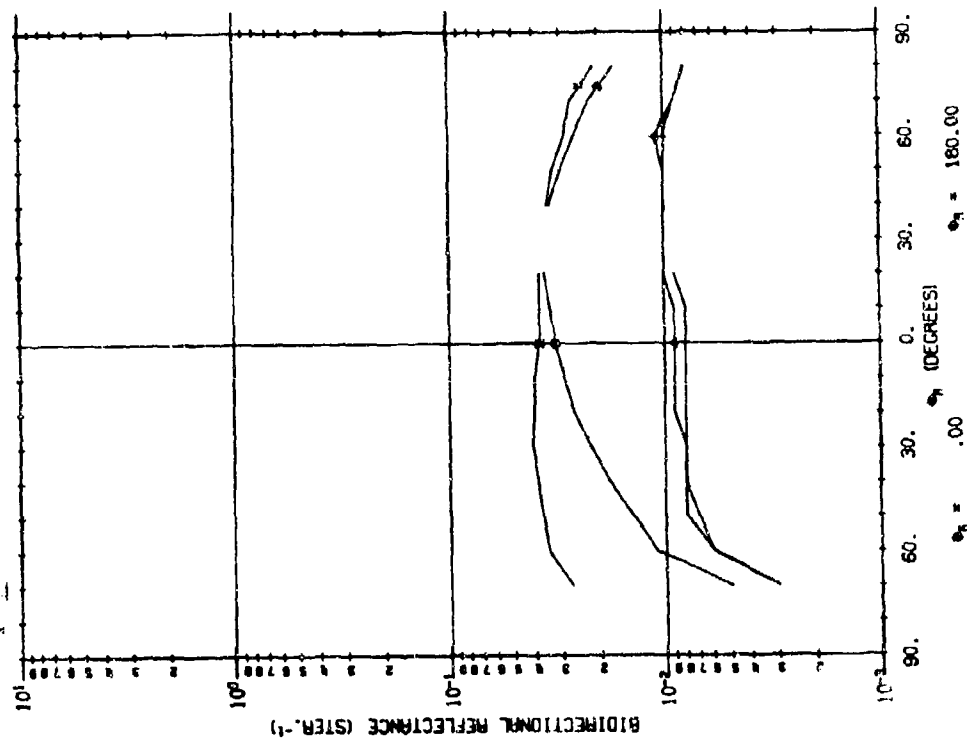
0 ||  
 + ||  
 x ||



A01457 005

Olive Drab Paint on Louvered Metal Panel

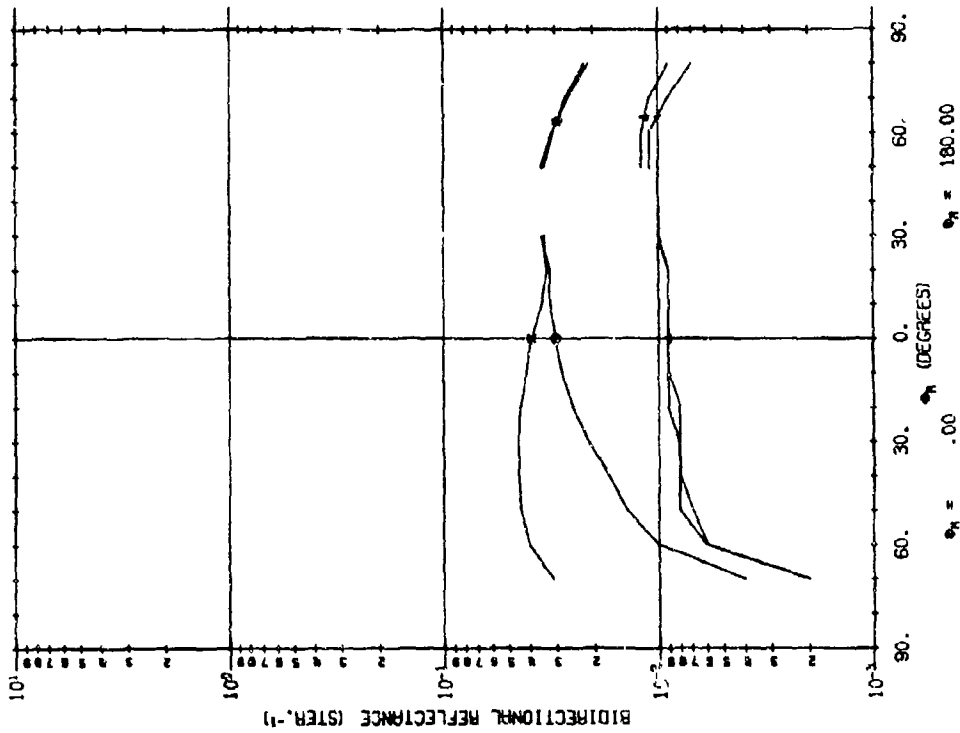
$\theta_i = 30.00$   
 $\theta_r = 180.00$   
 $\theta_t = 1.06$



A01457 005

Olive Drab Paint on Louvered Metal Panel

$\theta_i = 40.00$   
 $\theta_r = 180.00$   
 $\theta_t = 1.06$



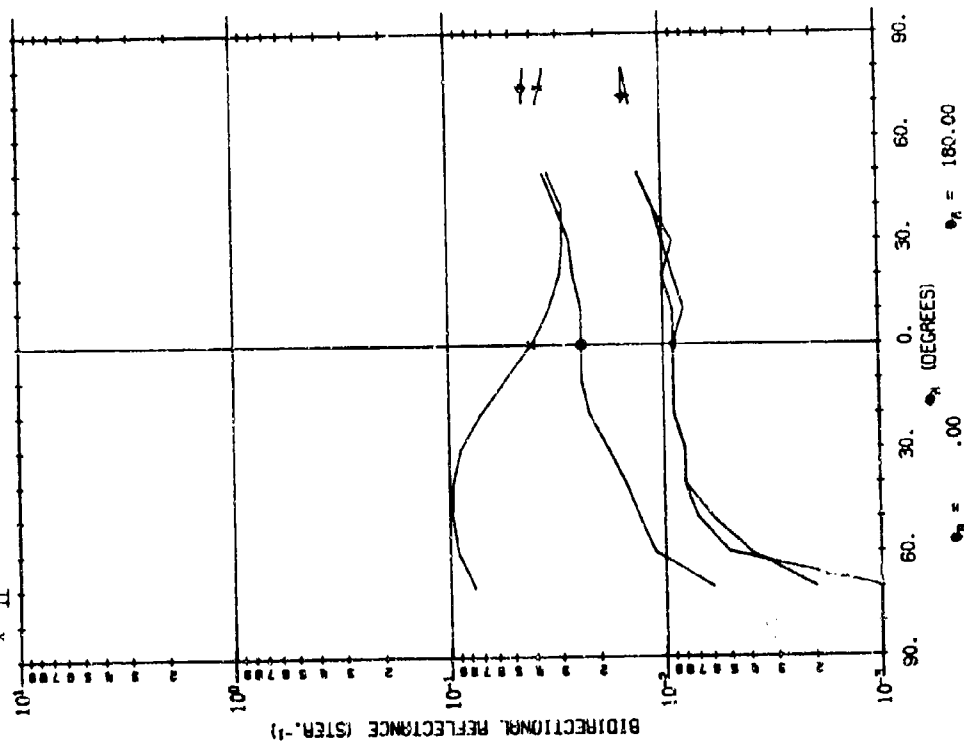
PAINT



A01457 005 Olive Drab Paint on Louvered Metal Panel

$\theta_i = 60.00$   
 $\phi_i = 180.00$   
 $\lambda = 1.06$

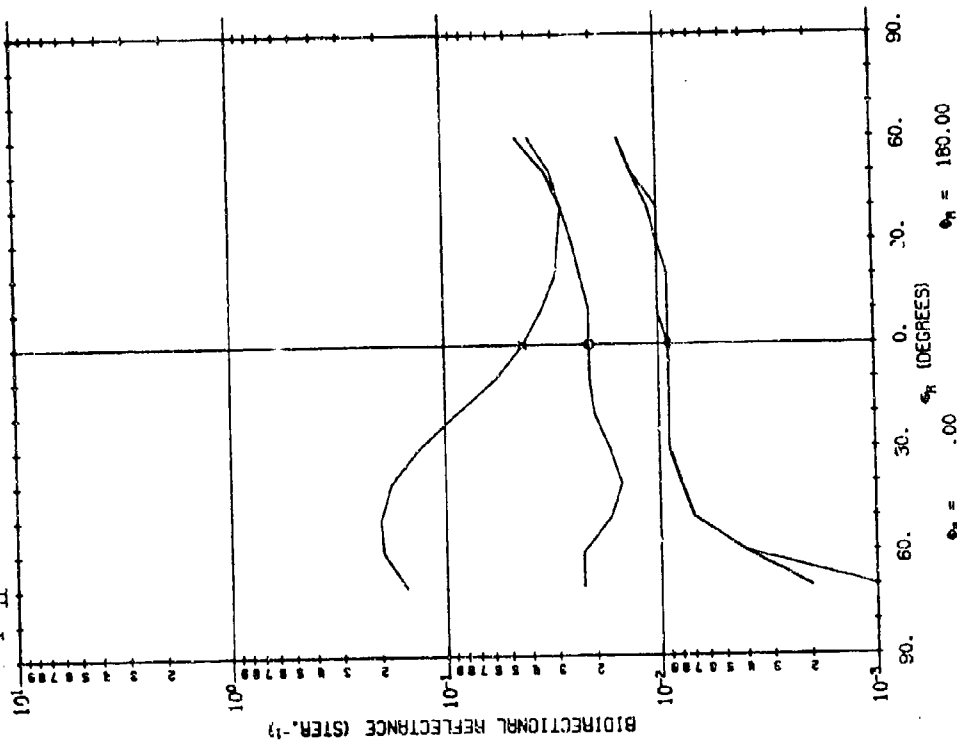
0 II  
 + II  
 Δ II  
 X II



A01457 005 Olive Drab Paint on Louvered Metal Panel

$\theta_i = 70.00$   
 $\phi_i = 180.00$   
 $\lambda = 1.06$

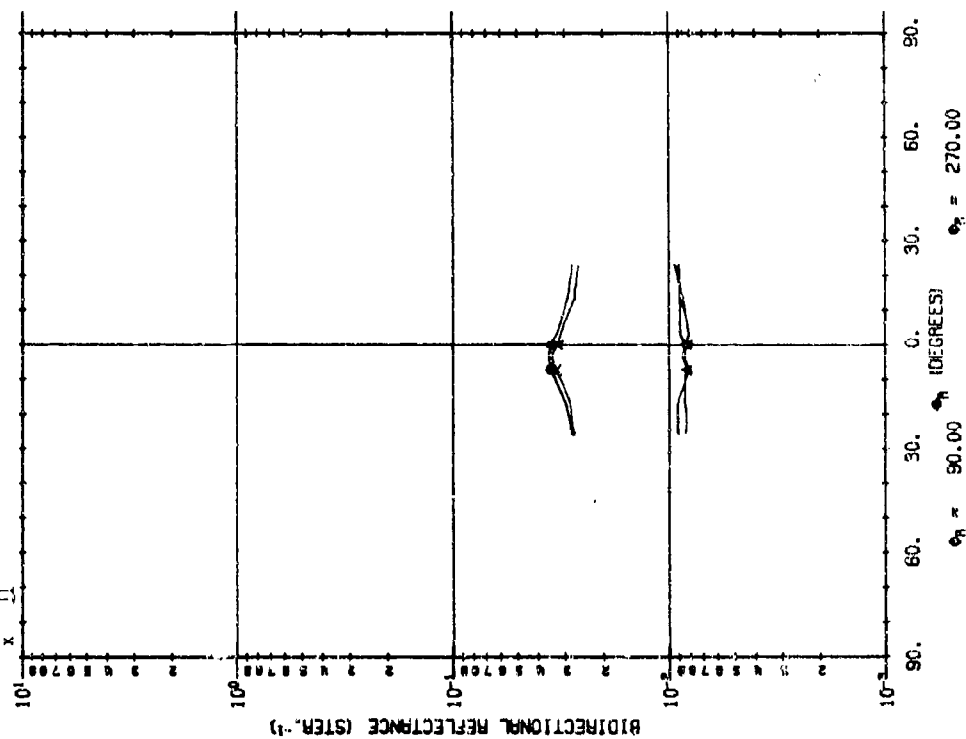
0 II  
 + II  
 Δ II  
 X II



A01457 005

OLIVE DRAB PAINT ON METAL

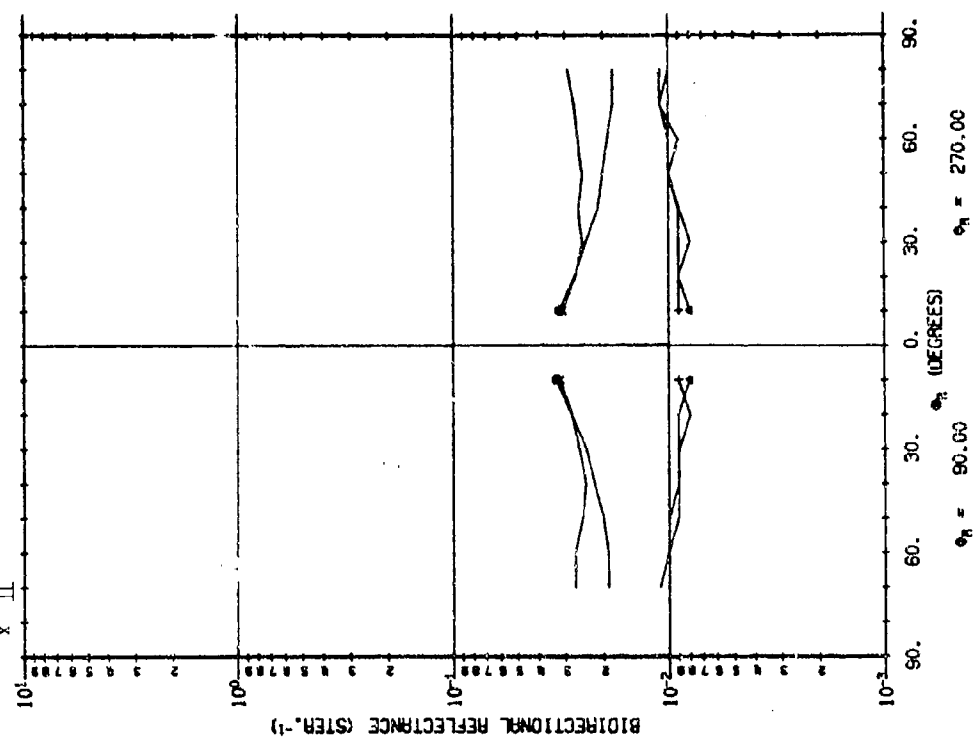
0 11 28 = 7.0  
+ 11 11 11 = 1.06  
- 11 11 11 = 1.06  
X 11 11



A01457 005

OLIVE DRAB PAINT ON LEVERED METAL PANEL

0 11 0.0  
+ 11 11 11 = 270.00  
- 11 11 11 = 1.06  
X 11 11

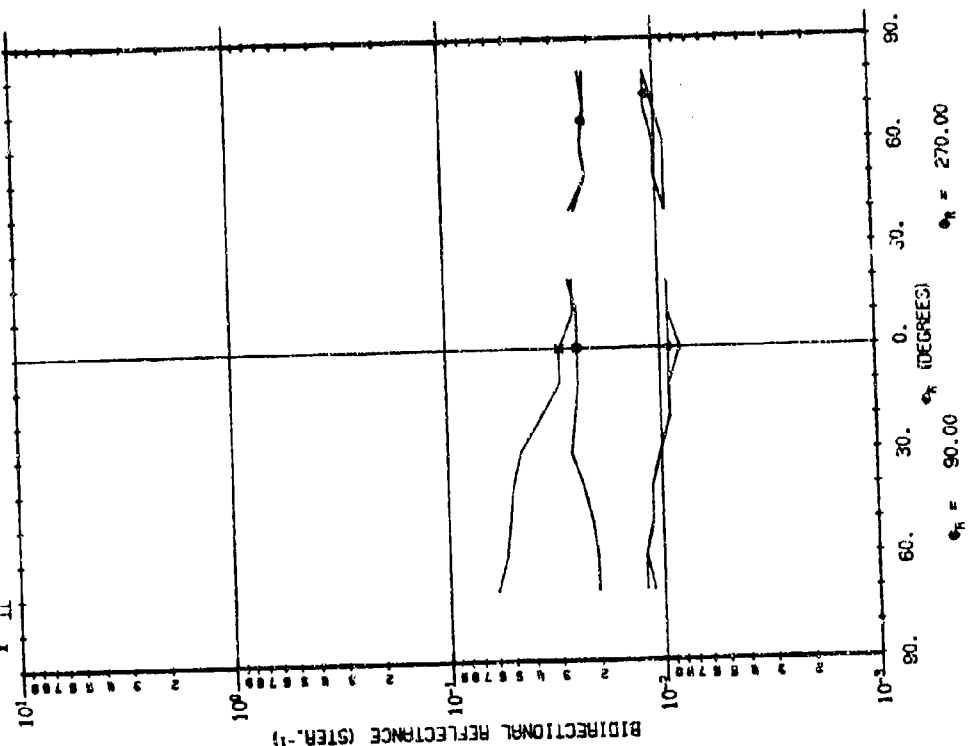


PAINT

A01457 005 Olive Drab Paint on Louvered Metal Panel

$\theta_i = 30.00$   
 $\phi_i = 270.00$   
 $\lambda = 1.06$

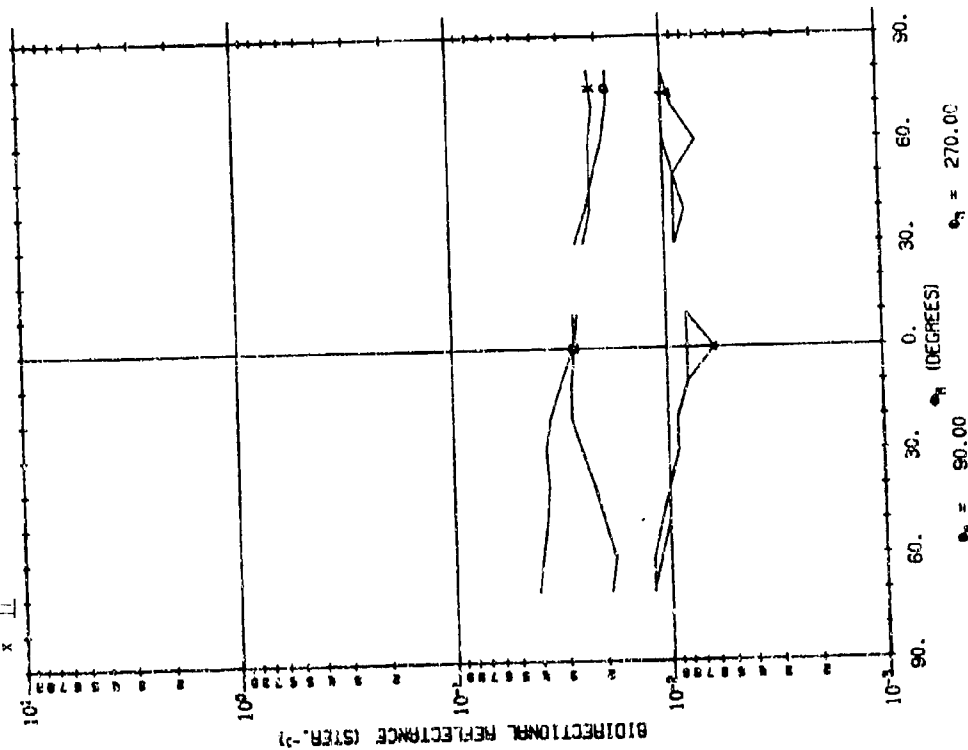
0 ||  
 + ||  
 Δ ||  
 x ||



A01457 005 Olive Drab Paint on Louvered Metal Panel

$\theta_i = 30.00$   
 $\phi_i = 270.00$   
 $\lambda = 1.06$

0 ||  
 + ||  
 Δ ||  
 x ||



R01457 005

Olive Drab Paint on Louvered Metal Panel

$\theta_i = 40.00$   
 $\phi_i = 270.00$   
 $\lambda = 1.06$

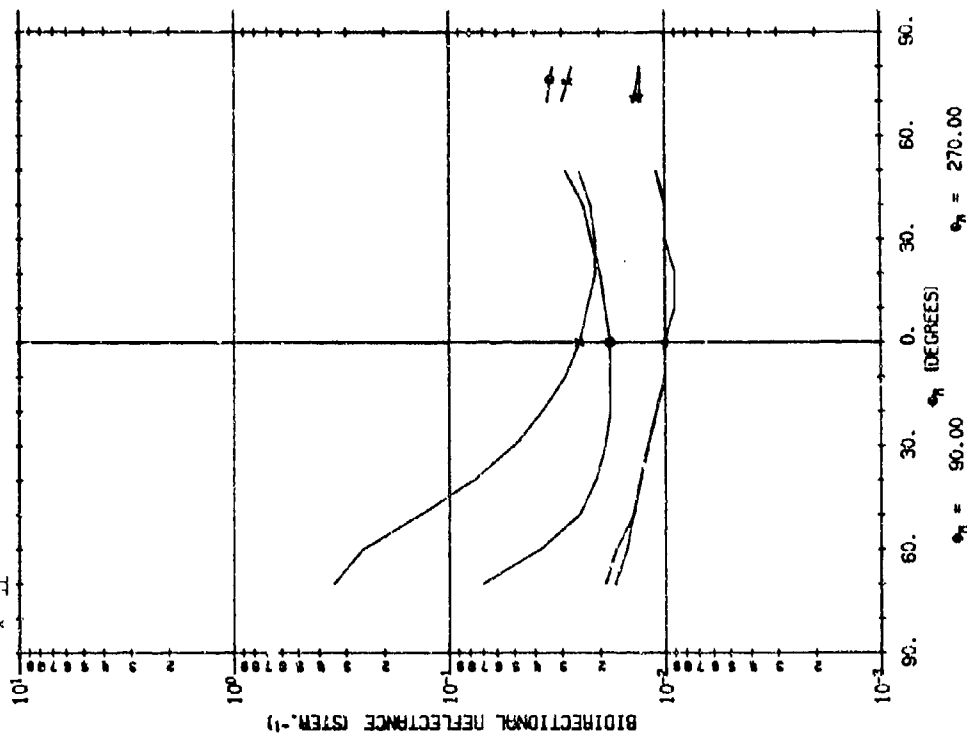
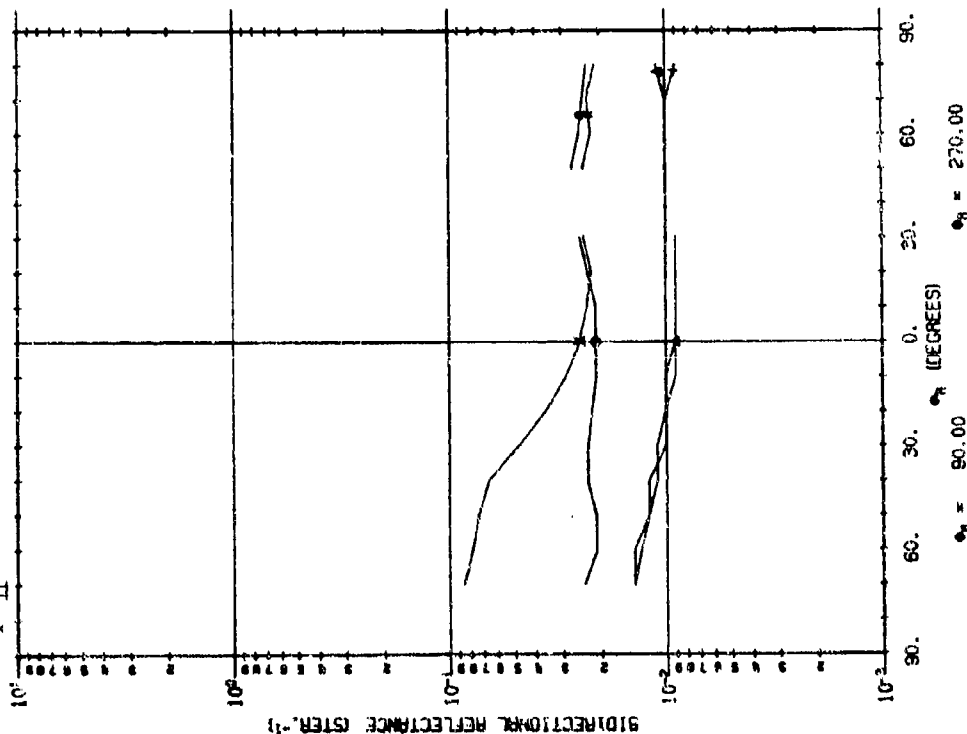
0 11

$\theta_i = 60.00$   
 $\phi_i = 270.00$   
 $\lambda = 1.06$

Olive Drab Paint on Louvered Metal Panel

0 11

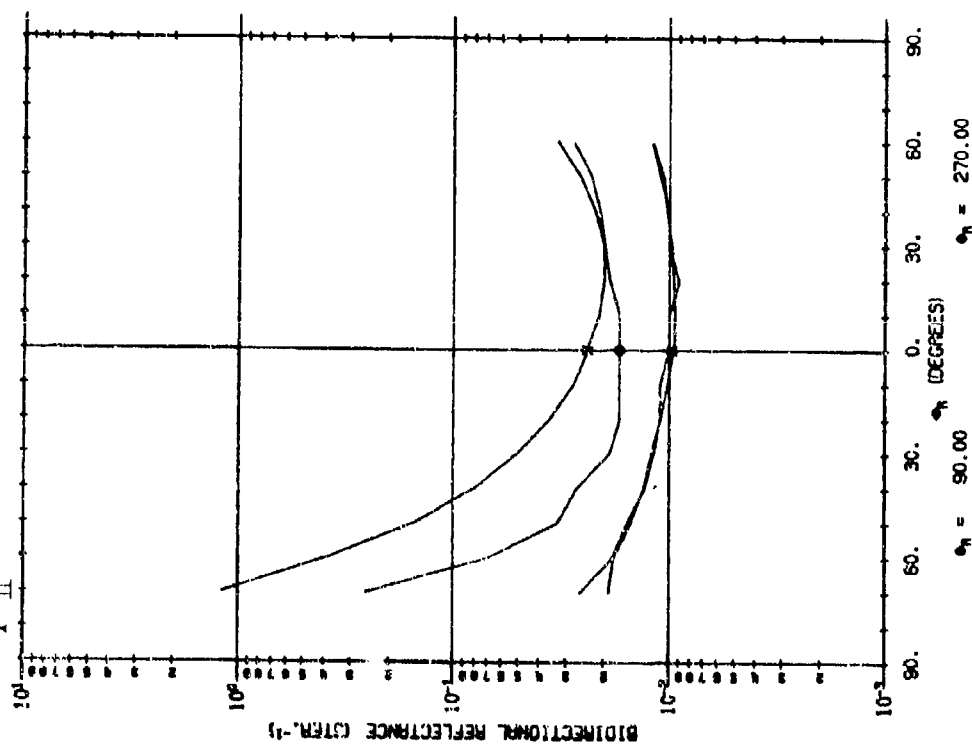
$\theta_i = 60.00$   
 $\phi_i = 270.00$   
 $\lambda = 1.06$



PAINT

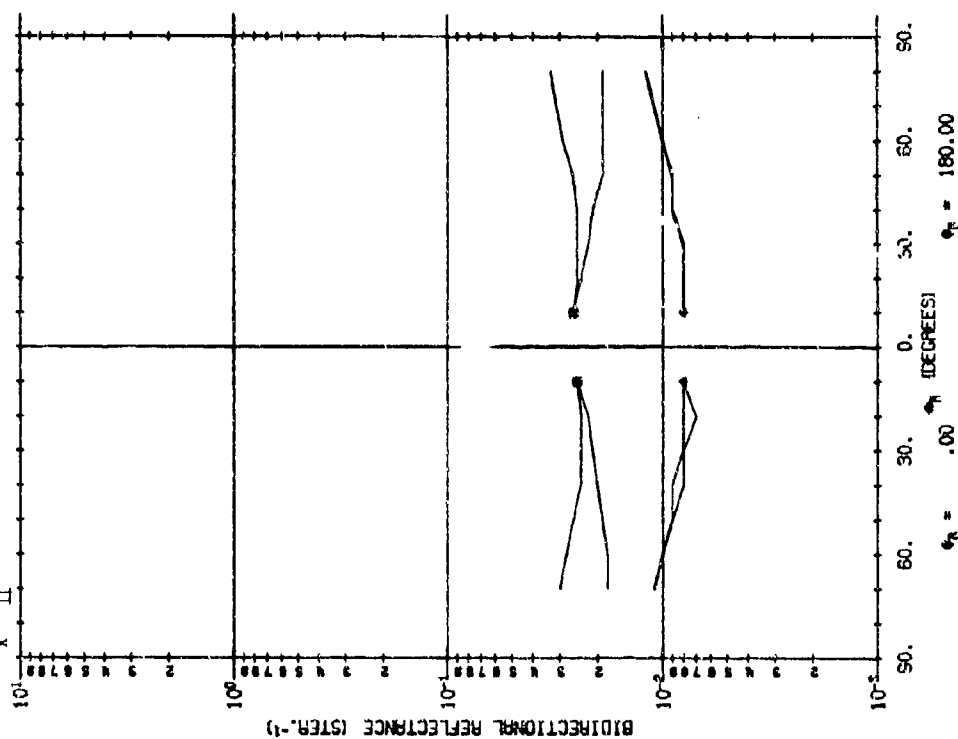
R01457 005  
 0 ||  $\theta_i = 70.00$   
 + ||  $\phi_i = 270.00$   
 x ||  $\lambda = 1.05$

Olive Drab Paint on Lowered Metal Panel



R01509 001  
 0 ||  $\theta_i = 0.0$   
 + ||  $\phi_i = 180.0$   
 x ||  $\lambda = 0.63$

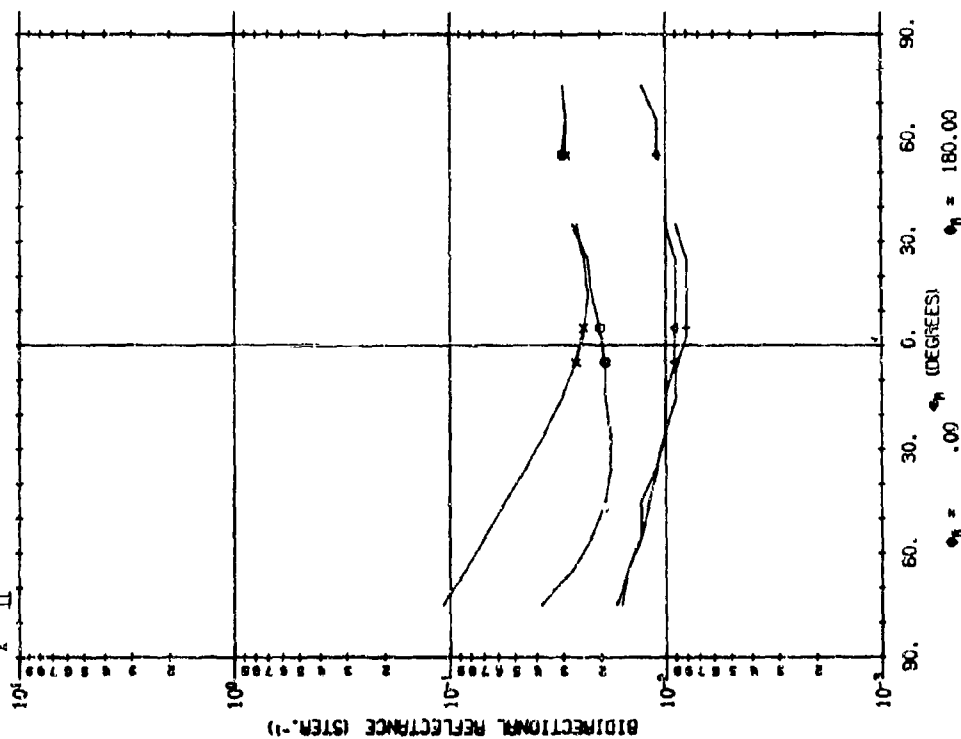
OLIVE DRAB PAINT ON STEEL



A01509 001

OLIVE DRAB PAINT ON STEEL

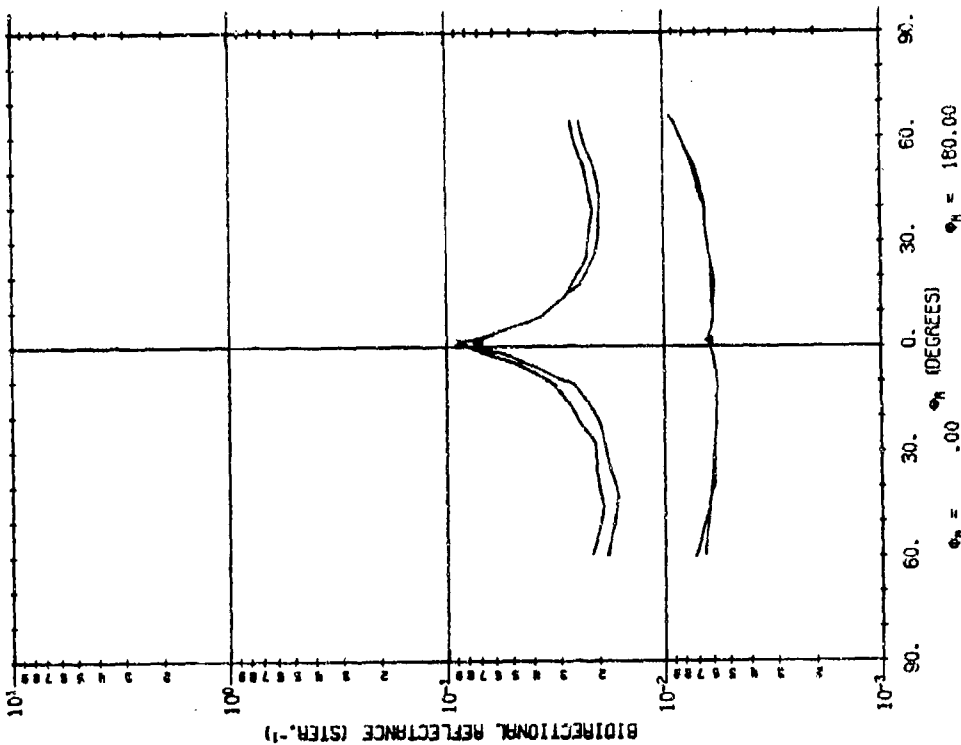
0 ||  $\theta_i = 45.0$   
 + ||  $\phi_i = 180.0$   
 x ||  $\lambda = 0.63$   
 ||



A01569 003

GREEN PAINT ON STEEL

0 ||  $\theta_i = 2.0$   
 + ||  $\phi_i = \phi_r$   
 x ||  $\lambda = 0.63$   
 ||

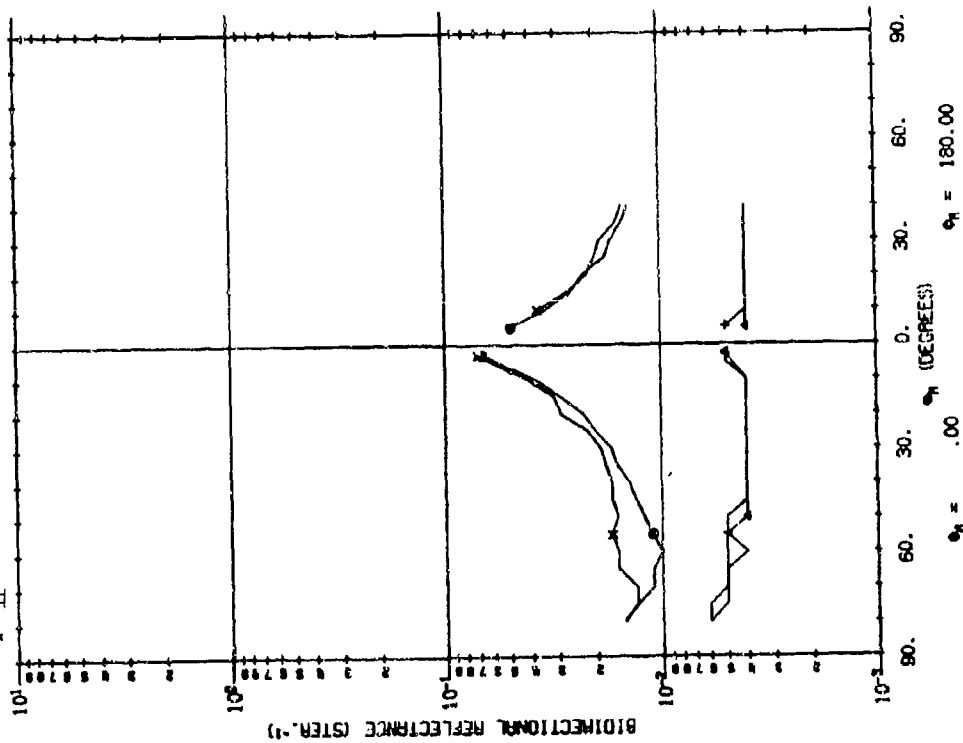


PAINT

A01569 003

Green Paint on Steel

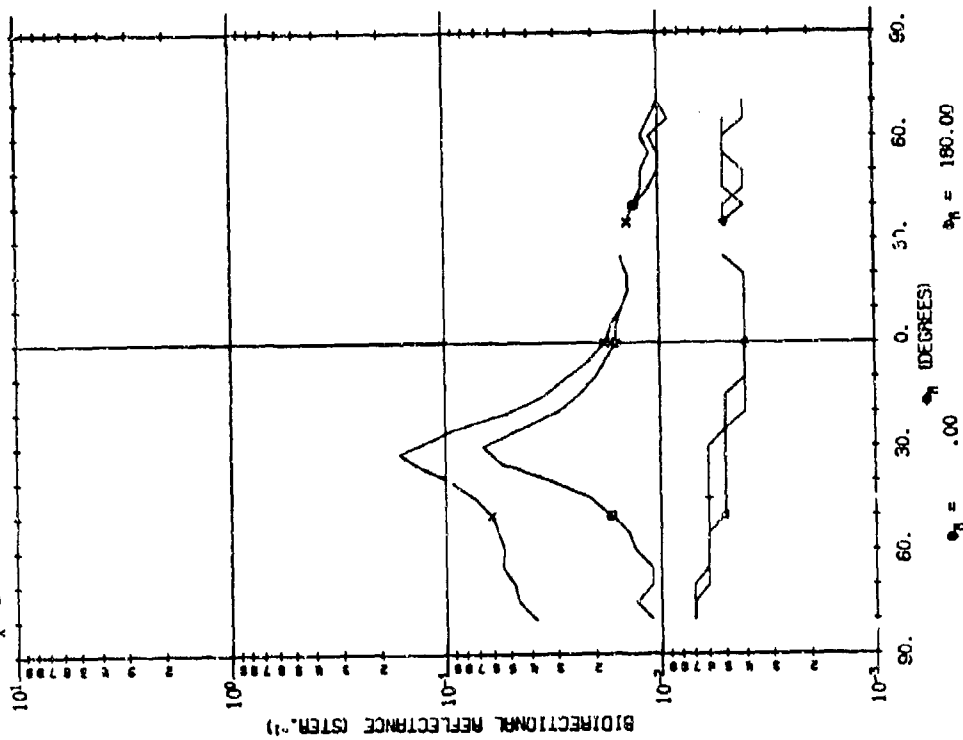
$\theta_1 = 0.0$   
 $\theta_2 = 180.00$   
 $\lambda = 0.63$



A01569 003

Green Paint on Steel

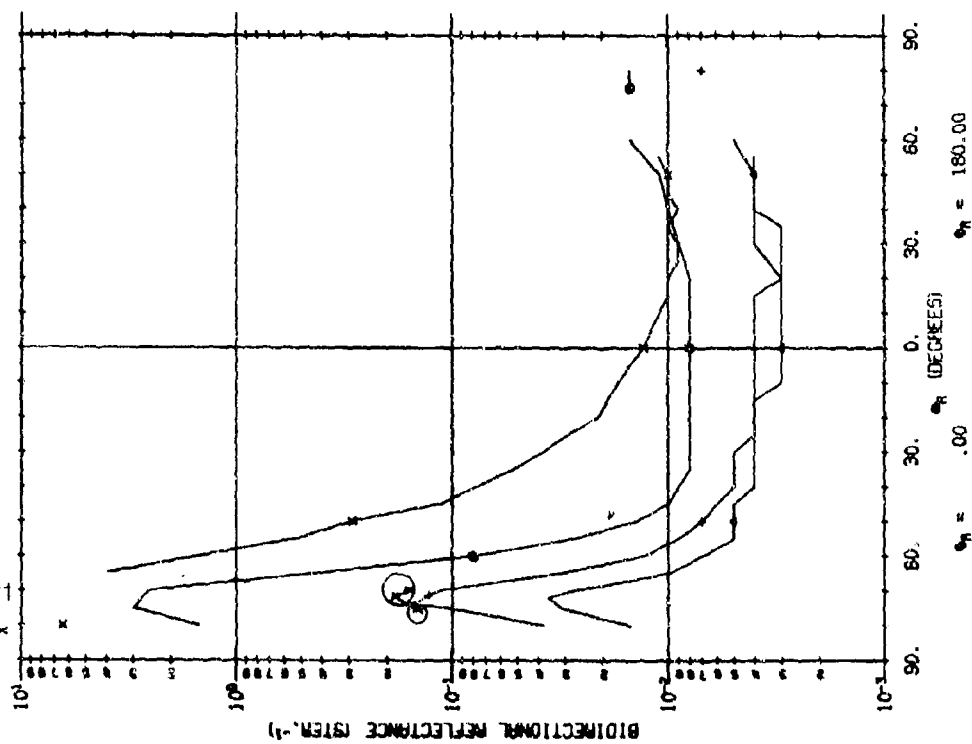
$\theta_1 = 30.00$   
 $\theta_2 = 180.00$   
 $\lambda = 0.63$



A01569 003

Green Paint on Steel

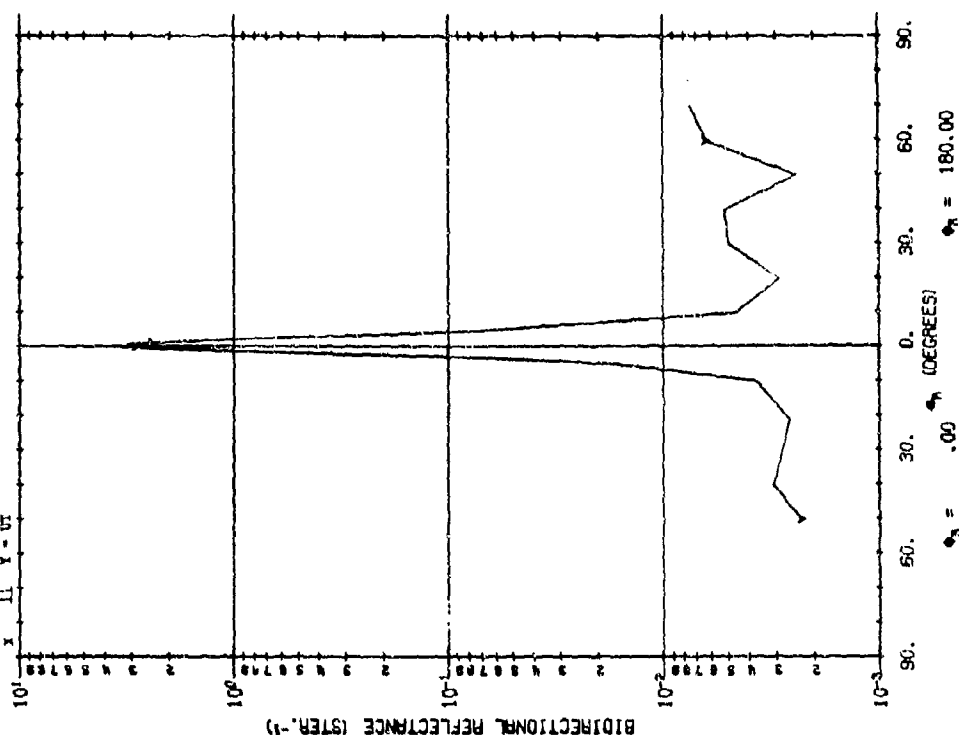
$\theta_1 = 70.00$   
 $\phi_1 = 180.00$   
 $\lambda = 0.63$



A01569 004

GREEN PAINT ON STEEL

$\theta_1 = 70.00$   
 $\phi_1 = 180.00$   
 $\lambda = 0.63$



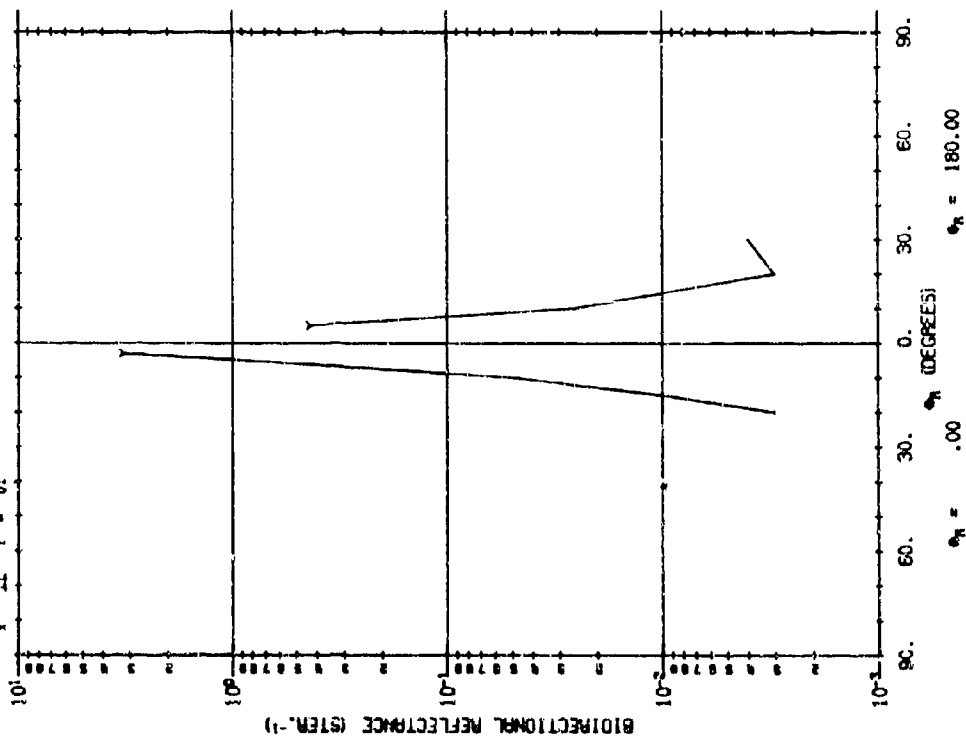
PAINT



A01569 004

Green Paint on Steel

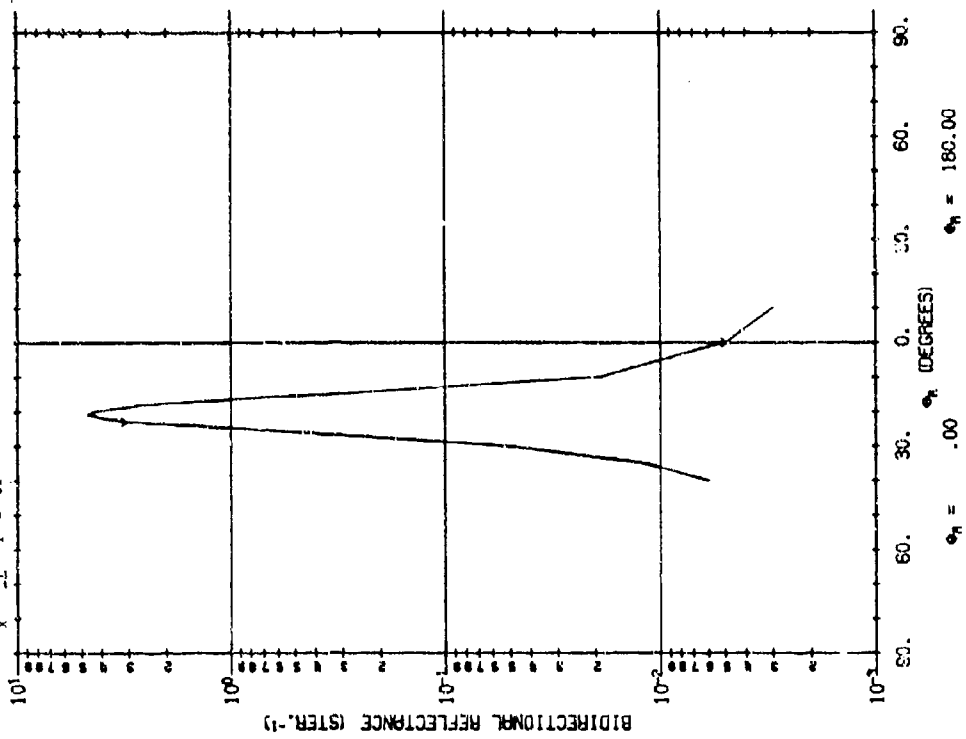
0 //  $\phi_1 = 0.0$   
 + //  $\phi_2 = 180.00$   
 - //  $\lambda = 10.6$   
 x //  $\gamma = 0$



A01569 004

Green Paint on Steel

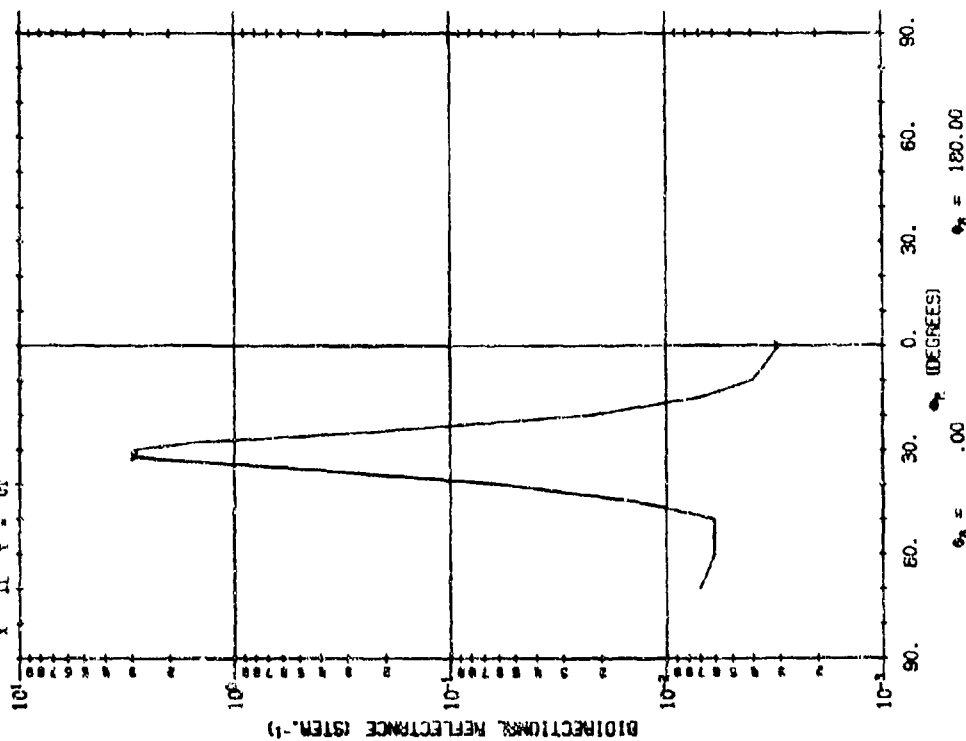
0 //  $\phi_1 = 20.00$   
 + //  $\phi_2 = 180.00$   
 - //  $\lambda = 10.6$   
 x //  $\gamma = 0$



A01569 004

Green Paint on Steel

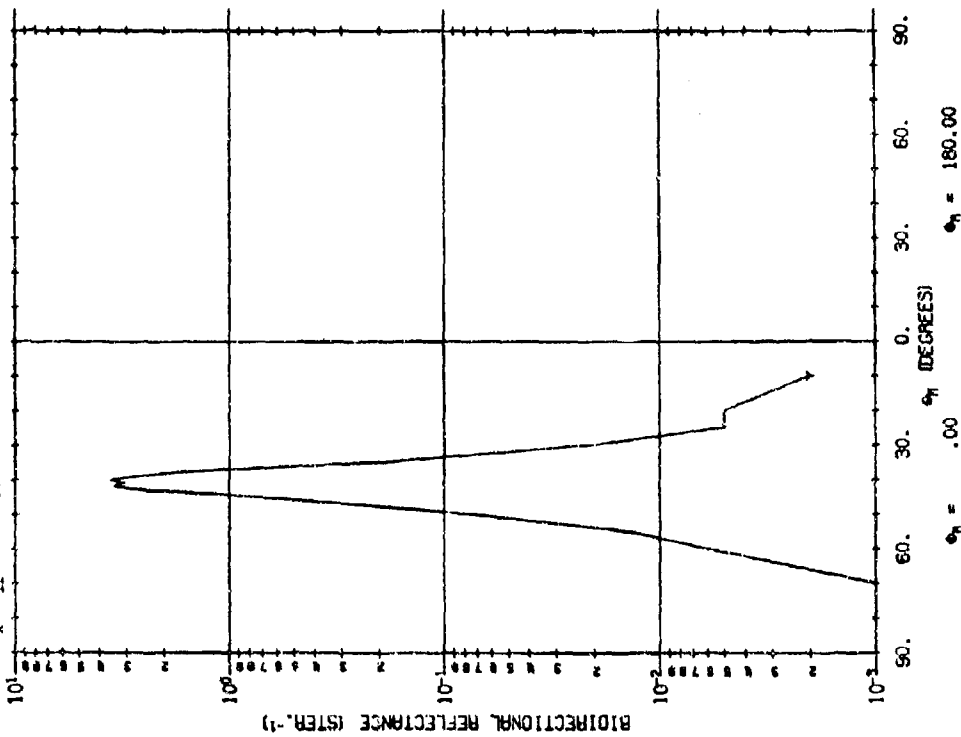
0 ||  $\theta_1 = 30.00$   
 + ||  $\theta_1 = 180.00$   
 x ||  $\lambda = 10.6$   
 x ||  $\gamma = 0^\circ$



A01569 004

Green Paint on Steel

0 ||  $\theta_1 = 40.00$   
 + ||  $\theta_1 = 180.00$   
 x ||  $\lambda = 10.5$   
 x ||  $\gamma = 0^\circ$

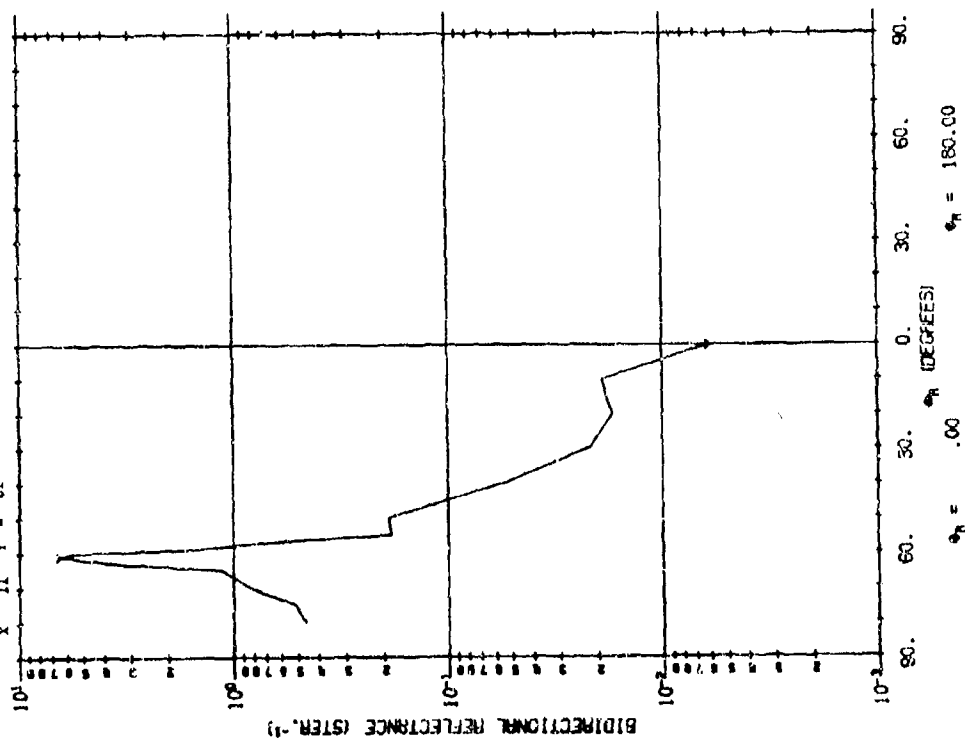


PAINT

R01569 C04

Green Paint on Steel

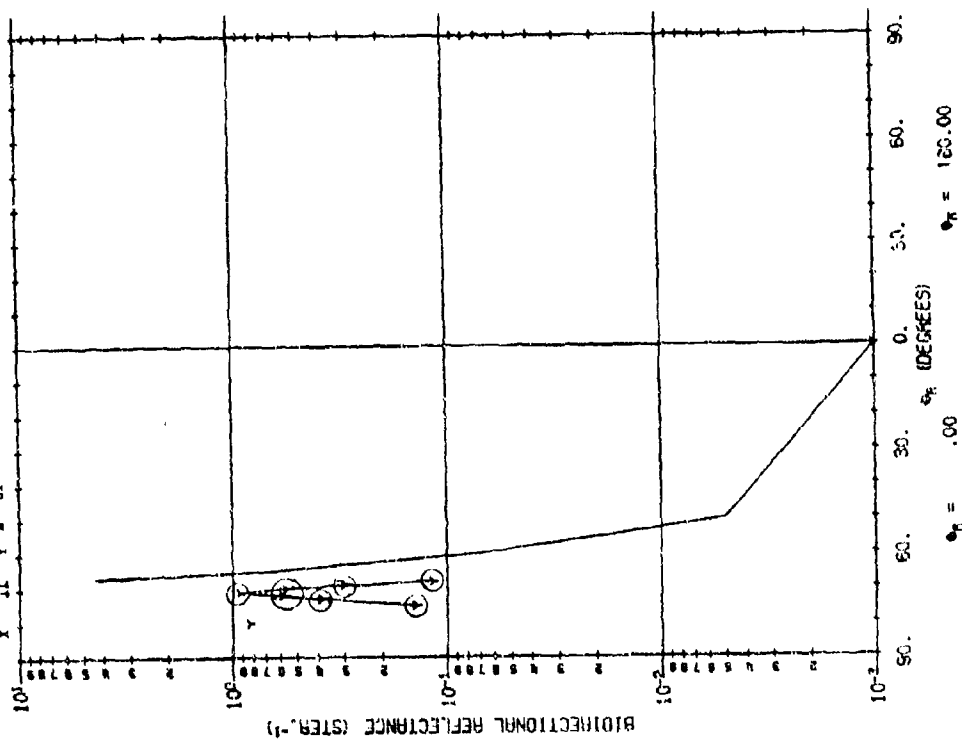
0 //  $\theta_1 = 60.00$   
 + //  $\theta_1 = 180.00$   
 Δ //  $\lambda = 10.6$   
 X //  $\gamma = 0$



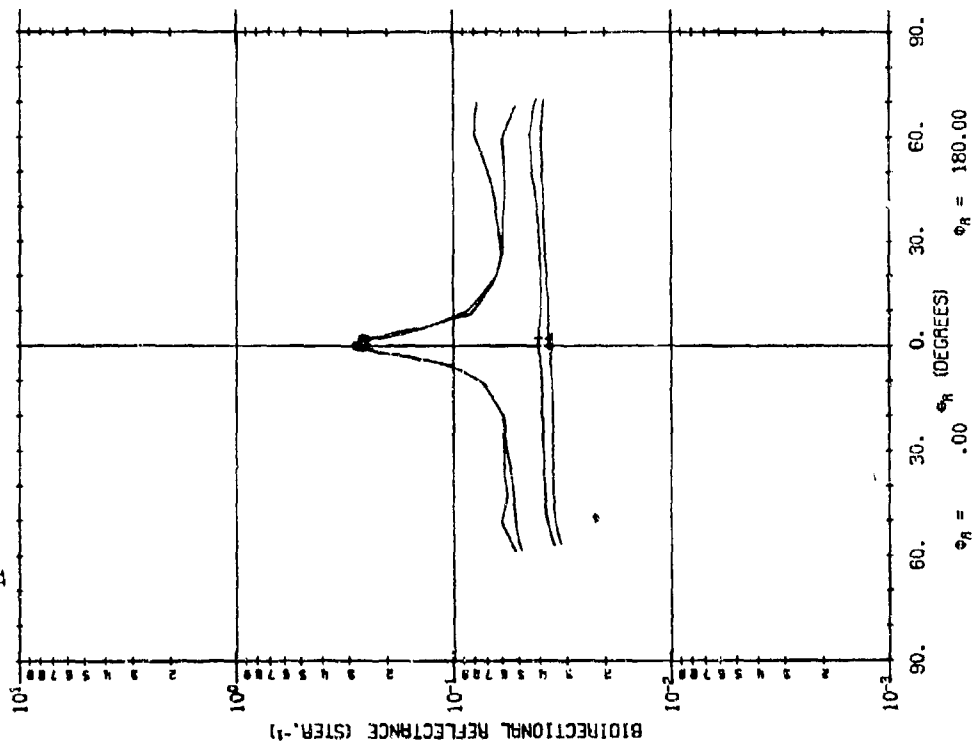
R01569 C04

Green Paint on Steel

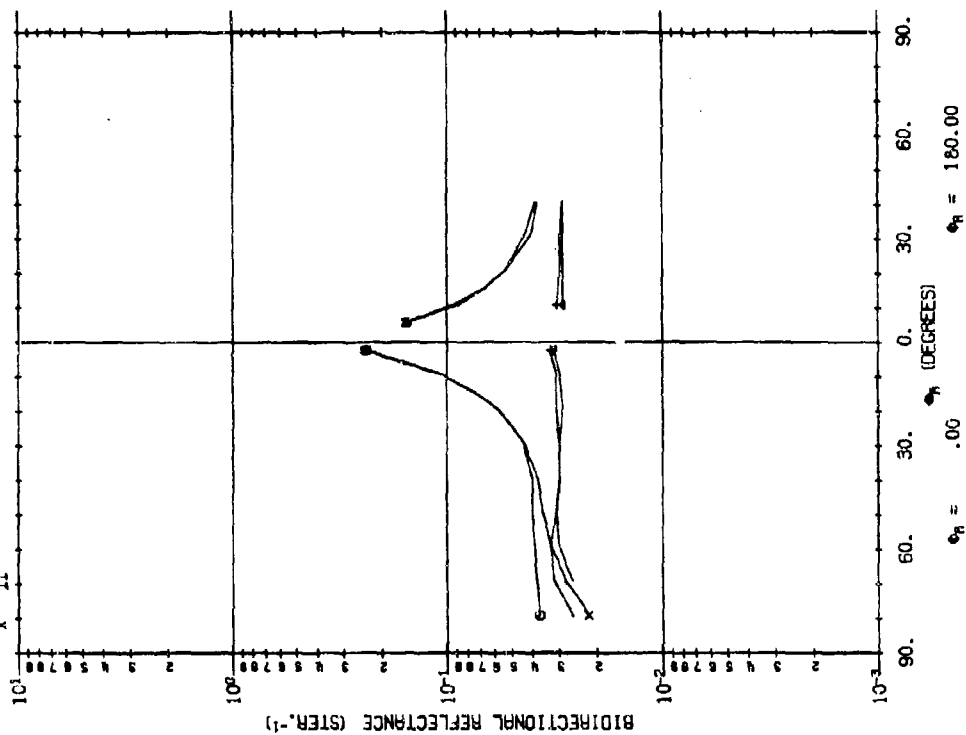
0 //  $\theta_1 = 70.00$   
 + //  $\theta_1 = 180.00$   
 Δ //  $\lambda = 10.6$   
 X //  $\gamma = 0$



R01570 004  
 0 || 22 = 2.0 LIGHT BROWN PAINT ON METAL  
 + ||  $\phi_1 = \phi_2$   
 Δ ||  $\lambda = 0.63$   
 x ||



R01570 004  
 0 ||  $\phi_1 = 0.0$  LIGHT BROWN PAINT ON METAL  
 + ||  $\phi_2 = 180.00$   
 Δ ||  $\lambda = 0.63$   
 x ||

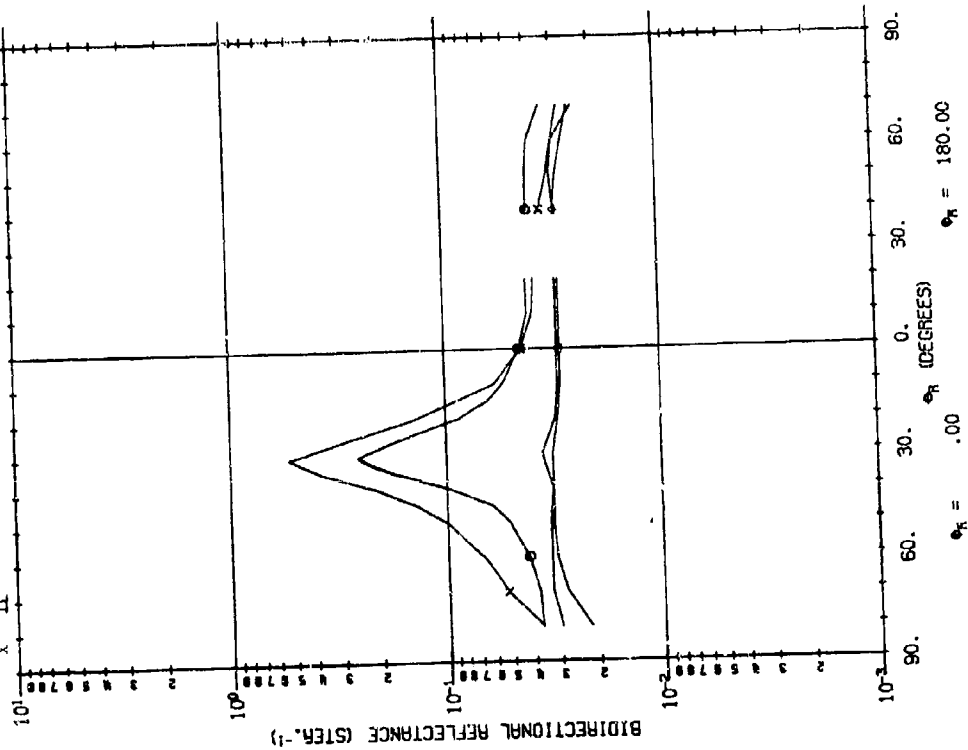


PAINT

A01570 004

Light Brown Paint on Metal

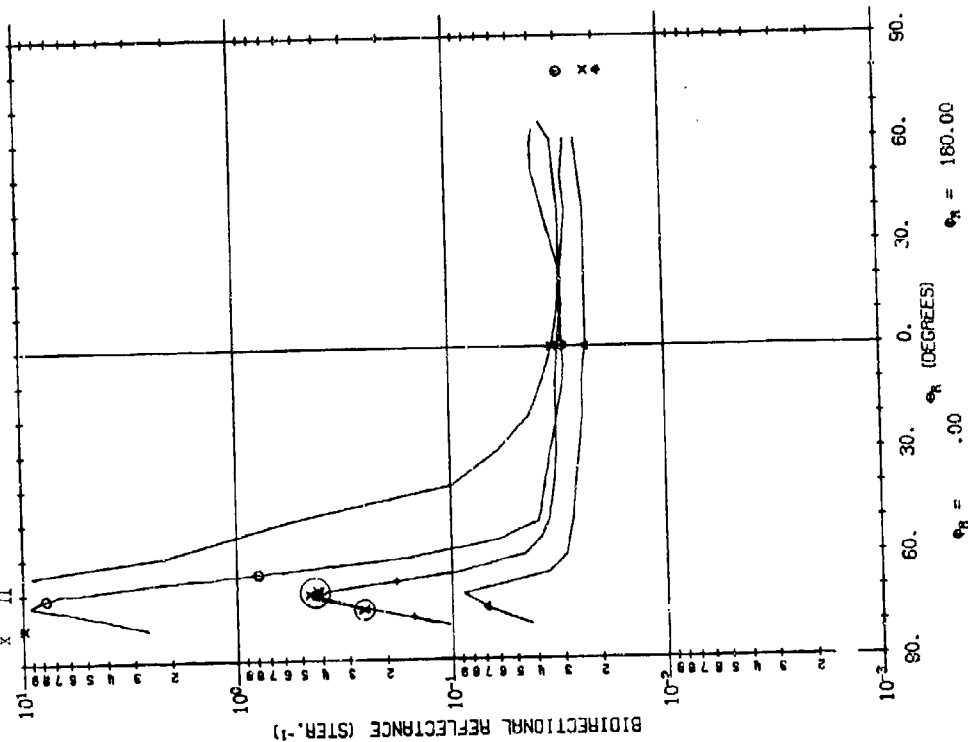
0 ||  $\epsilon_1 = 30.00$   
 + ||  $\epsilon_1 = 180.00$   
 Δ ||  $\lambda = 0.63$   
 x ||



A01570 004

Light Brown Paint on Metal

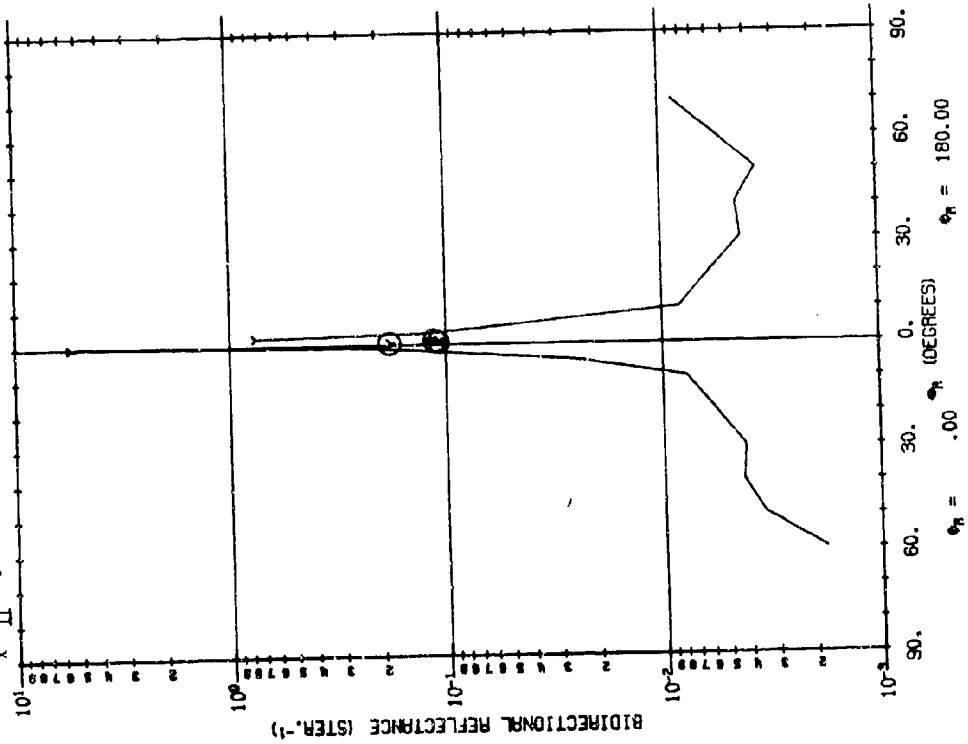
0 ||  $\epsilon_1 = 70.00$   
 + ||  $\epsilon_1 = 180.00$   
 Δ ||  $\lambda = 0.63$   
 x ||



R01570 003

LIGHT BROWN PAINT ON METAL

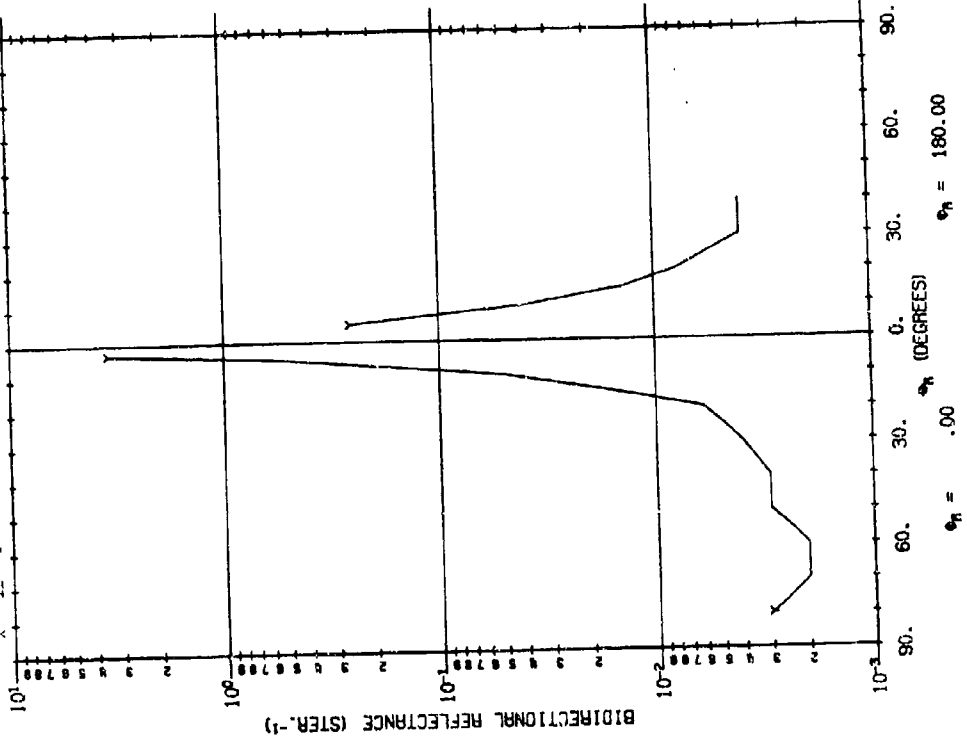
0 || 23 = 1.1  
+ ||  $\phi_1 = \phi_r$   
Δ ||  $\lambda = 10.6$   
X || Y = UT



R01570 003

Light Brown Paint on Metal

0 ||  $\phi_1 = 0.0$   
+ ||  $\phi_1 = 180.00$   
Δ ||  $\lambda = 10.6$   
X || Y = UT

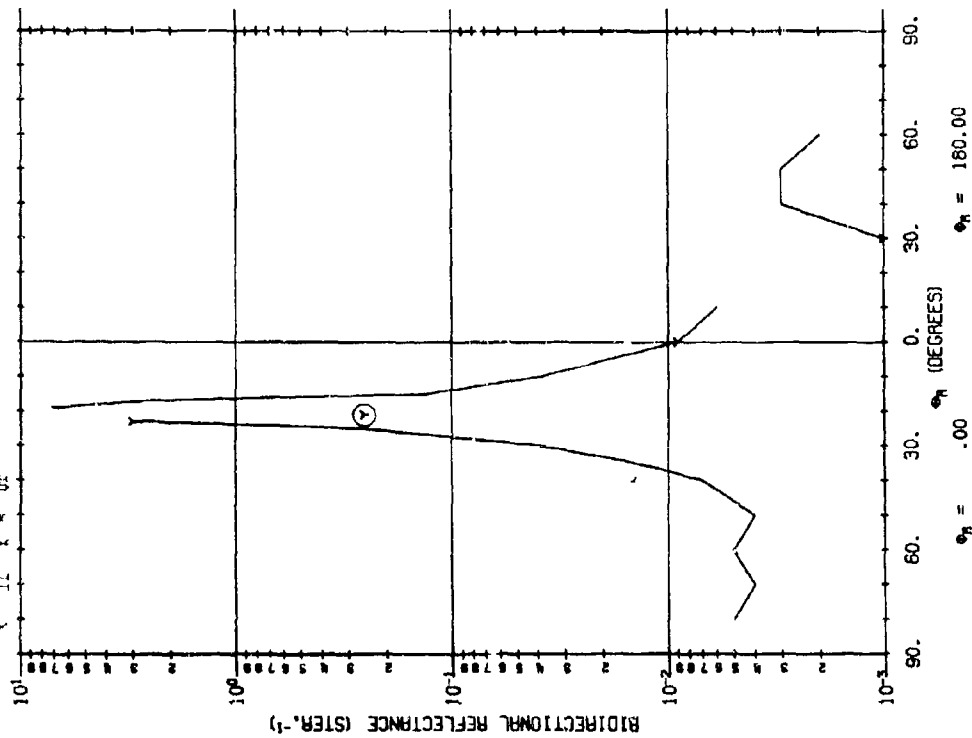


PAINT

R01570 003

Light Brown Paint on Metal

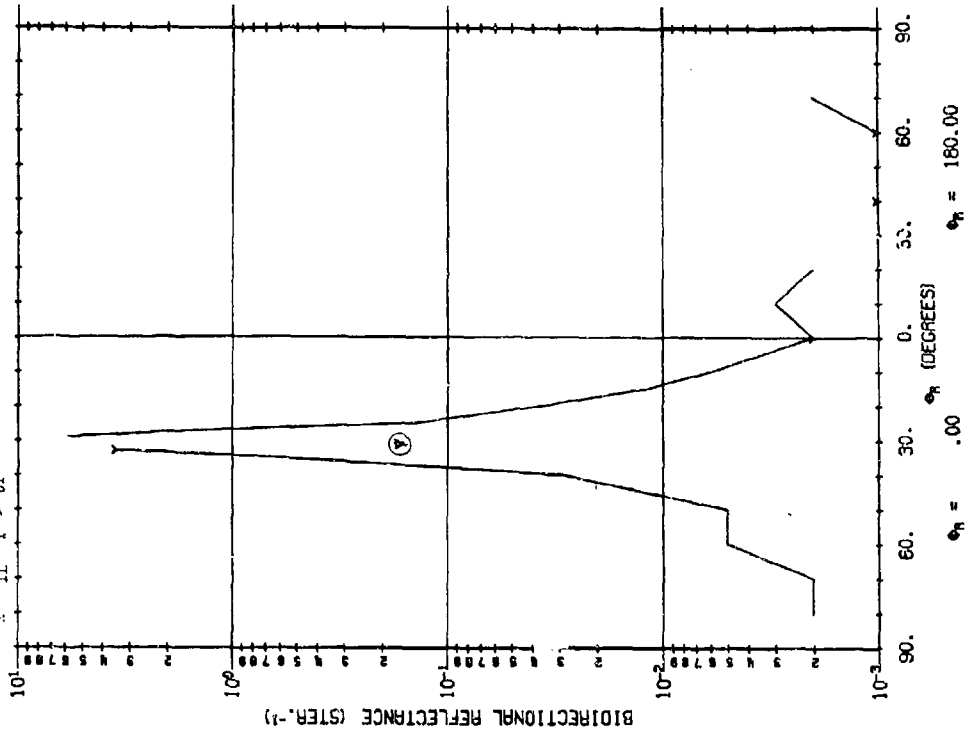
0 ||  $\theta_1 = 20.00$   
 + ||  $\phi_1 = 180.00$   
 2 ||  $\lambda = 10.6$   
 Y || X = UT



R01570 003

Light Brown Paint on Metal

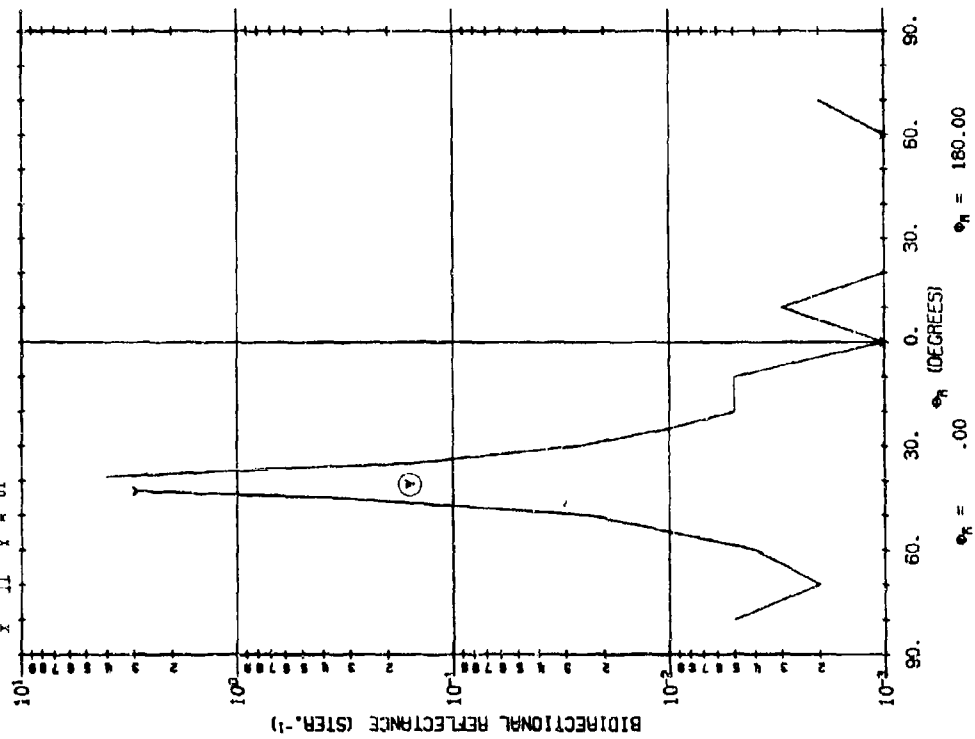
0 ||  $\theta_1 = 30.00$   
 + ||  $\phi_1 = 180.00$   
 2 ||  $\lambda = 10.6$   
 Y || X = UT



A01570 003

Light Brown Paint on Metal

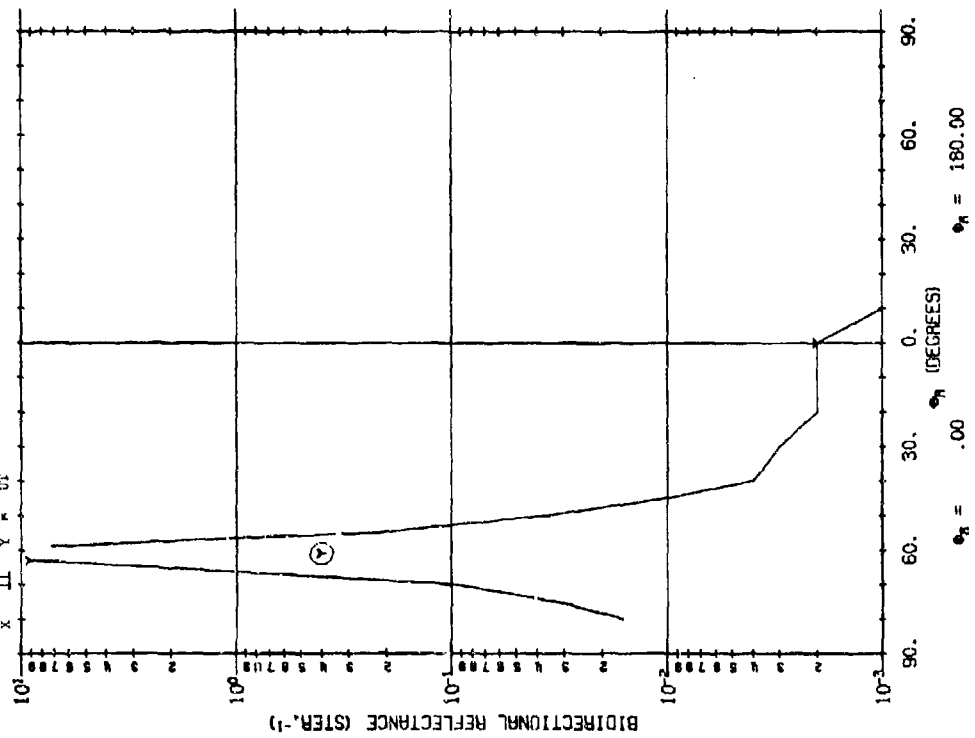
0 ||  $\theta_1 = 40.00$   
 + ||  $\theta_2 = 180.00$   
 Δ ||  $\lambda = 10.6$   
 X || Y R UT



A01570 003

Light Brown Paint on Metal

0 ||  $\theta_1 = 60.00$   
 + ||  $\theta_2 = 180.00$   
 Δ ||  $\lambda = 10.6$   
 X || Y R UT



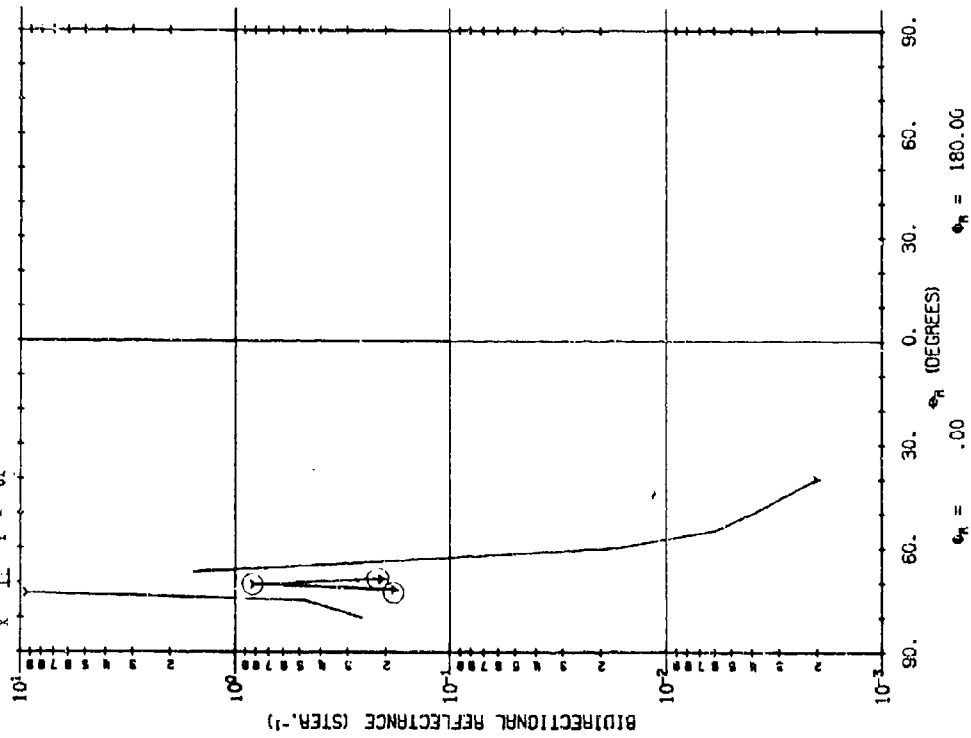
PAINT



A01570 003

Light Brown Paint on Metal

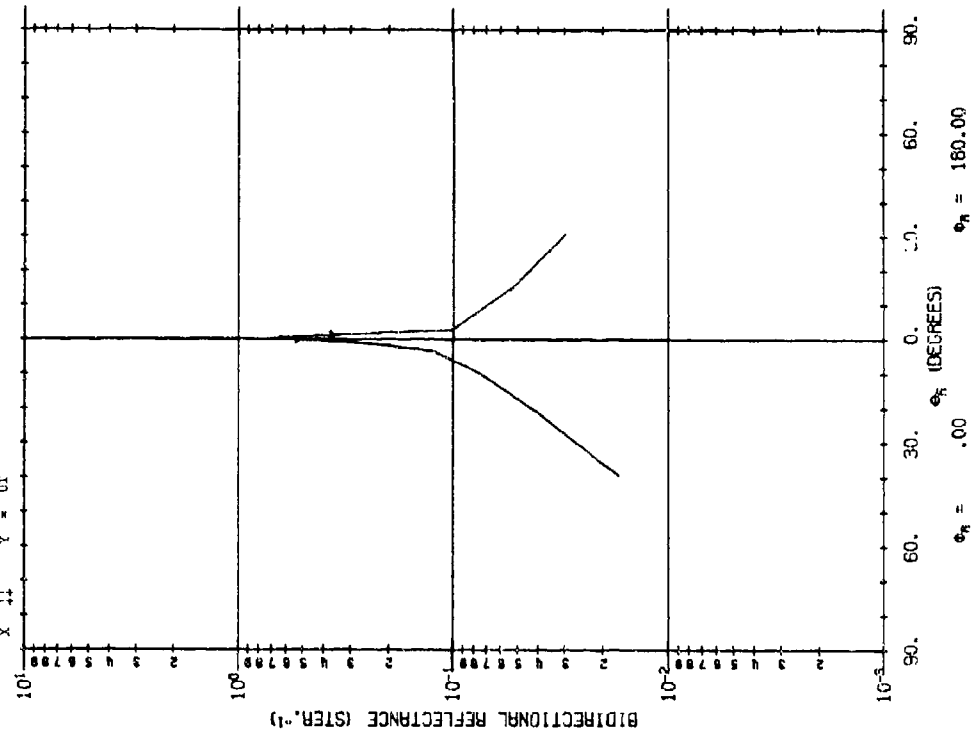
$\theta_i = 70.00$   
 $\phi_i = 180.00$   
 $\lambda = 10.6$   
 $\gamma = \text{UT}$



A01586 001

Blue Metallic Paint on Steel

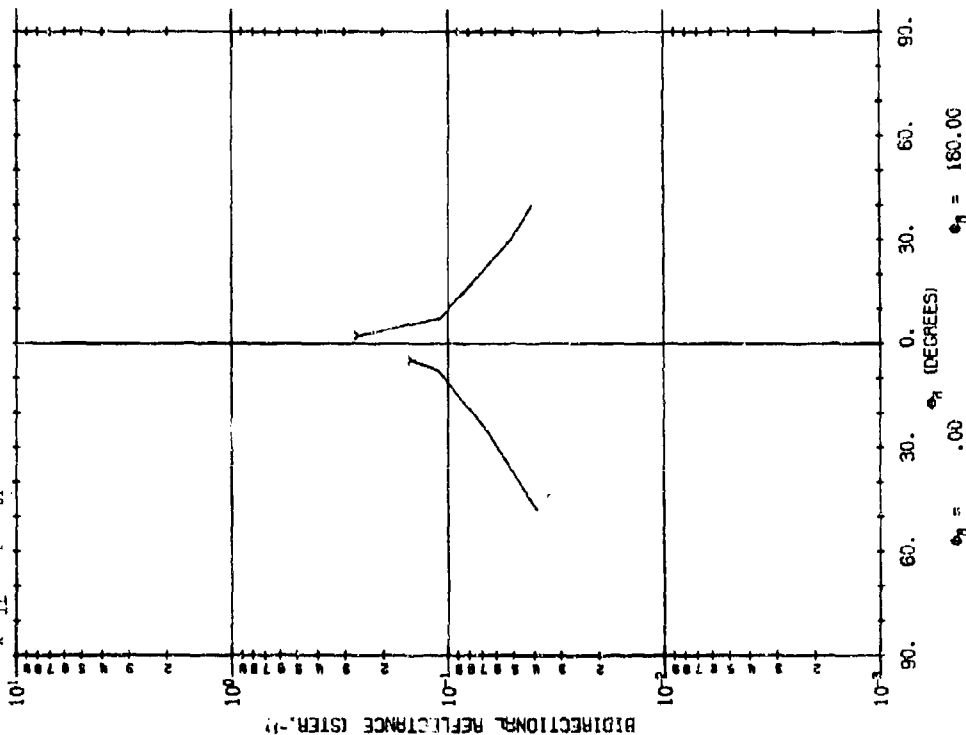
$\theta_i = 1.10$   
 $\phi_i = \phi_r$   
 $\lambda = 10.6$   
 $\gamma = \text{UT}$



R01586 001

Blue Metallic Paint on Steel

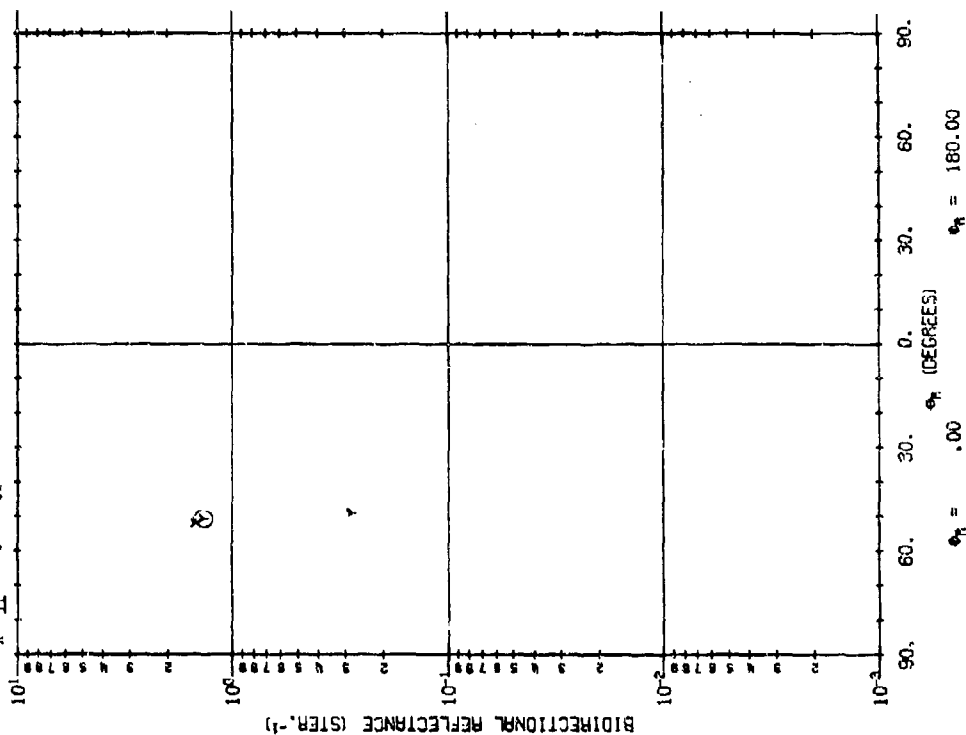
$\phi_1 = 0.0$   
 $\phi_2 = 180.0$   
 $\lambda = 10.6$   
 $\chi = 0.0$



R01586 001

Blue Metallic Paint on Steel

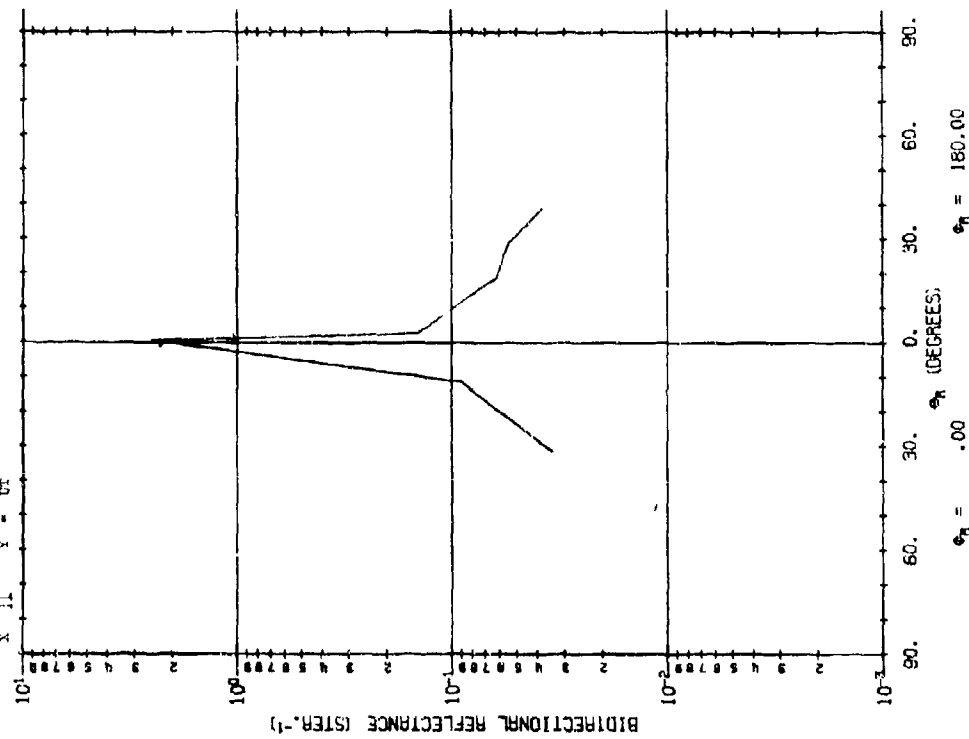
$\phi_1 = 50.0$   
 $\phi_2 = 180.0$   
 $\lambda = 10.6$   
 $\chi = 0.0$



PAINT

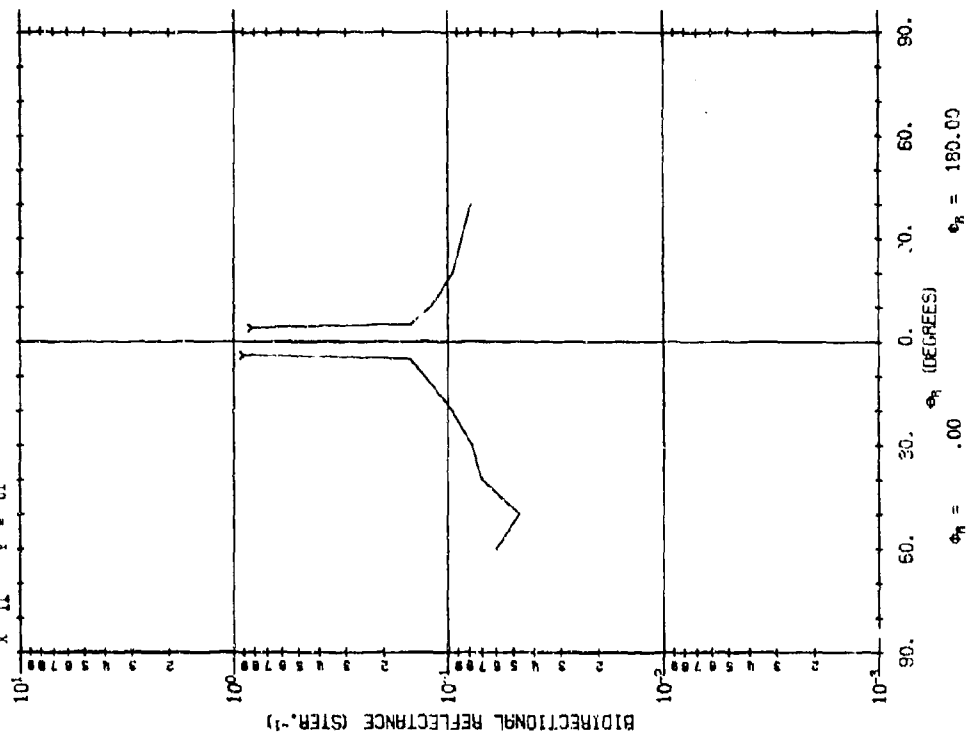
R01587 001  
 0 11 23 = 1.10  
 + 11  $\theta_1 = 0^\circ$   
 - 11  $\phi_1 = 180.0$   
 X 11  $\lambda = 10.6$   
 Y = UT

Green Metallic Paint on Steel



R01587 001  
 0 11  $\theta_1 = 0.0$   
 + 11  $\phi_1 = 180.0$   
 - 11  $\lambda = 10.6$   
 X 11 Y = UT

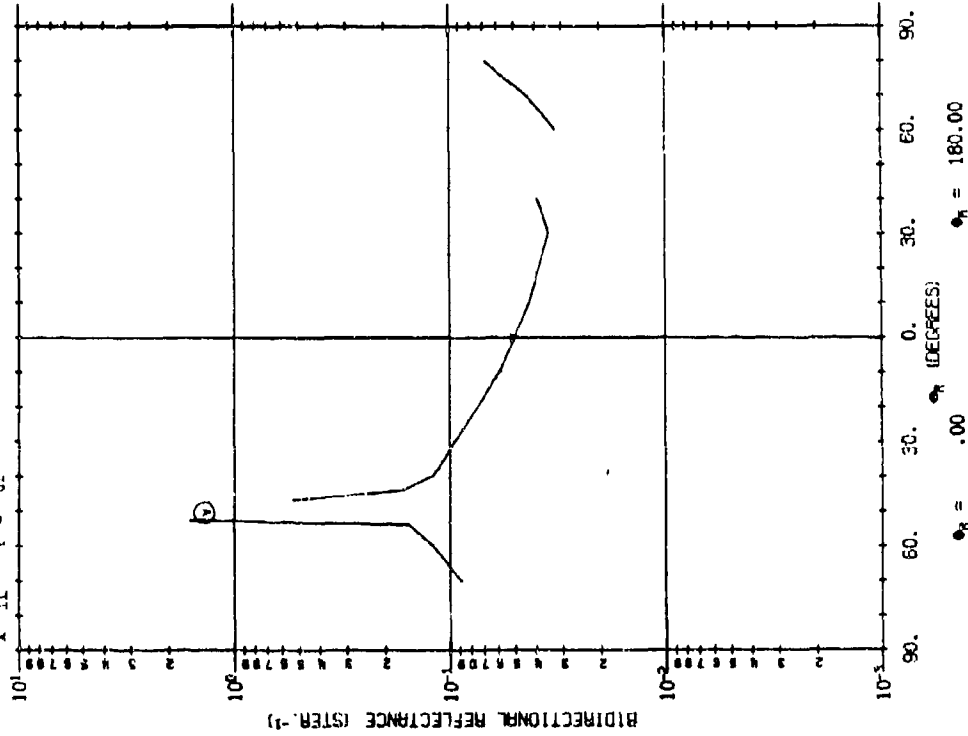
Green Metallic Paint on Steel



A01587 001

Green Metallic Paint on Steel

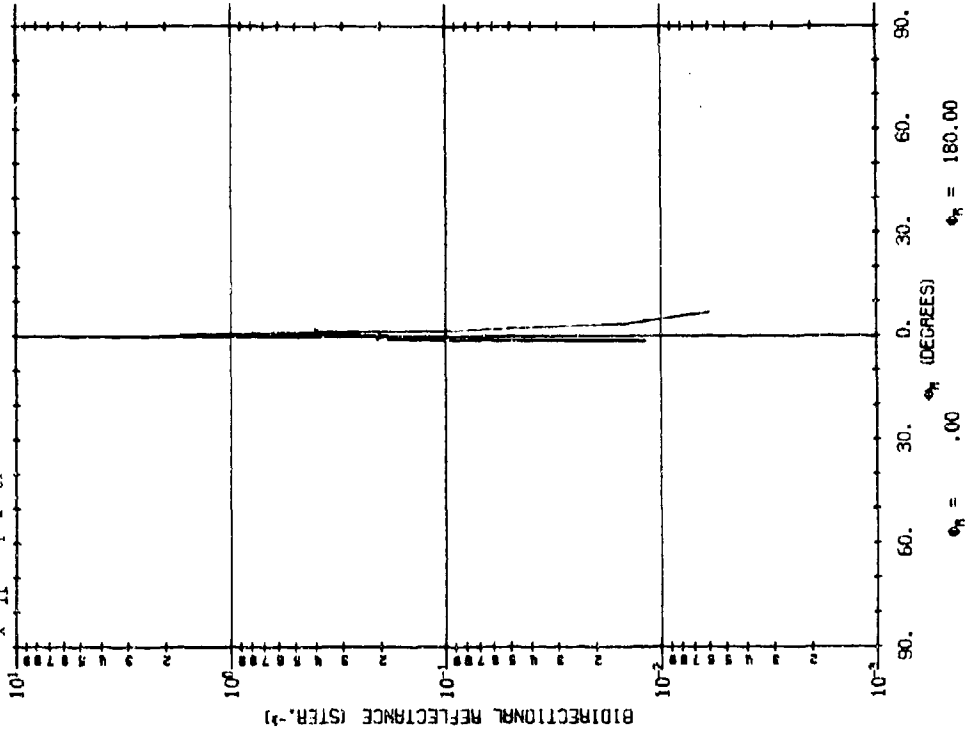
0 ||  $\theta_i = 50.0$   
 + ||  $\theta_r = 180.0$   
 Δ ||  $\lambda = 10.6$   
 X || Y = UT



A01588 001

Red Paint on Steel

0 ||  $2\lambda = 1.10$   
 + ||  $\theta_i = \theta_r$   
 Δ ||  $\lambda = 10.6$   
 X || Y = UT

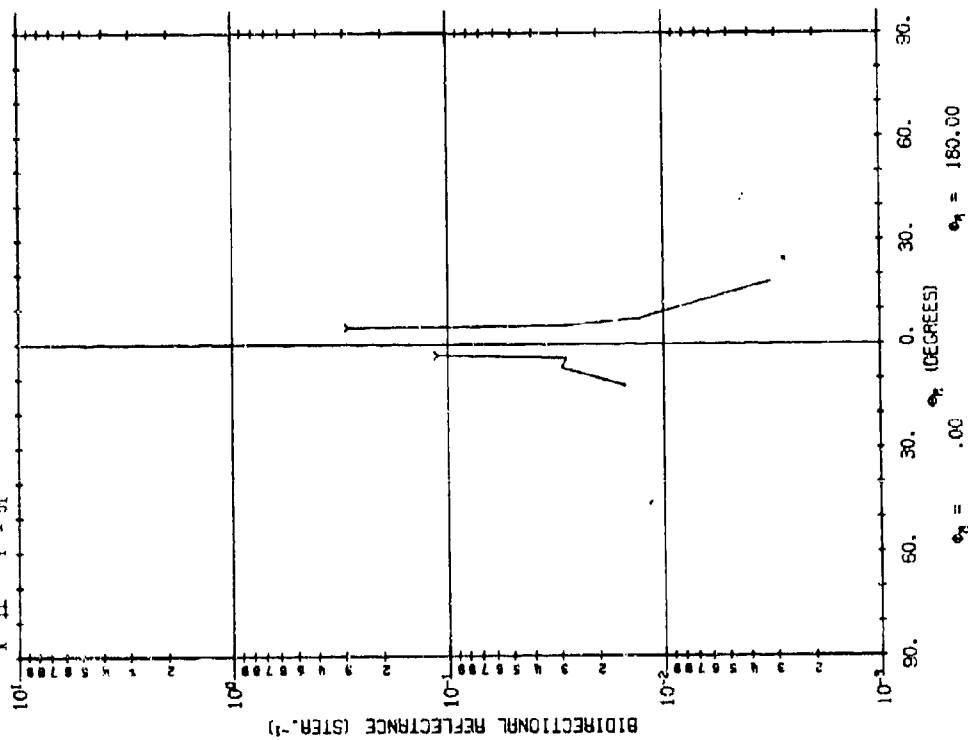


PAINT

A01588 001

Red Paint on Steel

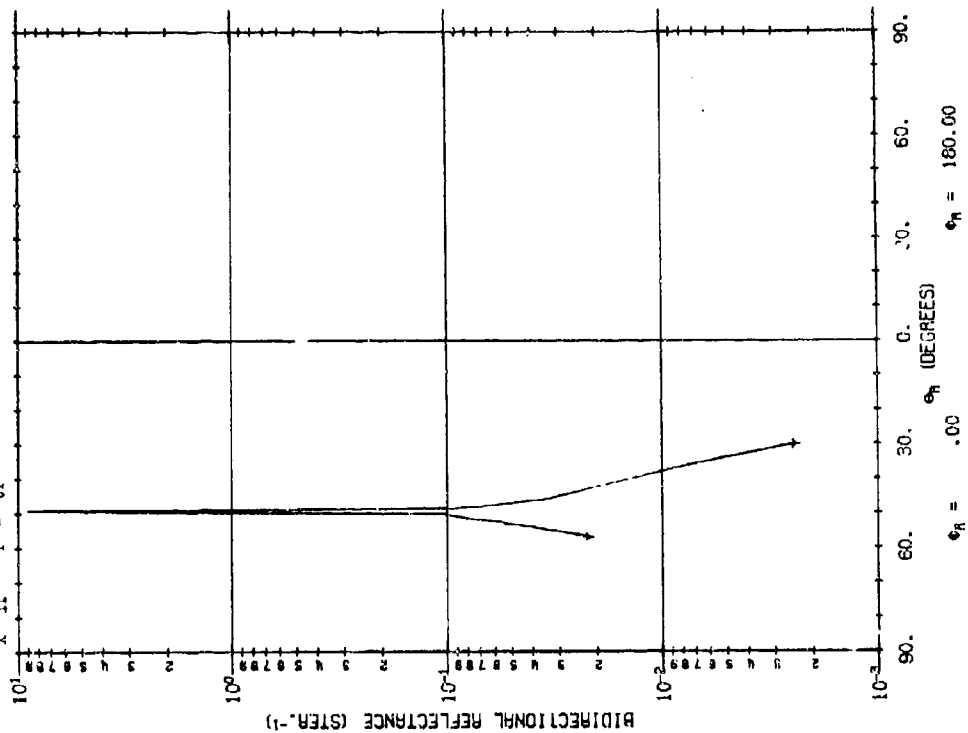
$\phi_i = 0.0$   
 $\phi_1 = 180.0$   
 $\lambda = 10.6$   
 $Y = UT$



A01588 001

Red Paint on Steel

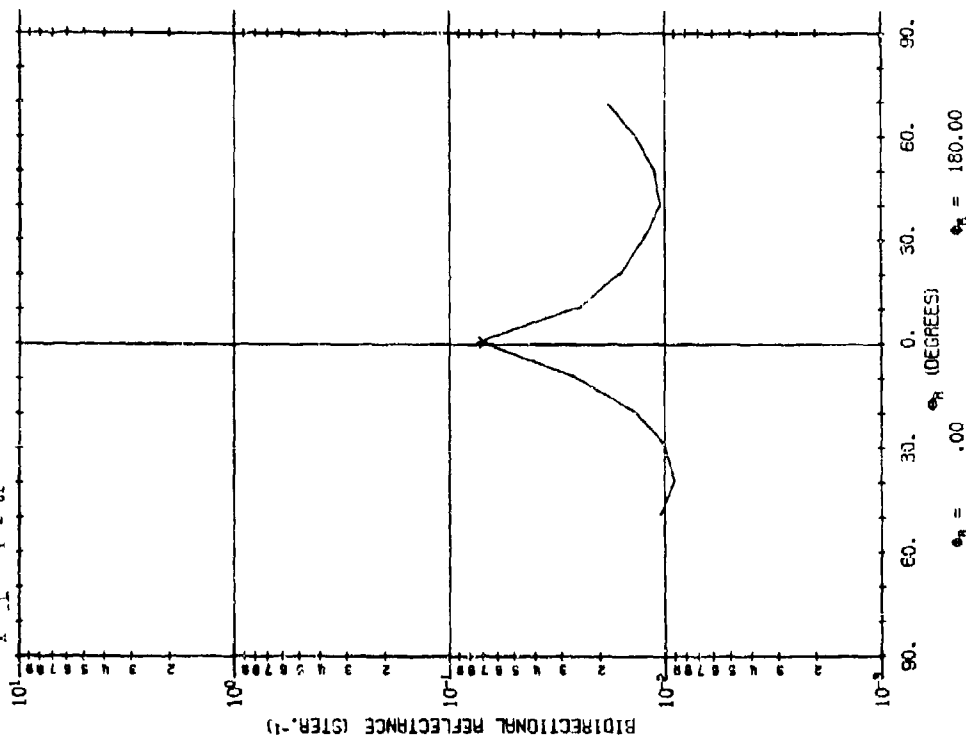
$\phi_i = 50.0$   
 $\phi_1 = 180.0$   
 $\lambda = 10.6$   
 $Y = VT$



R01589 001

White Paint on Plywood

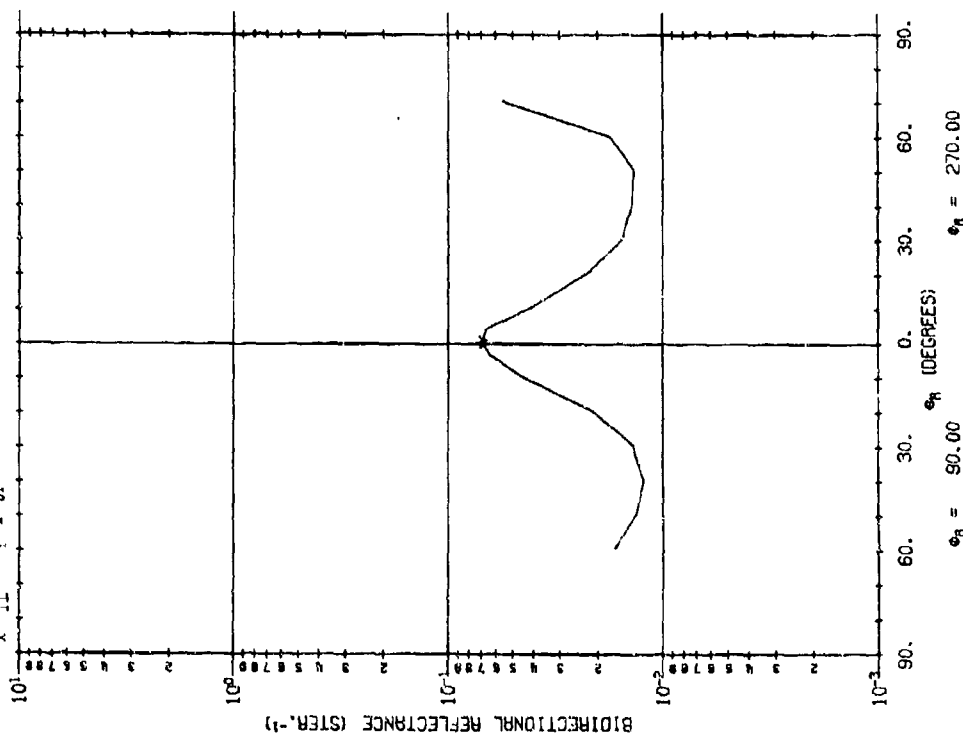
0 // 2 $\theta$  = 1.10  
 + //  $\theta_i$  =  $\theta_r$   
 - //  $\lambda$  = 10.6  
 X //  $\gamma$  = UT



R01589 001

White Paint on Plywood

0 // 2 $\theta$  = 1.10  
 + //  $\theta_i$  =  $\theta_r$   
 - //  $\lambda$  = 10.6  
 X //  $\gamma$  = UT

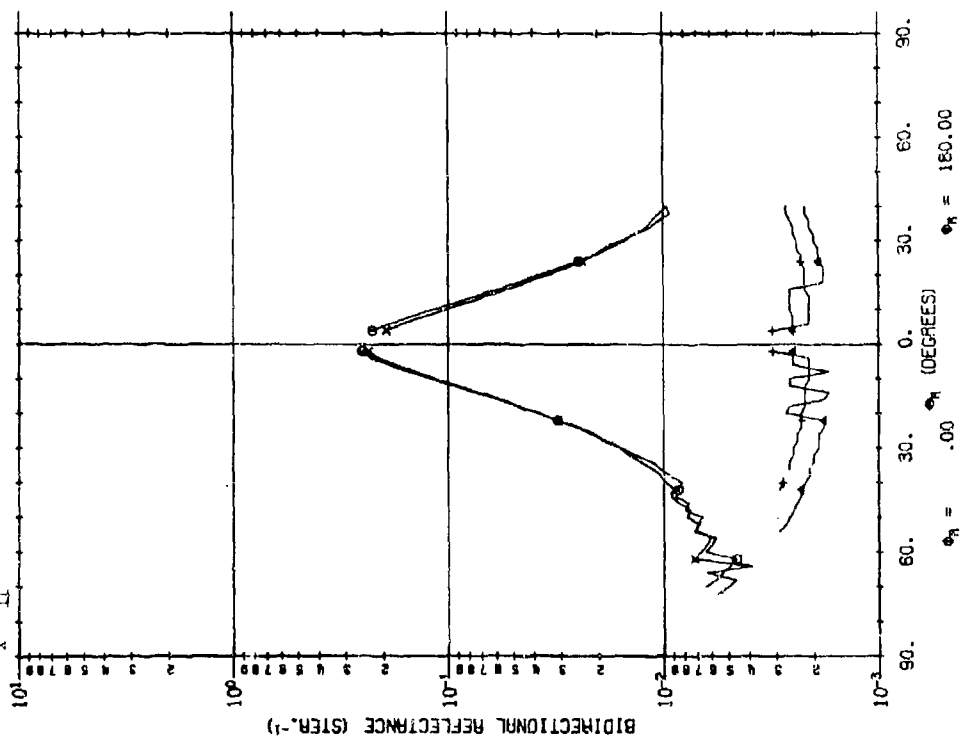


PAINT

R01608 201

OLIVE DRAB PAINT ON STEEL

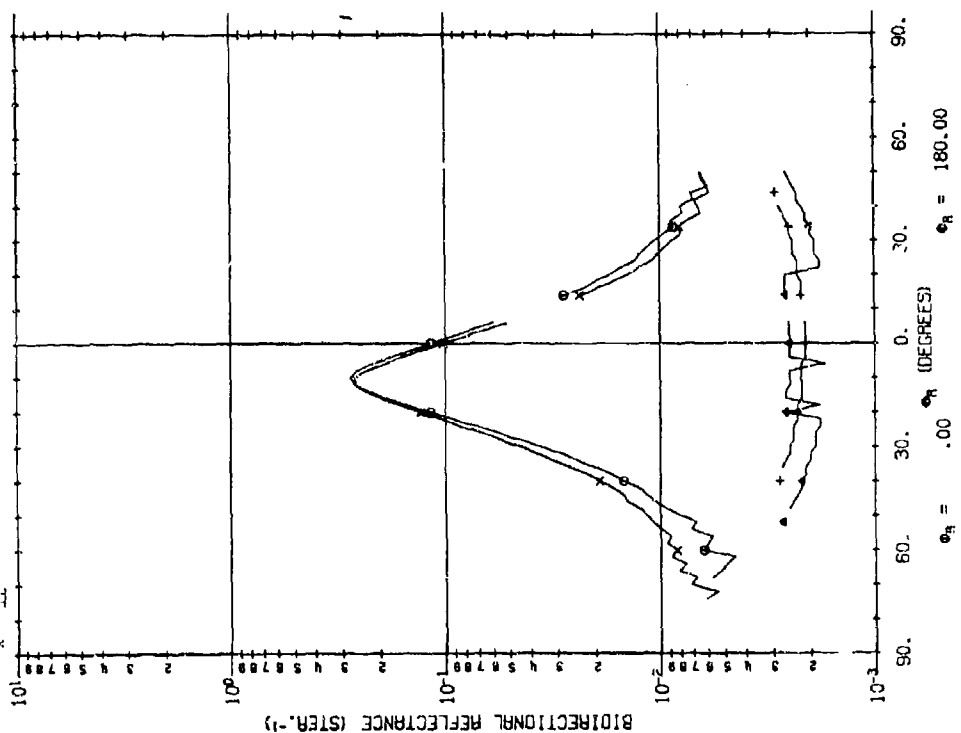
0  $\theta_i = 0.0$   
 +  $\theta_i = 180.0$   
 x  $\theta_i = 0.63$



R01608 201

OLIVE DRAB PAINT ON STEEL

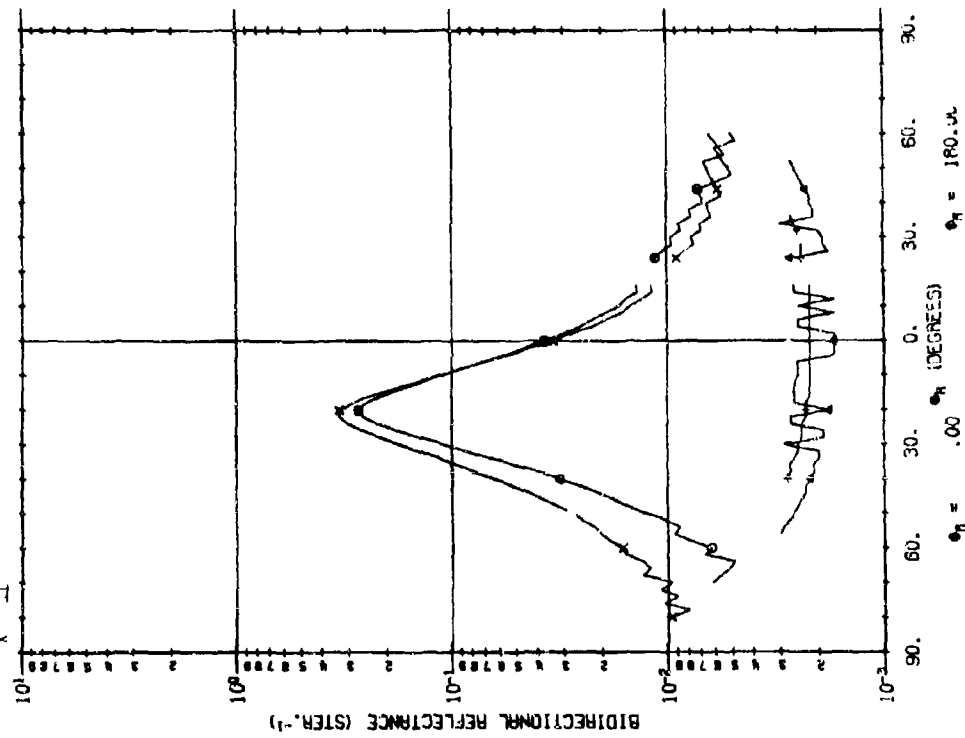
0  $\theta_i = 10.0$   
 +  $\theta_i = 180.0$   
 x  $\theta_i = 0.63$



R01608 201

OLIVE DRAB PAINT ON STEEL

0  $\theta_1 = 20.0$   
 +  $\theta_1 = 180.0$   
 x  $\lambda = 0.63$

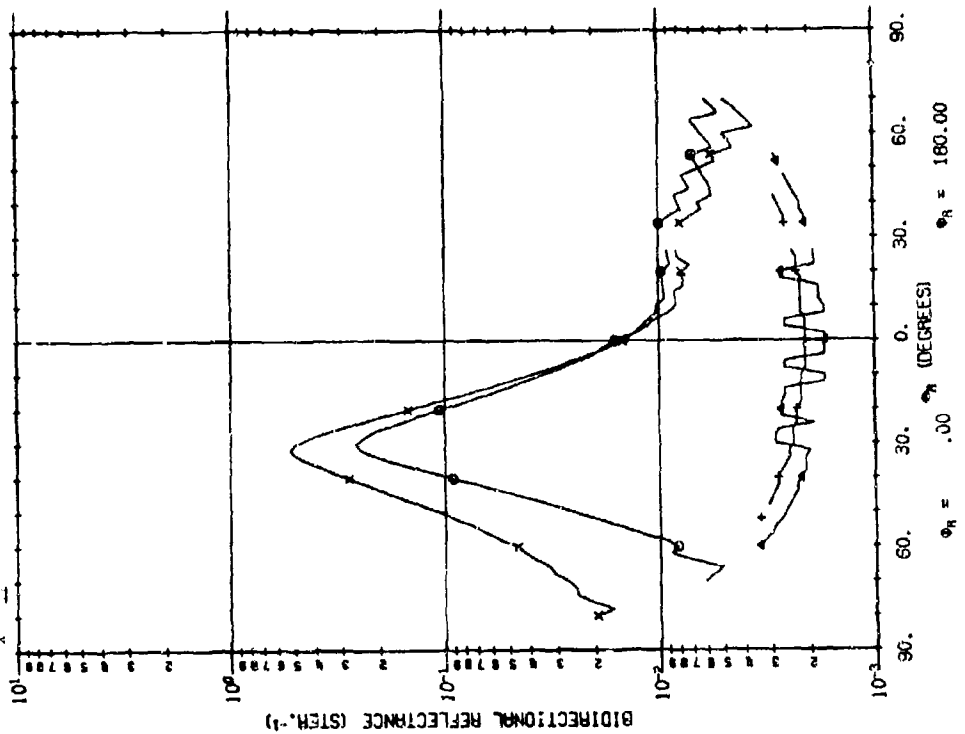


101

R01608 201

OLIVE DRAB PAINT ON STEEL

0  $\theta_1 = 30.0$   
 +  $\theta_1 = 180.0$   
 x  $\lambda = 0.63$



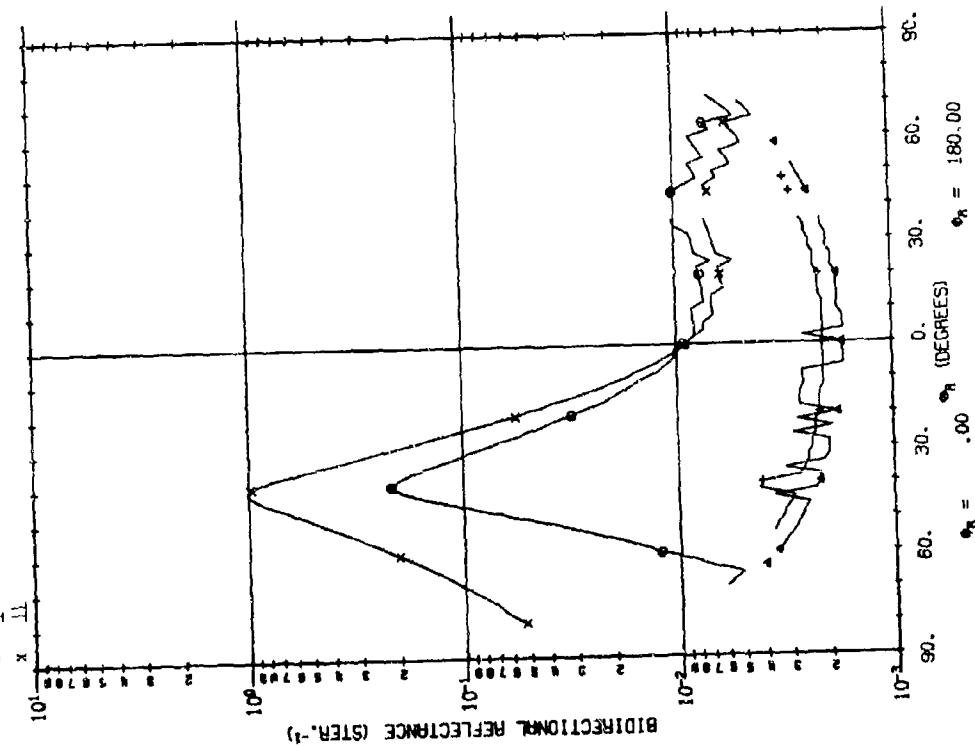
PAINT



OLIVE DRAB PAINT ON STEEL

R01608 201

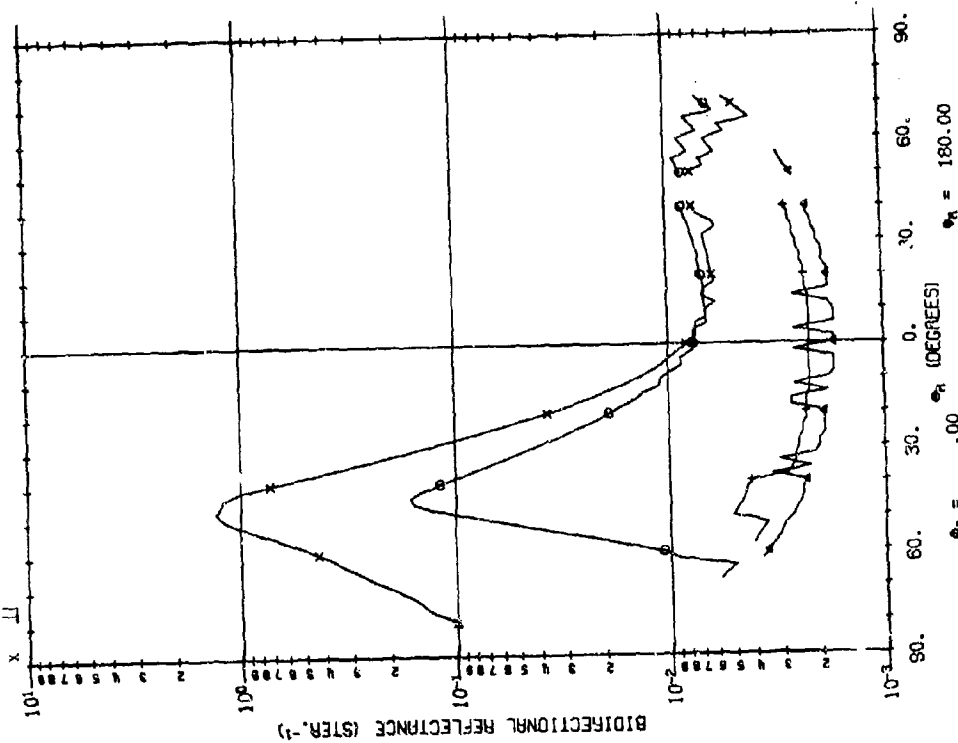
0 ||  $\theta_1 = 45.0$   
 + ||  $\phi_1 = 180.0$   
 Δ ||  $\lambda = 0.63$



OLIVE DRAB PAINT ON STEEL

R01608 201

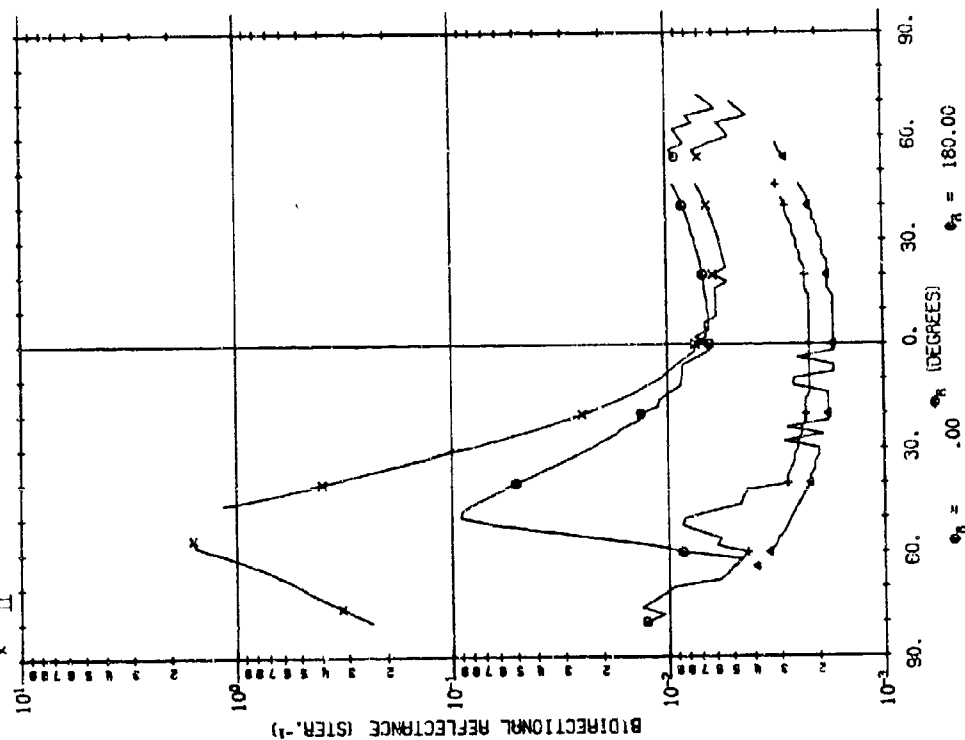
0 ||  $\theta_1 = 45.0$   
 + ||  $\phi_1 = 180.0$   
 Δ ||  $\lambda = 0.63$



A01608 201

OLIVE DRAB PAINT ON STEEL

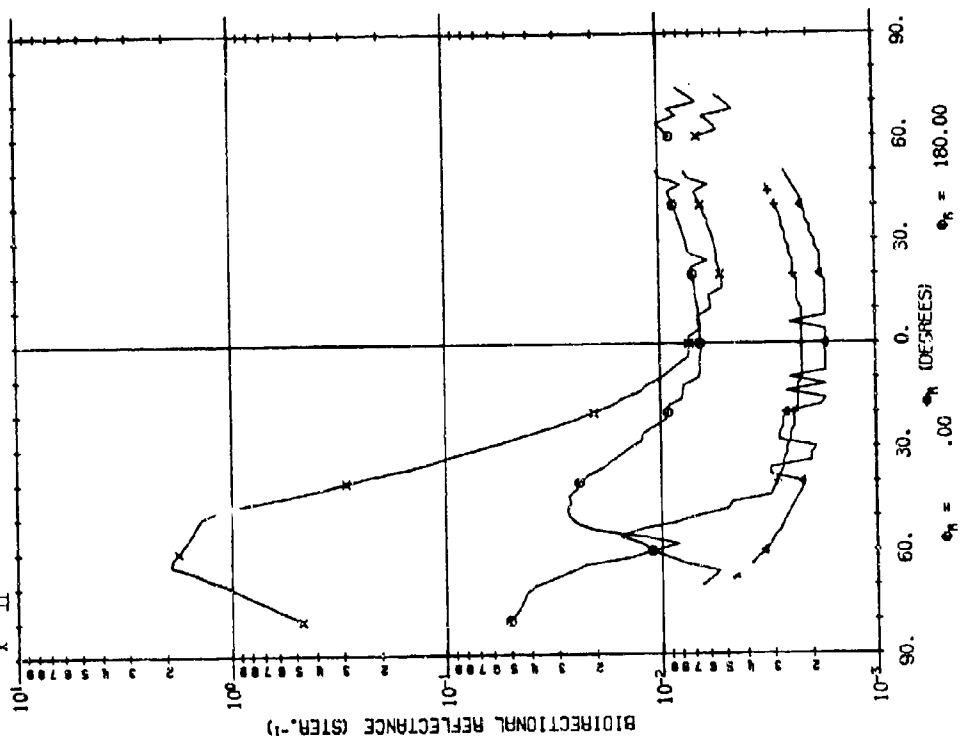
0 ||  $\theta_1 = 50.0$   
 + ||  $\phi_1 = 180.0$   
 Δ ||  $\lambda = 0.63$   
 x ||



A01608 201

OLIVE DRAB PAINT ON STEEL

0 ||  $\theta_1 = 55.0$   
 + ||  $\phi_1 = 180.0$   
 Δ ||  $\lambda = 0.63$   
 x ||

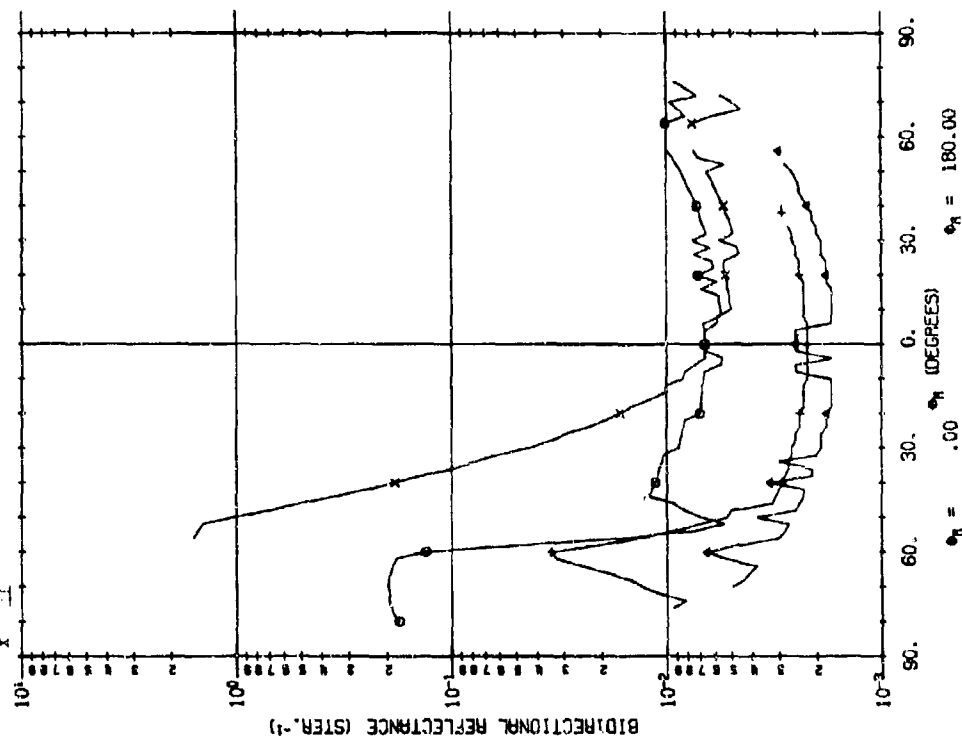


PAINT

R01608 201

OLIVE DRAB PAINT ON STEEL

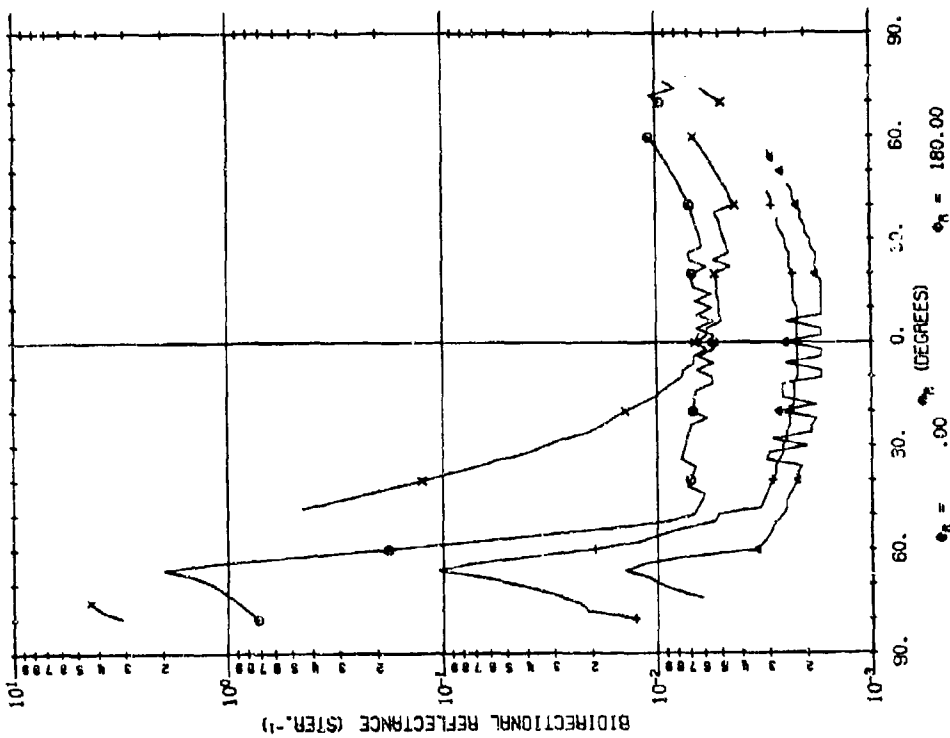
0 ||  $\phi_1 = 65.0$   
 + ||  $\phi_2 = 180.0$   
 Δ ||  $\phi_3 = 0.63$   
 x ||



R01608 201

OLIVE DRAB PAINT ON STEEL

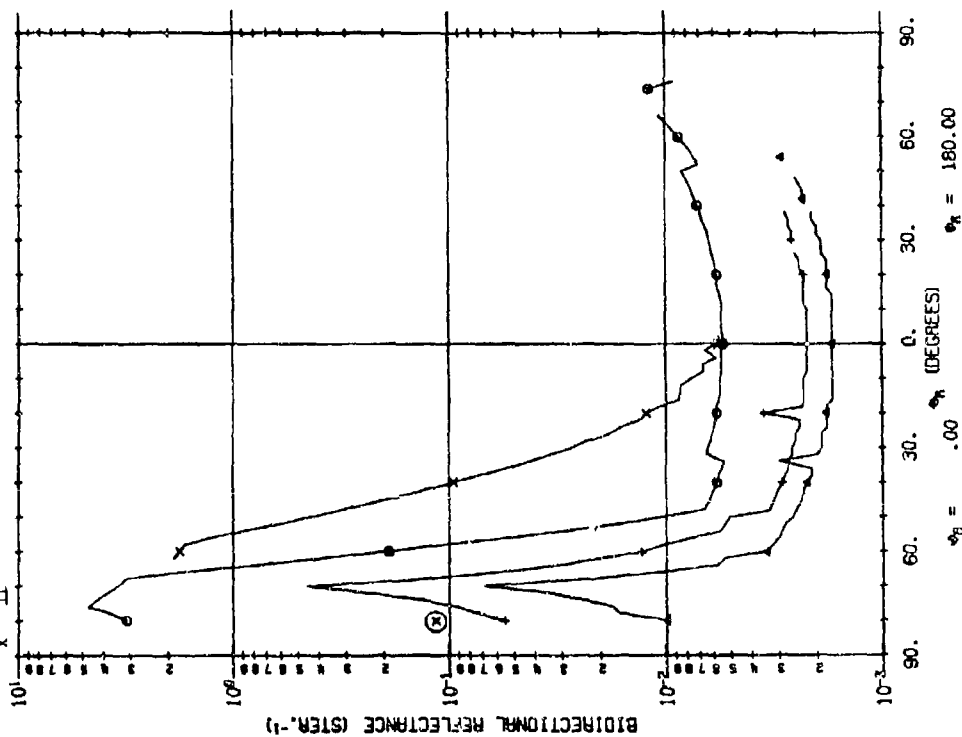
0 ||  $\phi_1 = 65.0$   
 + ||  $\phi_2 = 180.0$   
 Δ ||  $\phi_3 = 0.63$   
 x ||



A01608 201

OLIVE DRAB PAINT ON STEEL

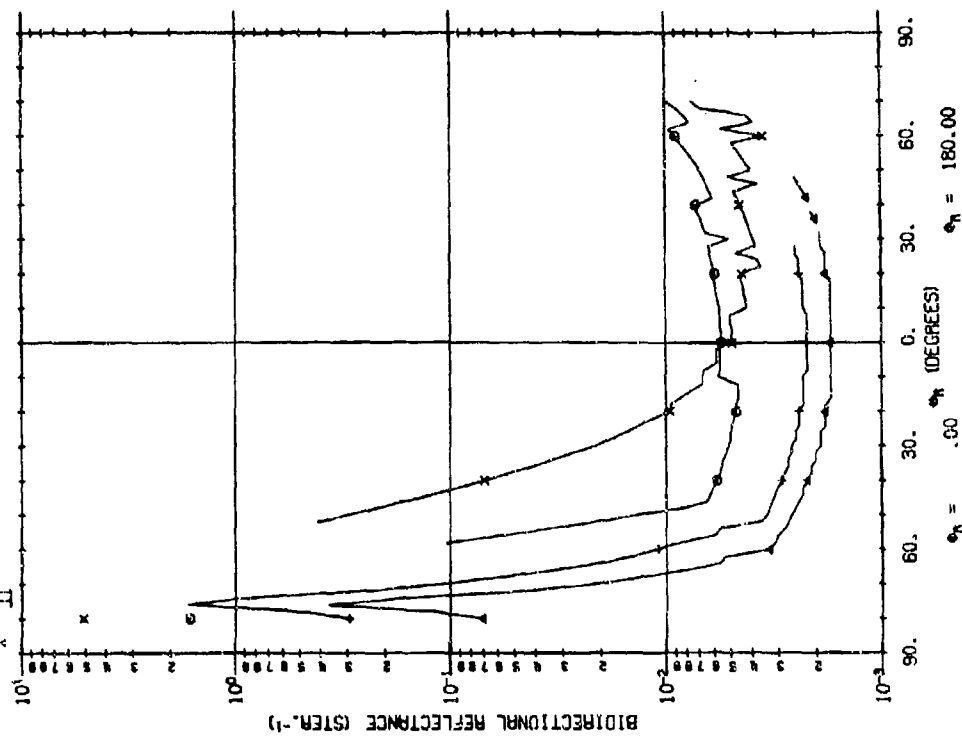
0 //  $\phi_1 = 70.0$   
 + //  $\phi_1 = 180.0$   
 x //  $\lambda = 0.63$   
 //



A01608 201

OLIVE DRAB PAINT ON STEEL

0 //  $\phi_1 = 75.0$   
 + //  $\phi_1 = 180.0$   
 x //  $\lambda = 0.63$   
 //

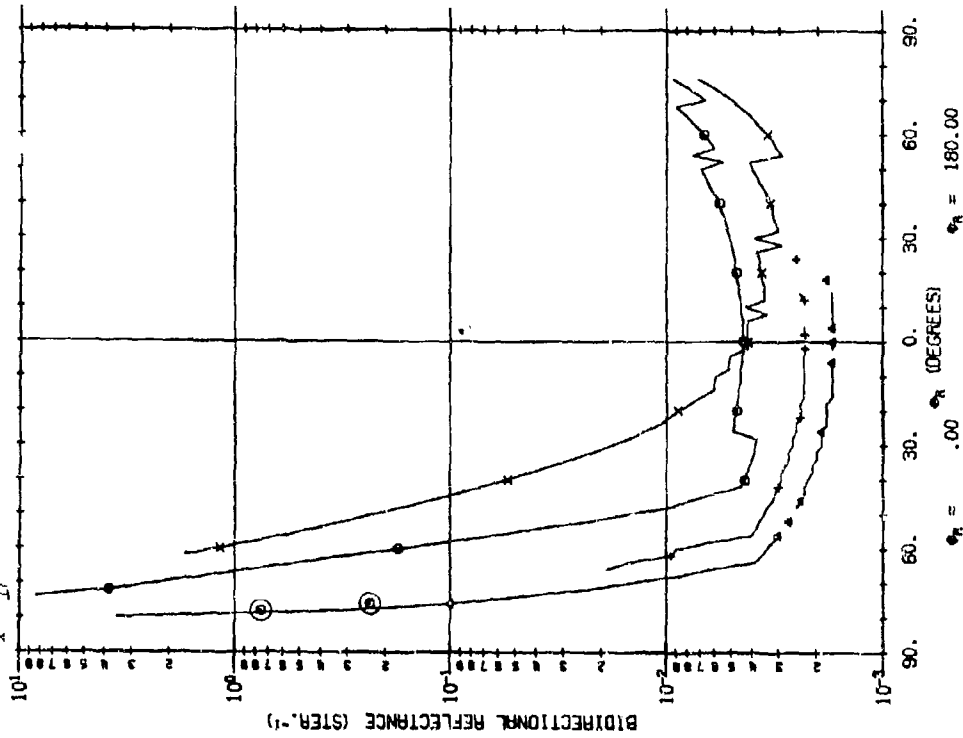


PAINT

A01608 201

OLIVE DRAB PAINT ON STEEL

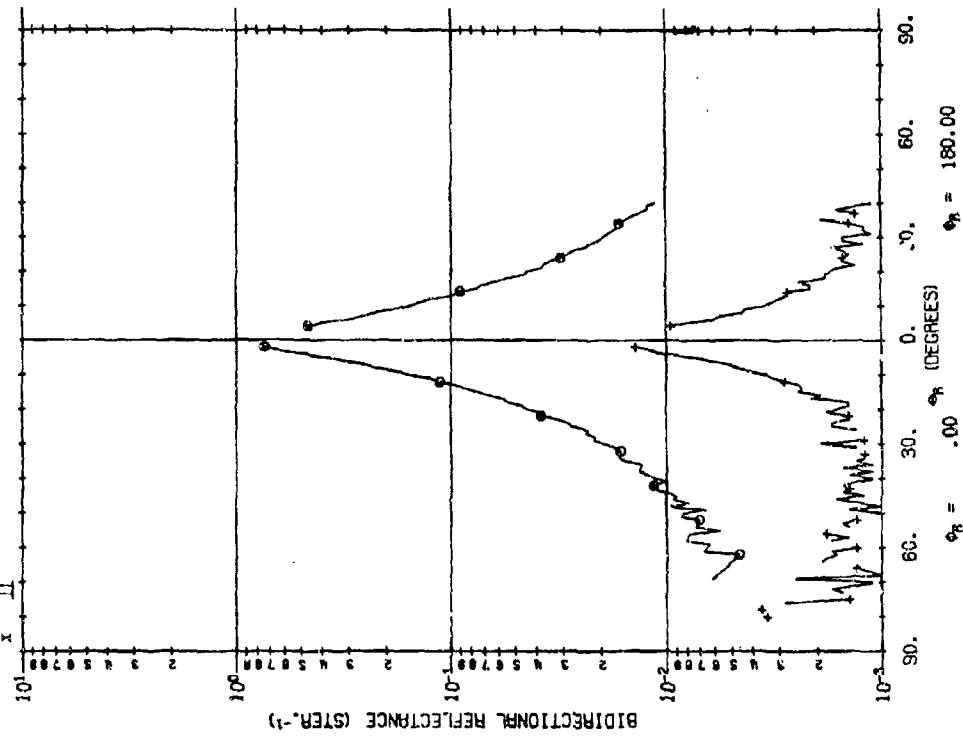
0  $\theta_i = 80.0$   
 $\theta_f = 180.0$   
 $\lambda = 0.63$



A01610 101

OLIVE DRAB PAINT ON STEEL

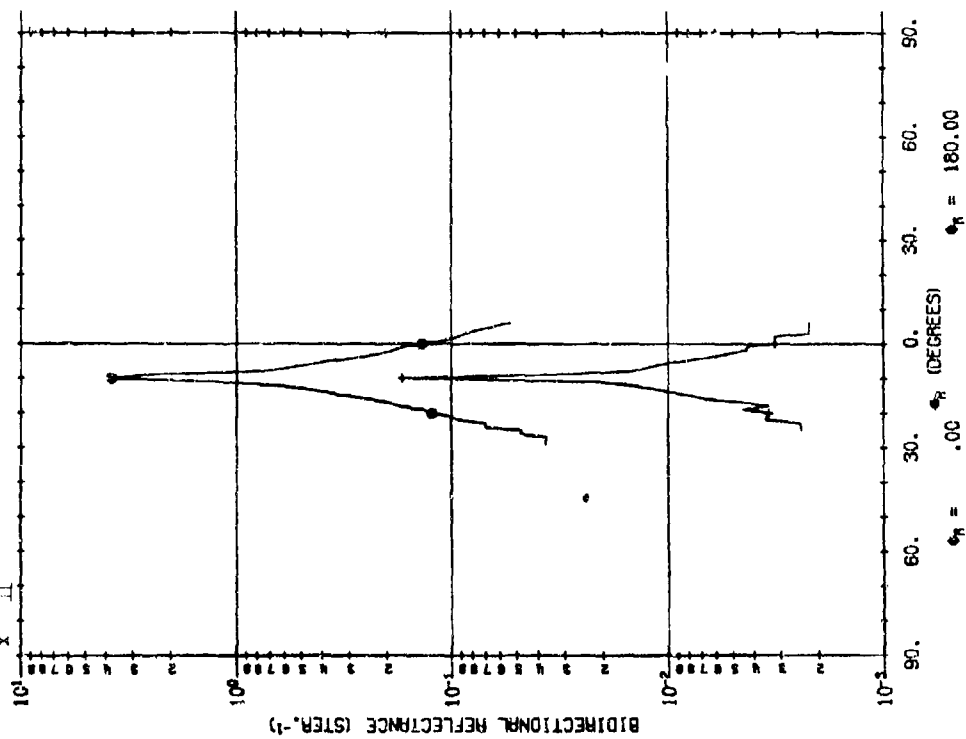
0  $\theta_i = 0.0$   
 $\theta_f = 180.0$   
 $\lambda = 10.6$



R01610 101

OLIVE DRAB PAINT ON STEEL

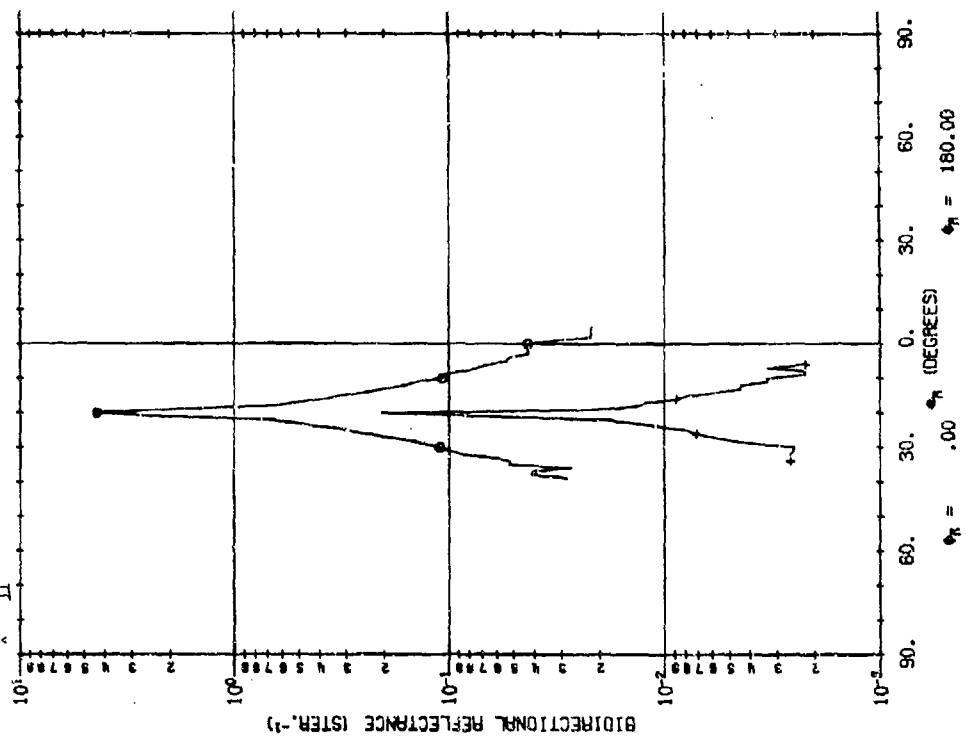
0 ||  $\phi_1 = 10.0$   
 + ||  $\phi_2 = 180.0$   
 Δ ||  $\lambda = 10.6$   
 x ||



R01610 101

OLIVE DRAB PAINT ON STEEL

0 ||  $\phi_1 = 20.0$   
 + ||  $\phi_2 = 180.0$   
 Δ ||  $\lambda = 10.6$   
 x ||

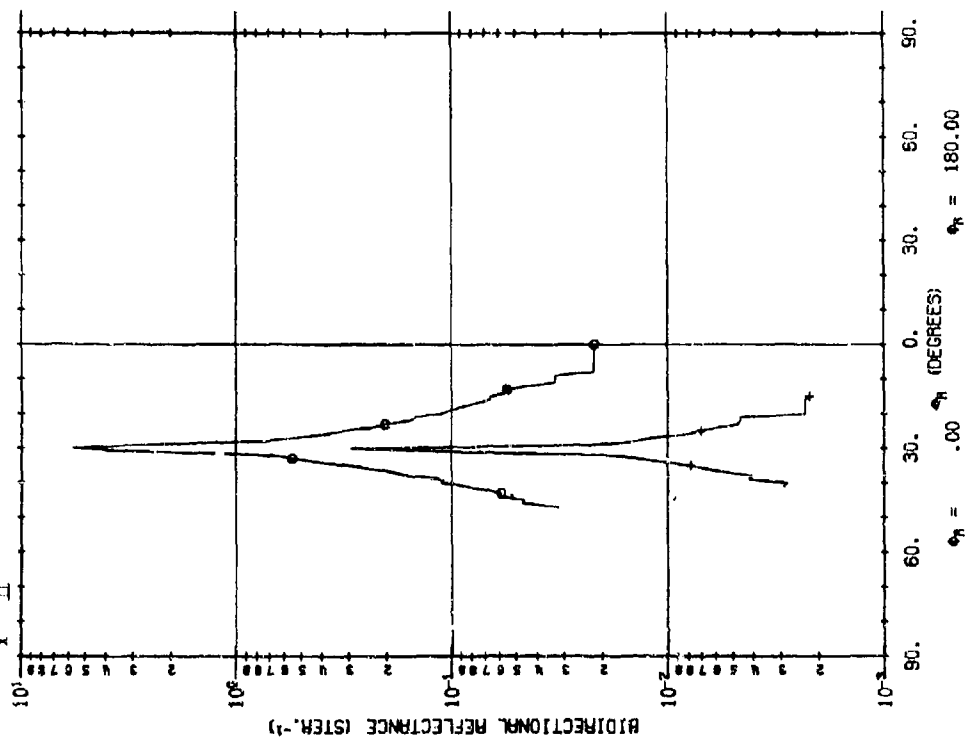


PAINT

R01610 101

OLIVE DRAB PAINT ON STEEL

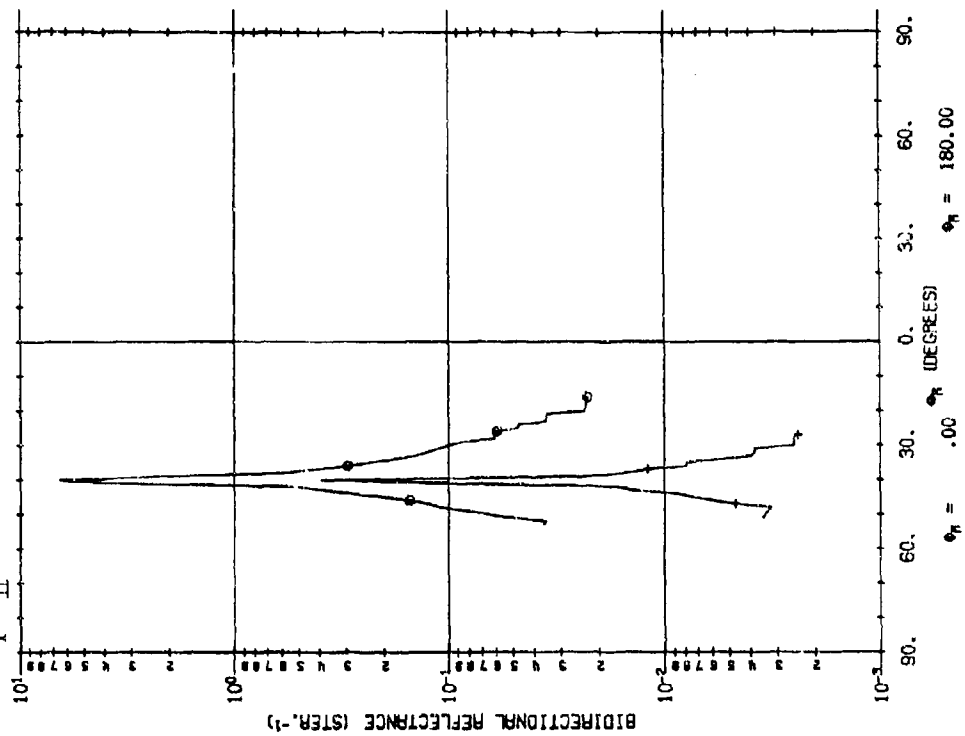
0  $\theta_i = 30.0$   
 +  $\theta_i = 180.0$   
 A  $\lambda = 10.6$



R01610 101

OLIVE DRAB PAINT ON STEEL

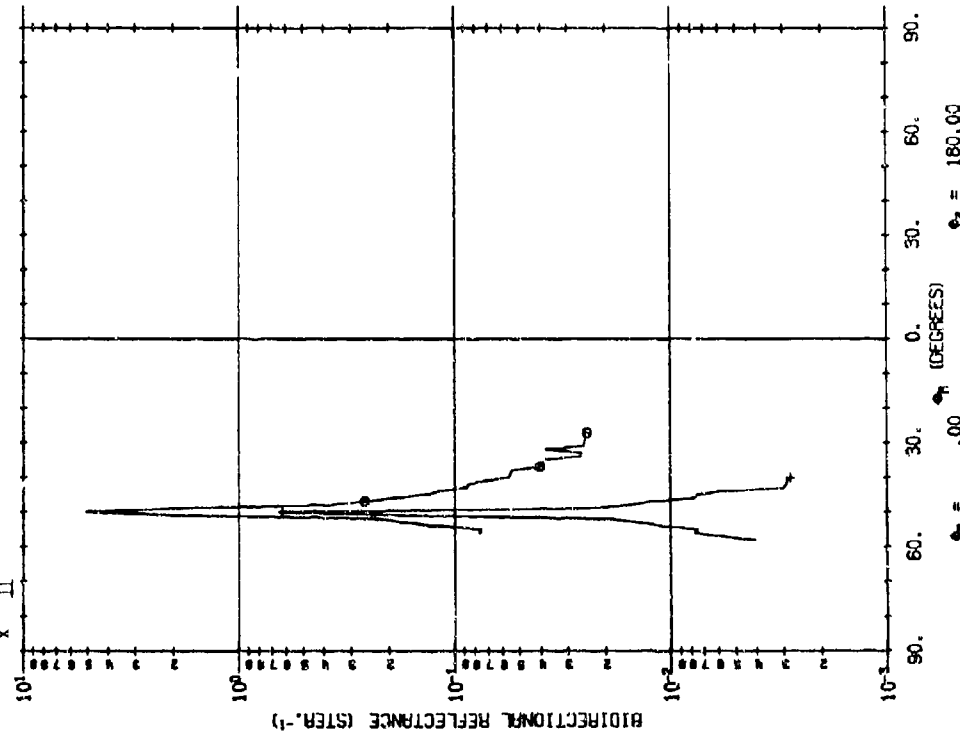
0  $\theta_i = 40.0$   
 +  $\theta_i = 180.0$   
 A  $\lambda = 10.6$



R01610 101

OLIVE DRAB PAINT ON STEEL

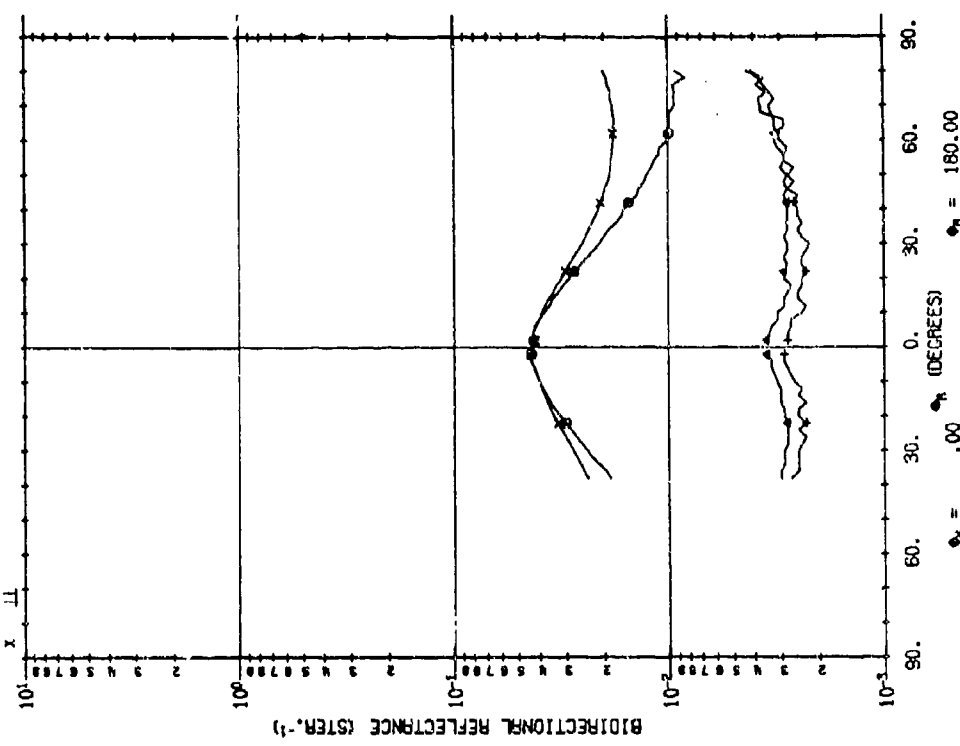
0  $\phi_1 = 50.0$   
 +  $\phi_2 = 180.0$   
 Δ  $\lambda = 10.6$



R01629 101

OLIVE DRAB PAINT ON STEEL

0  $\phi_1 = 0.0$   
 +  $\phi_2 = 0.0$   
 Δ  $\lambda = 0.63$



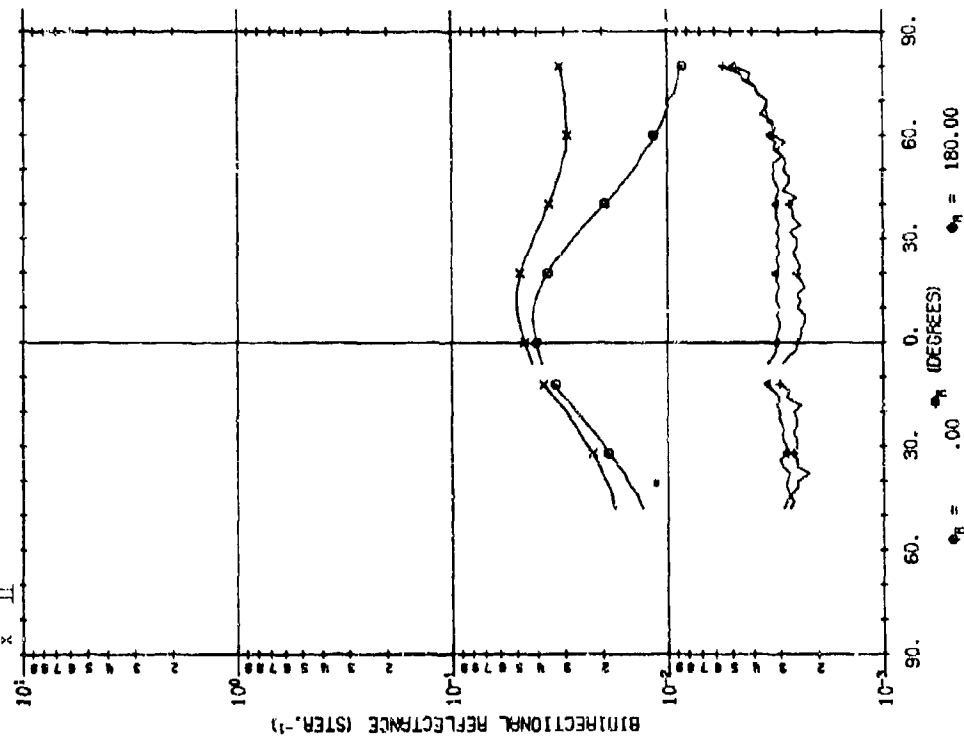
PAINT



R01629 101

OLIVE DRAB PAINT ON STEEL

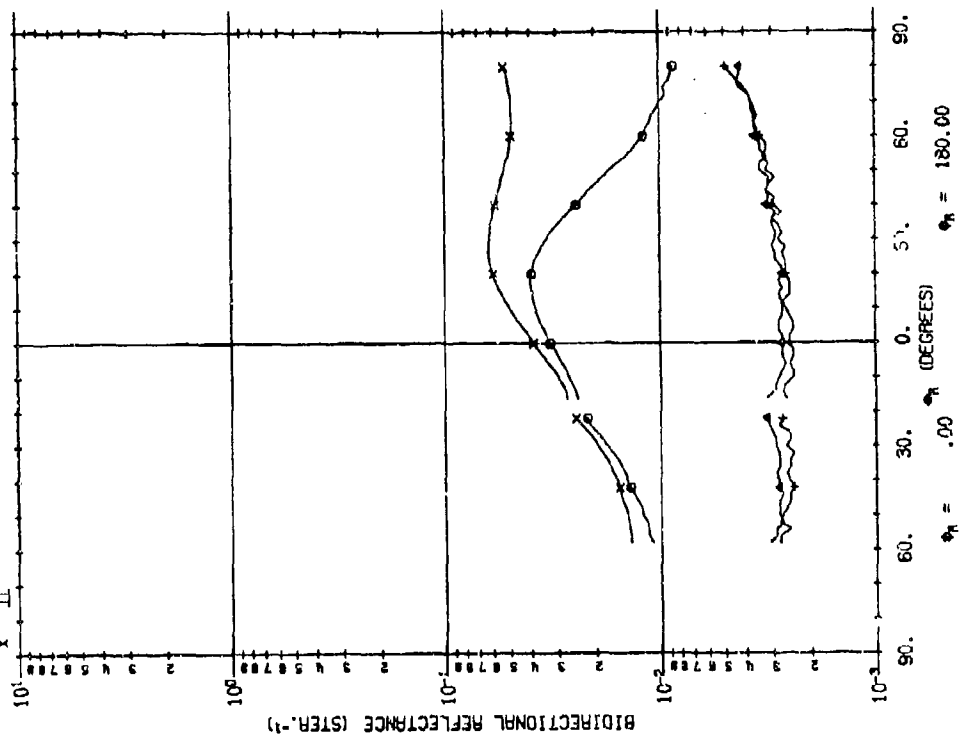
0  $\theta_1 = 10.0$   
 +  $\theta_2 = 0.0$   
 x  $\theta_3 = 0.63$



R01629 101

OLIVE DRAB PAINT ON STEEL

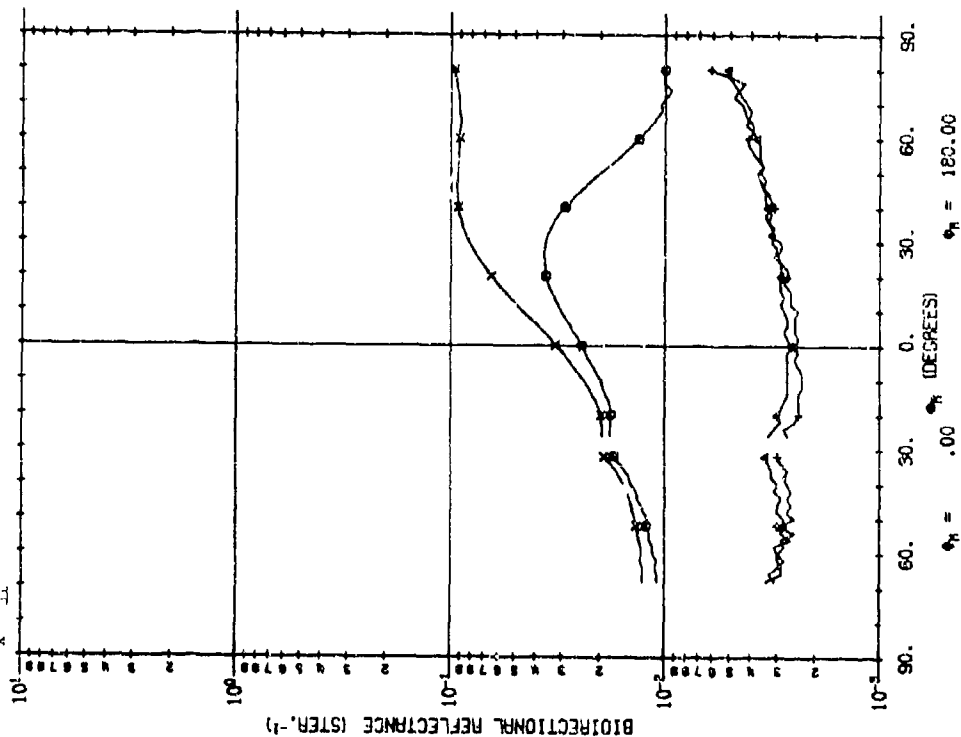
0  $\theta_1 = 20.0$   
 +  $\theta_2 = 0.0$   
 x  $\theta_3 = 0.63$



A01629 101

OLIVE DRAB PAINT ON STEEL

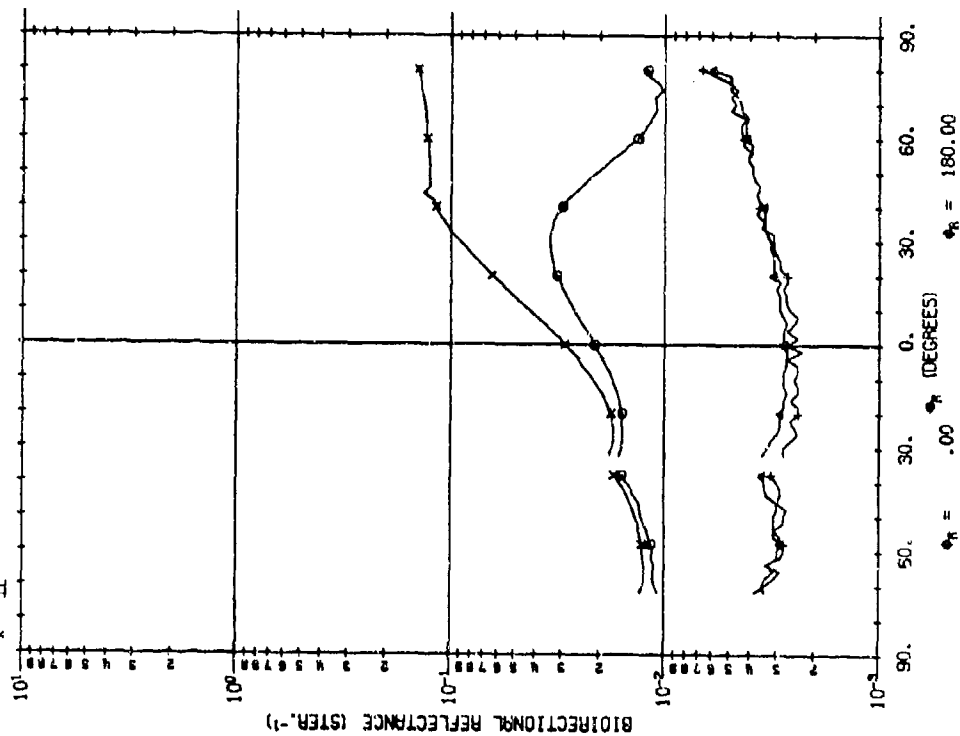
0  $\epsilon_1 = 30.0$   
 +  $\epsilon_2 = 0.0$   
 x  $\epsilon_3 = 0.63$



A01629 101

OLIVE DRAB PAINT ON STEEL

0  $\epsilon_1 = 35.0$   
 +  $\epsilon_2 = 0.0$   
 x  $\epsilon_3 = 0.63$

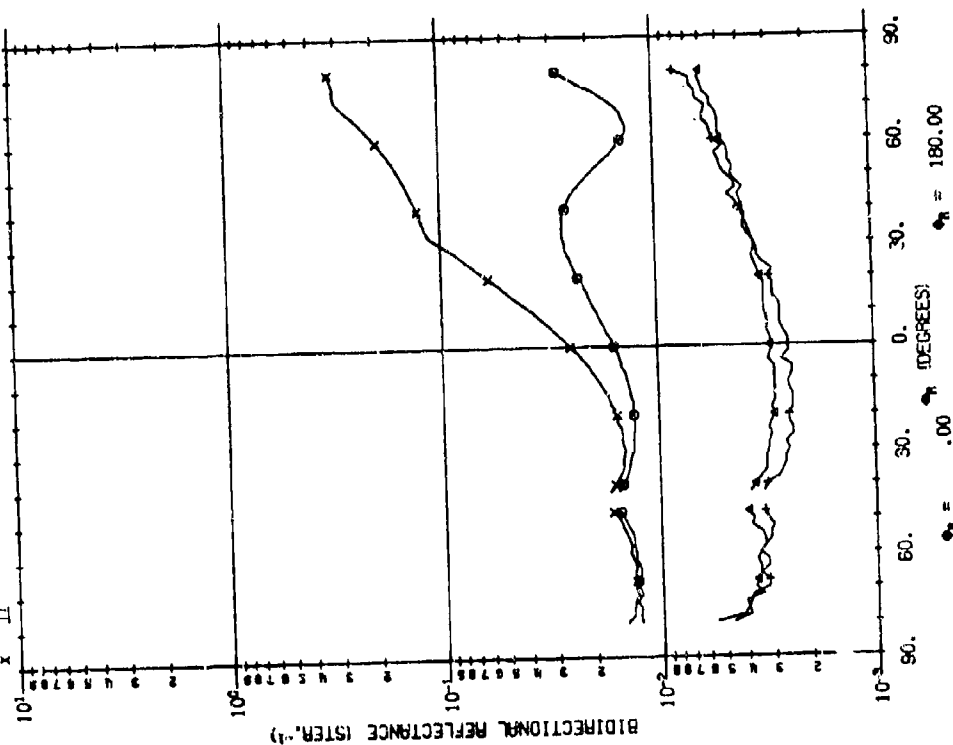


PAINT

R01629 101

OLIVE DRAB PAINT ON STEEL

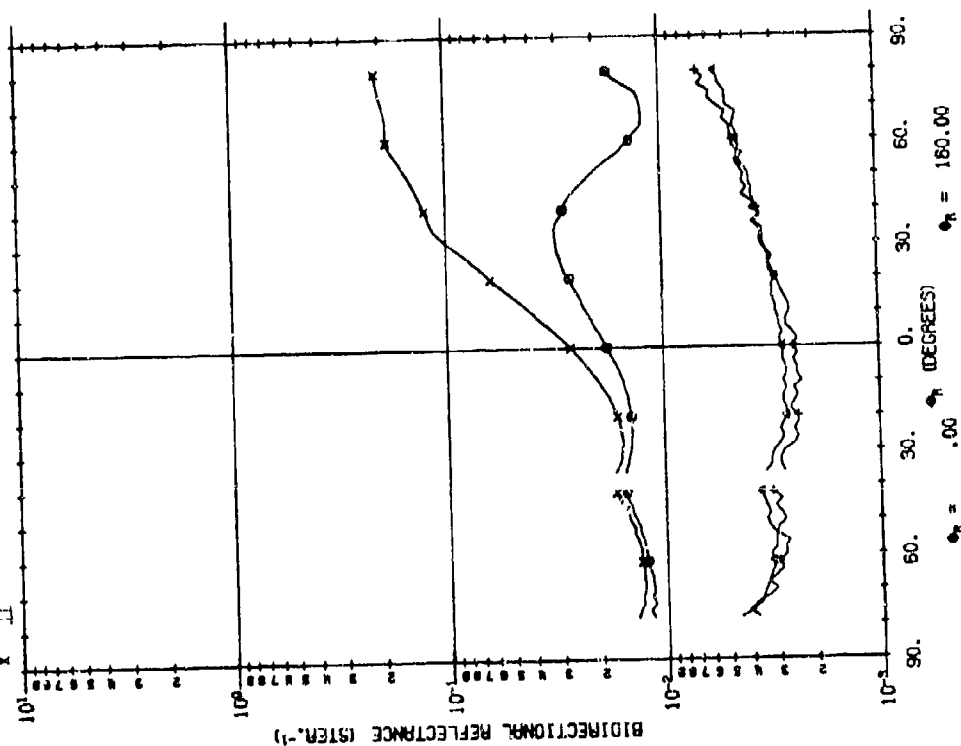
0  $\theta_1 = 45.0$   
 +  $\theta_2 = 0.0$   
 x  $\theta_3 = 0.63$



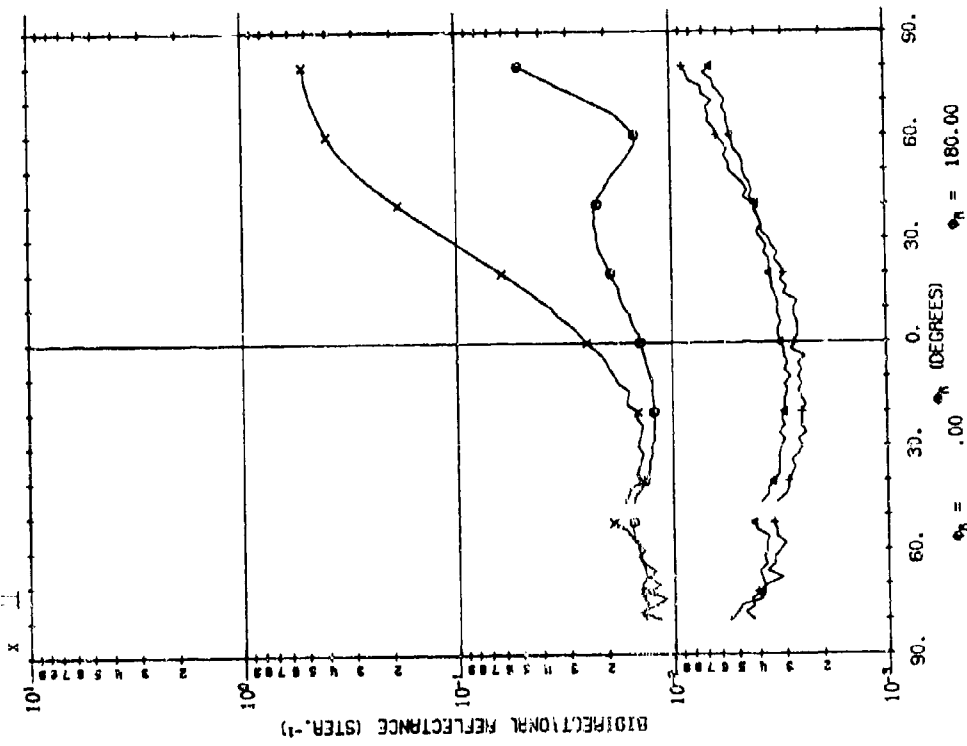
R01629 101

OLIVE DRAB PAINT ON STEEL

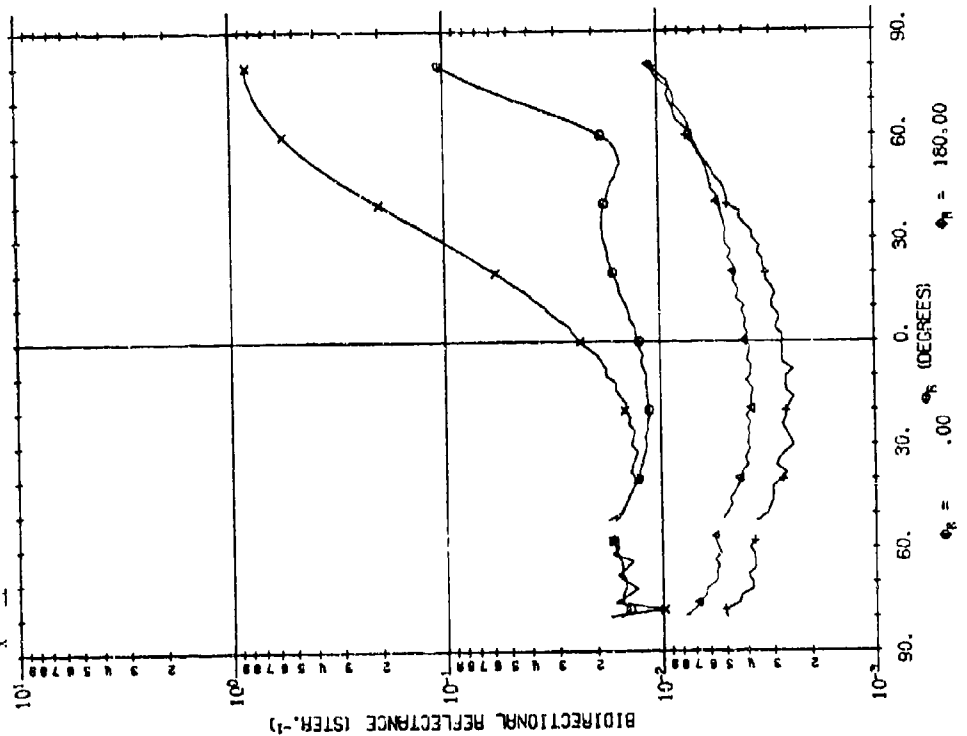
0  $\theta_1 = 40.0$   
 +  $\theta_2 = 0.0$   
 x  $\theta_3 = 0.63$



A01629 101  
 OLIVE DRAB PAINT ON STEEL  
 $\phi_1 = 50.0$   
 $\phi_2 = 0.0$   
 $\lambda = 0.63$



A01629 101  
 OLIVE DRAB PAINT ON STEEL  
 $\phi_1 = 55.0$   
 $\phi_2 = 0.0$   
 $\lambda = 0.63$

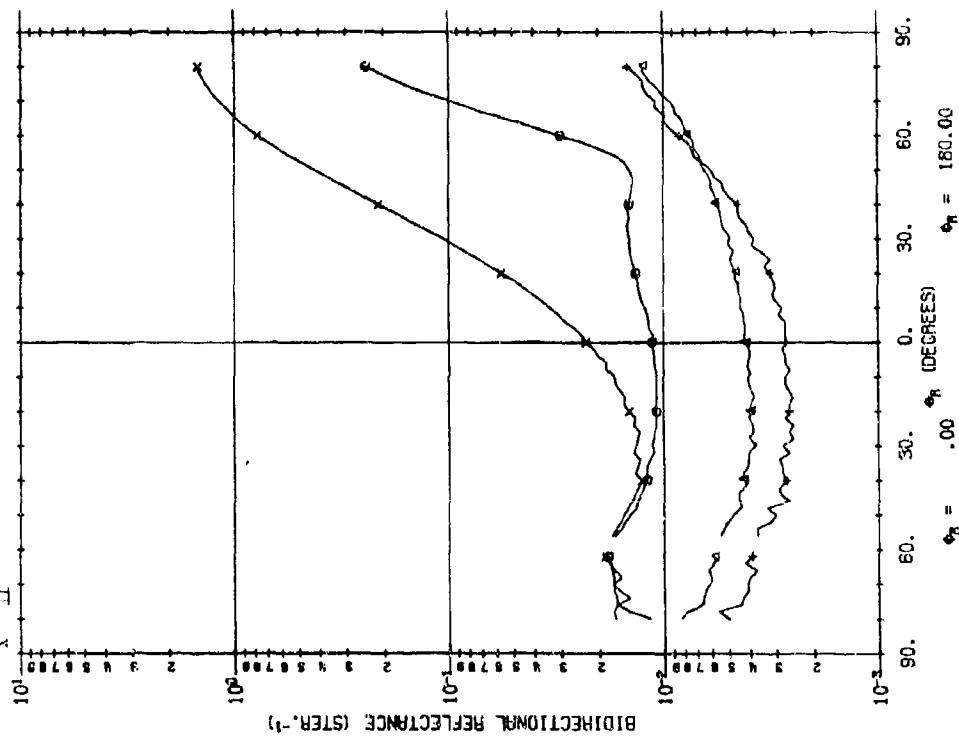


PAINT

A01629 101

OLIVE DRAB PAINT ON STEEL

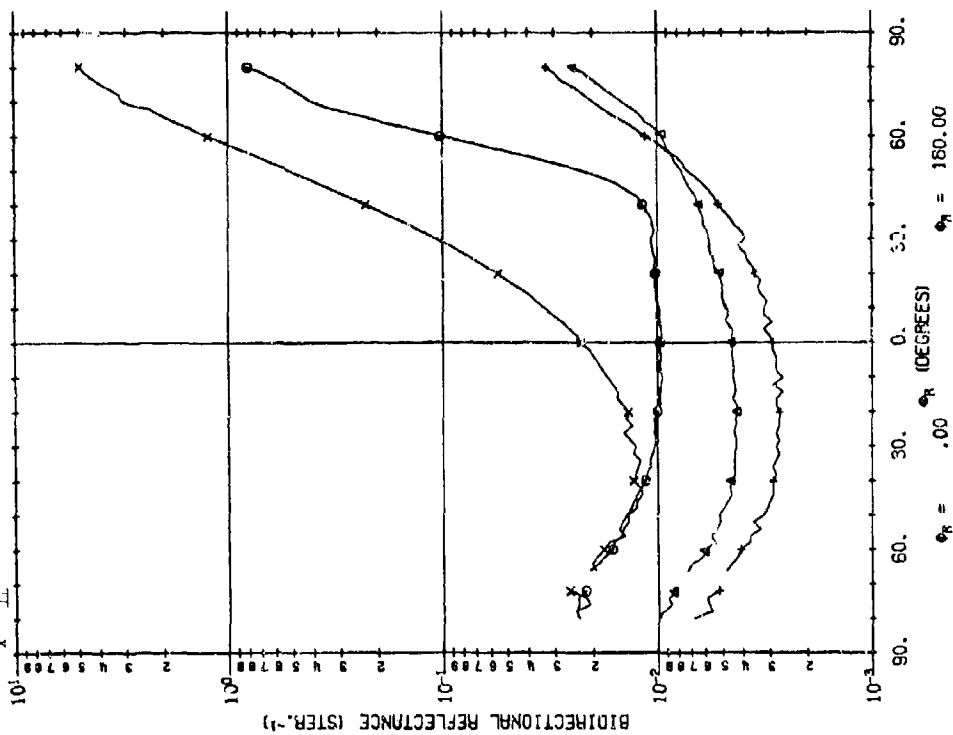
0  $\phi_1 = 60.0$   
 +  $\phi_1 = 0.0$   
 x  $\phi_1 = 0.63$

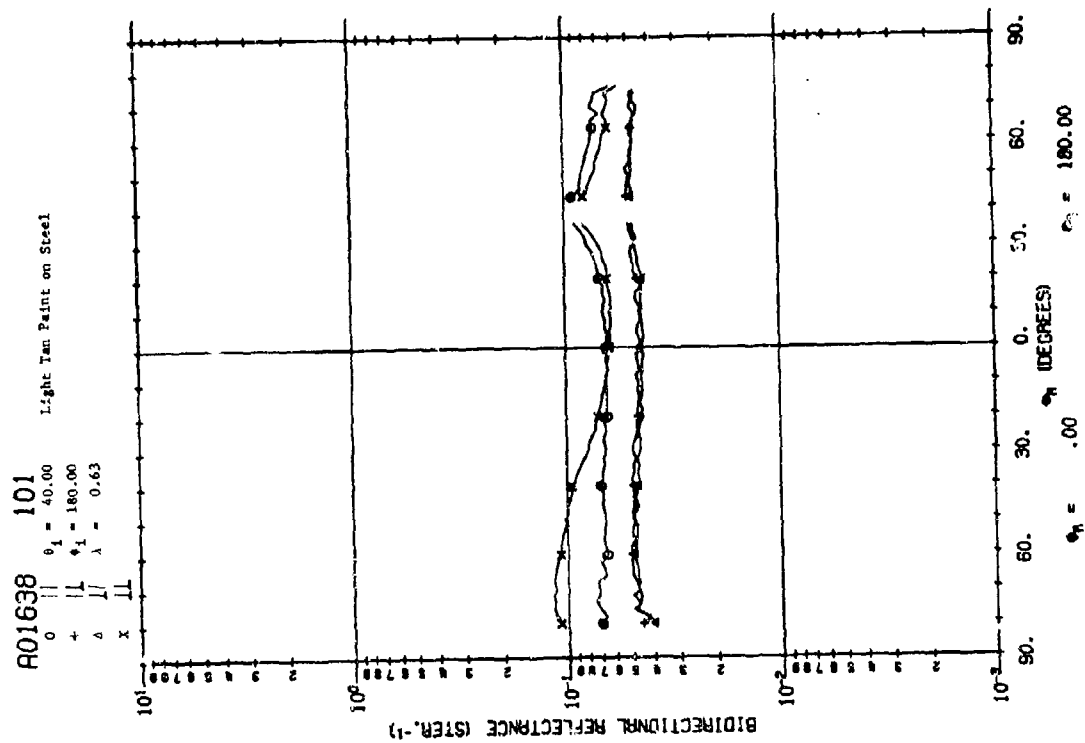
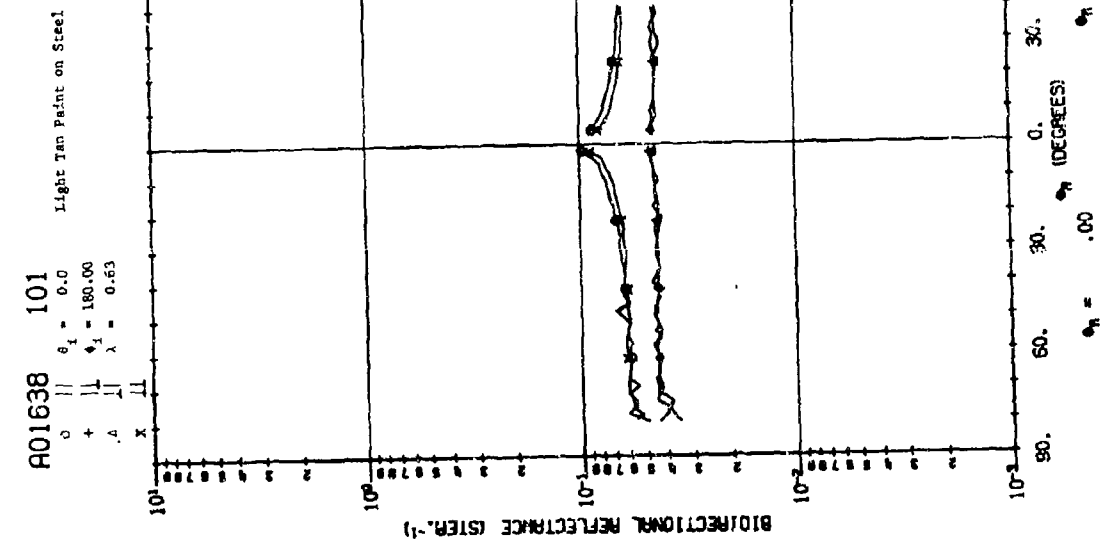


A01629 101

OLIVE DRAB PAINT ON STEEL

0  $\phi_1 = 70.0$   
 +  $\phi_1 = 0.0$   
 x  $\phi_1 = 0.63$



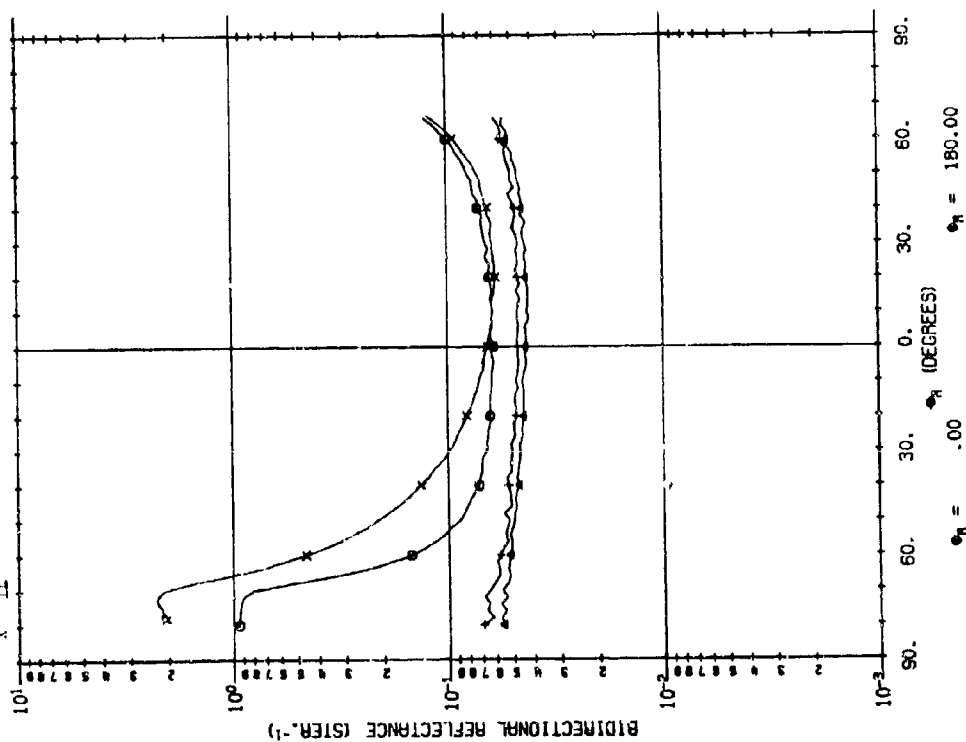


PAINT

R01638 101

Light Tan Paint on Steel

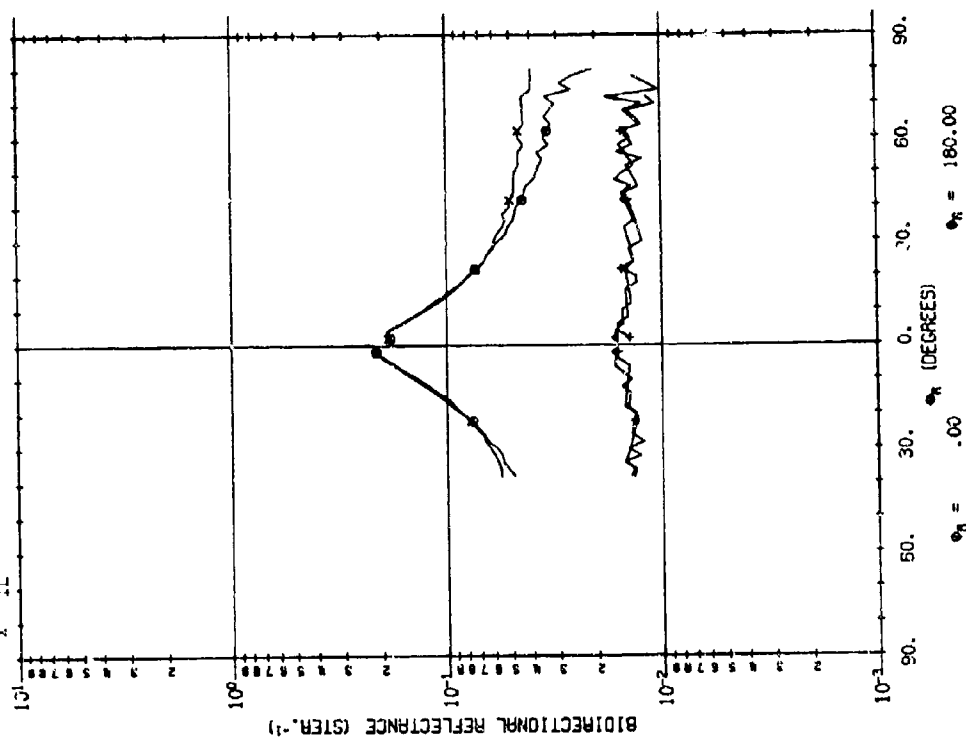
0 //  $\theta_i = 70.00$   
 + //  $\phi_i = 180.00$   
 x //  $\psi_i = 0.63$



R01640 101

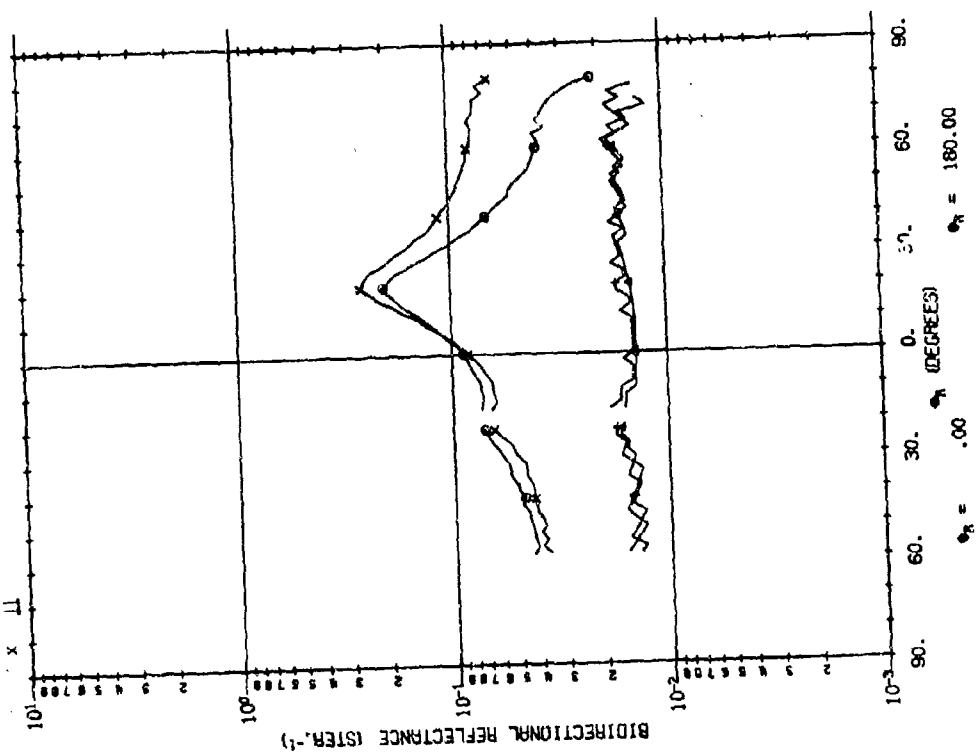
Olive Drab Paint on Steel

0 //  $\theta_i = 0.0$   
 + //  $\phi_i = 0.0$   
 x //  $\psi_i = 0.63$



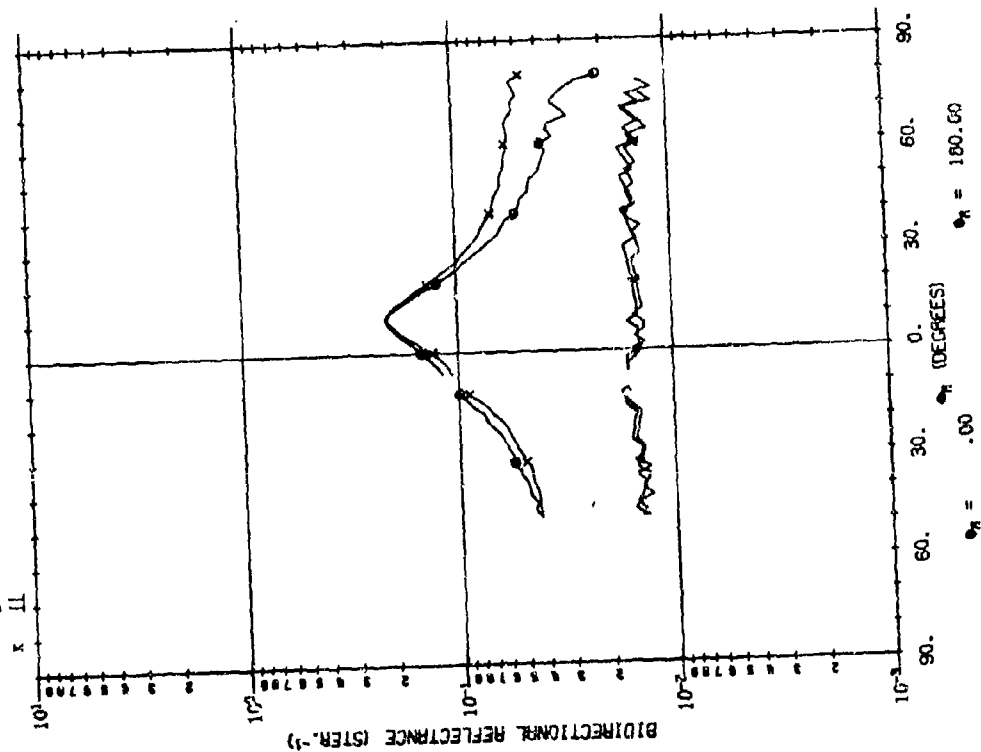
AD1640 101 Olive Drab Paint on Steel

0 ||  $\theta_i = 20.00$   
 + ||  $\phi_i = 0.0$   
 x ||  $\lambda = 0.63$   
 ||



AD1640 101 Olive Drab Paint on Steel

0 ||  $\theta_i = 10.00$   
 + ||  $\phi_i = 0.0$   
 x ||  $\lambda = 0.63$   
 ||



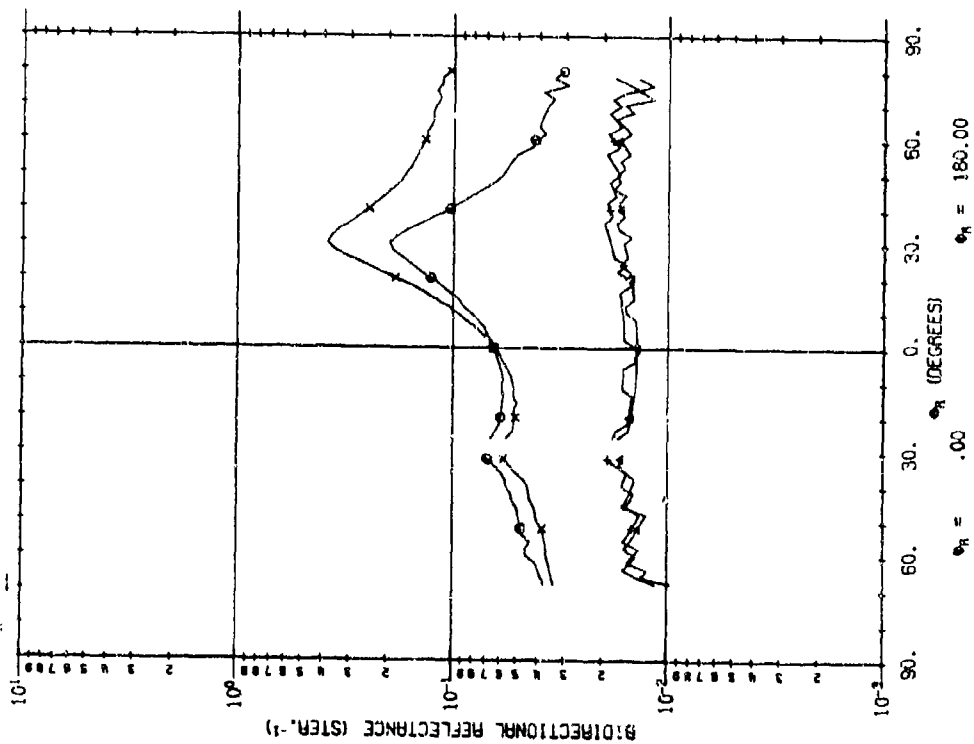
PAINT



A01640 101

Olive Drab Paint on Steel

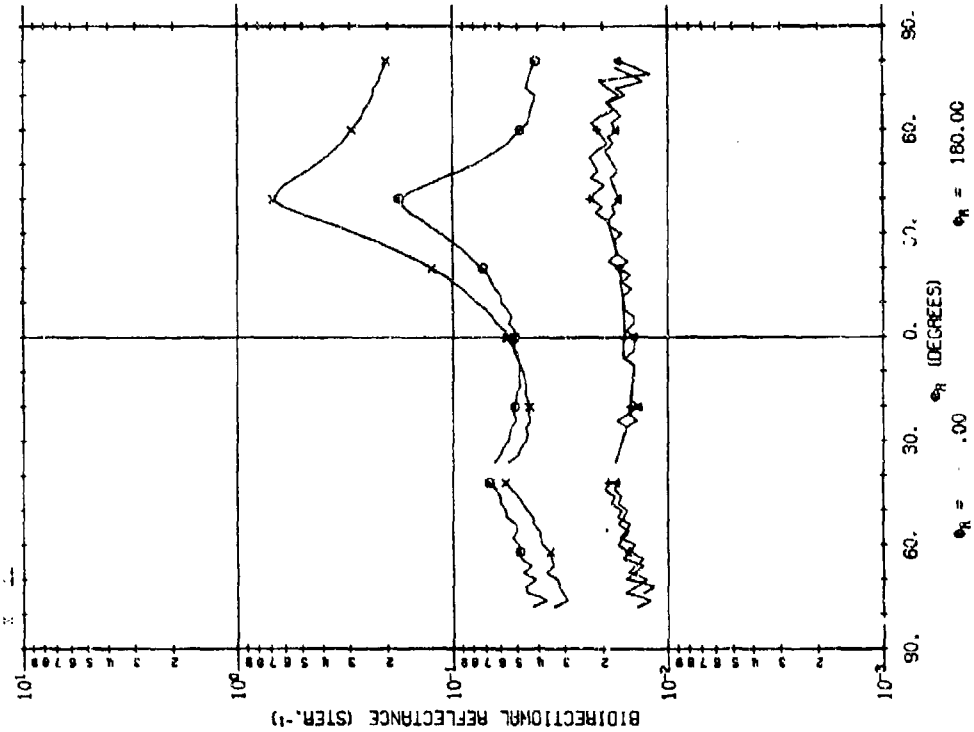
$\epsilon_1 = 30.00$   
 $\epsilon_2 = 0.0$   
 $\epsilon_3 = 0.63$



A01640 101

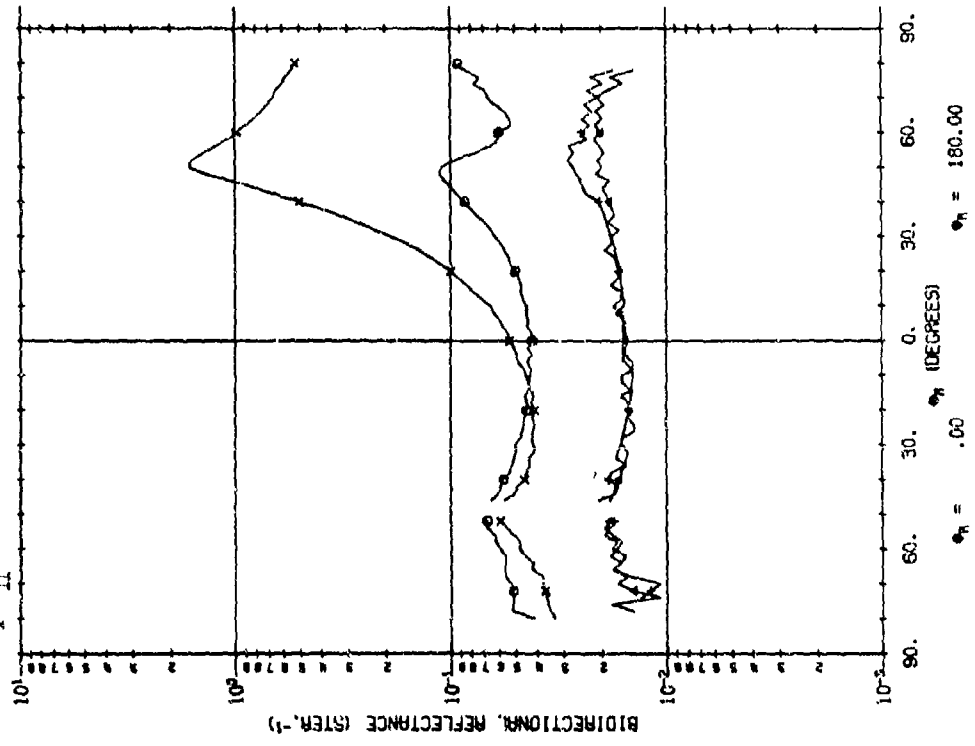
Olive Drab Paint on Steel

$\epsilon_1 = 40.00$   
 $\epsilon_2 = 0.0$   
 $\epsilon_3 = 0.63$



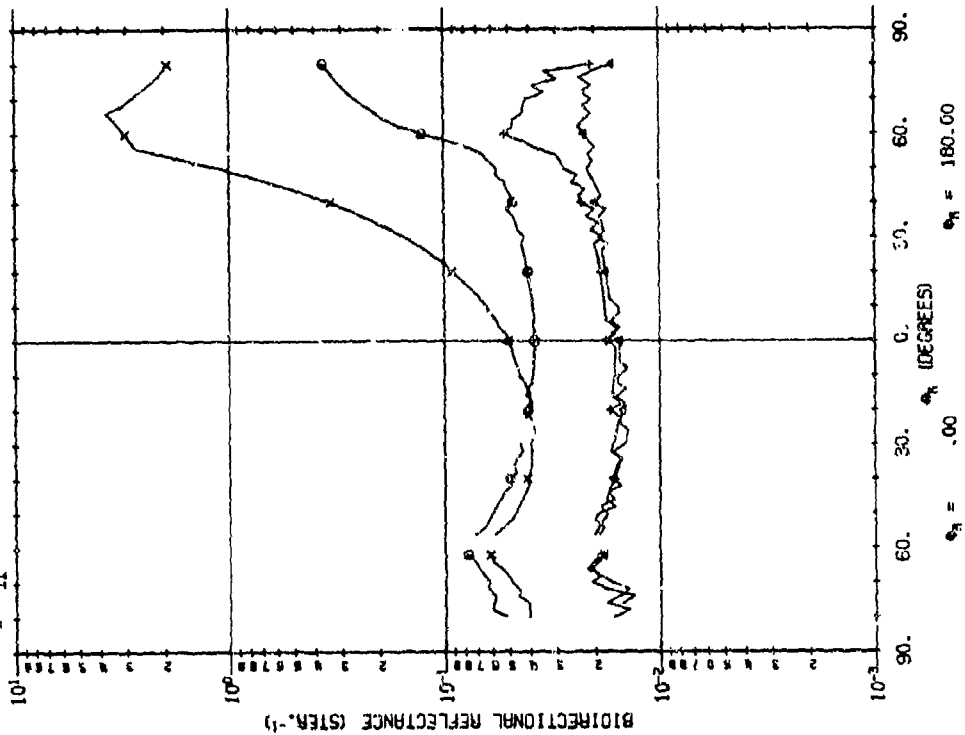
R01640 101  
 $\theta_i = 50.00$   
 $\theta_t = 0.0$   
 $\lambda = 0.63$

Olive Drab Paint on Steel



R01640 101  
 $\theta_i = 60.00$   
 $\theta_t = 0.0$   
 $\lambda = 0.63$

Olive Drab Paint on Steel

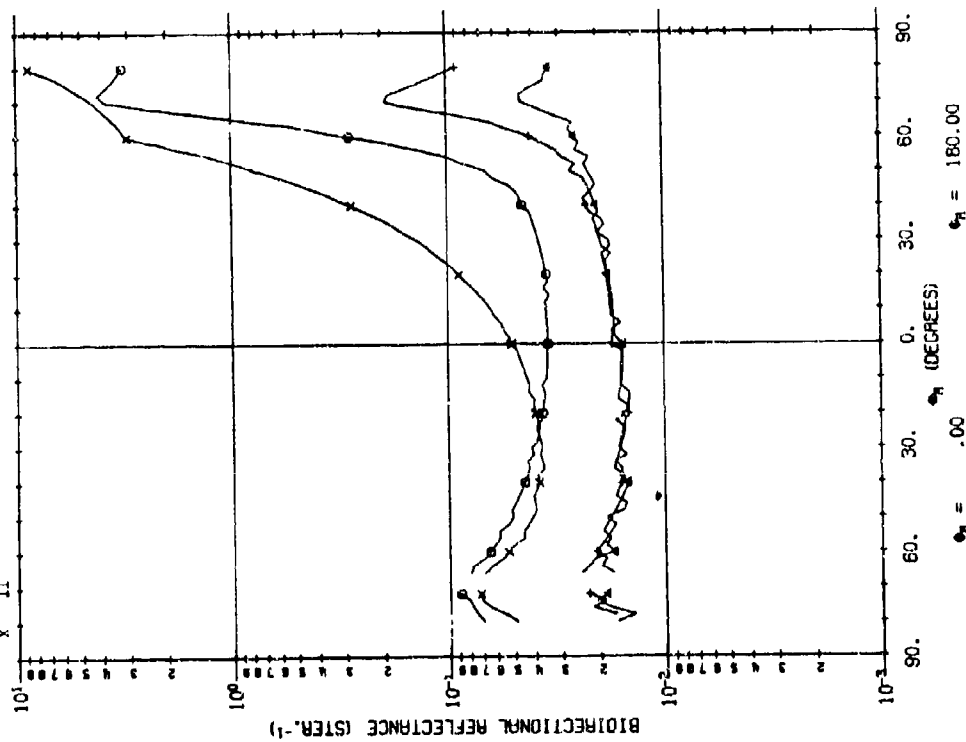


PAINT

A01640 101

Olive Drab Paint on Steel

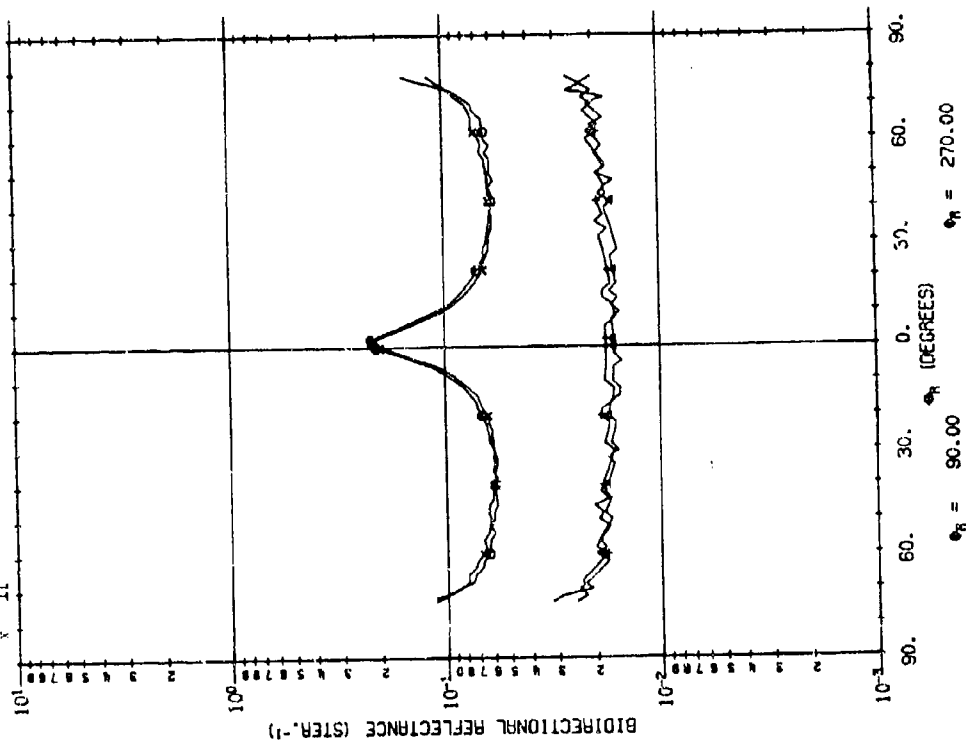
0 11 70.00  
+ 11 0.0  
- 11 0.63  
x 11



A01640 101

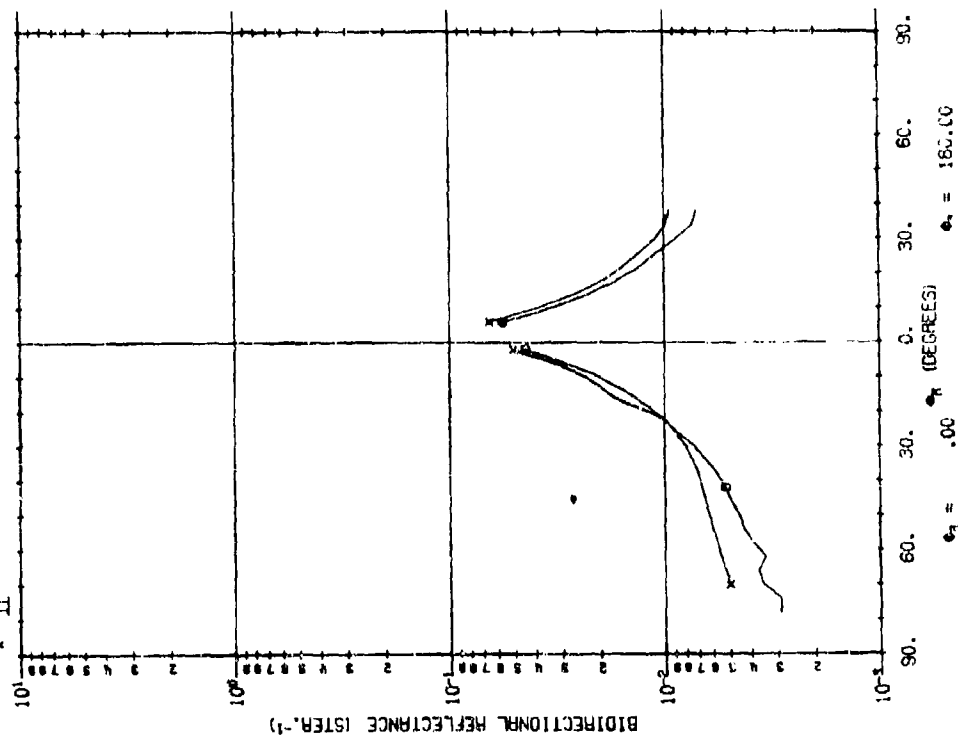
Olive Drab Paint on Steel

0 11 2.0  
+ 11 0.63  
- 11 0.63  
x 11



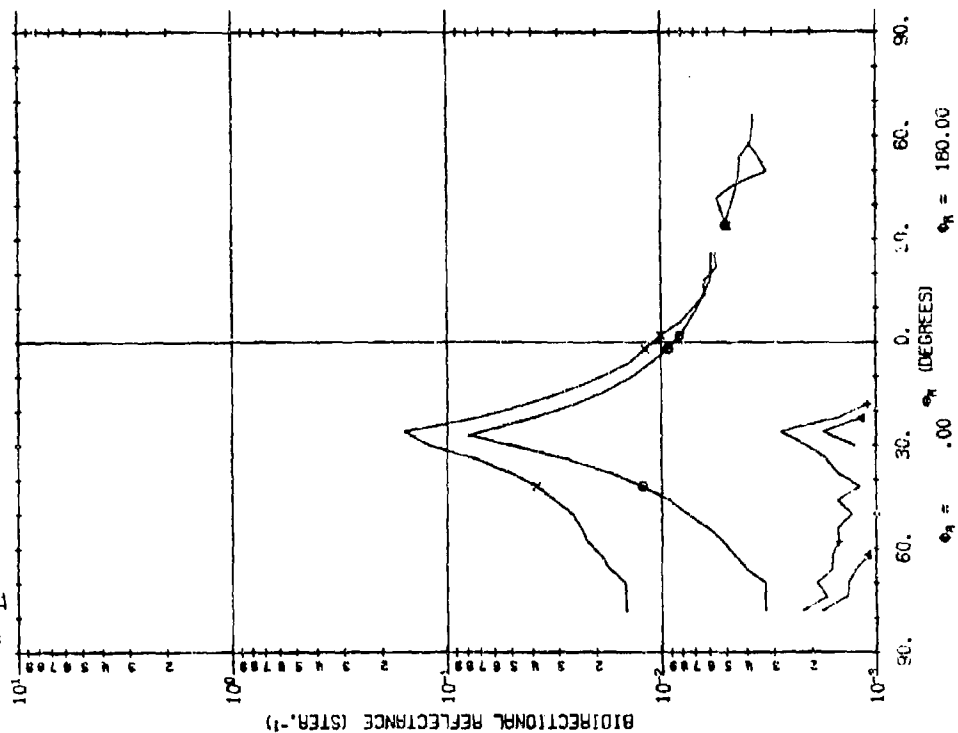
BLACK PAINT ON CURVED METAL

R01699 301  
 $\theta_i = 0.0$   
 $\phi_i = 180.0$   
 $\lambda = 0.63$



BLACK PAINT ON CURVED METAL

R01699 301  
 $\theta_i = 33.6$   
 $\phi_i = 180.0$   
 $\lambda = 0.63$

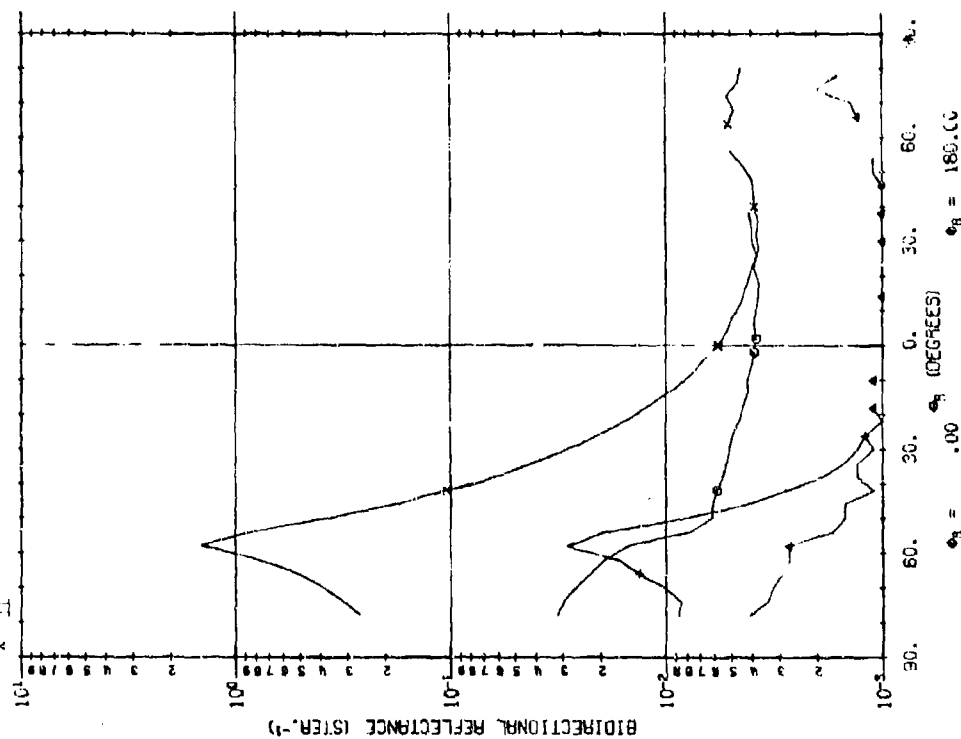


PAINT

A01699 301

BLACK PAINT ON CURVED METAL

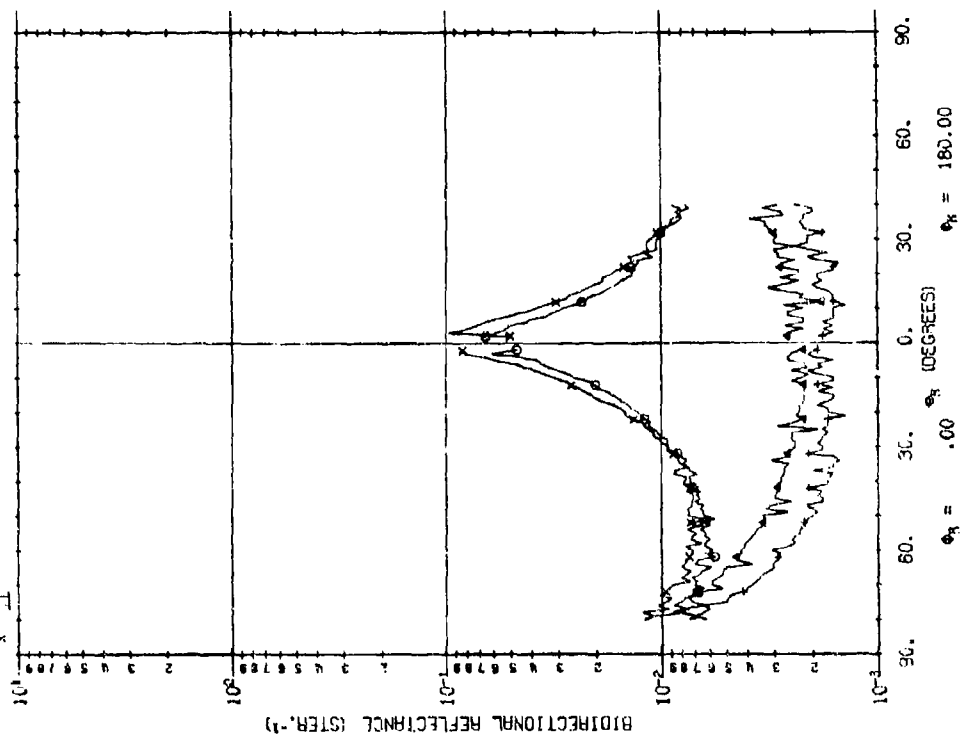
$\theta_1 = 60.0$   
 $\theta_2 = 180.0$   
 $\lambda = 0.63$



A01693 302

BLACK PAINT ON CURVED METAL

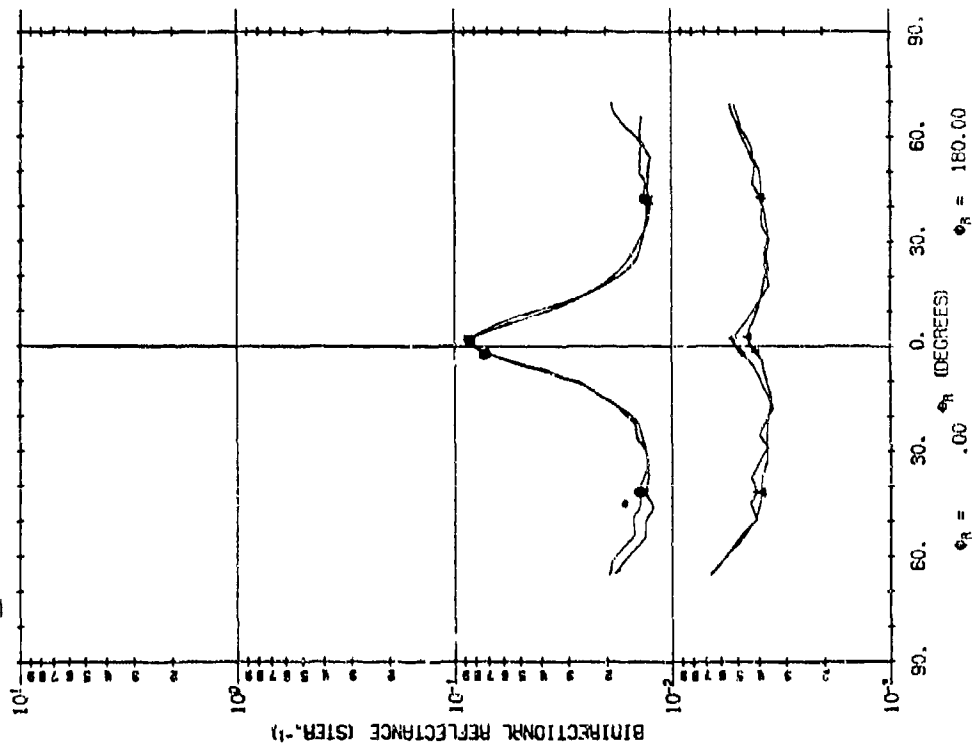
$\theta_1 = 0.0$   
 $\theta_2 = 0.0$   
 $\lambda = 1.06$



R01701 102

DARK OLIVE DRAB PAINT ON METAL

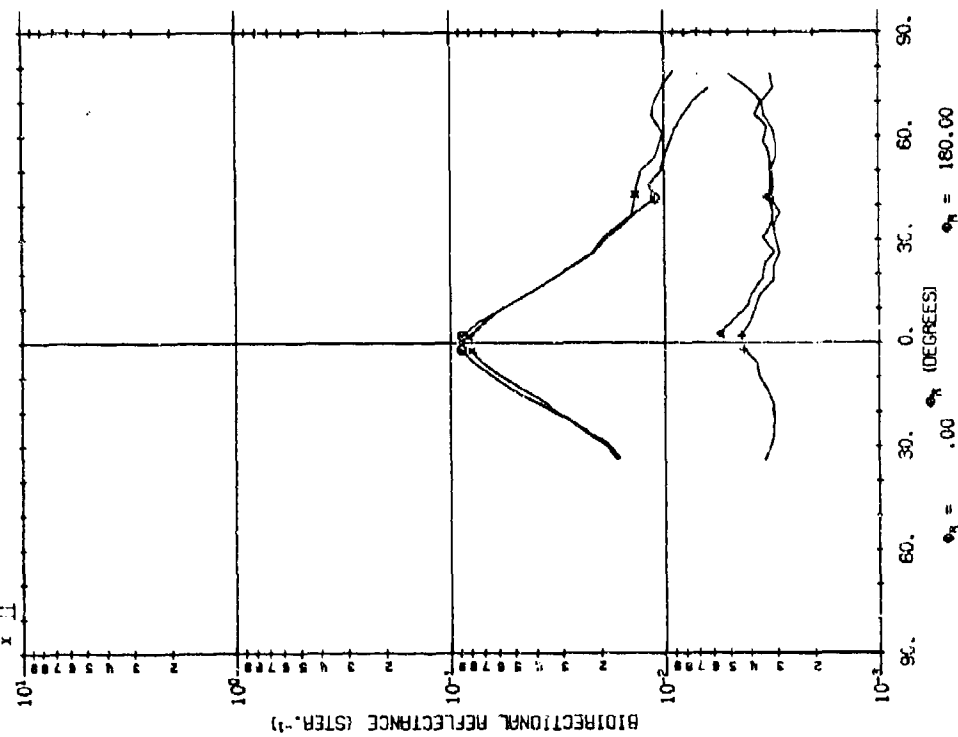
0 ||  $2S = 2.0$   
+ ||  $\phi_1 = \phi_r$   
x ||  $\lambda = 0.63$



R01701 102

DARK OLIVE DRAB PAINT ON METAL

0 ||  $2S = 0.0$   
+ ||  $\phi_1 = 0.0$   
x ||  $\lambda = 0.63$

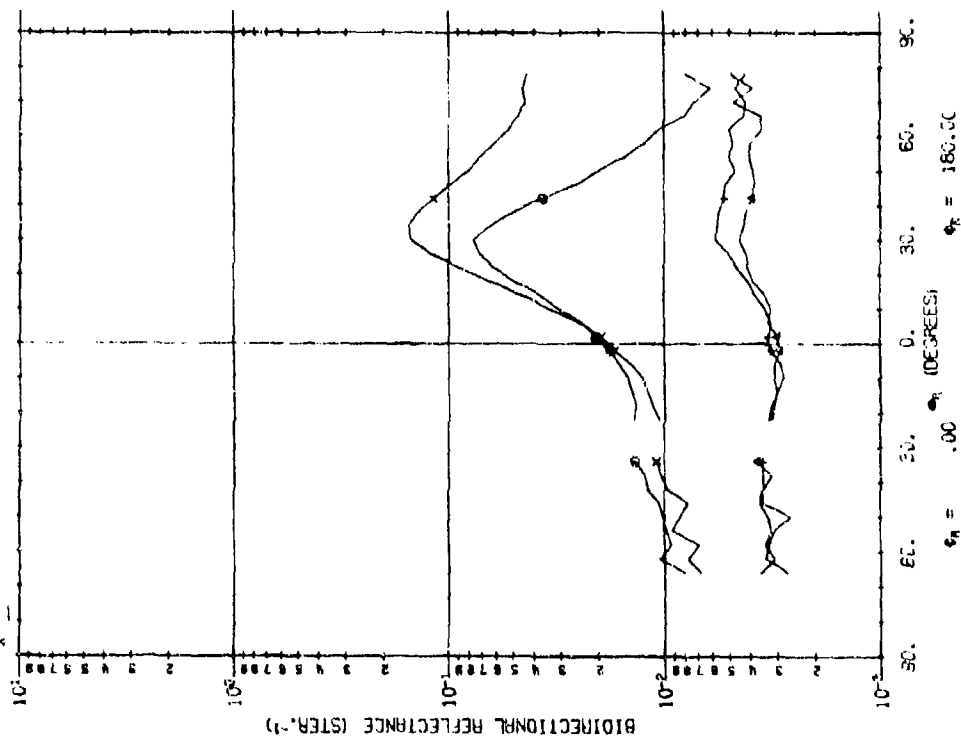


PAINT

AC1701 102

DARK OLIVE DRAB PAINT ON METAL

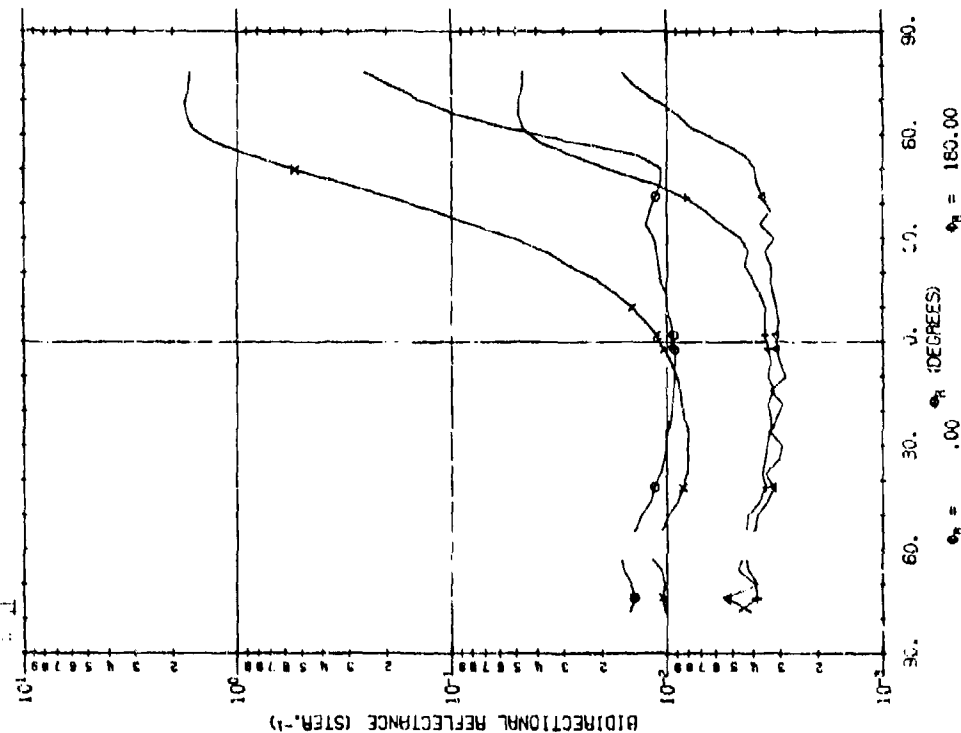
$\epsilon_1 = 30.0$   
 $\epsilon_2 = 0.0$   
 $\epsilon_3 = 0.63$



AC1701 102

DARK OLIVE DRAB PAINT ON METAL

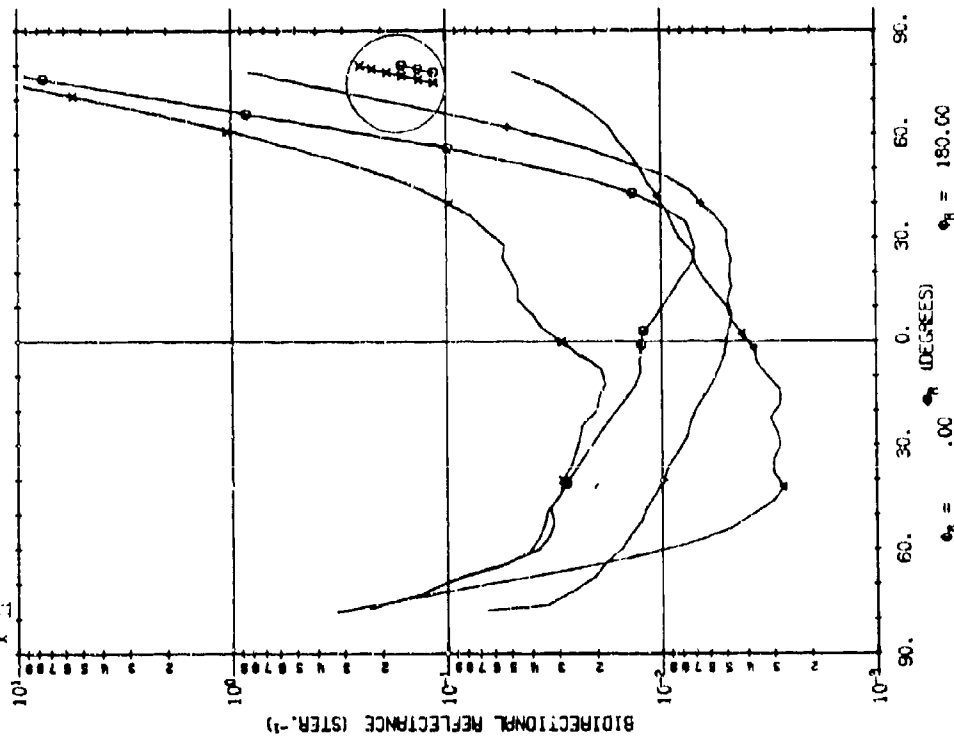
$\epsilon_1 = 60.0$   
 $\epsilon_2 = 0.0$   
 $\epsilon_3 = 0.63$



A01701 102

DARK OLIVE DRAB PAINT ON METAL

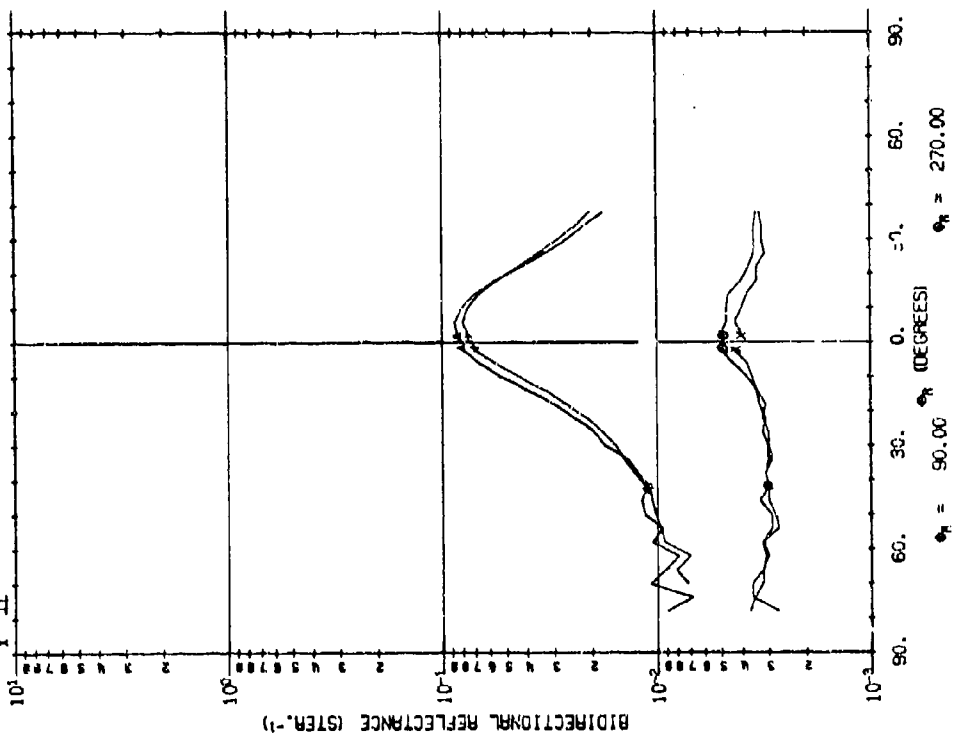
0 ||  $\phi_1 = 80.0$   
 + ||  $\phi_2 = 0.0$   
 x ||  $\lambda = 0.63$



A01701 102

DARK OLIVE DRAB PAINT ON METAL

0 ||  $\phi_1 = 0.0$   
 + ||  $\phi_2 = 0.0$   
 x ||  $\lambda = 0.63$

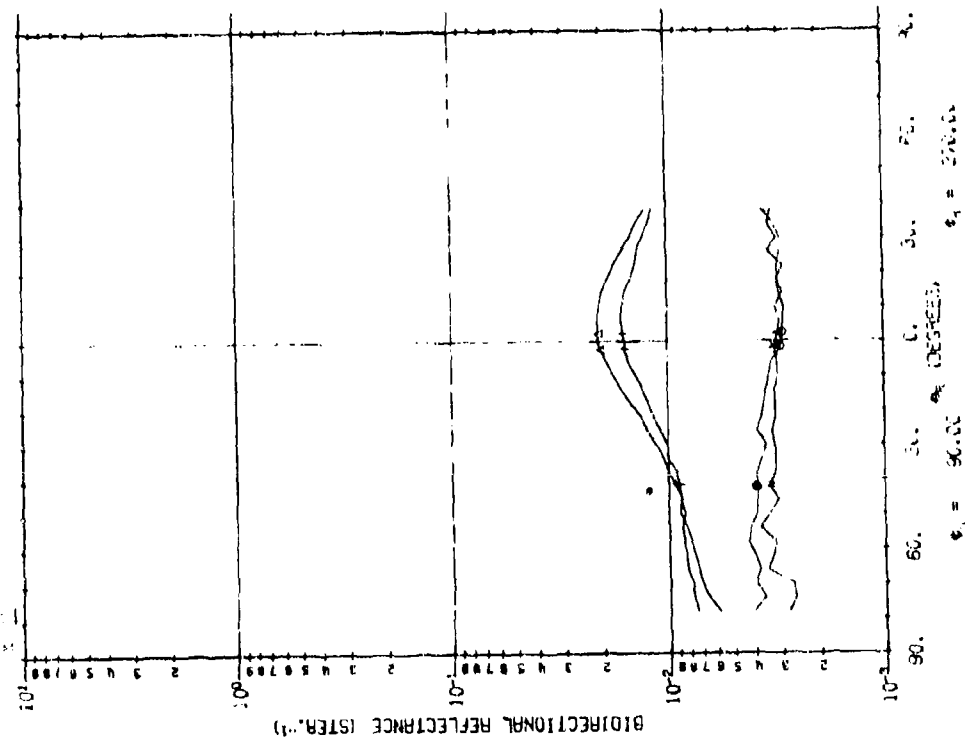


PAINT



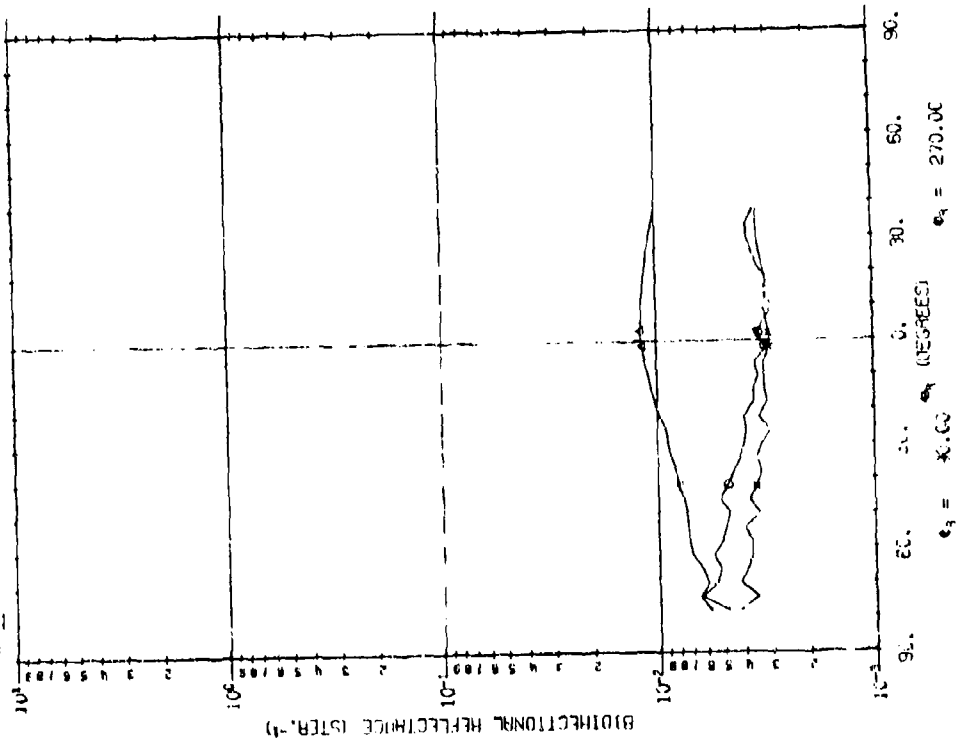
401701 102  
DARK OLIVE DRAB PAINT ON METAL

$\epsilon_1 = 30.0$   
 $\epsilon_2 = 0.0$   
 $\epsilon_3 = 0.63$



401701 102  
DARK OLIVE DRAB PAINT ON METAL

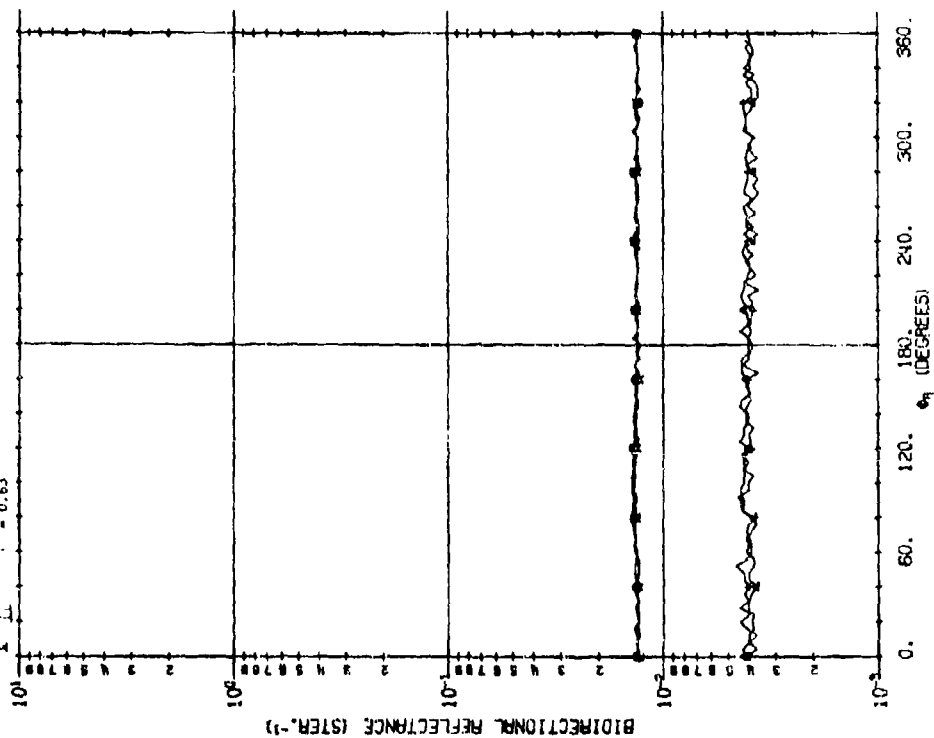
$\epsilon_1 = 60.0$   
 $\epsilon_2 = 0.0$   
 $\epsilon_3 = 0.63$



A01701 102

DARK OLIVE DRAB PAINT ON METAL

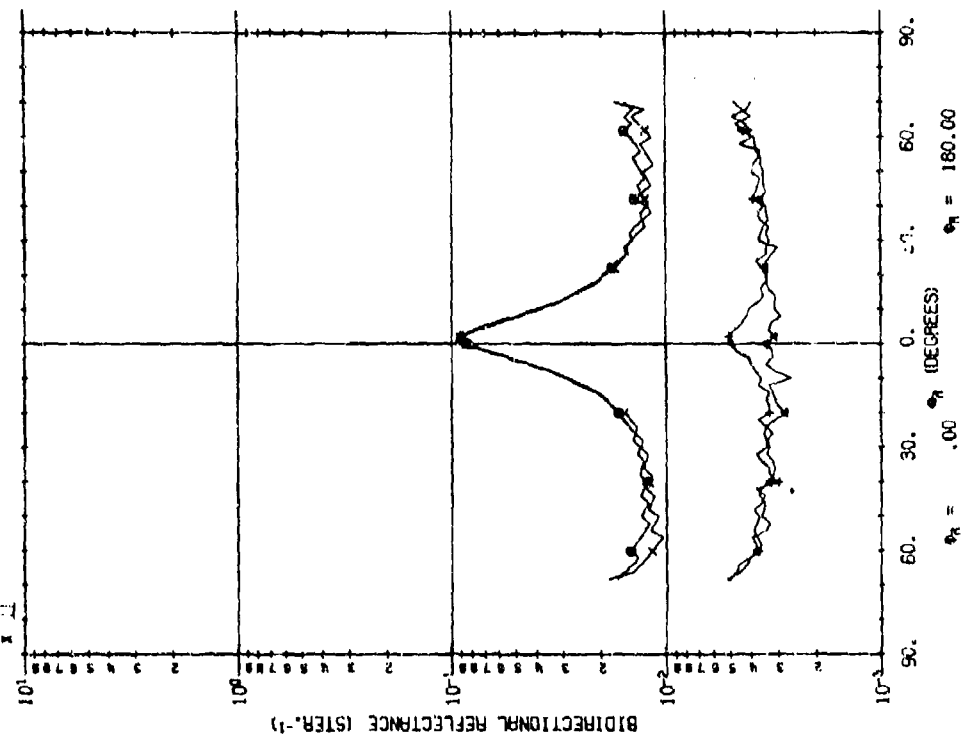
$\theta_i = 45.0$   
 $\theta_r = 47.0$   
 $\theta_t = 6_r$   
 $i = 0.63$



A01701 201

DARK OLIVE DRAB PAINT ON METAL

$\theta_i = 2.0$   
 $\theta_r = 4_r$   
 $i = 0.63$

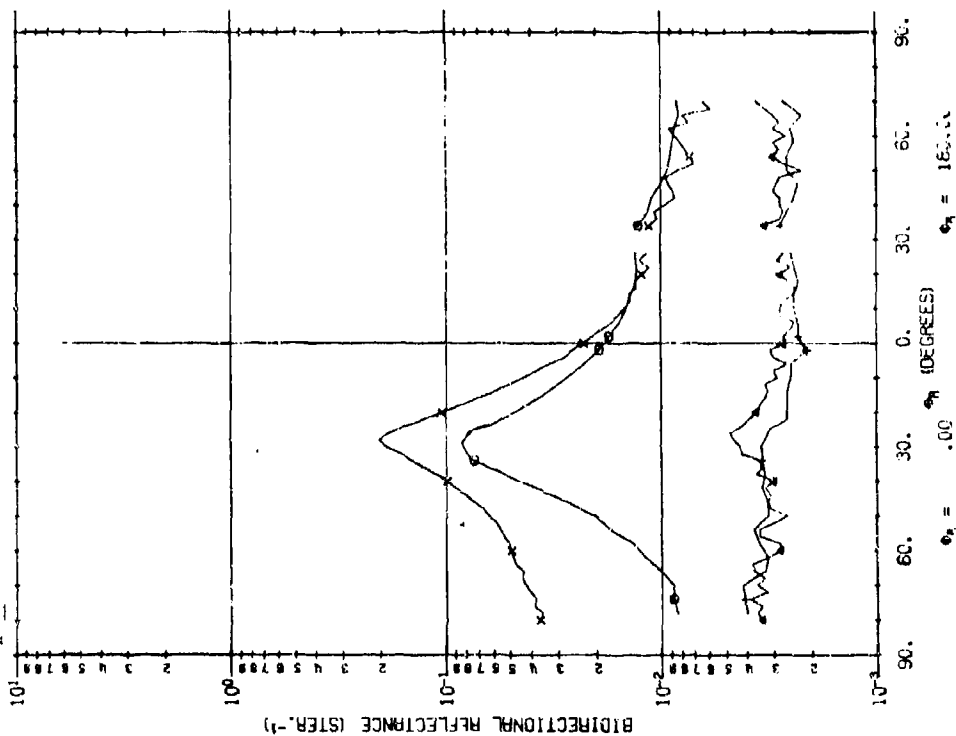


PAINT

A01701 201

DARK OLIVE DRAB PAINT ON METAL

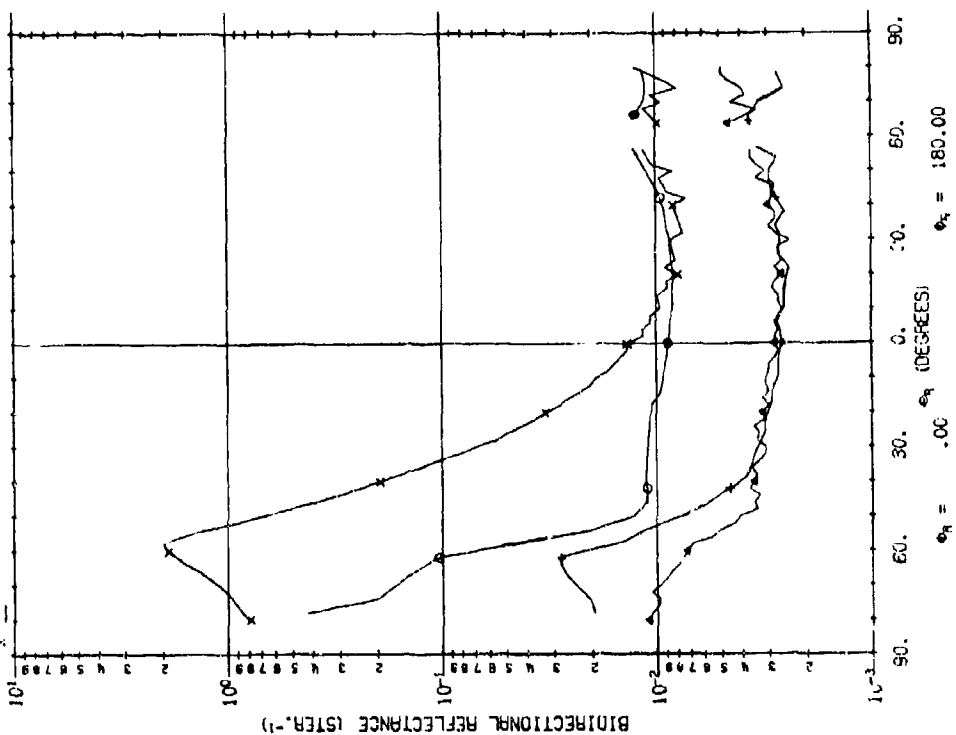
$\theta_i = 30.0$   
 $\theta_r = 180.0$   
 $\phi = 0.63$

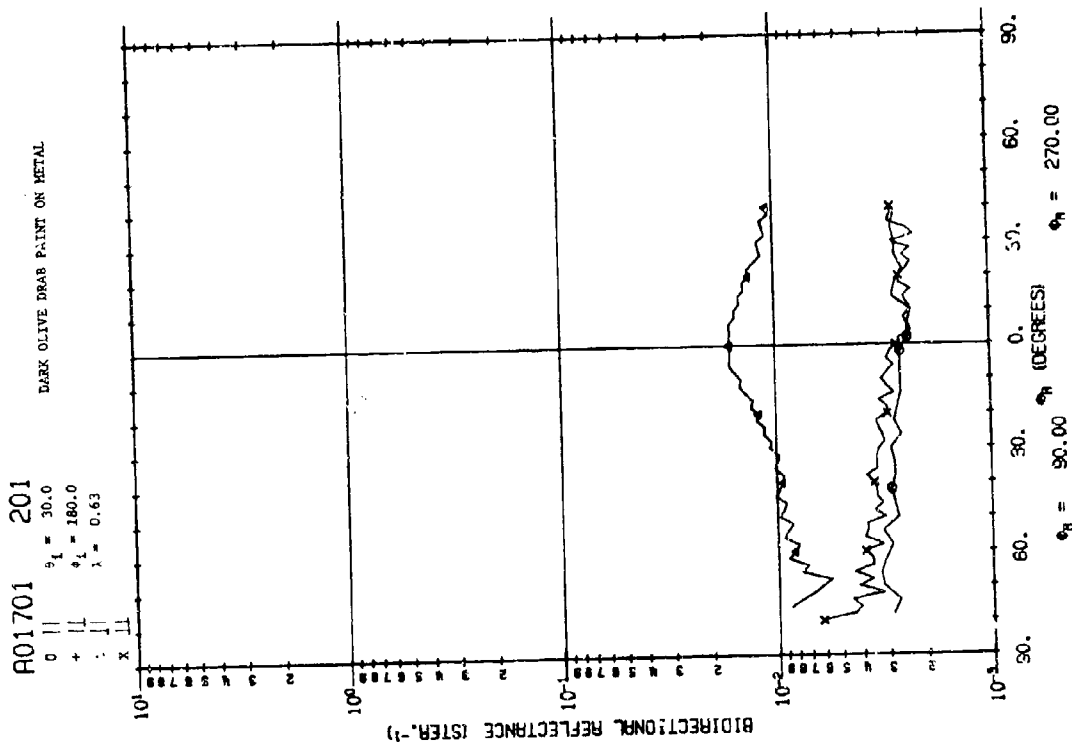
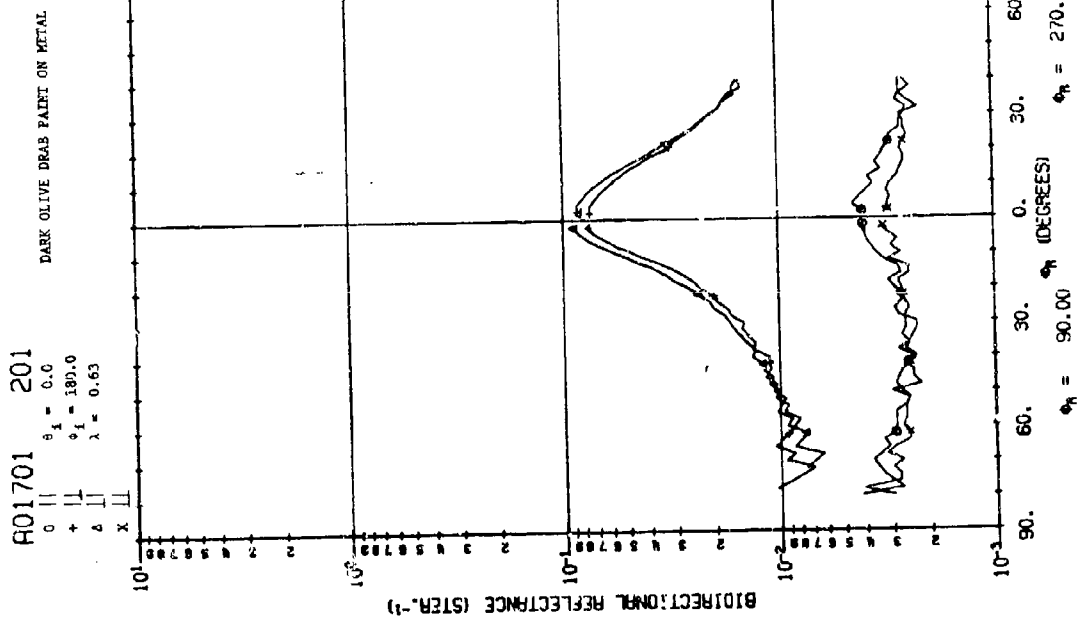


A01701 201

DARK OLIVE DRAB PAINT ON METAL

$\theta_i = 60.0$   
 $\theta_r = 180.0$   
 $\phi = 0.63$



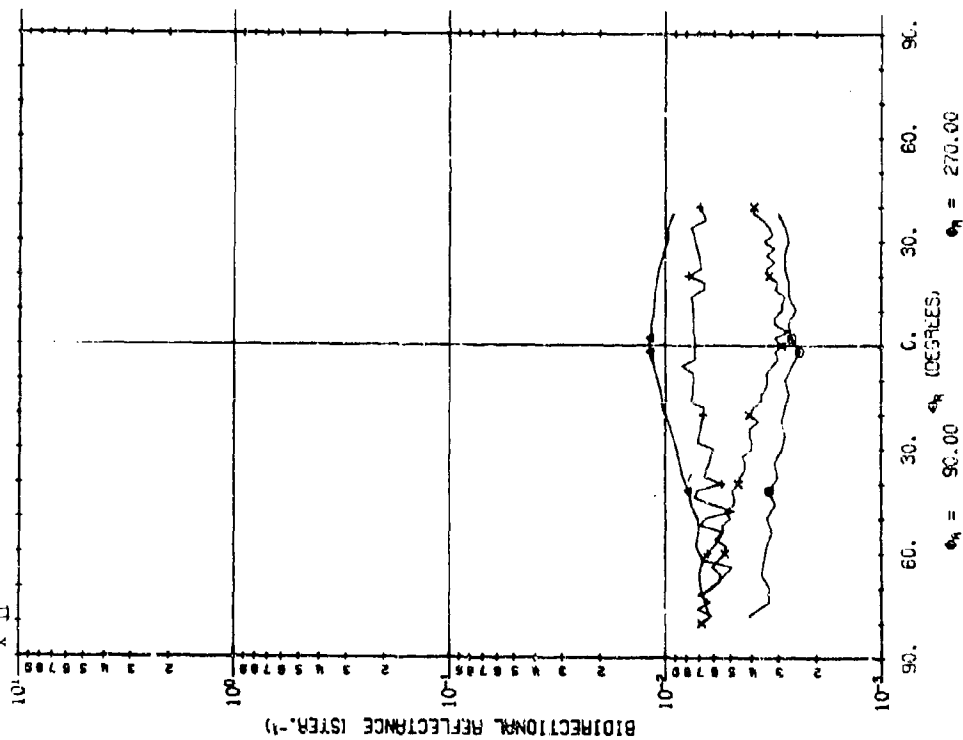


PAINT

R01701 201

DARK OLIVE DRAB PAINT ON METAL

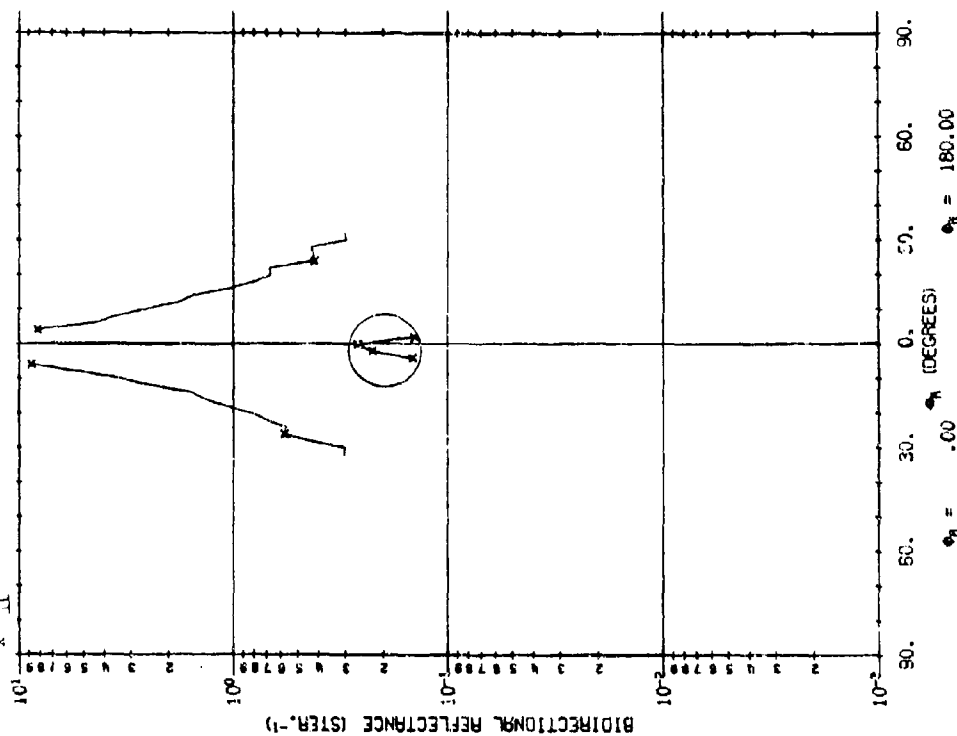
0 II  $\epsilon_1 = 60.0$   
 + II  $\epsilon_1 = 180.0$   
 x II  $\lambda = 0.63$



R01701 101

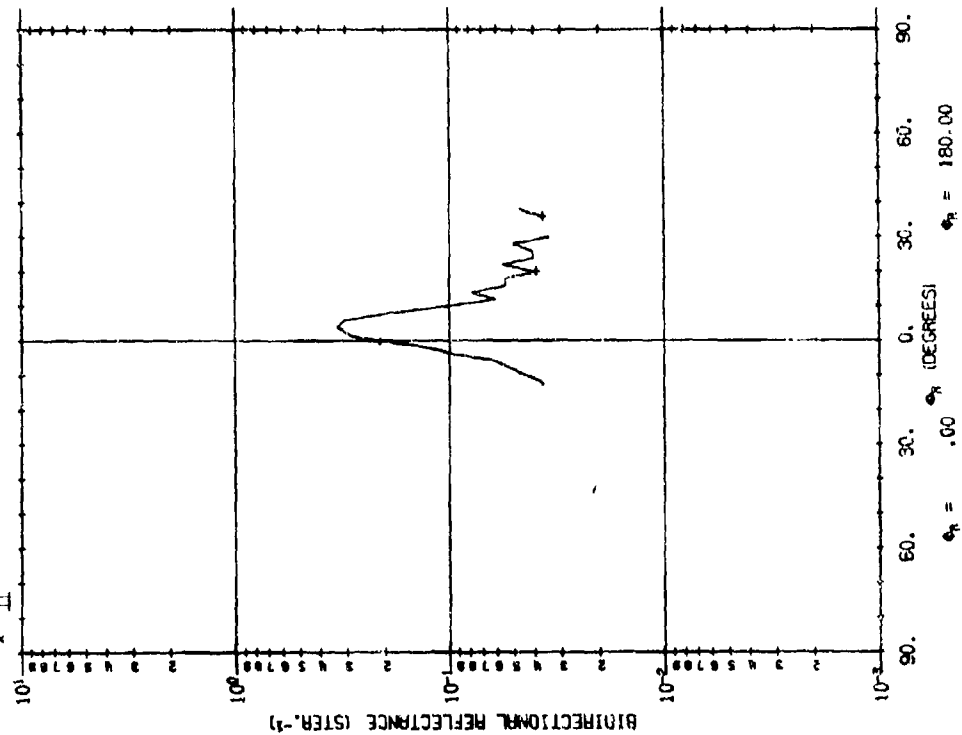
DARK OLIVE DRAB PAINT ON METAL

0 II  $\epsilon_1 = 1.0$   
 + II  $\epsilon_1 = 6.0$   
 x II  $\lambda = 10.6$



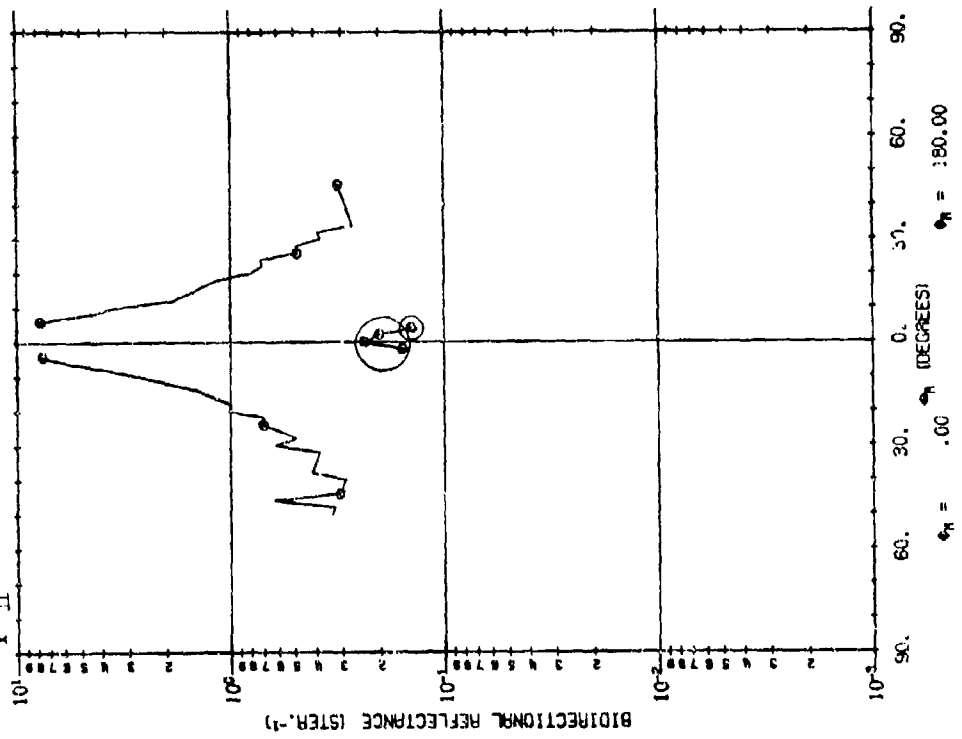
A01701 101  
 0 || 25 = 1.0  
 + ||  $\phi_1 = \phi_2$   
 Δ ||  $\lambda = 10.6$   
 x ||

DARK OLIVE DRAB PAINT ON METAL



A01701 101  
 0 || 25 = 1.0  
 + ||  $\phi_1 = \phi_2$   
 Δ ||  $\lambda = 10.6$   
 x ||

DARK OLIVE DRAB PAINT ON METAL



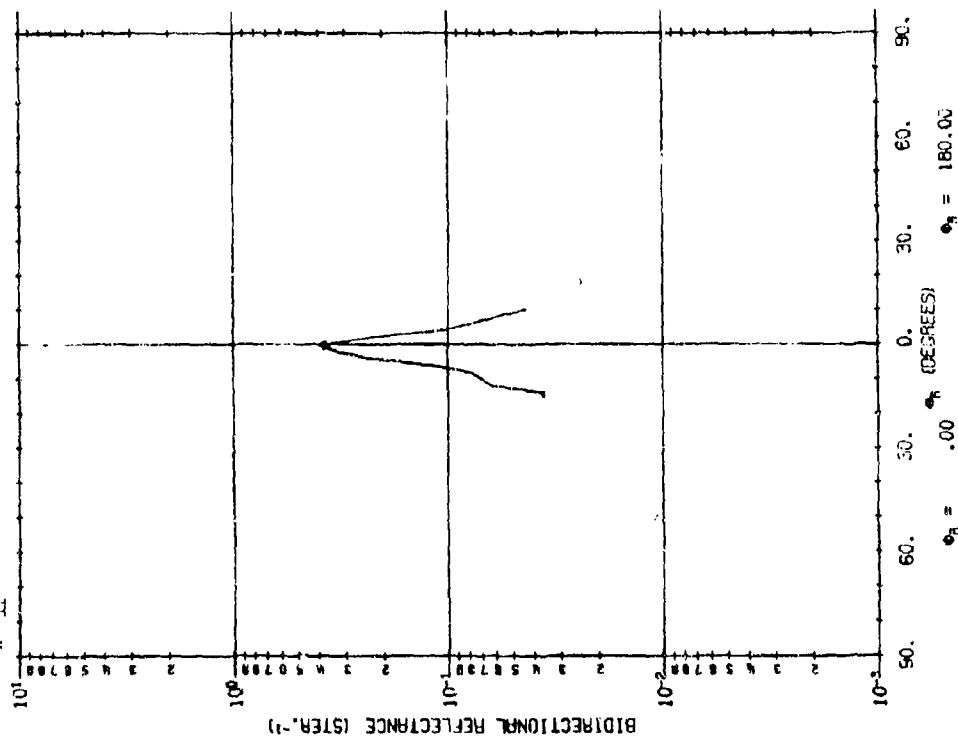
PAINT

R01701 101

DARK OLIVE DRAB PAINT ON METAL

$2\theta = 1.0$   
 $\phi_1 = \phi_r$   
 $\lambda = 10.6$

0 11  
 + 11  
 x 11

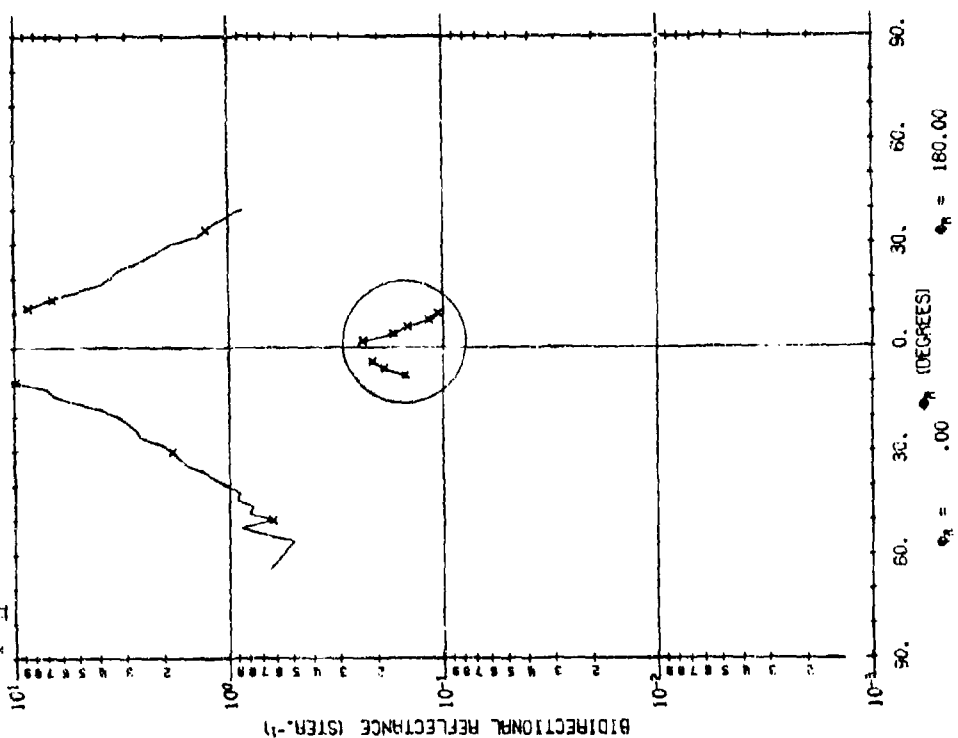


R01701 101

DARK OLIVE DRAB PAINT ON METAL

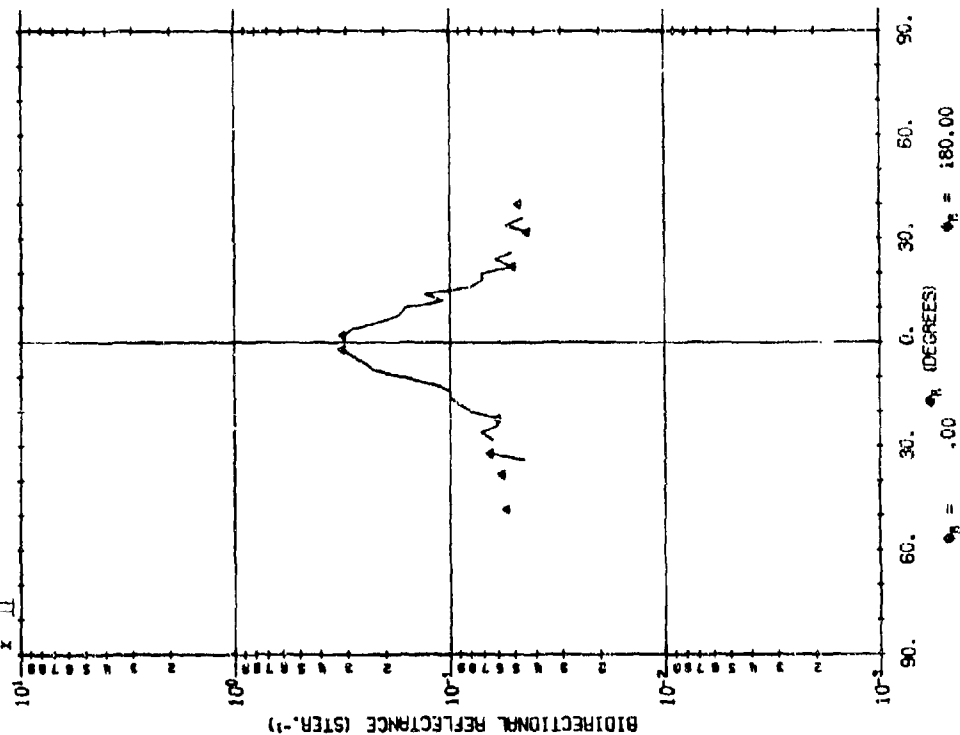
$2\theta = 0.0$   
 $\phi_1 = 180.0$   
 $\lambda = 10.6$

0 11  
 + 11  
 x 11



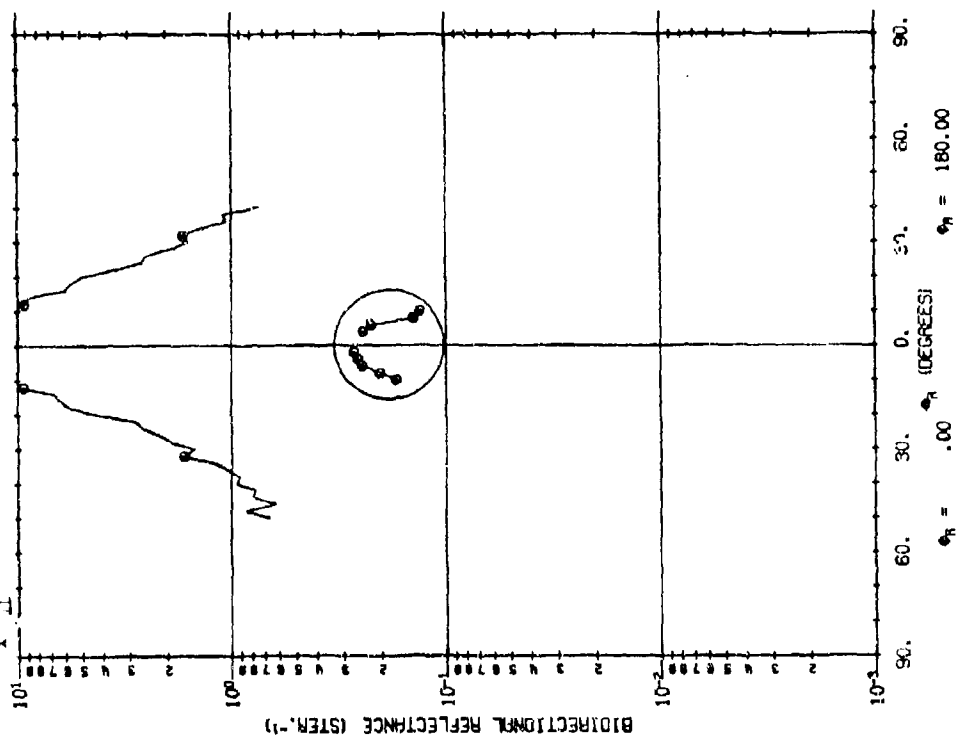
R01701 101

DARK OLIVE DRAB PAINT ON METAL  
 $\theta_1 = 0.0$   
 $\phi_1 = 180.0$   
 $\lambda = 10.6$



R01701 101

DARK OLIVE DRAB PAINT ON METAL  
 $\theta_1 = 0.0$   
 $\phi_1 = 180.0$   
 $\lambda = 10.6$



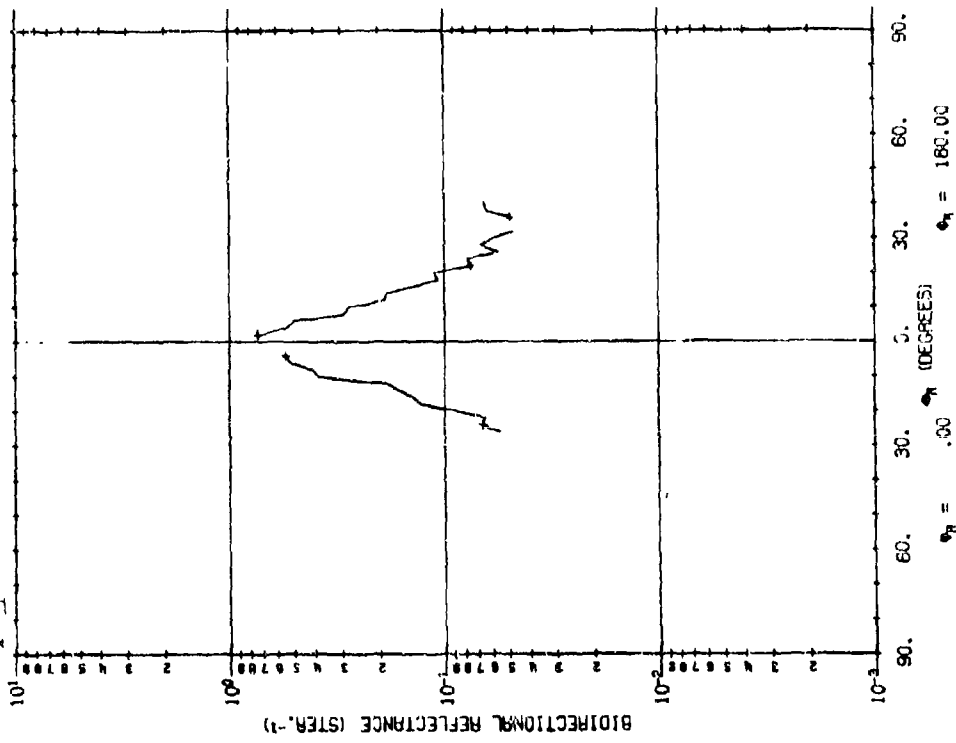
PAINT



AO1701 101

DARK OLIVE DRAB PAINT ON METAL

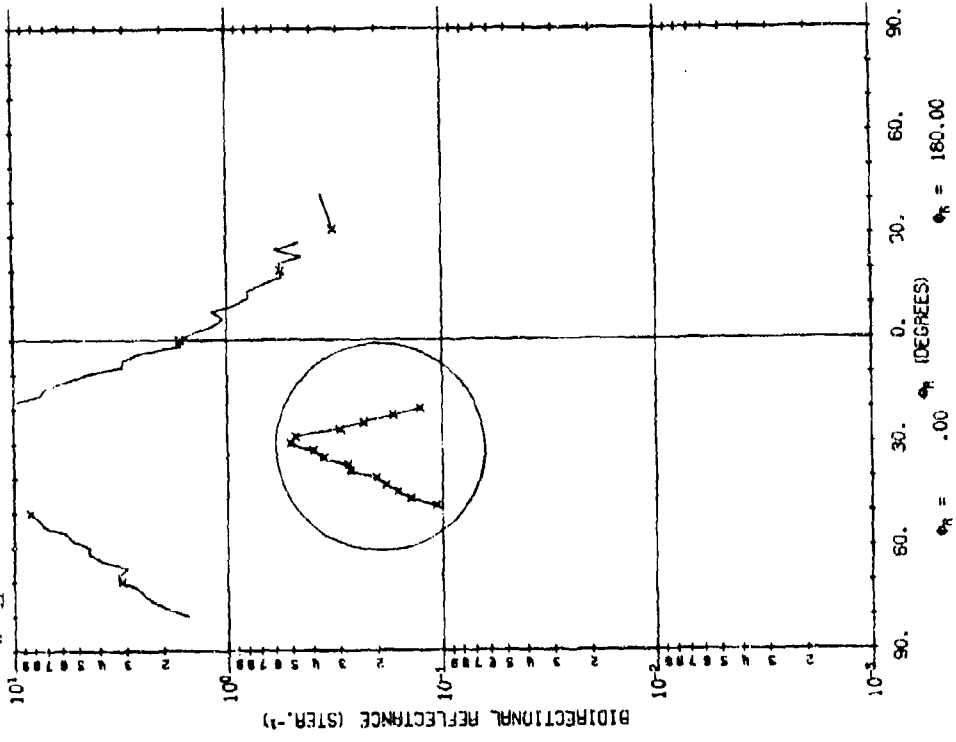
$\theta_i = 0.0$   
 $\theta_r = 180.0$   
 $\lambda = 10.6$



AO1701 101

DARK OLIVE DRAB PAINT ON METAL

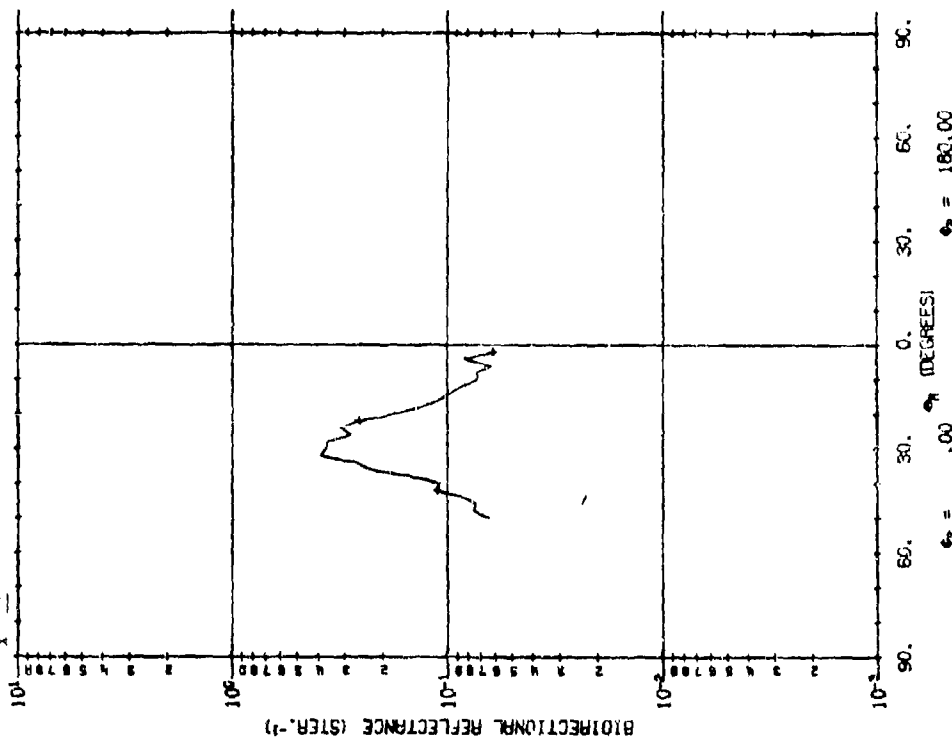
$\theta_i = 30.0$   
 $\theta_r = 180.0$   
 $\lambda = 10.6$



R01701 101  
 0 11  
 + 11  
 A 11  
 X 11

DARK OLIVE DRAB PAINT ON METAL

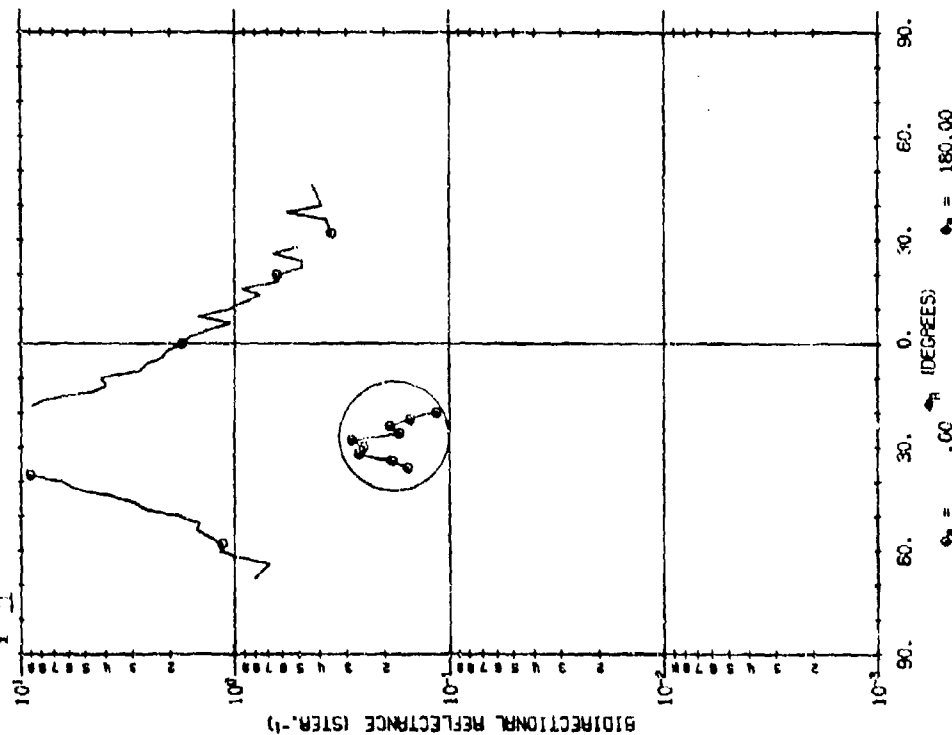
$\theta_1 = 30.0$   
 $\theta_2 = 180.0$   
 $\lambda = 10.6$



R01701 101  
 0 11  
 + 11  
 A 11  
 X 11

DARK OLIVE DRAB PAINT ON METAL

$\theta_1 = 30.0$   
 $\theta_2 = 180.0$   
 $\lambda = 10.6$

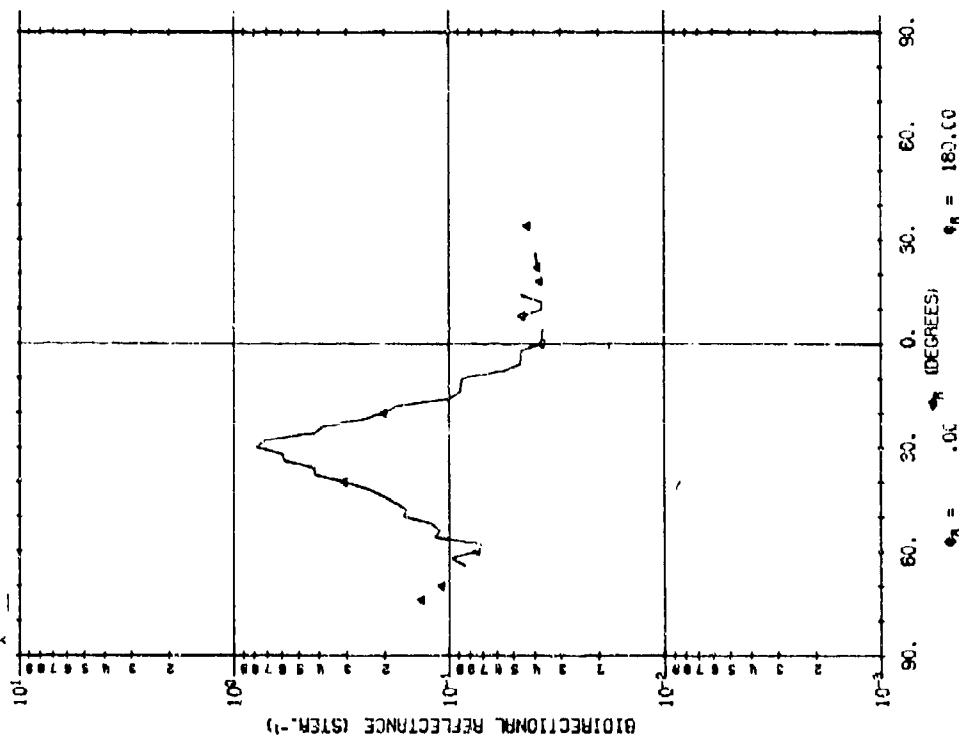


PAINT

R01/01 101

DARK OLIVE DRAB PAINT ON METAL

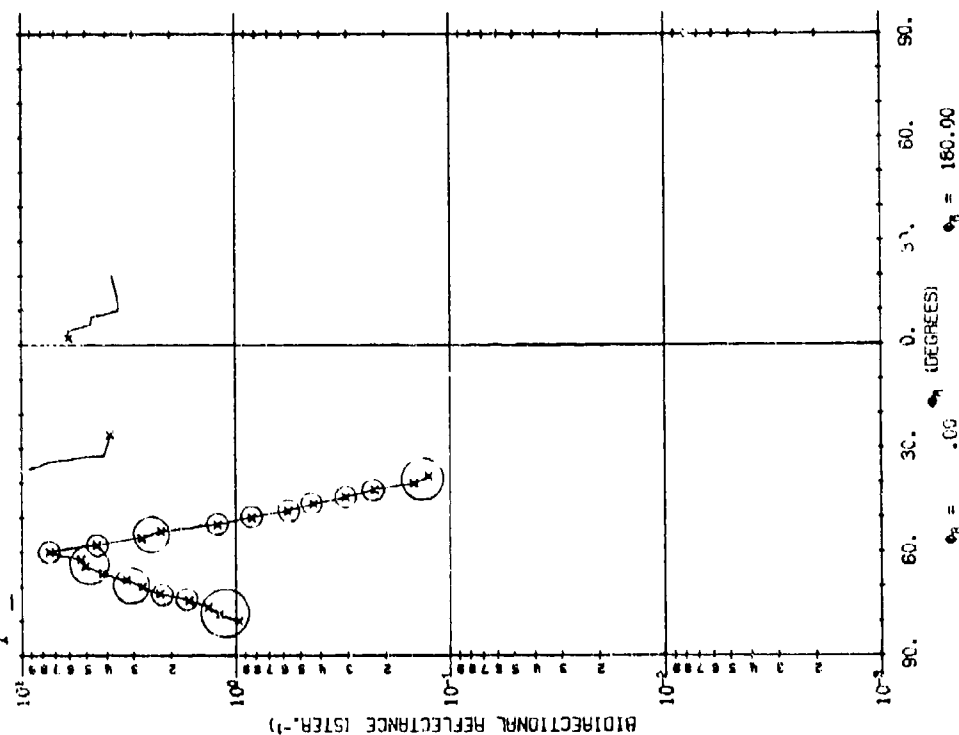
$\theta_1 = 30.0$   
 $\theta_2 = 180.0$   
 $\lambda = 10.6$



R01/01 101

DARK OLIVE DRAB PAINT ON METAL

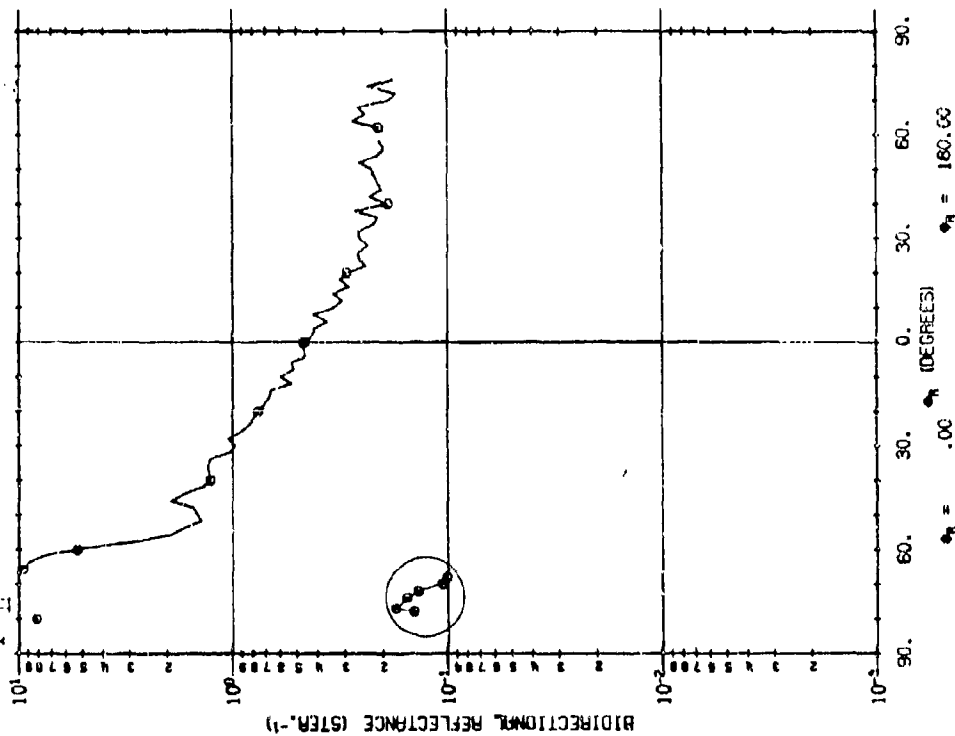
$\theta_1 = 60.0$   
 $\theta_2 = 180.0$   
 $\lambda = 10.6$



R01701 101

DARK OLIVE DRAB PAINT ON METAL

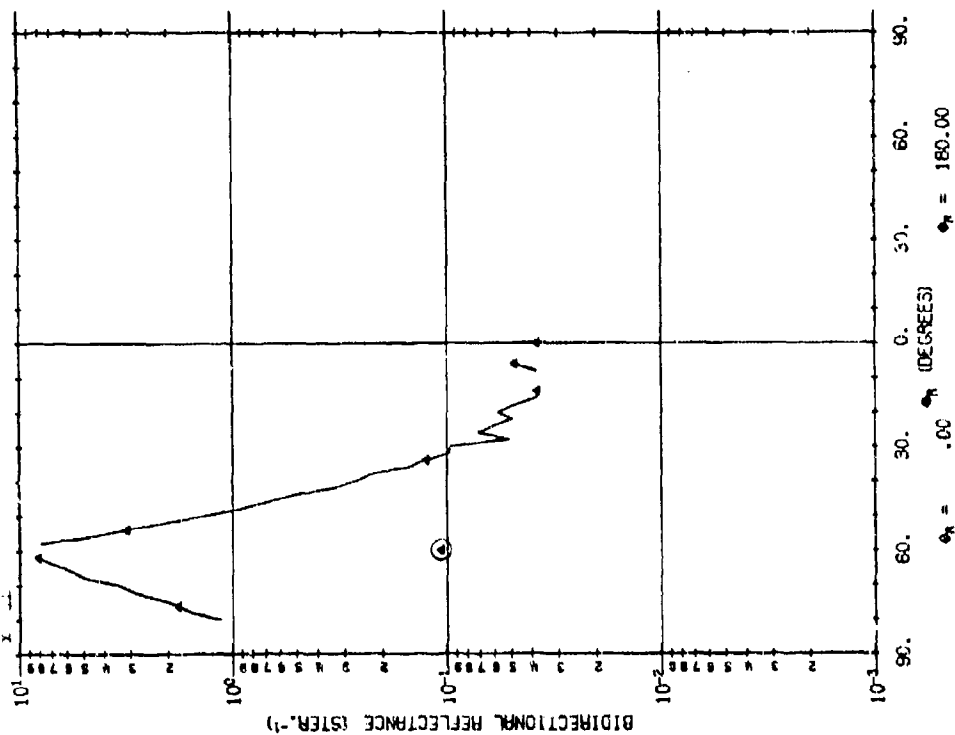
$\theta_1 = 60.0$   
 $\phi_1 = 180.0$   
 $\lambda = 10.6$



R01701 101

DARK OLIVE DRAB PAINT ON METAL

$\theta_1 = 60.0$   
 $\phi_1 = 180.0$   
 $\lambda = 10.6$

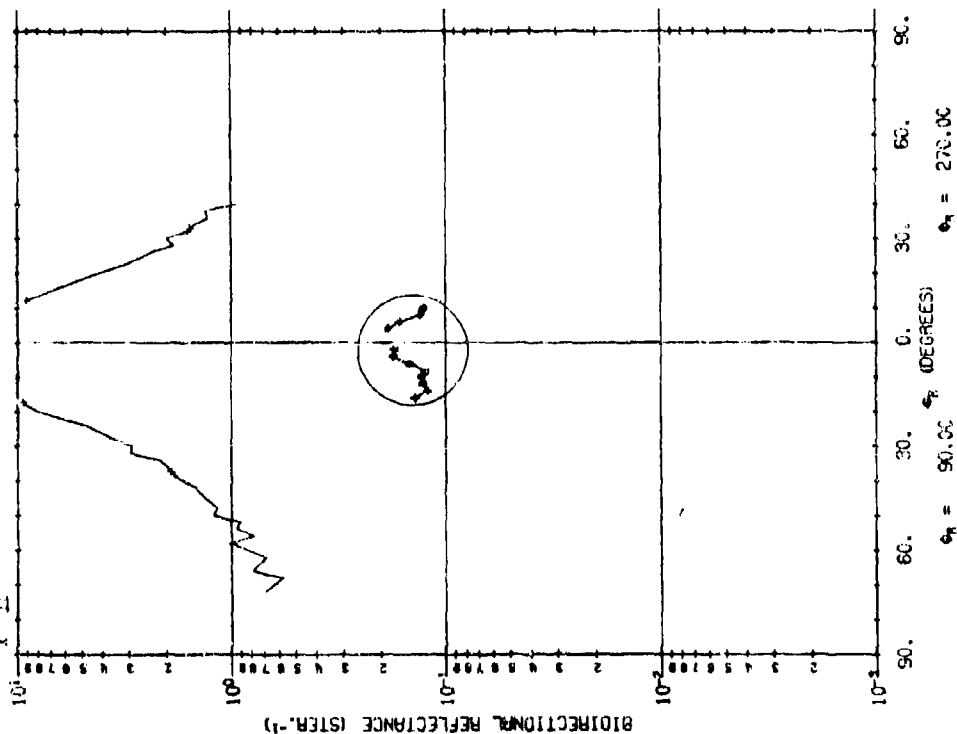


PAINT

801701 101

DARK OLIVE DRAB PAINT ON METAL

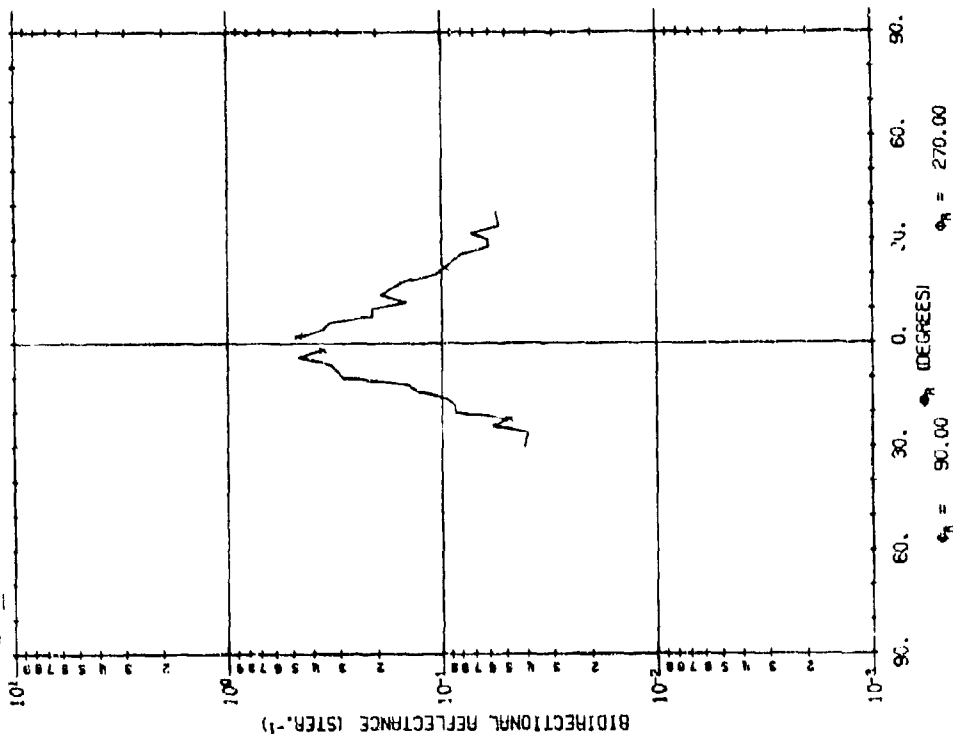
$\epsilon_1 = 0.0$   
 $\epsilon_2 = 0.0$   
 $\epsilon_3 = 10.6$

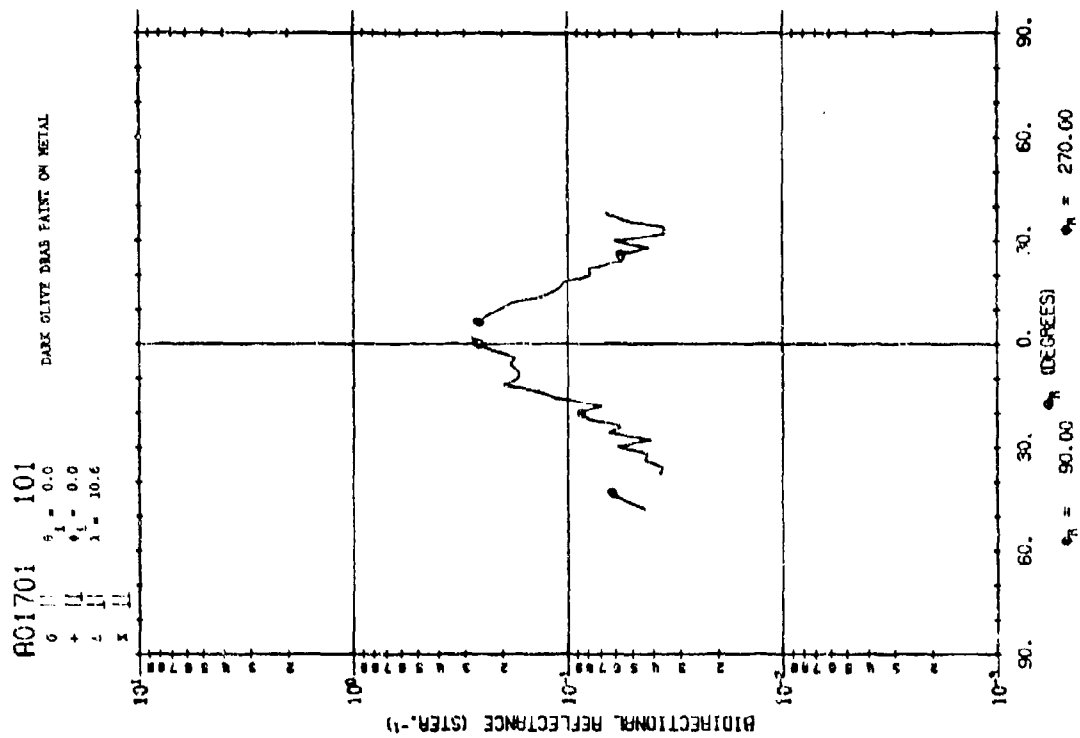
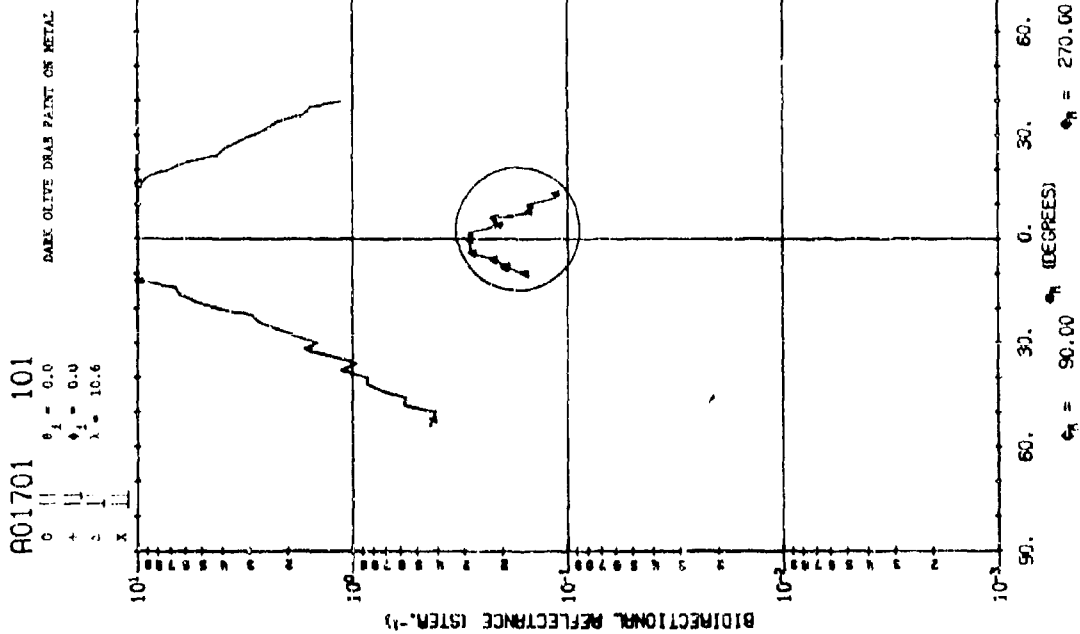


801701 101

DARK OLIVE DRAB PAINT ON METAL

$\epsilon_1 = 0.0$   
 $\epsilon_2 = 0.0$   
 $\epsilon_3 = 10.6$



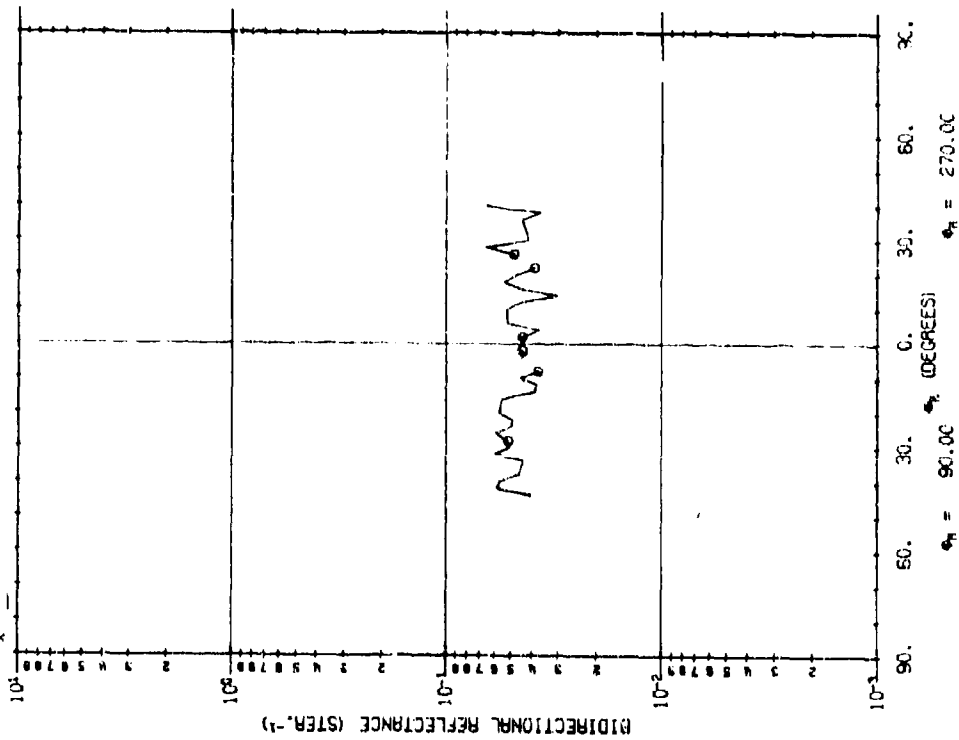


PAINT

RO1701 101

DARK OLIVE DRAB PAINT ON METAL

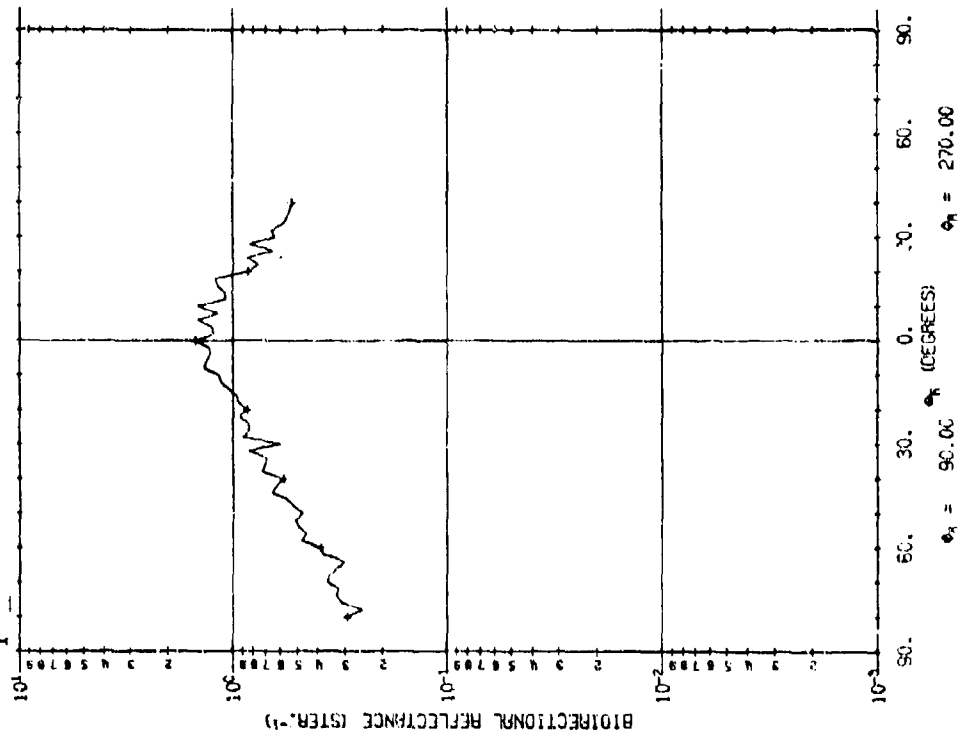
$\theta_1 = 59.0$   
 $\theta_2 = 0.0$   
 $\lambda = 10.6$



RO1701 101

DARK OLIVE DRAB PAINT ON METAL

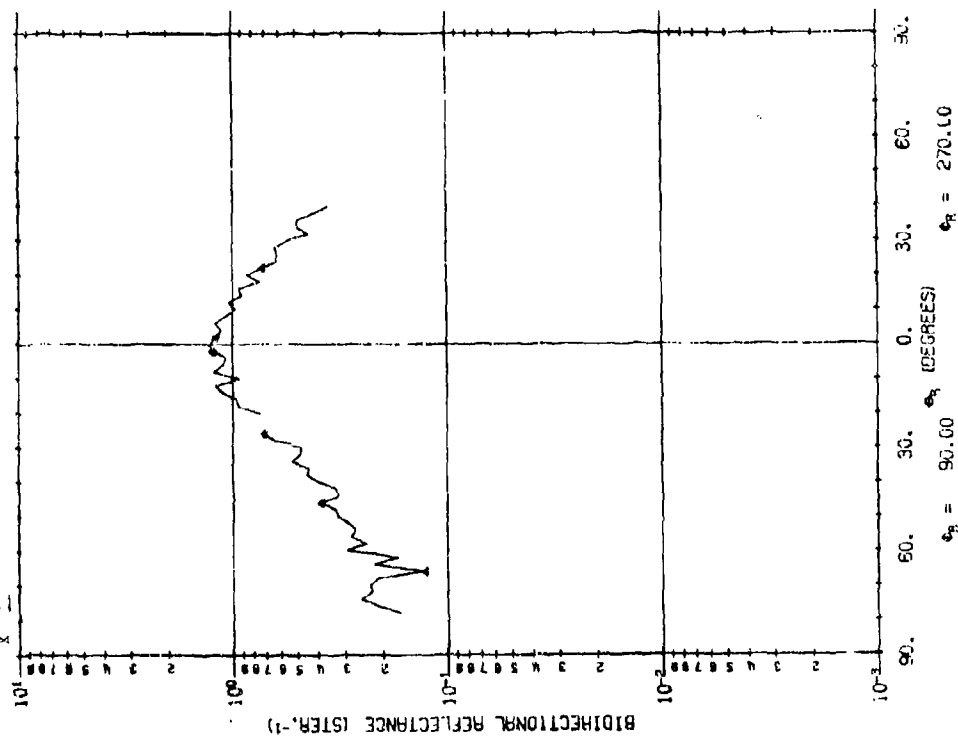
$\theta_1 = 30.0$   
 $\theta_2 = 0.0$   
 $\lambda = 10.6$



A01701 101

DARK OLIVE DRAB PAINT ON METAL

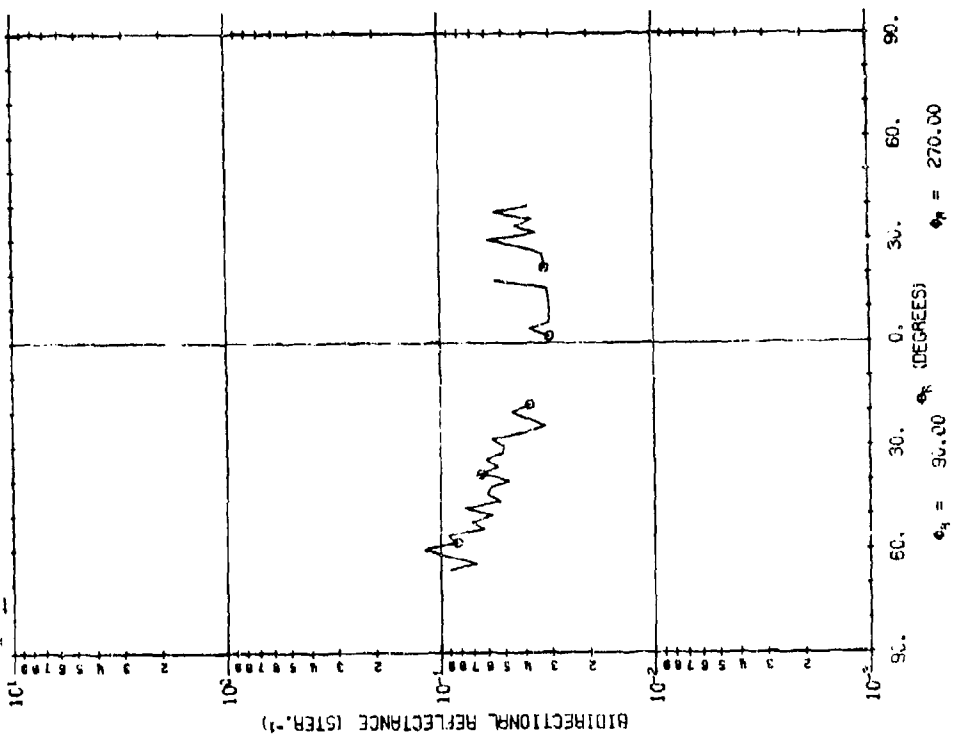
$\phi_1 = 30.0$   
 $\phi_2 = 0.0$   
 $\lambda = 10.6$



A01701 101

DARK OLIVE DRAB PAINT ON METAL

$\phi_1 = 60.0$   
 $\phi_2 = 0.0$   
 $\lambda = 10.6$



PAINT



RC1701 101

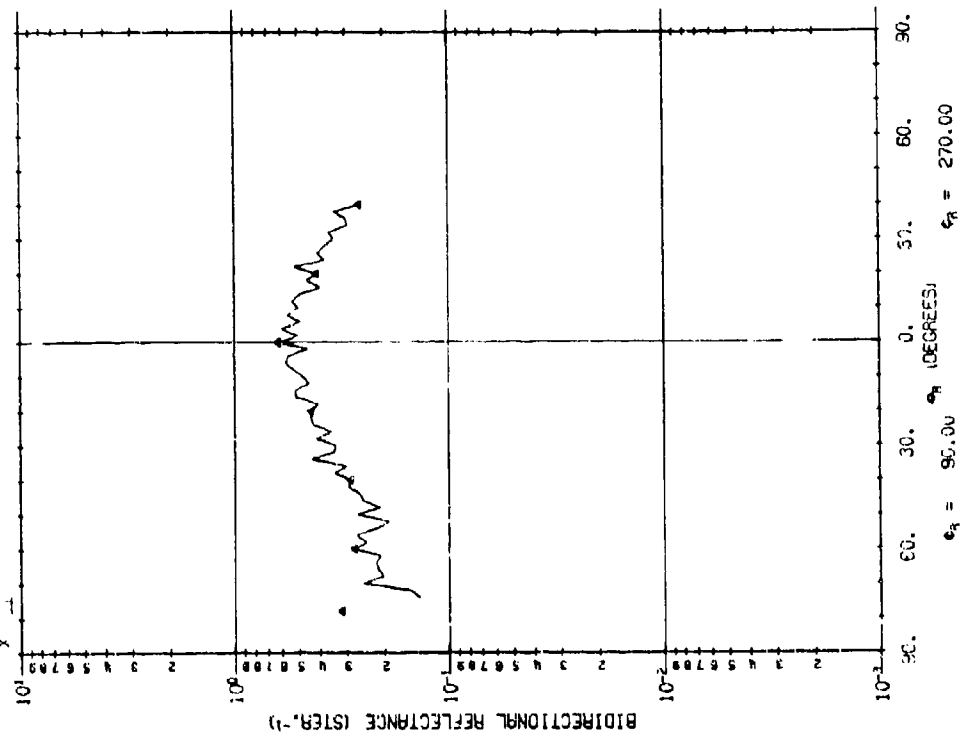
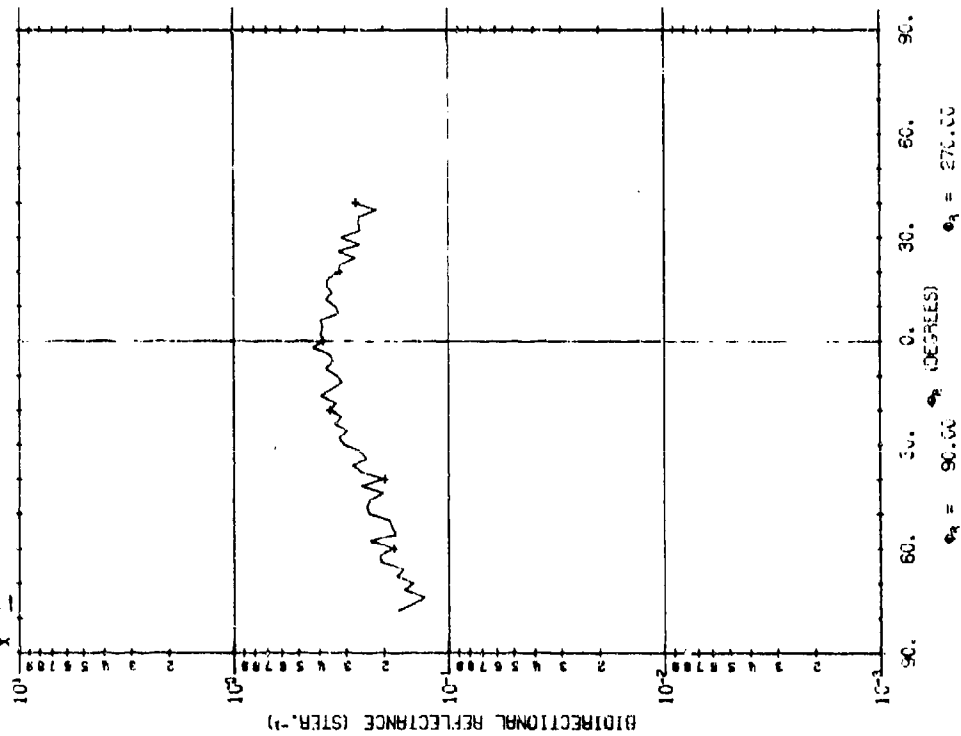
DARK OLIVE DEAR PAINT ON METAL

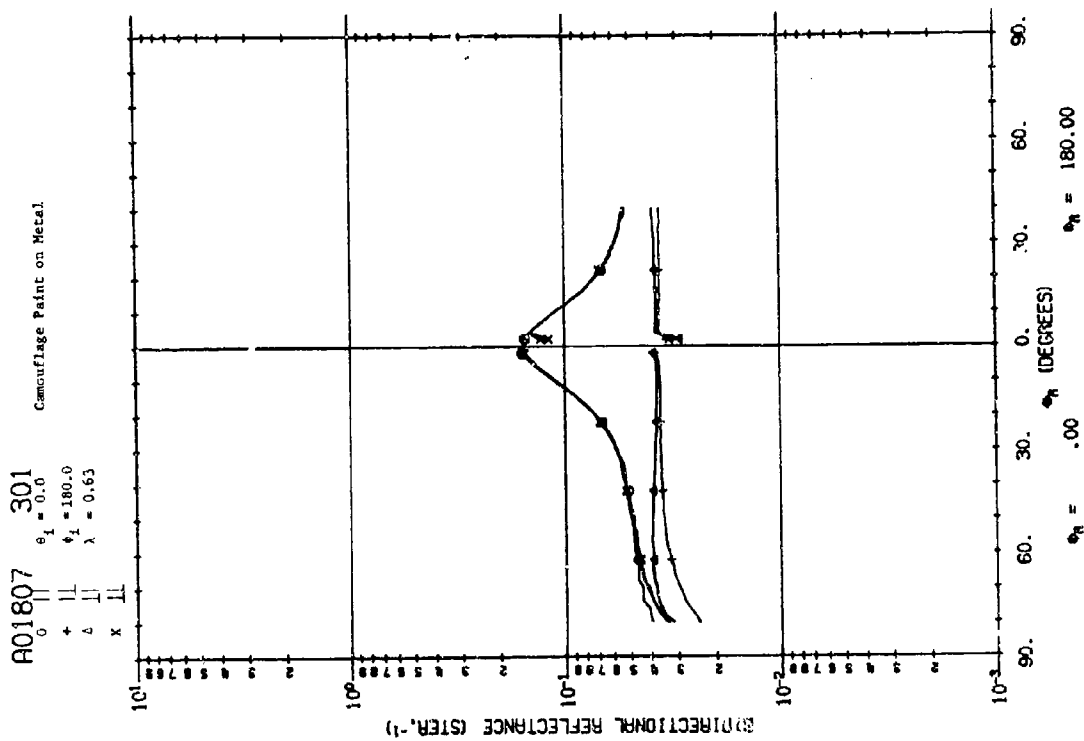
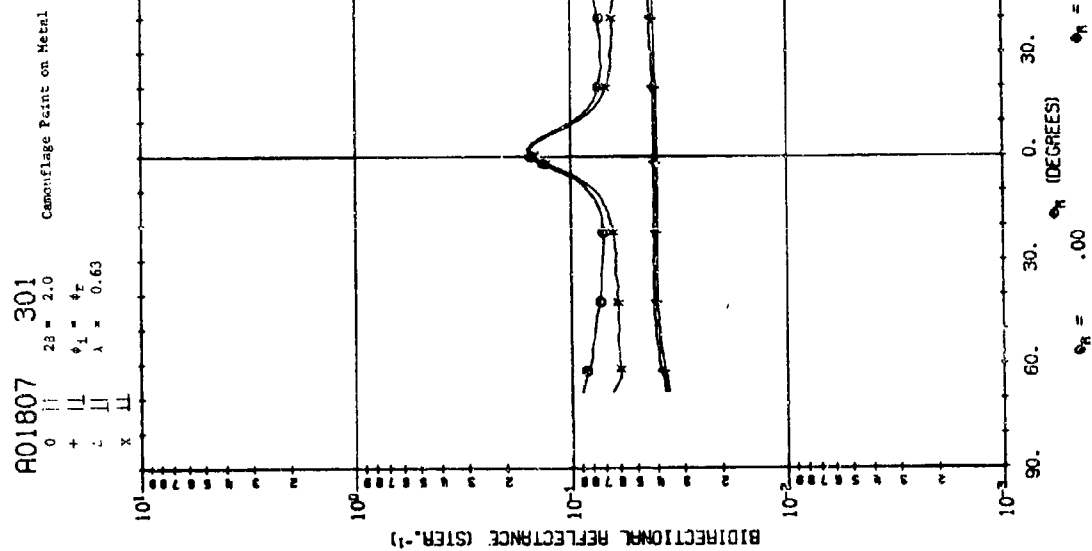
$\theta_1 = 60.0$   
 $\theta_2 = 0.0$   
 $\lambda = 10.6$

DARK OLIVE DEAR PAINT ON METAL

RC1701 101

$\theta_1 = 60.0$   
 $\theta_2 = 0.0$   
 $\lambda = 10.6$

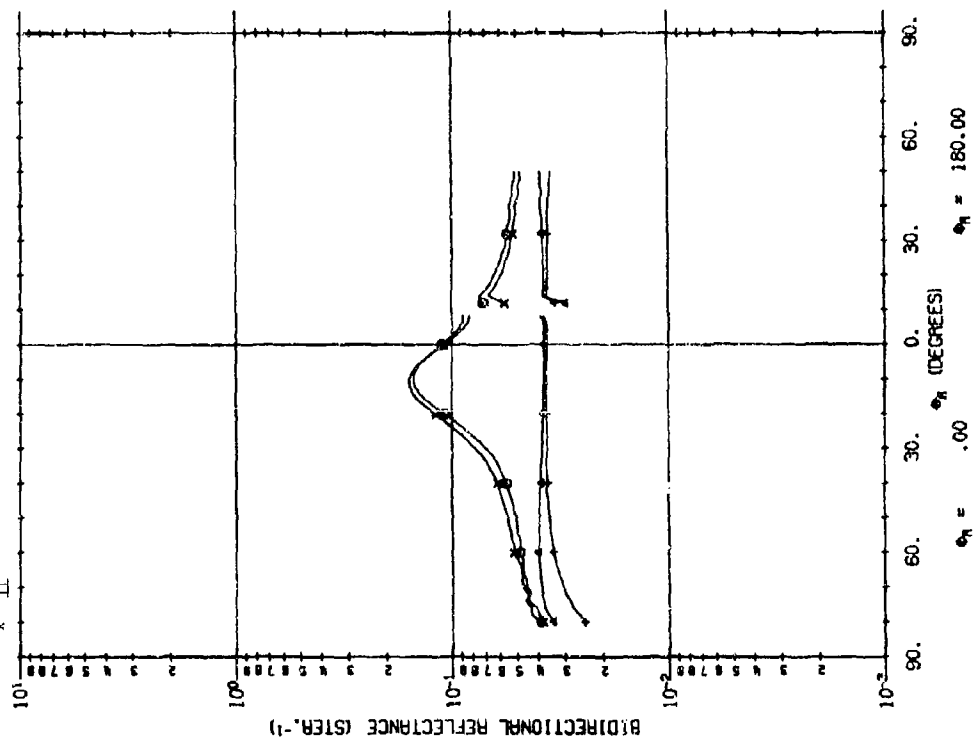




PAINT

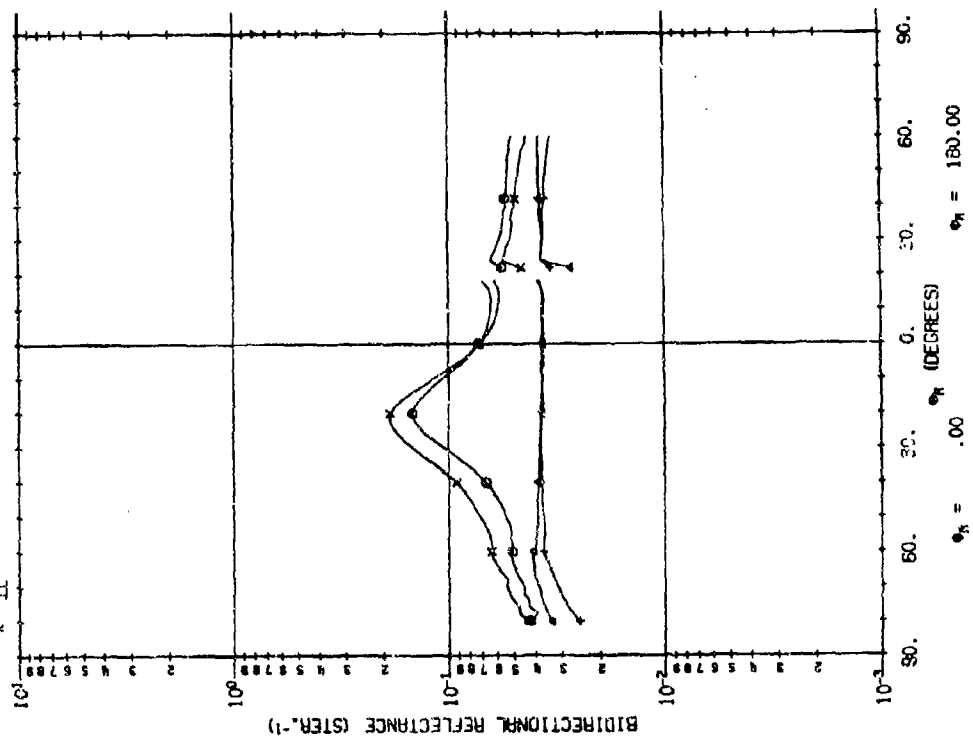
R01807 301  
 $\epsilon_1 = 10.00$   
 $\epsilon_2 = 180.00$   
 $\lambda = 0.63$

Camouflage Paint on Metal

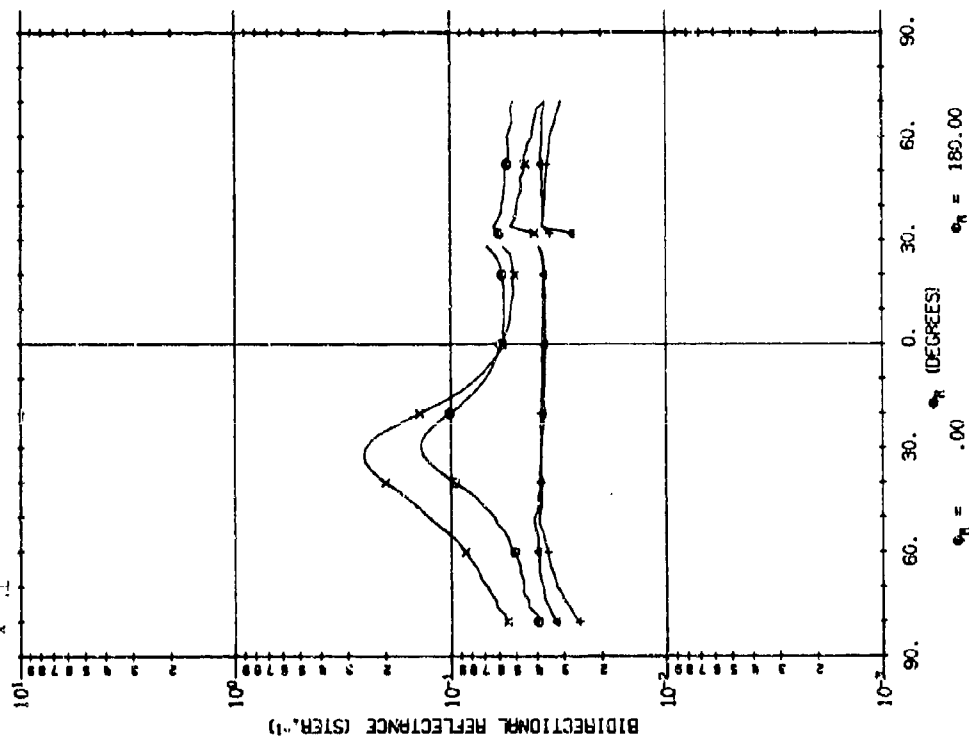


R01807 301  
 $\epsilon_1 = 20.00$   
 $\epsilon_2 = 180.00$   
 $\lambda = 0.63$

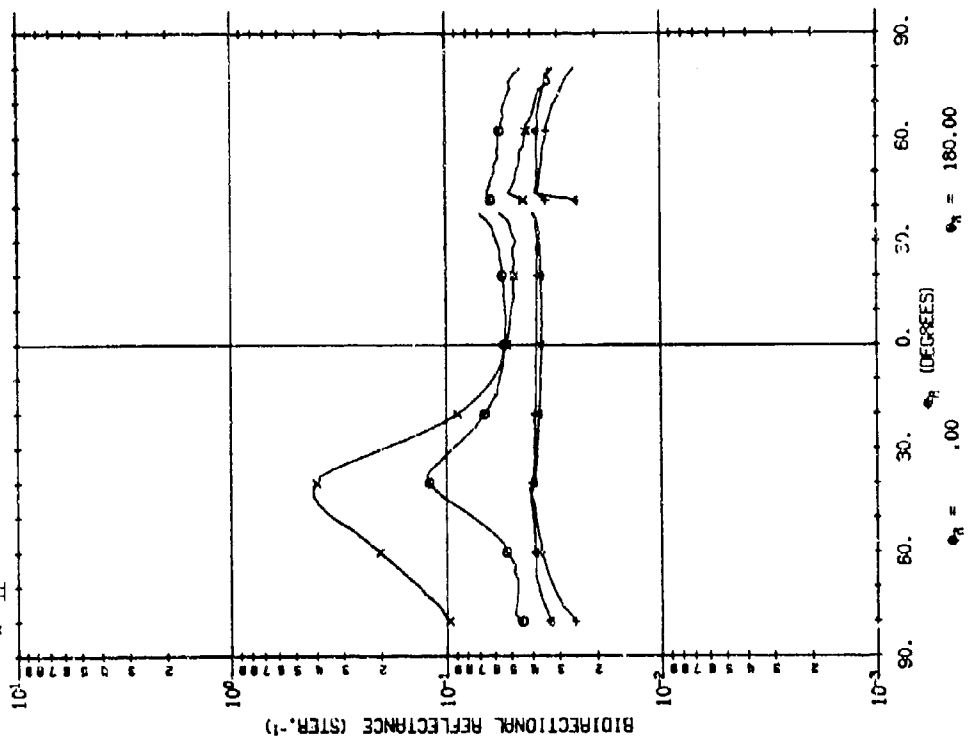
Camouflage Paint on Metal



A01807 301  
Camouflage Paint on Metal  
 $\theta_i = 30.00$   
 $\theta_r = 180.00$   
 $\lambda = 0.63$



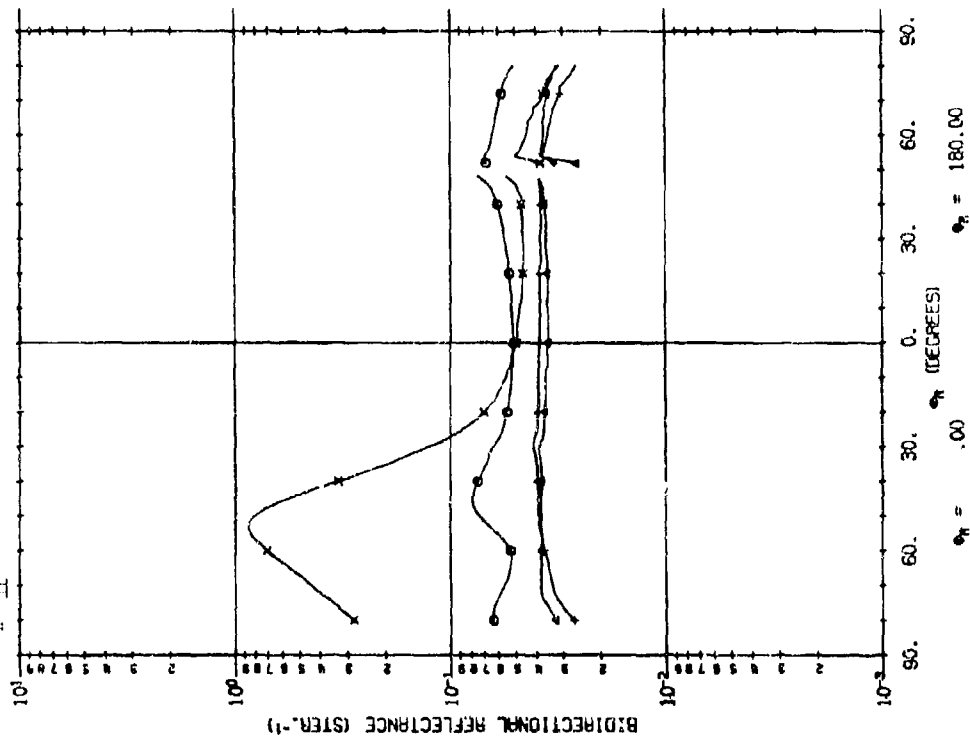
A01807 301  
Camouflage Paint on Metal  
 $\theta_i = 40.00$   
 $\theta_r = 180.00$   
 $\lambda = 0.63$



PAINT

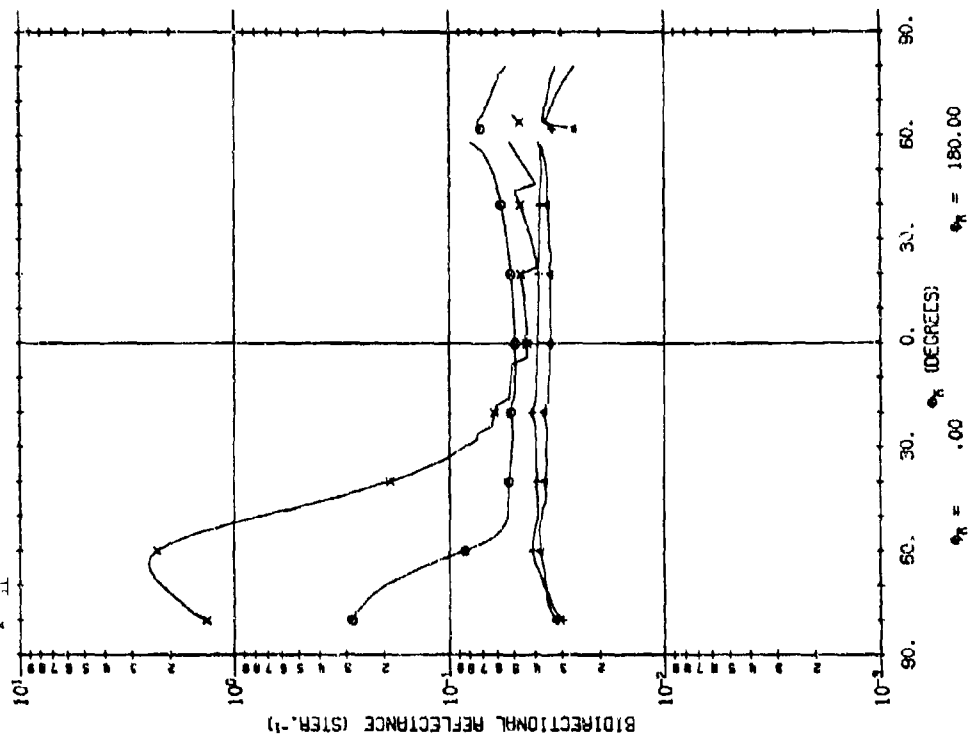
A01807 301  
 0 II  $\theta_i = 50.00$   
 + II  $\theta_r = 180.00$   
 - II  $\lambda = 0.63$   
 x II

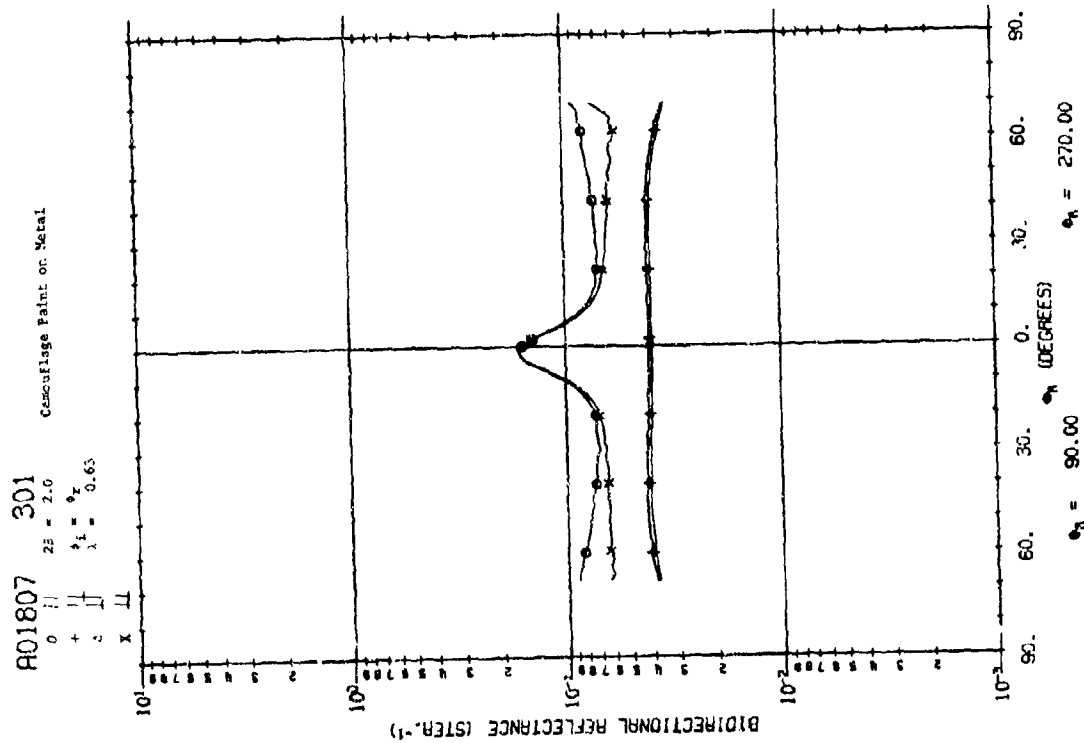
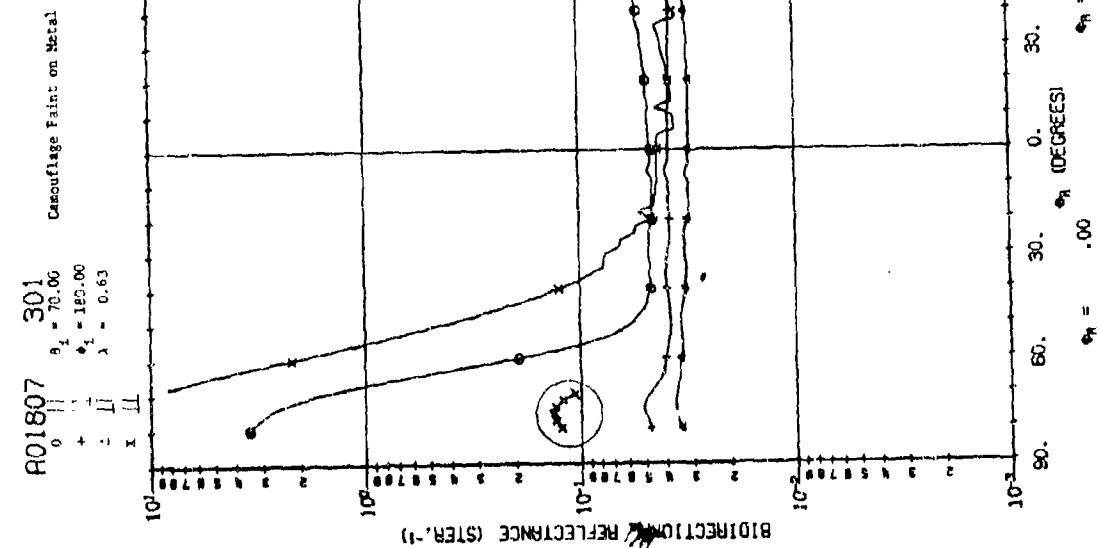
Camouflage Paint on Metal



A01807 301  
 0 II  $\theta_i = 50.00$   
 + II  $\theta_r = 180.00$   
 - II  $\lambda = 0.63$   
 x II

Camouflage Paint on Metal





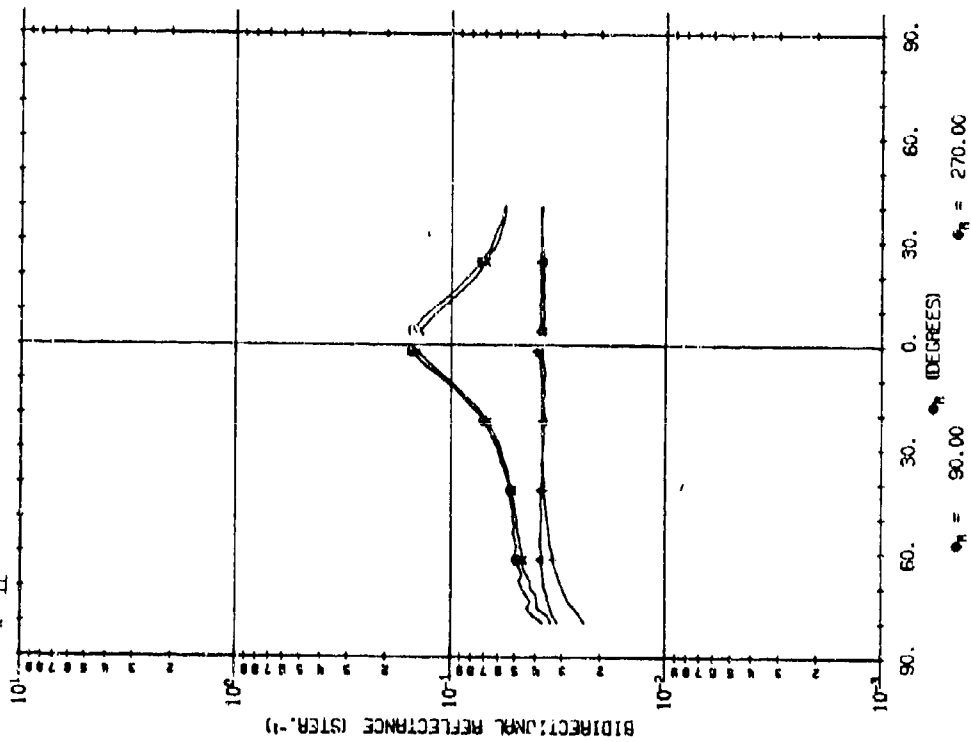
PAINT

R01807 301

Camouflage Paint on Metal

$\theta_i = 0.0$   
 $\theta_r = 270.00$   
 $\lambda = 0.63$

0 II  
 + II  
 - II  
 x II

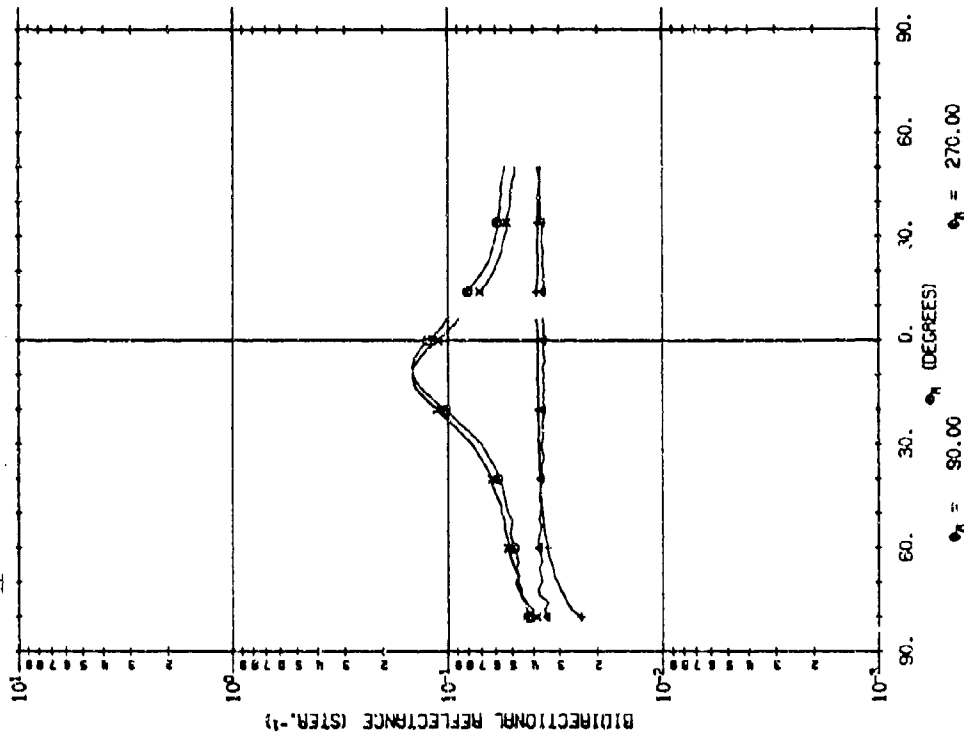


R01807 301

Camouflage Paint on Metal

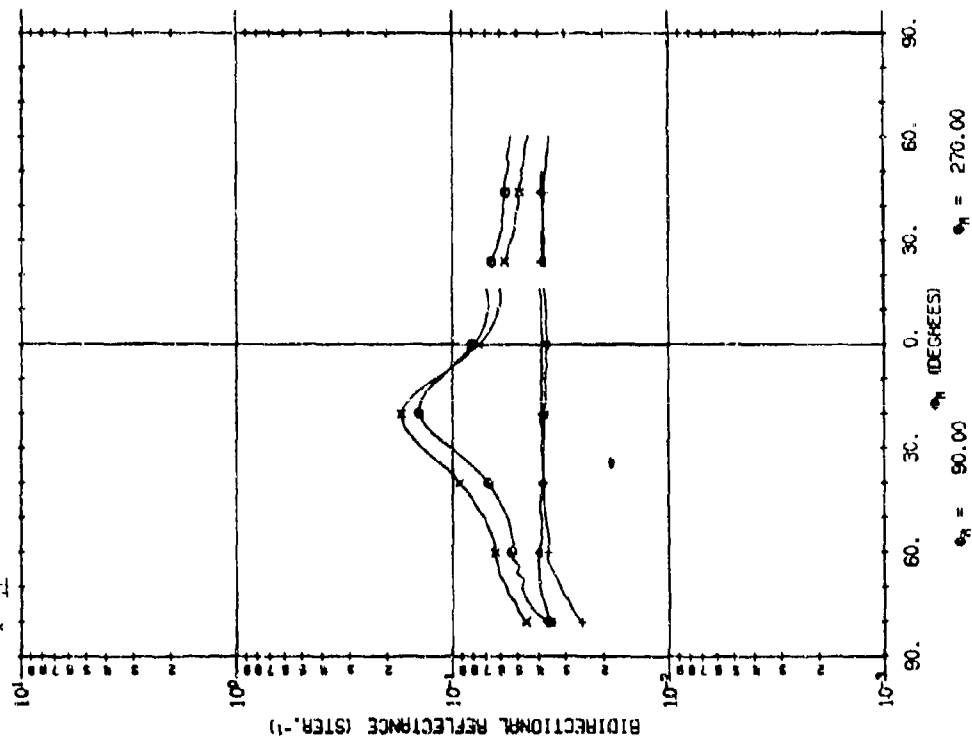
$\theta_i = 10.00$   
 $\theta_r = 270.00$   
 $\lambda = 0.63$

0 II  
 + II  
 - II  
 x II



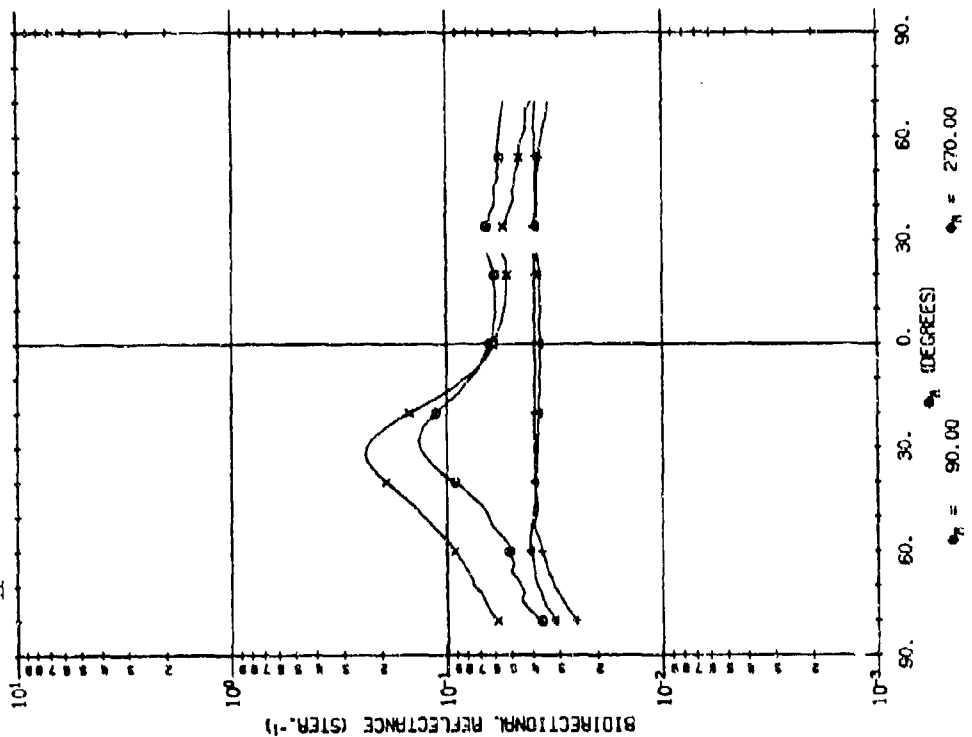
R01807 301  
 $\epsilon_1 = 20.00$   
 $\phi_1 = 270.00$   
 $\lambda = 0.63$

Camouflage Paint on Metal



R01807 301  
 $\epsilon_1 = 30.00$   
 $\phi_1 = 270.00$   
 $\lambda = 0.63$

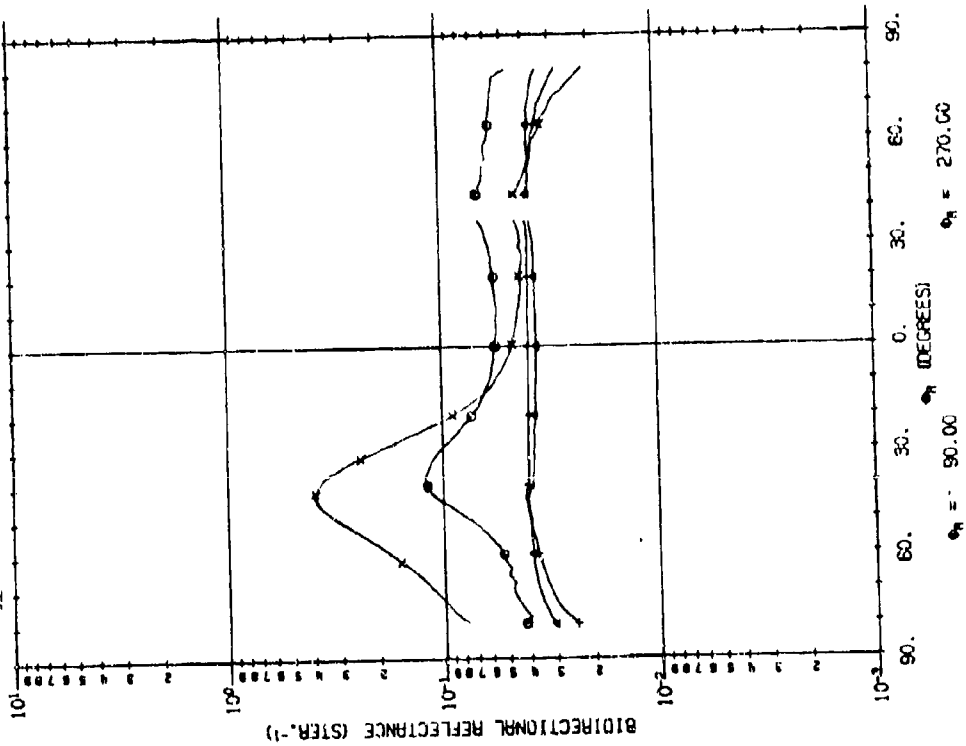
Camouflage Paint on Metal



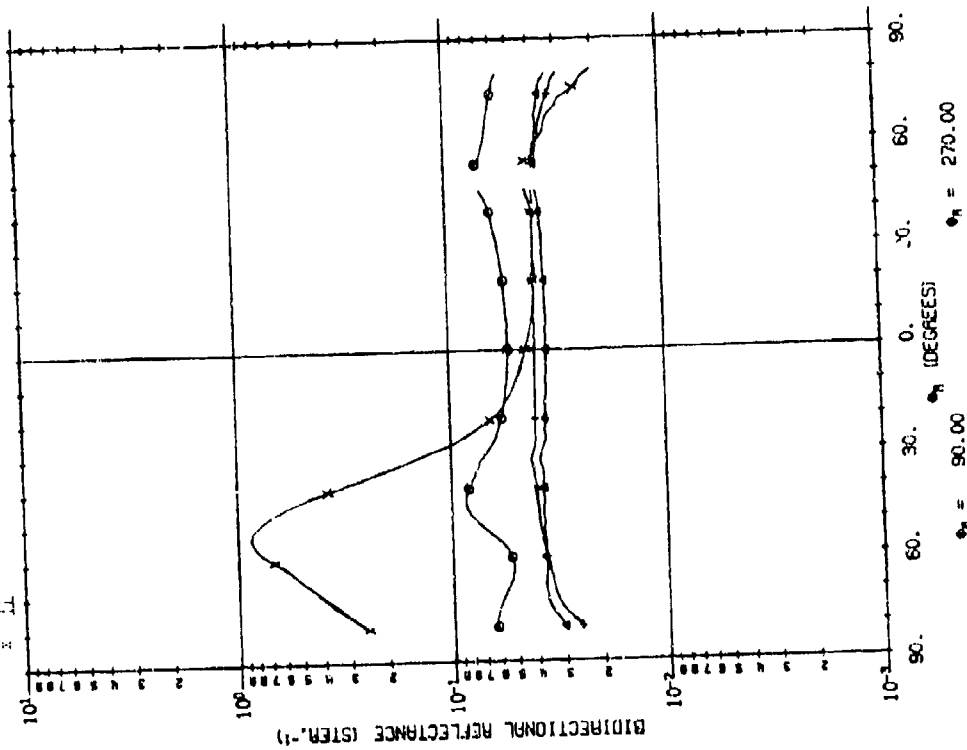
PAINT

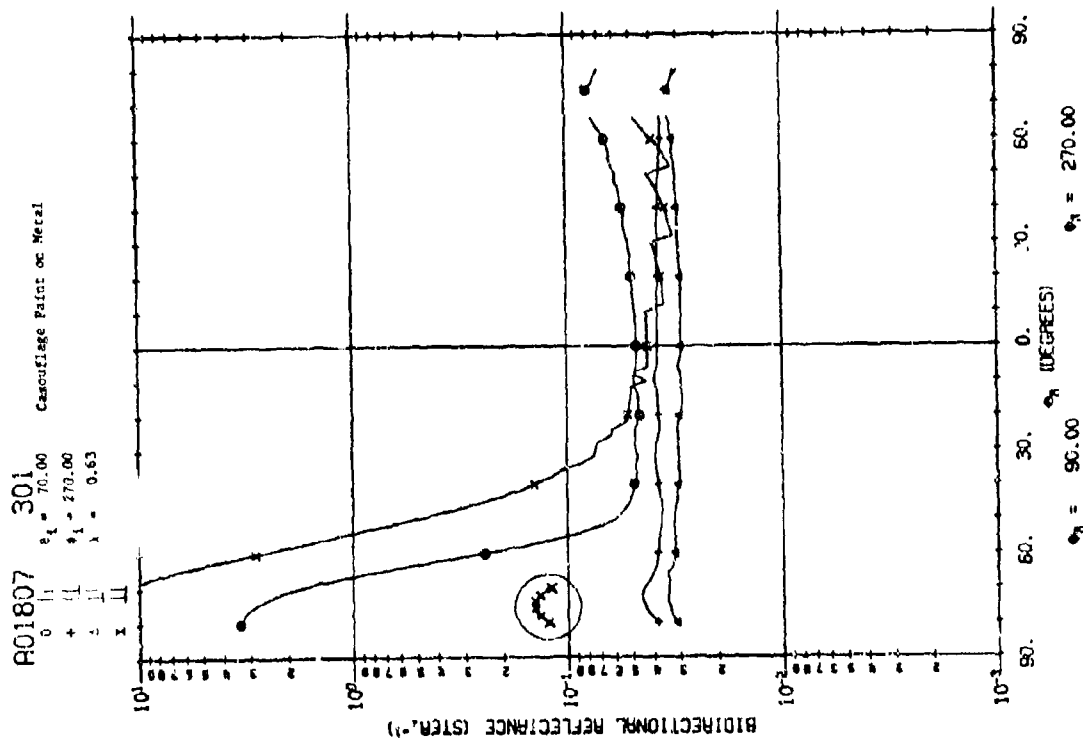
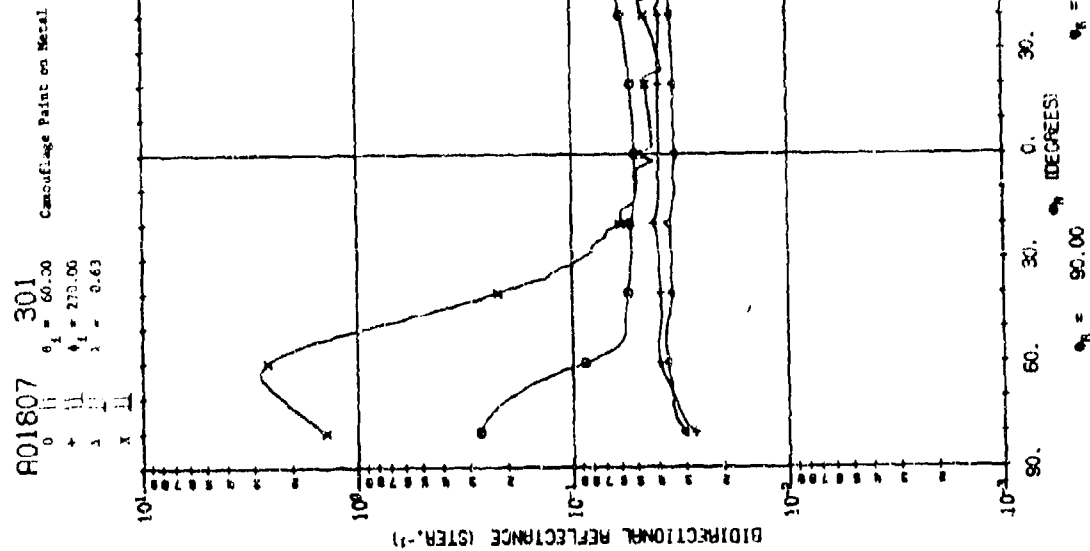


A01807 301 Camouflage Paint on Metal  
 $\epsilon_1 = 40.00$   
 $\epsilon_2 = 270.00$   
 $\lambda = 0.63$



A01807 301 Camouflage Paint on Metal  
 $\epsilon_1 = 50.00$   
 $\epsilon_2 = 270.00$   
 $\lambda = 0.63$



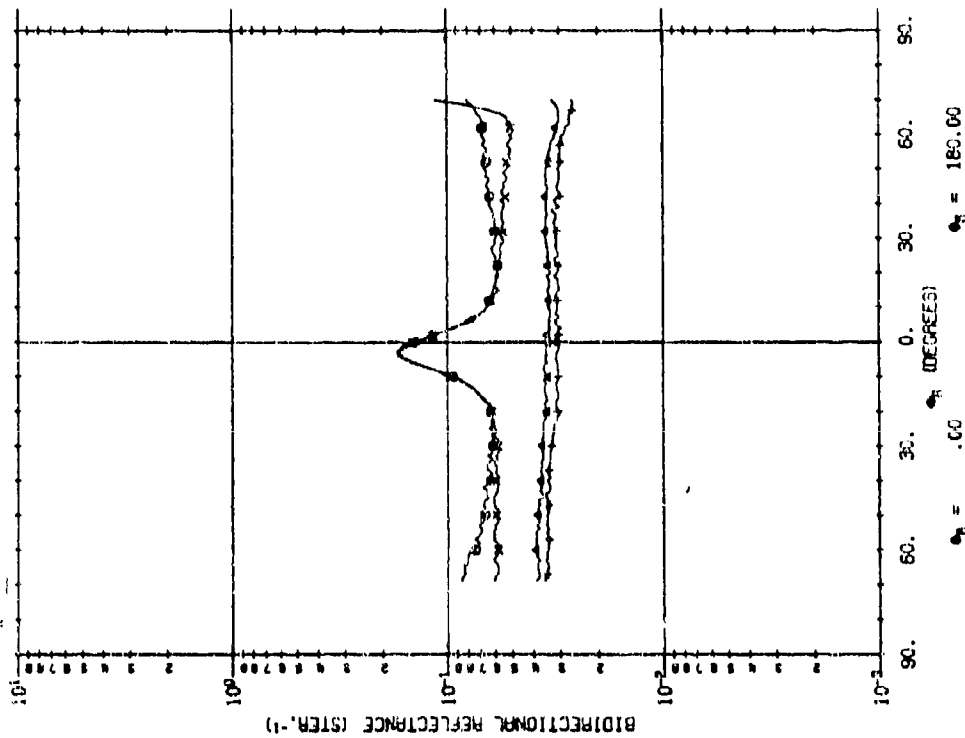


PAINT

R01807 101

Camouflage Paint on Metal

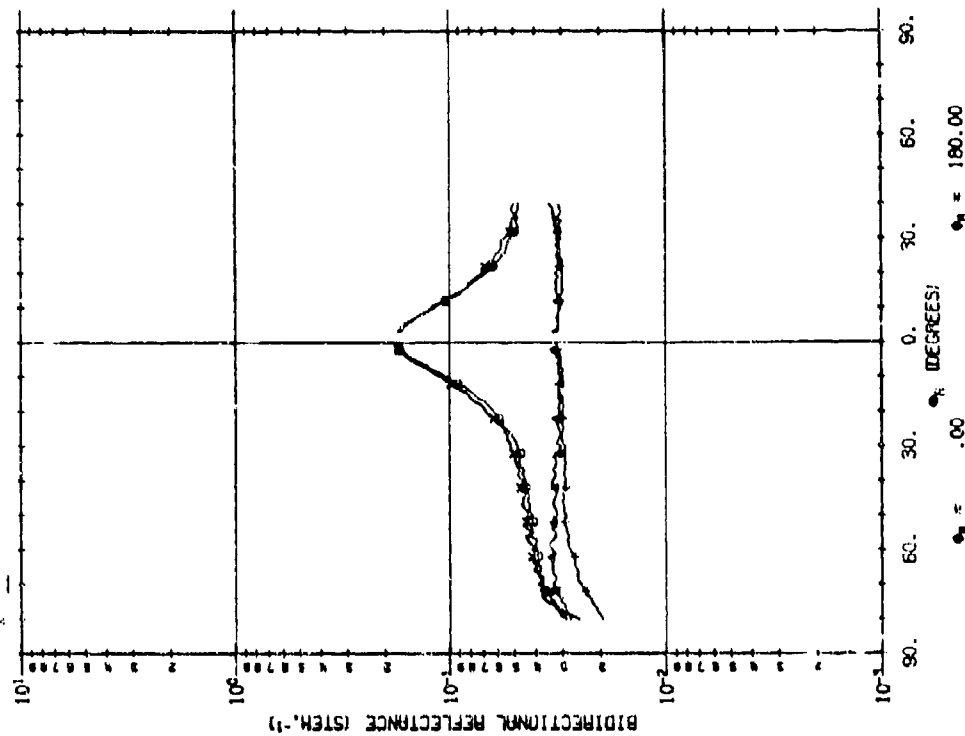
$2\theta = 2.0$   
 $\phi_1 = 4$   
 $\phi_2 = 1.06$   
 $\lambda = 1.06$



R01807 101

Camouflage Paint on Metal

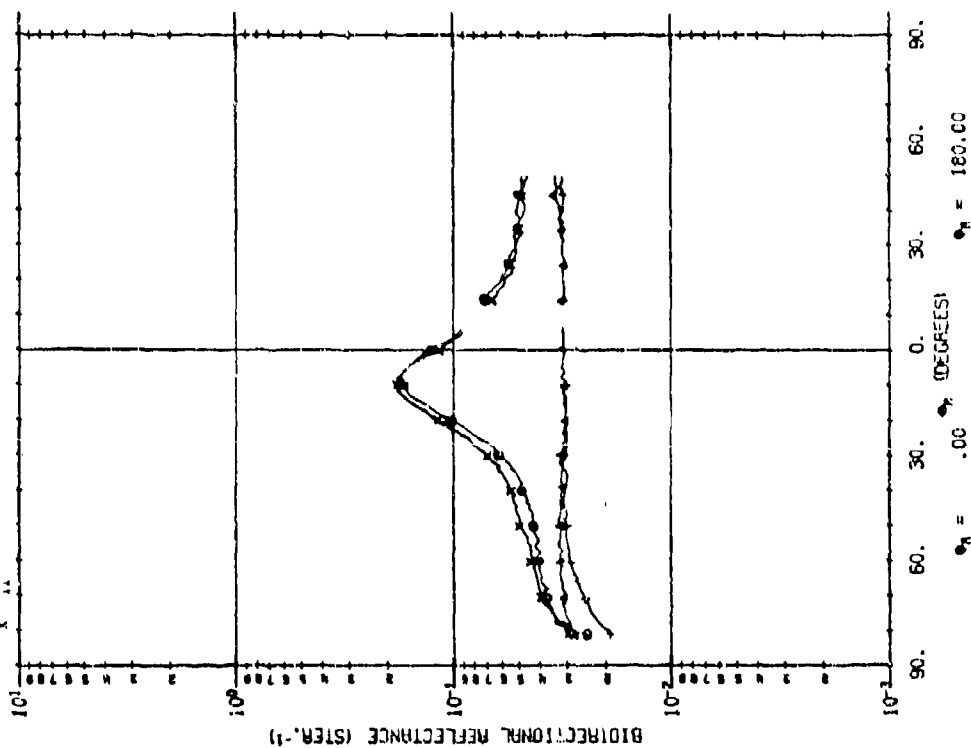
$2\theta = 0.0$   
 $\phi_1 = 130.00$   
 $\phi_2 = 1.06$   
 $\lambda = 1.06$



R01807 101

Camouflage Paint on Metal

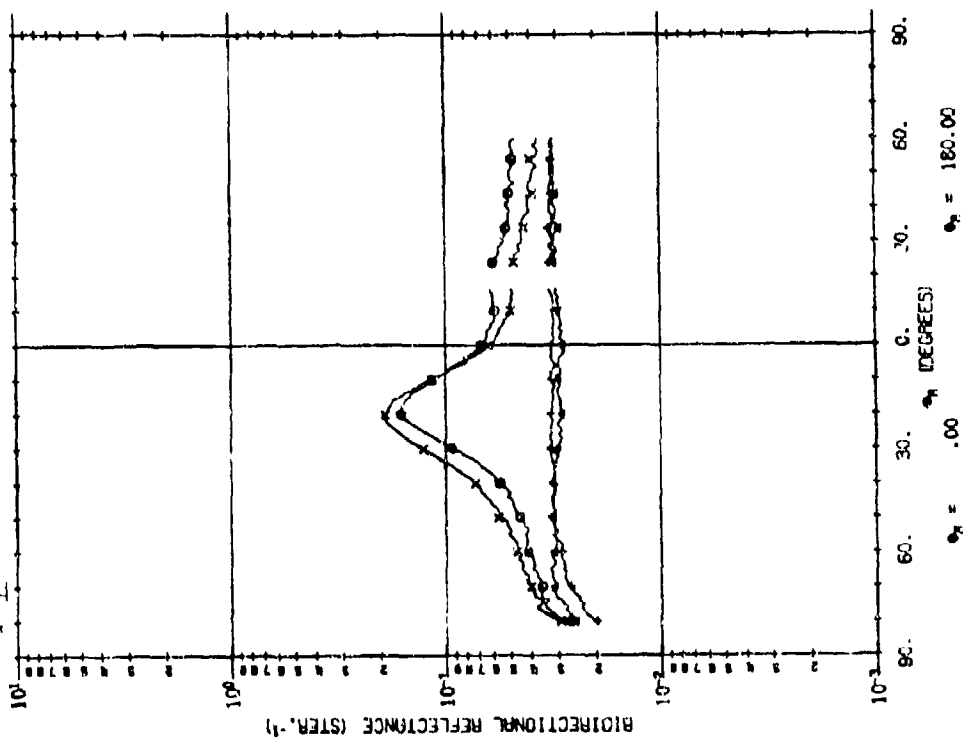
0 |  $\theta_1 = 10.0$   
 + |  $\theta_1 = 180.0$   
 x |  $\lambda = 0.63$   
 x |  $\lambda = 0.63$



R01807 101

Camouflage Paint on Metal

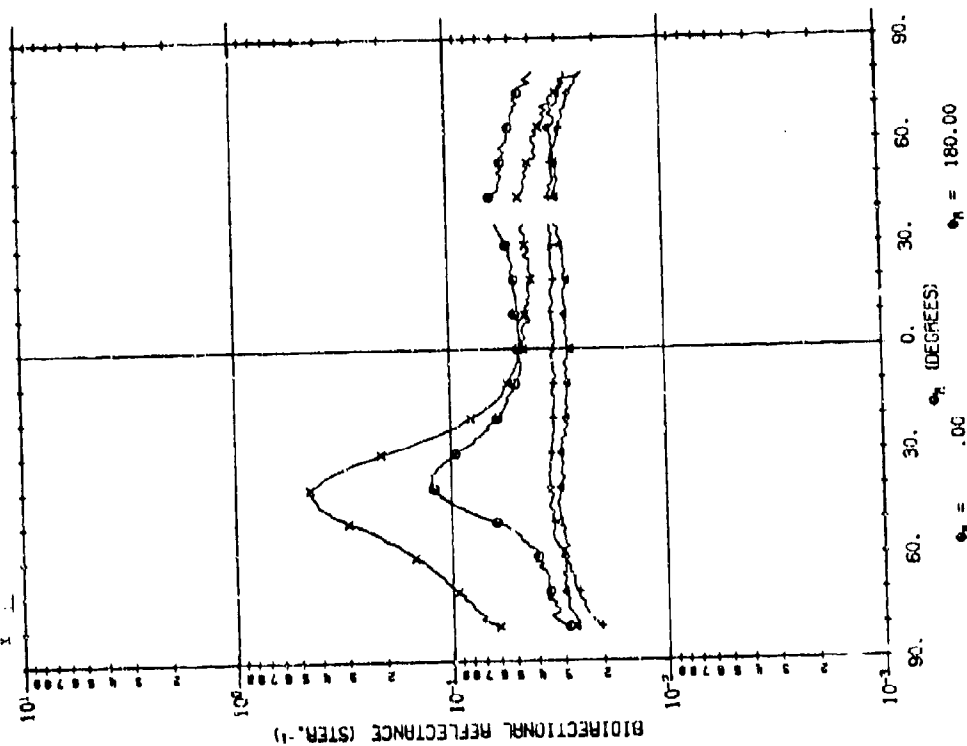
0 |  $\theta_1 = 20.00$   
 + |  $\theta_1 = 180.00$   
 x |  $\lambda = 1.06$   
 x |  $\lambda = 1.06$



PAINT

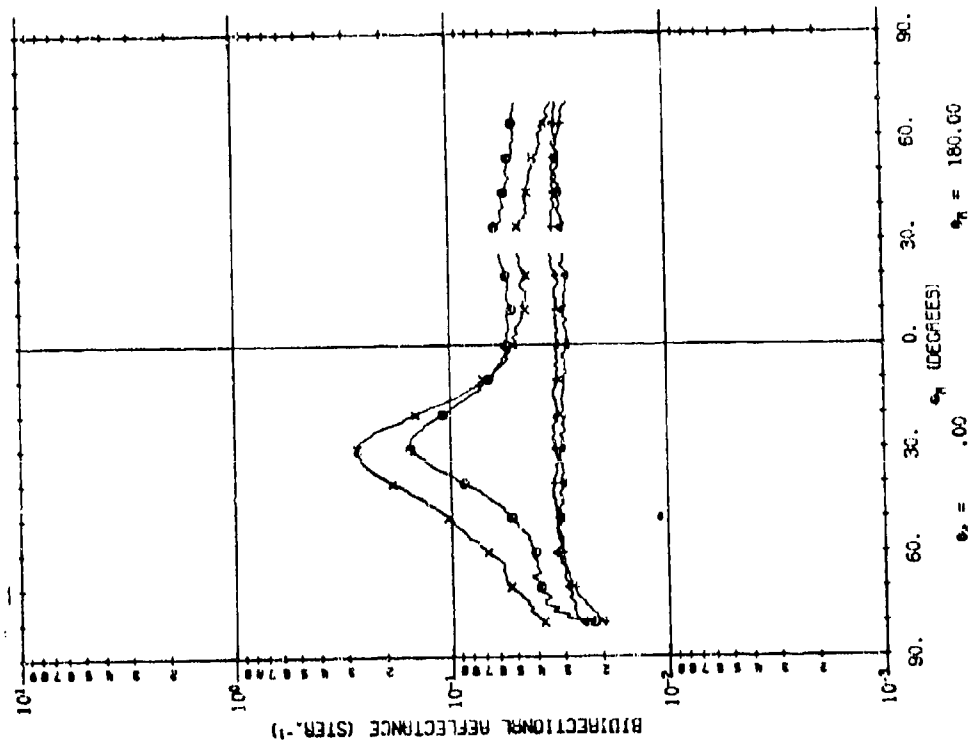
AO1807 101 Camouflage Paint on Metal

$\theta_i = 45.00$   
 $\theta_r = 180.00$   
 $\theta_n = 180.00$   
 $\theta_t = 1.06$



AO1807 101 Camouflage Paint on Metal

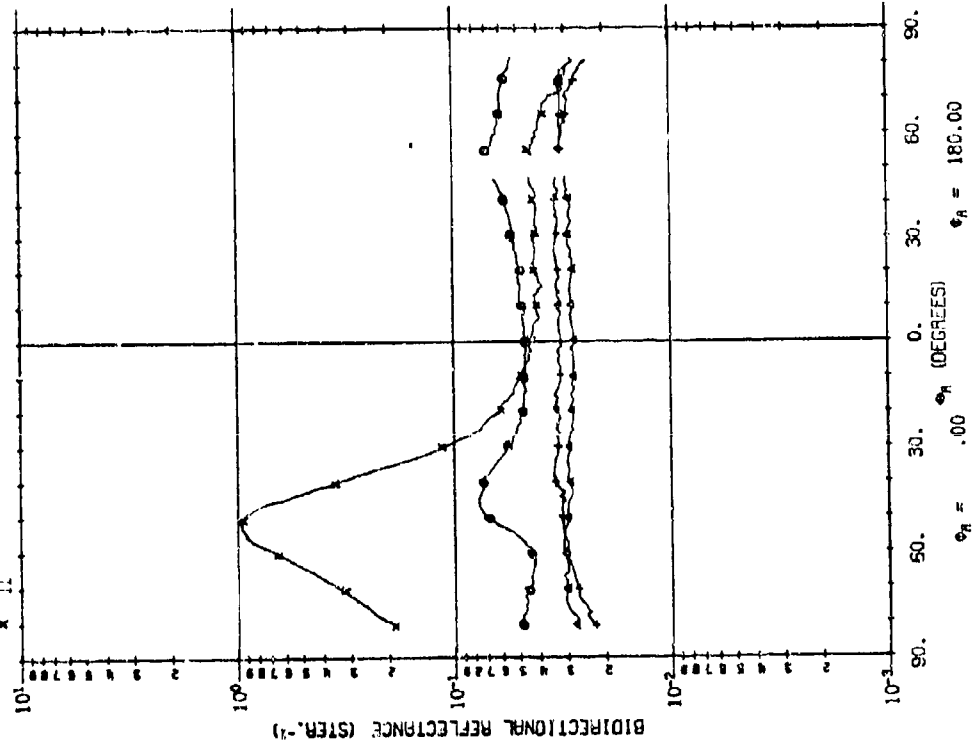
$\theta_i = 45.00$   
 $\theta_r = 180.00$   
 $\theta_n = 180.00$   
 $\theta_t = 1.06$



A01807 101

Camouflage Paint on Metal

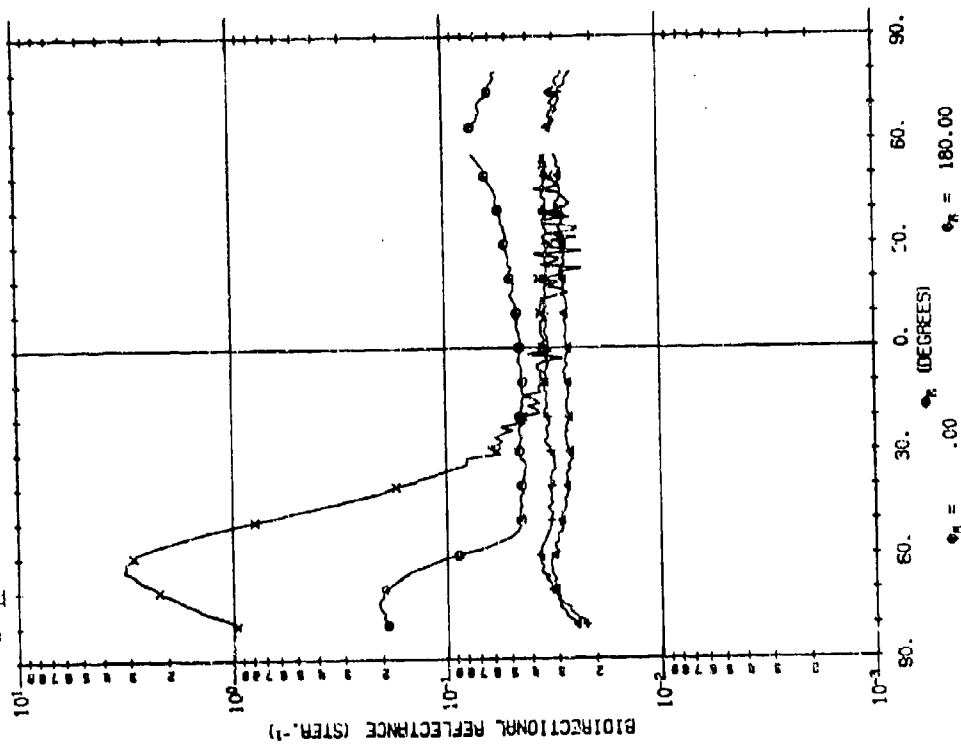
$\phi_i = 50.0$   
 $\phi_t = 180.0$   
 $\lambda = 0.63$



A01807 101

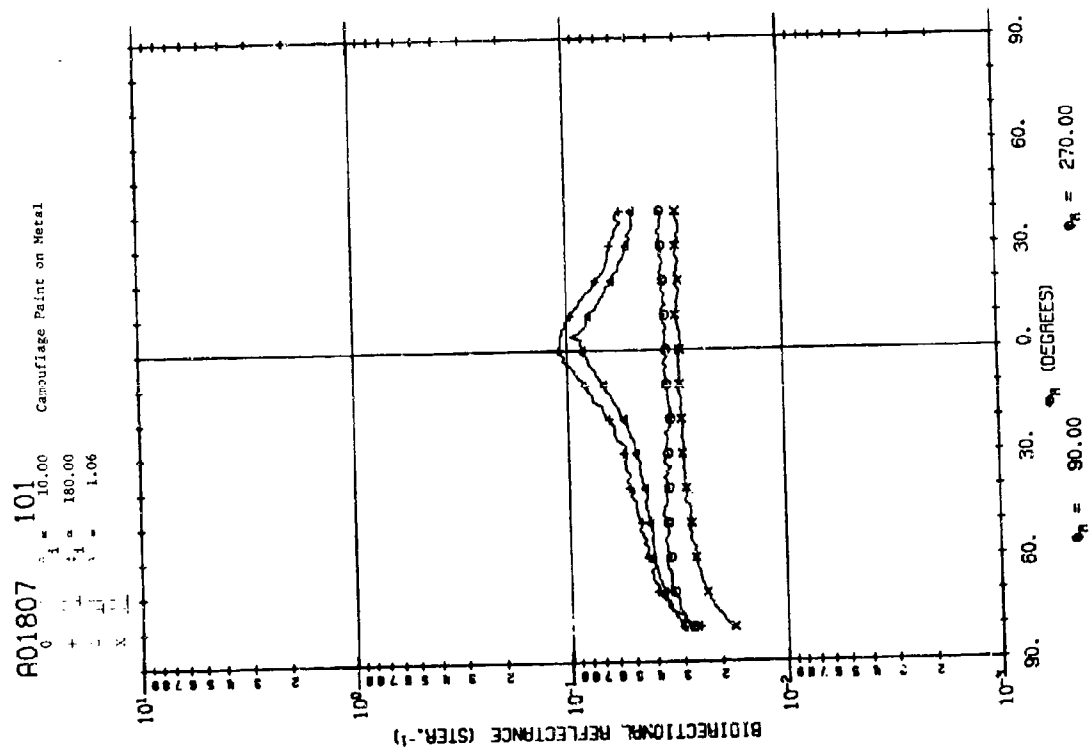
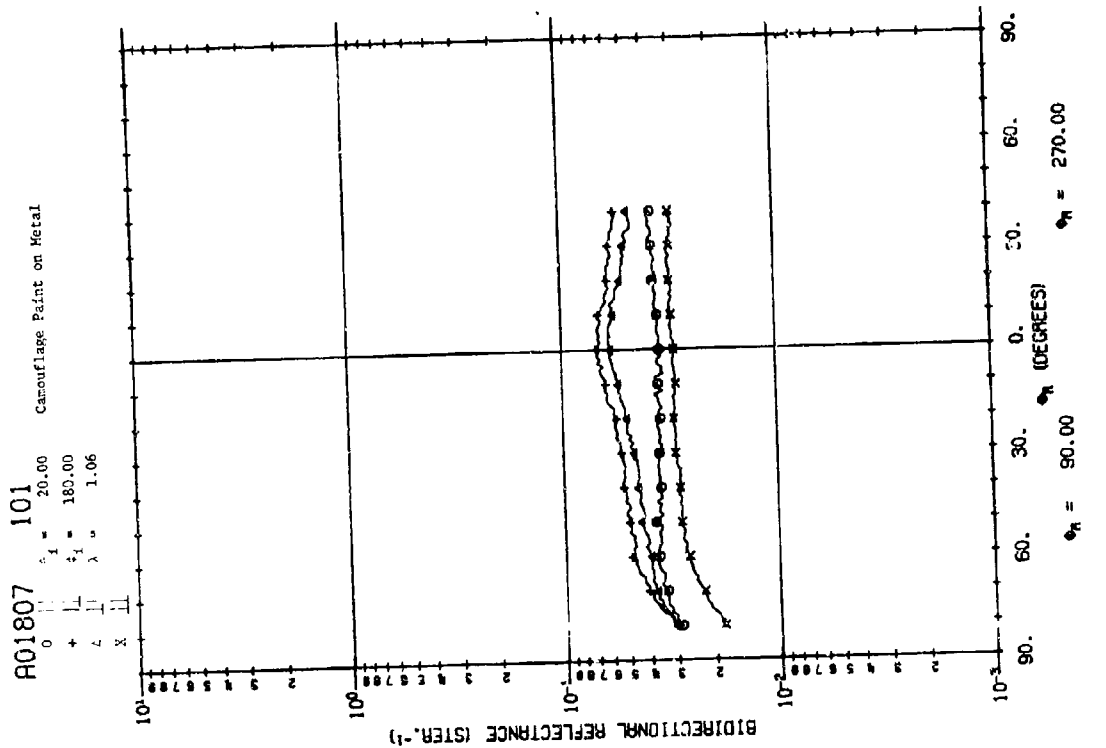
Camouflage Paint on Metal

$\phi_i = 60.00$   
 $\phi_t = 180.00$   
 $\lambda = 1.06$



PAINT

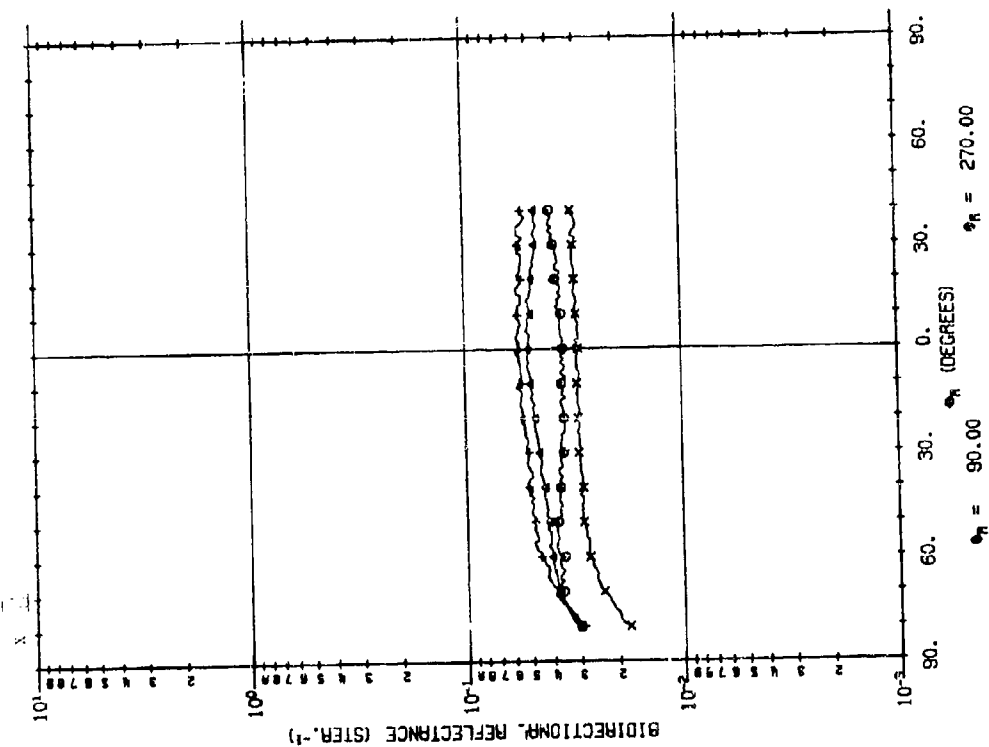




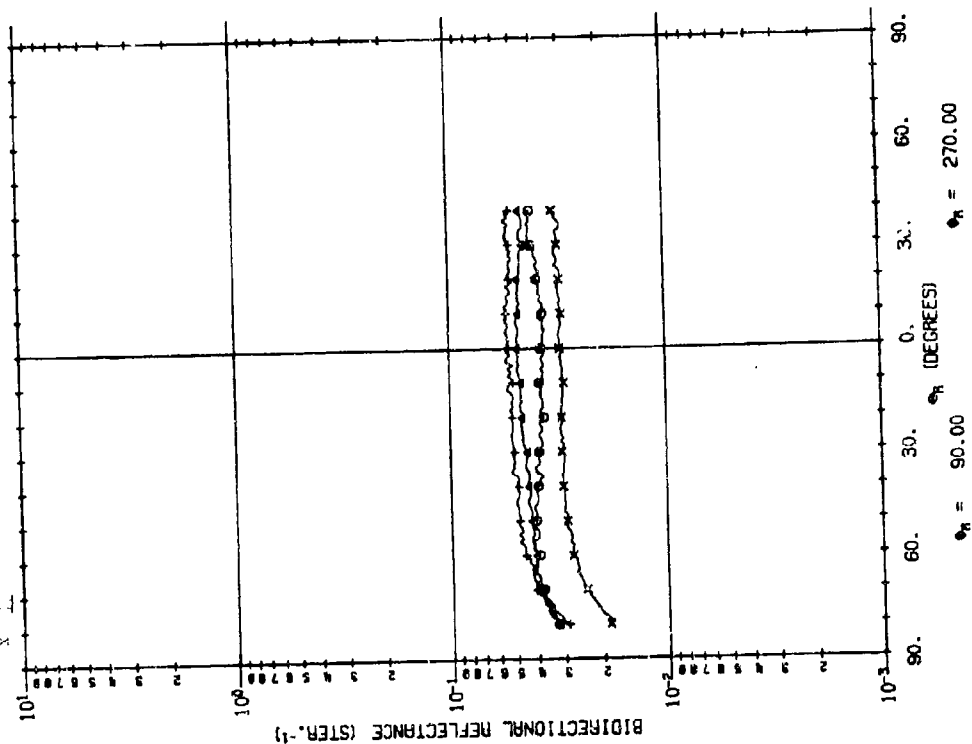
PAINT



A01807 101 Camouflage Paint on Metal  
 $\lambda = 30.00$   
 $\lambda = 100.00$   
 $\lambda = 1.06$



A01807 101 Camouflage Paint on Metal  
 $\lambda = 40.00$   
 $\lambda = 180.00$   
 $\lambda = 1.06$

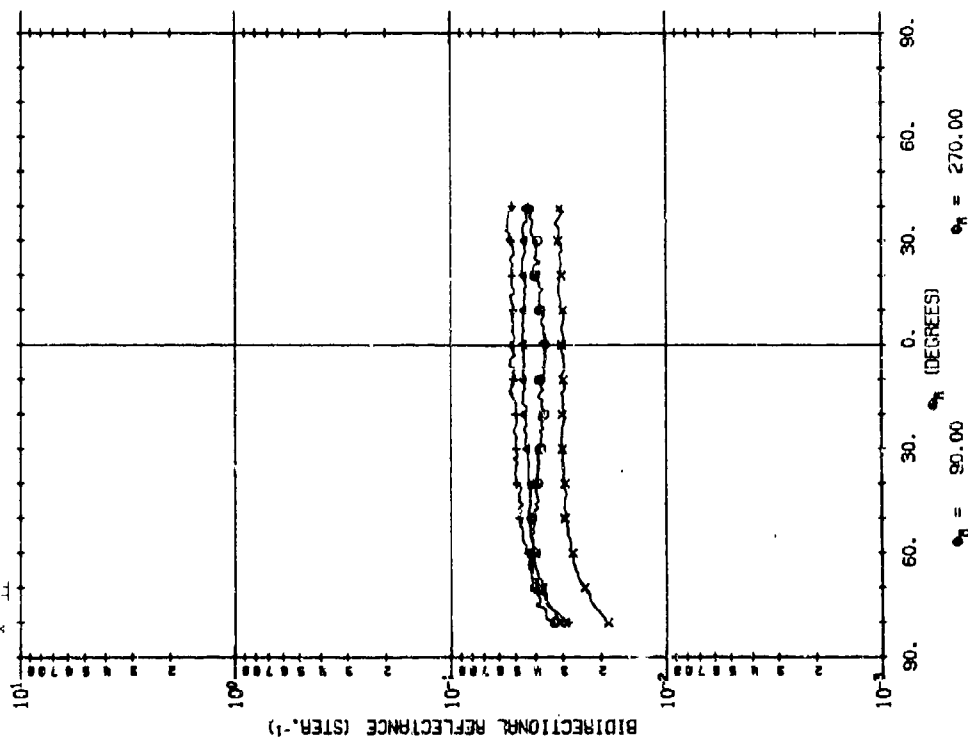


R01807 101

Camouflage Paint on Metal

$\theta_1 = 50.00$   
 $\theta_2 = 180.00$   
 $\lambda = 1.06$

0 II  
 + II  
 x II

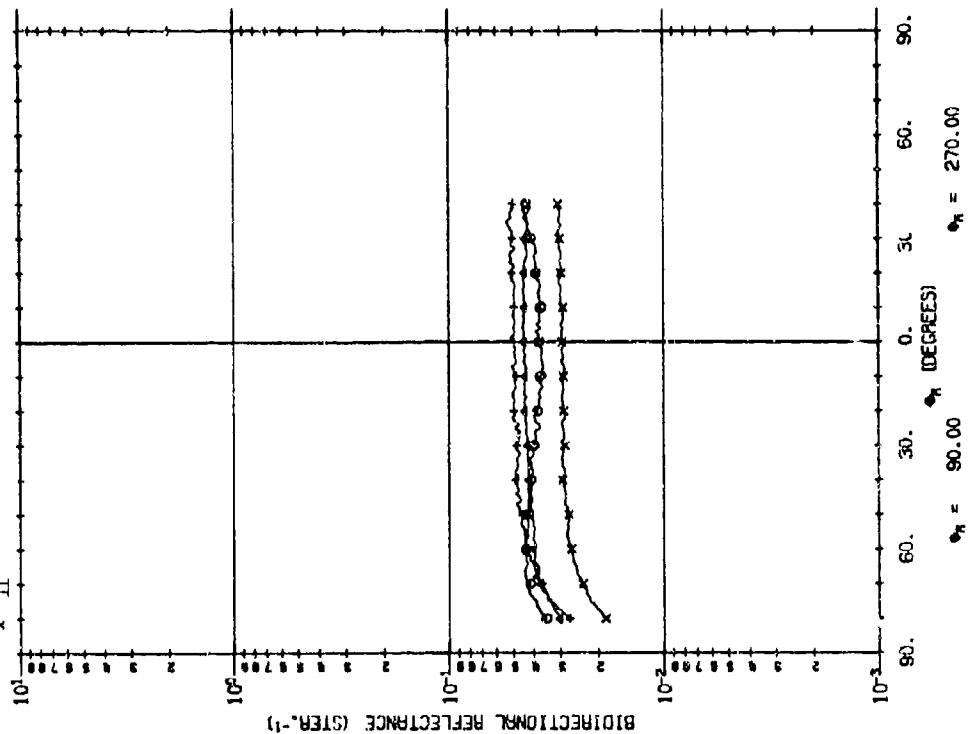


R01807 101

Camouflage Paint on Metal

$\theta_1 = 60.00$   
 $\theta_2 = 180.00$   
 $\lambda = 1.06$

0 II  
 + II  
 x II

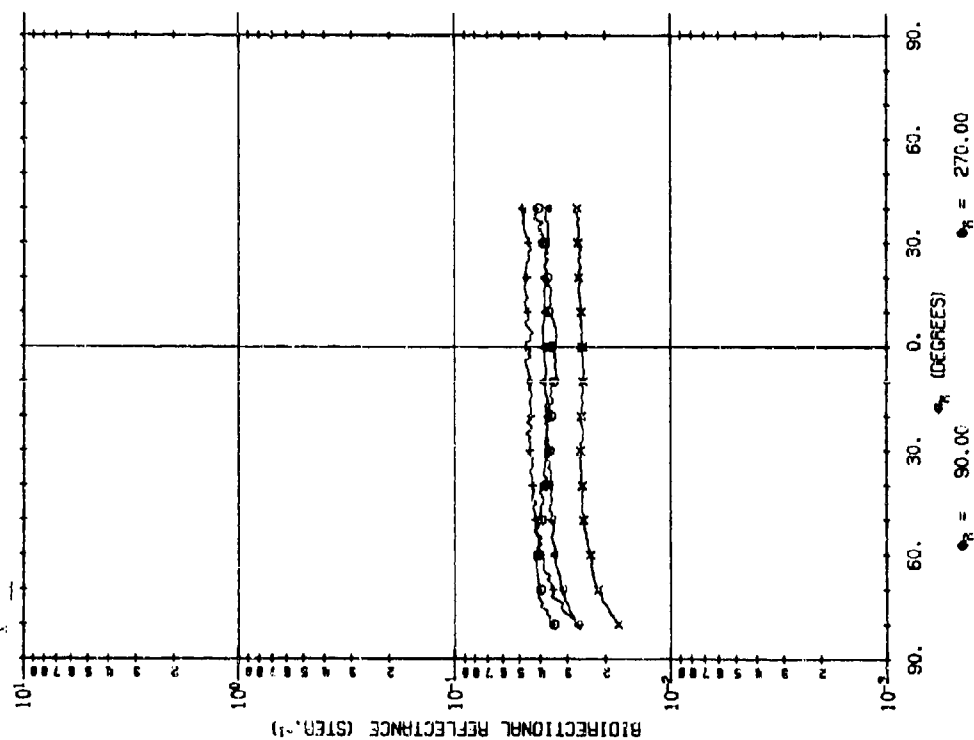


PAINT

R01807 101

Camouflage Paint on Metal

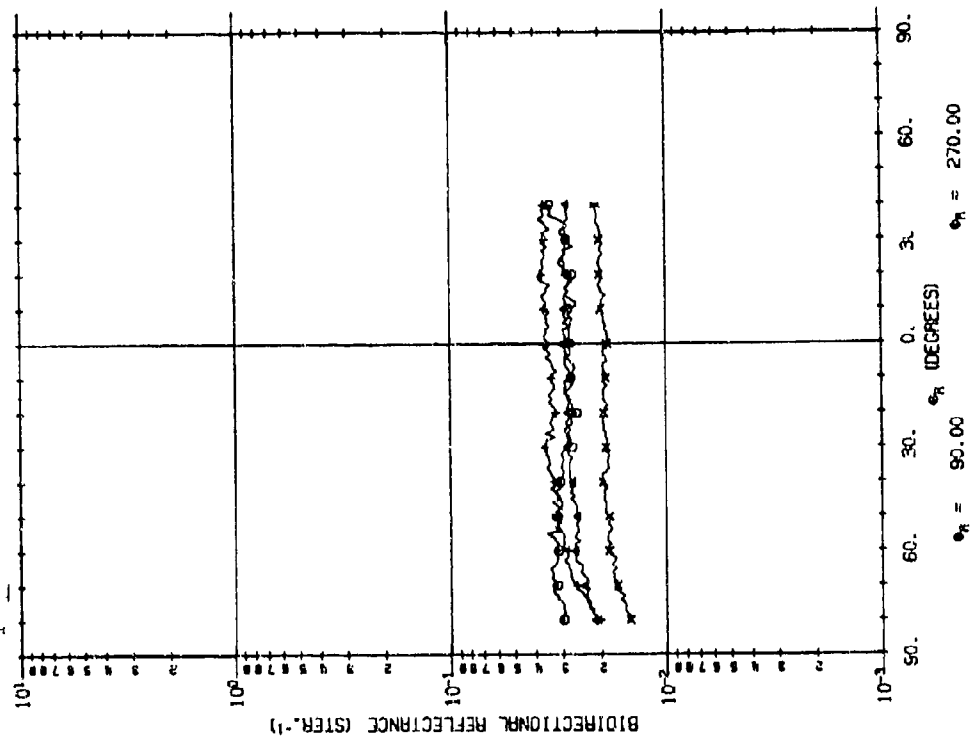
$\theta_i = 70.00$   
 $\theta_r = 180.00$   
 $\phi = 1.06$



R01807 101

Camouflage Paint on Metal

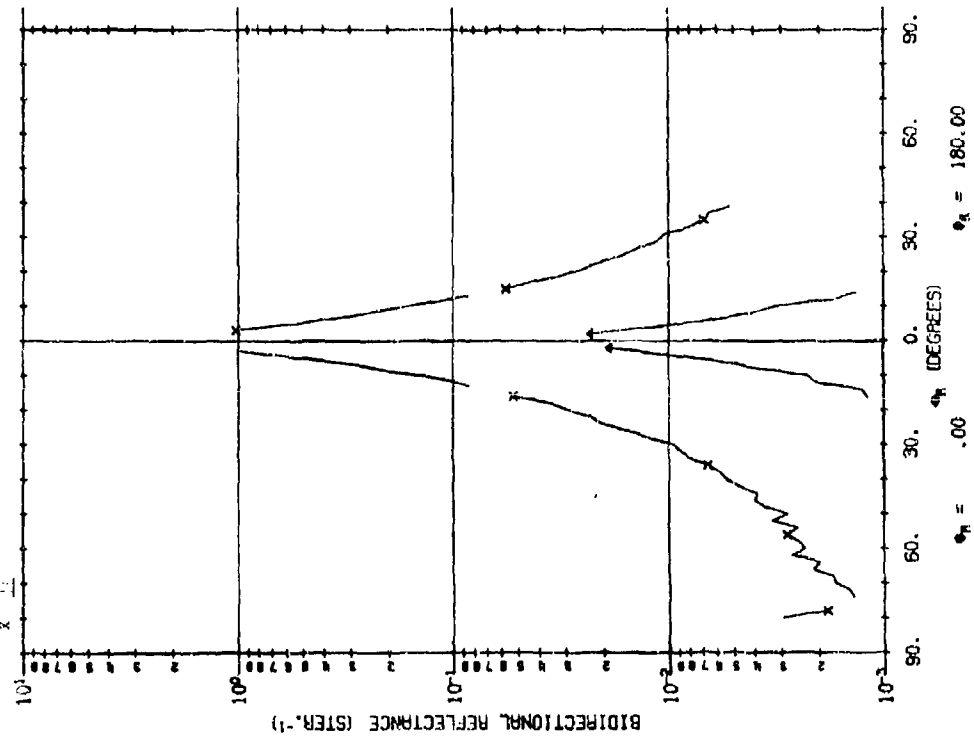
$\theta_i = 75.00$   
 $\theta_r = 180.00$   
 $\phi = 1.06$



AD1807 302

Camouflage Paint on Metal

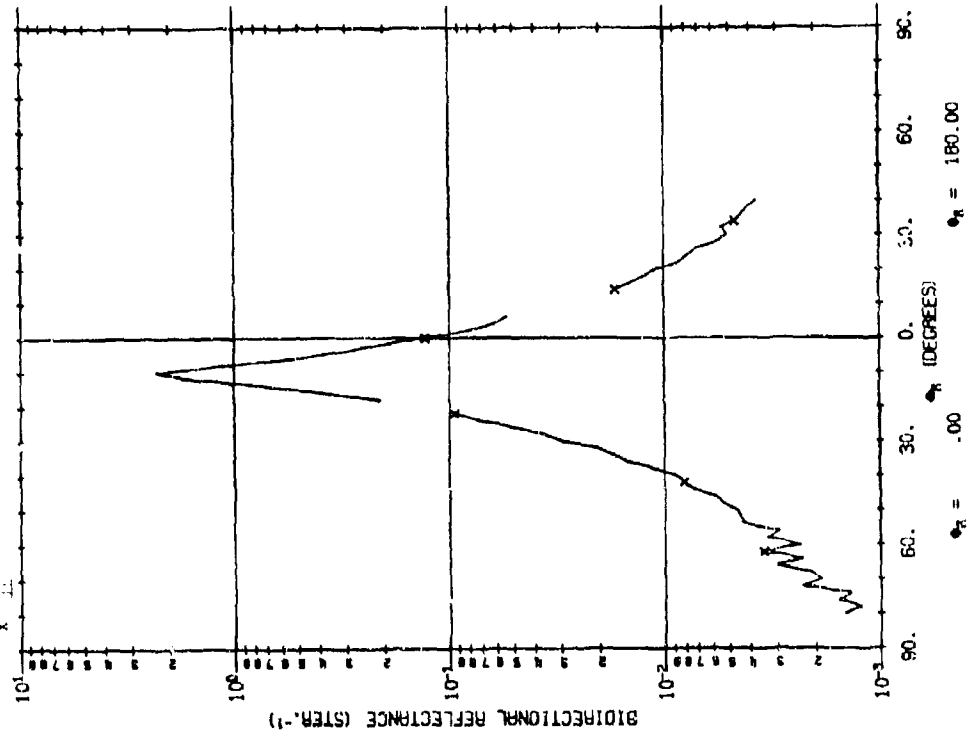
0 11 0.0  
+ 11 180.00  
x 11 10.60



AD1807 302

Camouflage Paint on Metal

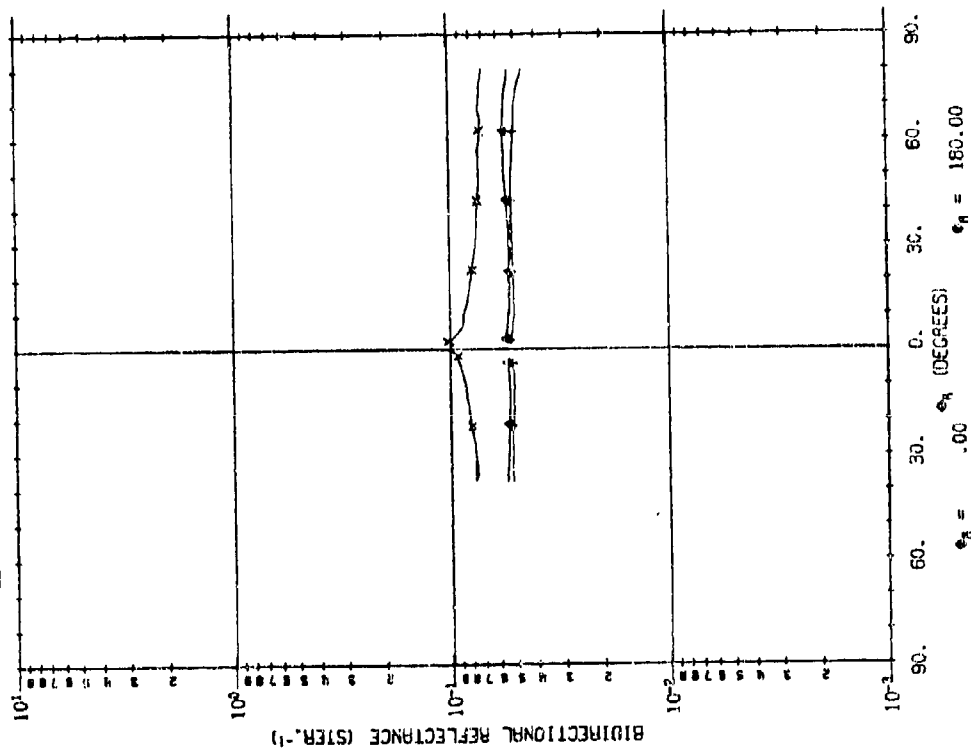
0 11 10.00  
+ 11 180.00  
x 11 10.60



PAINT

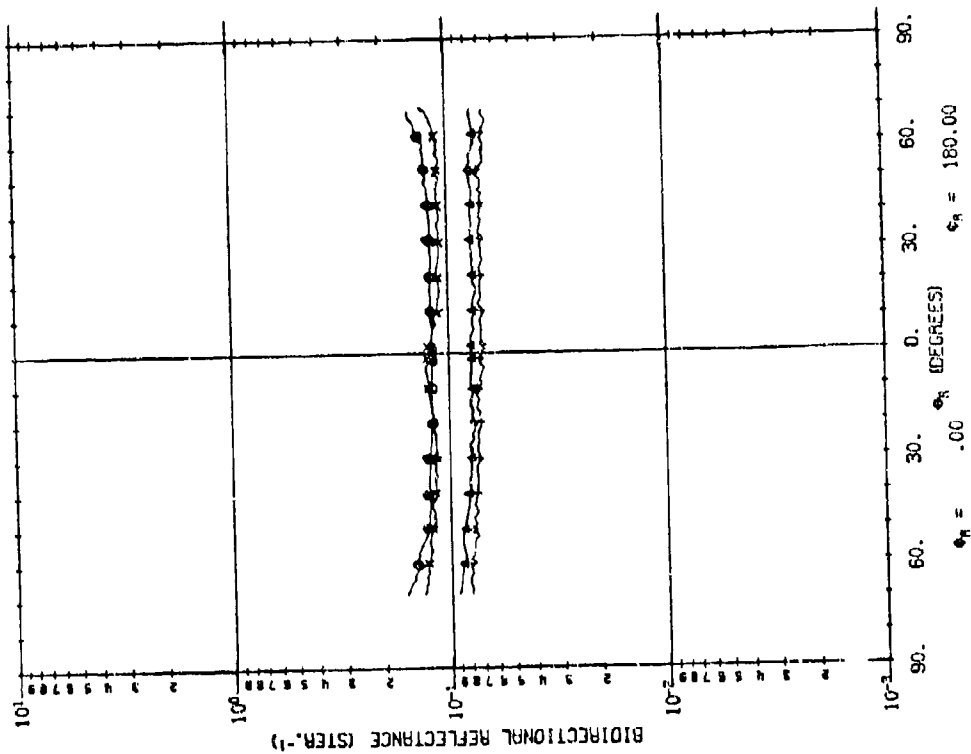
Camouflage Paint on Metal

R01808 301  
 $\hat{a}_1 = 0.0$   
 $\hat{a}_2 = 0.0$   
 $\hat{a}_3 = 0.0$   
 $\hat{a}_4 = 0.63$

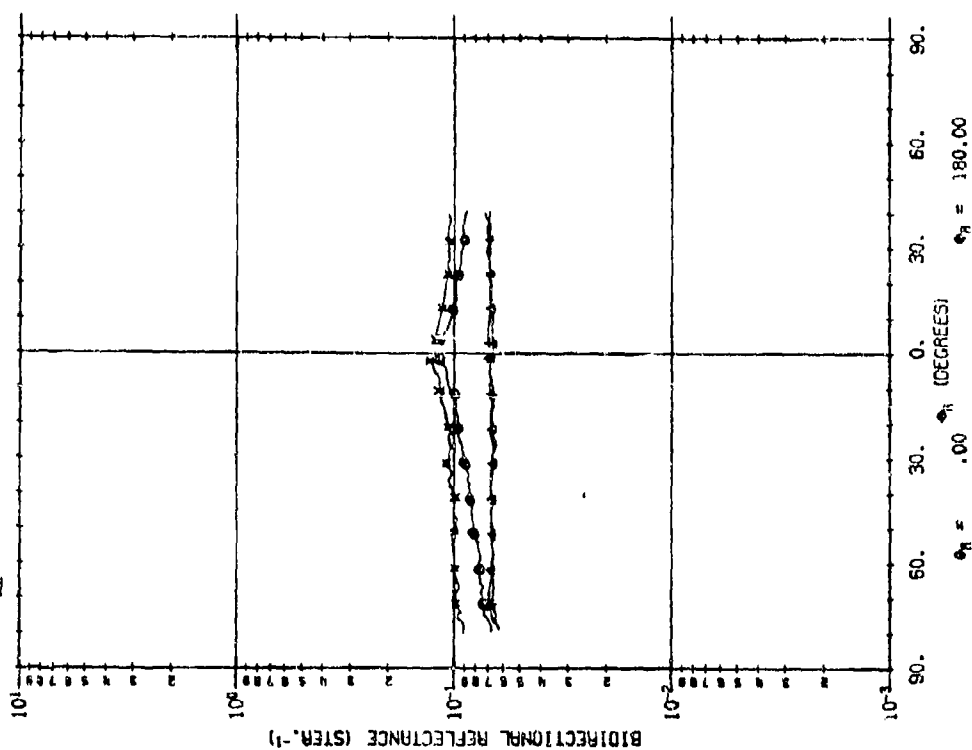


Camouflage Paint on Metal

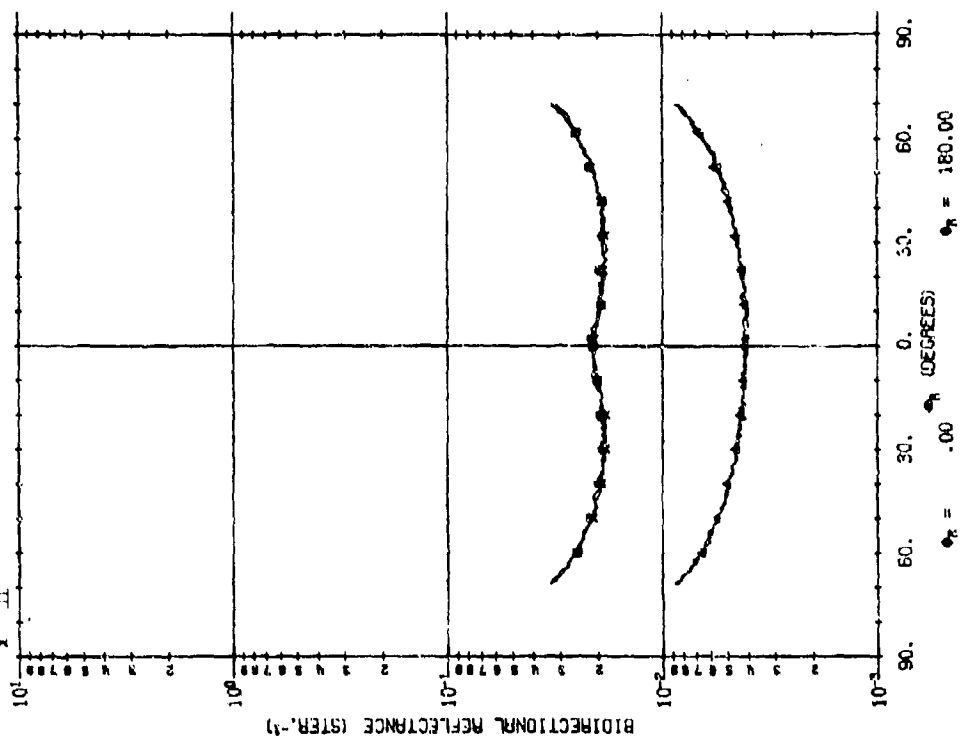
R01808 101  
 $\hat{a}_1 = 2.0$   
 $\hat{a}_2 = 1.0$   
 $\hat{a}_3 = 1.06$



R01808 101  
 Camouflage Paint on Metal  
 $\theta_i = 0.0$   
 $\theta_r = 0.0$   
 $\lambda = 1.06$



R01839 301  
 OLIVE DRAB PAINT ON METAL  
 $\theta_i = 2.0$   
 $\theta_r = 0.0$   
 $\lambda = 1.06$

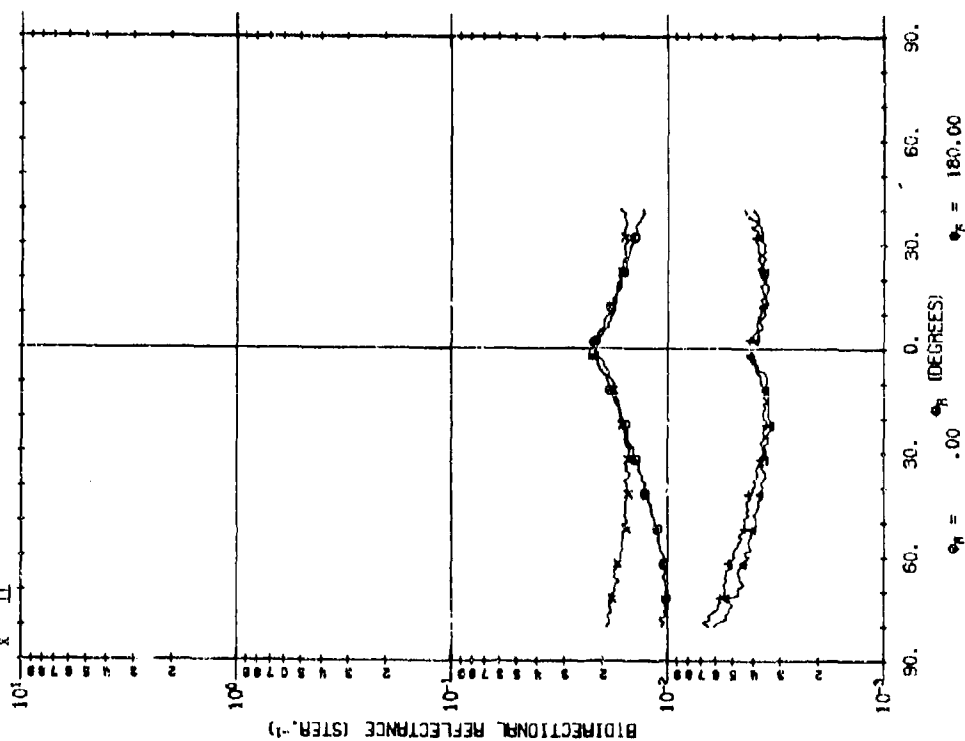


PAINT

R01839 301

OLIVE DRAB PAINT ON METAL

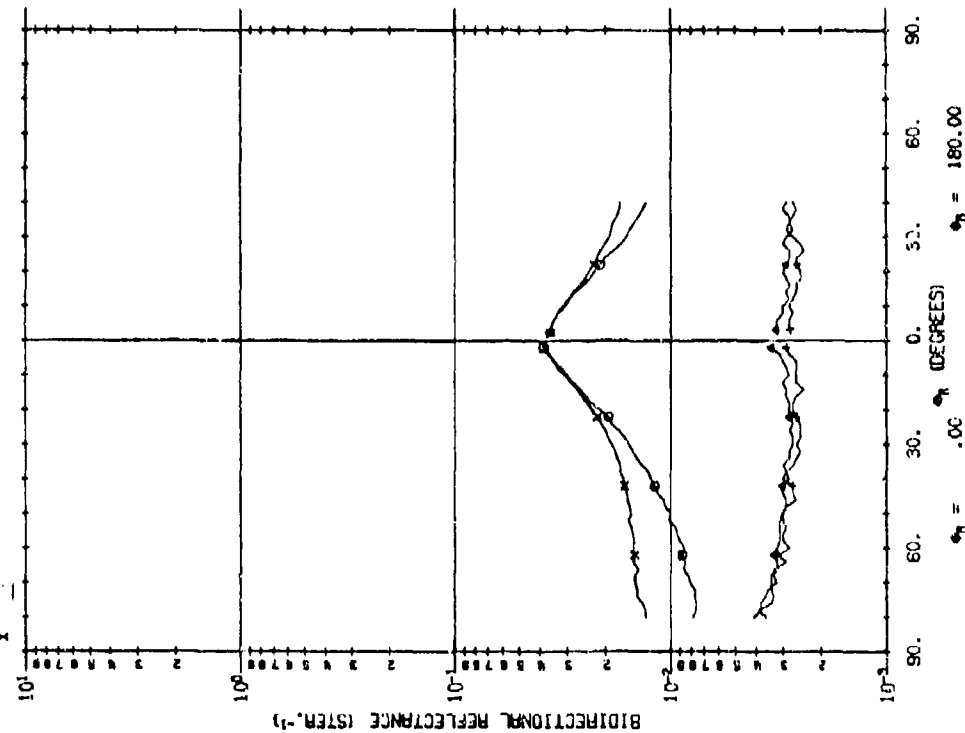
0  $\epsilon_1 = 0.0$   
 +  $\epsilon_2 = 0.0$   
 x  $\epsilon_3 = 1.06$

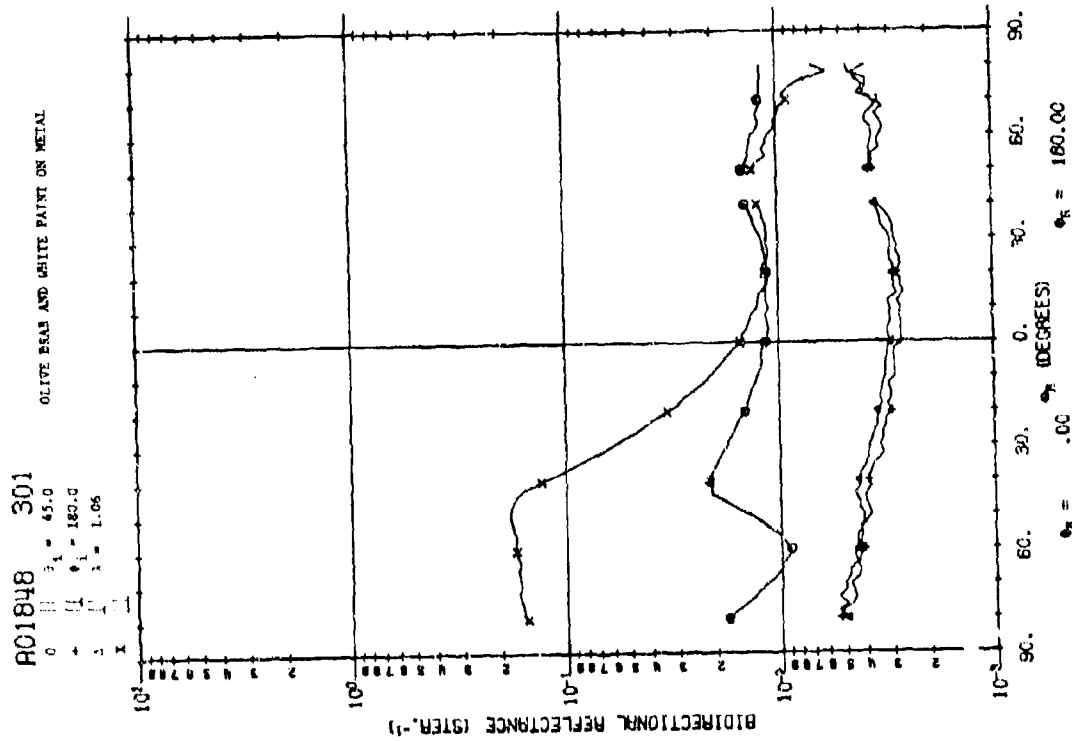
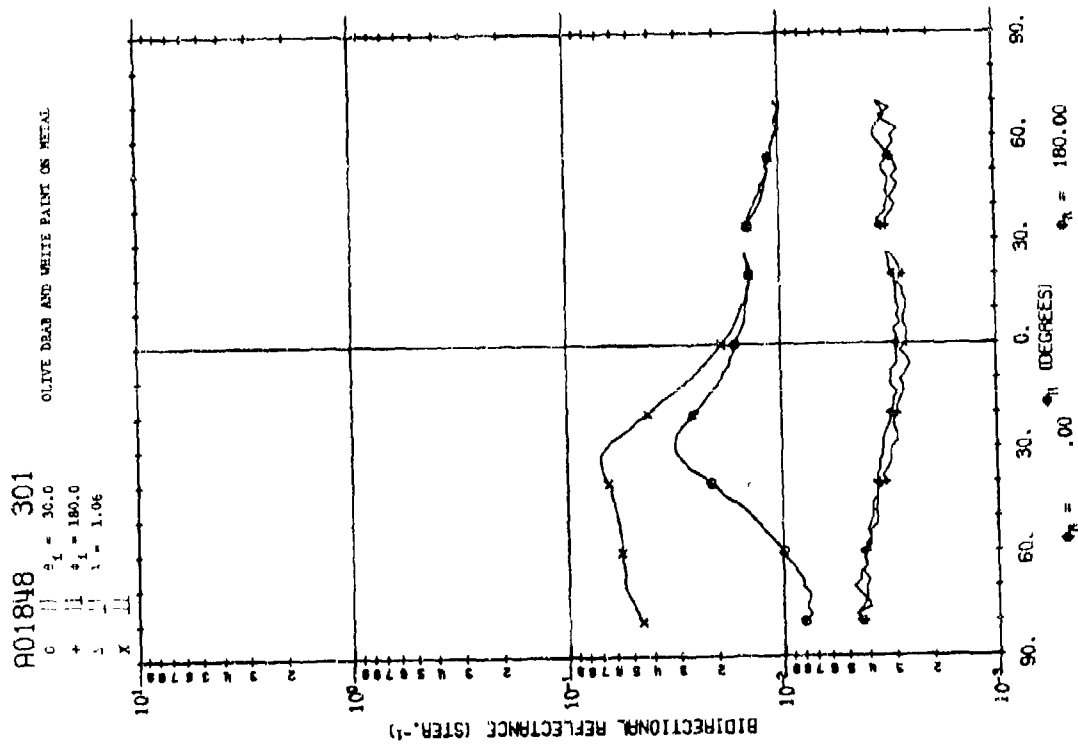


R01848 301

OLIVE DRAB AND WHITE PAINT ON METAL

0  $\epsilon_1 = 0.0$   
 +  $\epsilon_2 = 180.9$   
 x  $\epsilon_3 = 1.06$





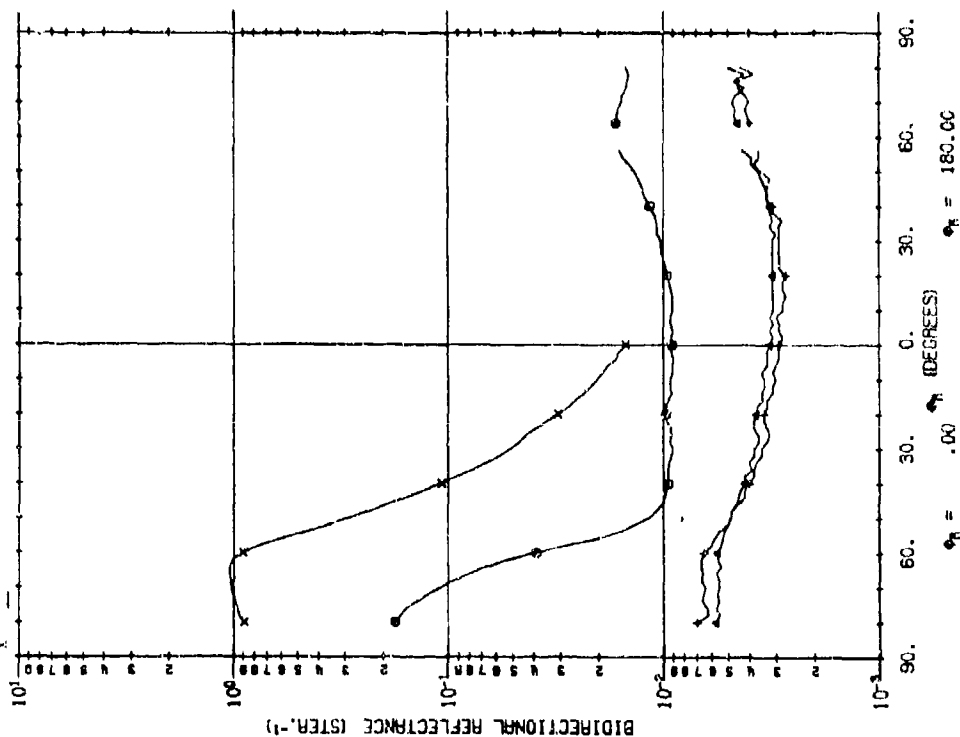
PAINT



R01848 301

OLIVE DRAB AND WHITE PAINT ON METAL

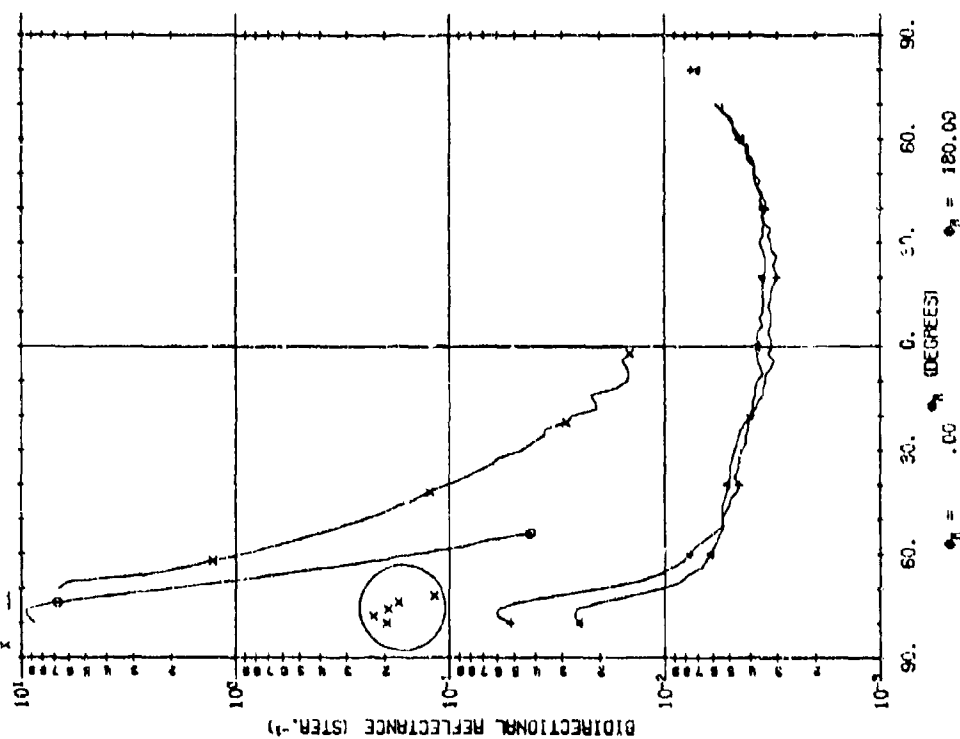
$\theta_i = 60.0$   
 $\theta_r = 180.0$   
 $\phi = 1.06$



R01848 301

OLIVE DRAB AND WHITE PAINT ON METAL

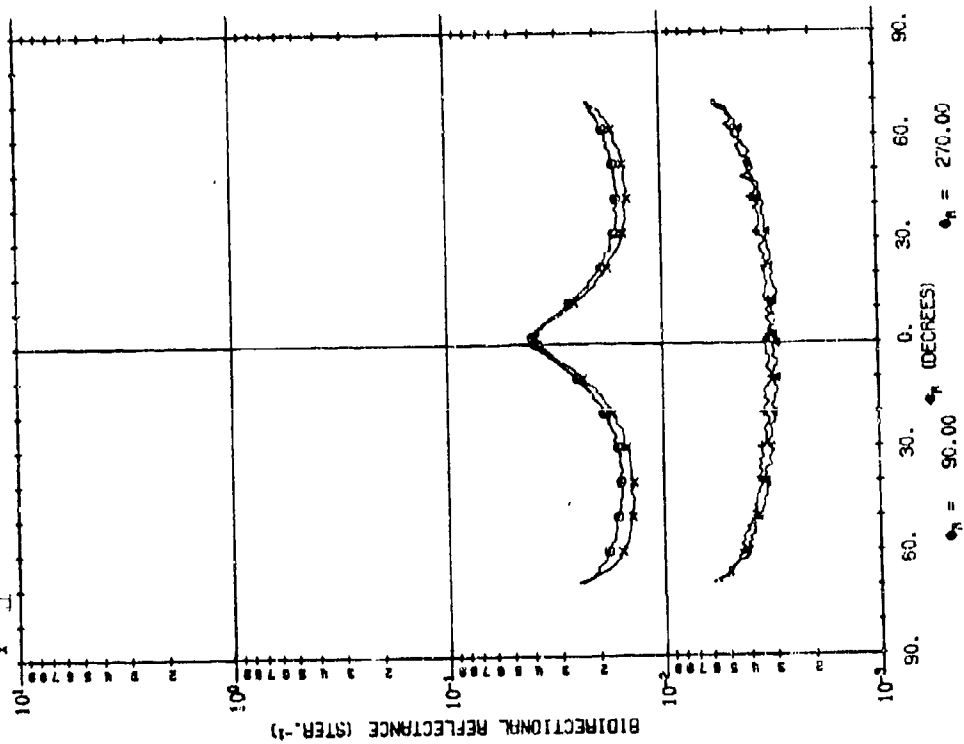
$\theta_i = 75.0$   
 $\theta_r = 180.0$   
 $\phi = 1.06$



R01848 301

OLIVE DRAB AND WHITE PAINT ON METAL

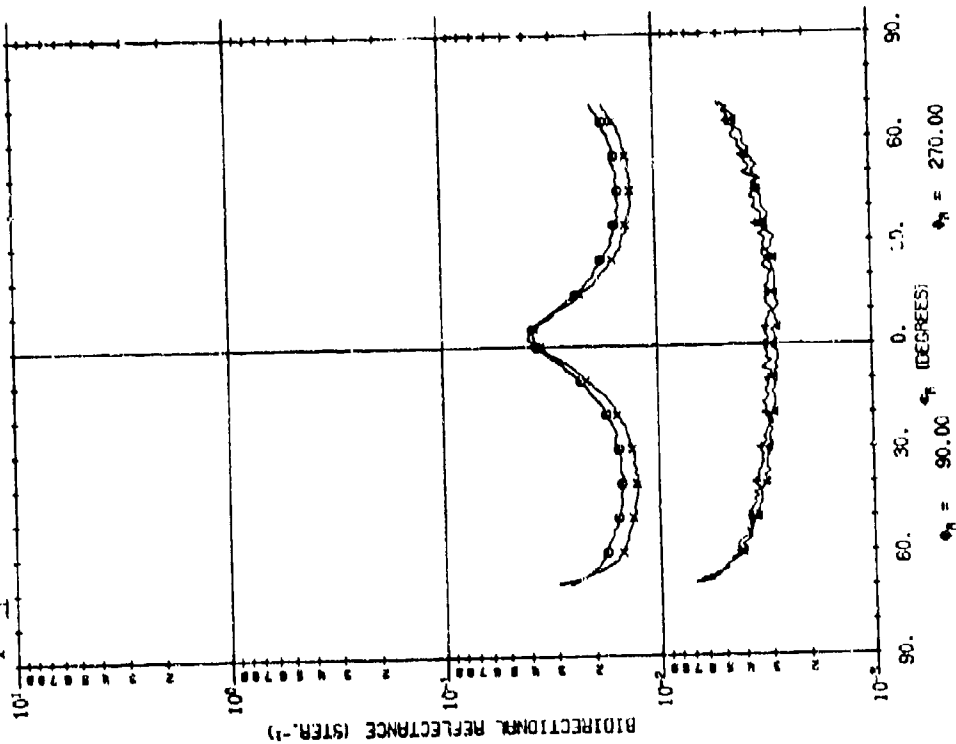
0 ||  $2\theta = 2.0$   
+ ||  $\theta_i = \theta_r$   
- ||  $\lambda = 1.06$   
x ||



R01848 301

OLIVE DRAB AND WHITE PAINT ON METAL

0 ||  $2\theta = 5.0$   
+ ||  $\theta_i = \theta_r$   
- ||  $\lambda = 1.06$   
x ||

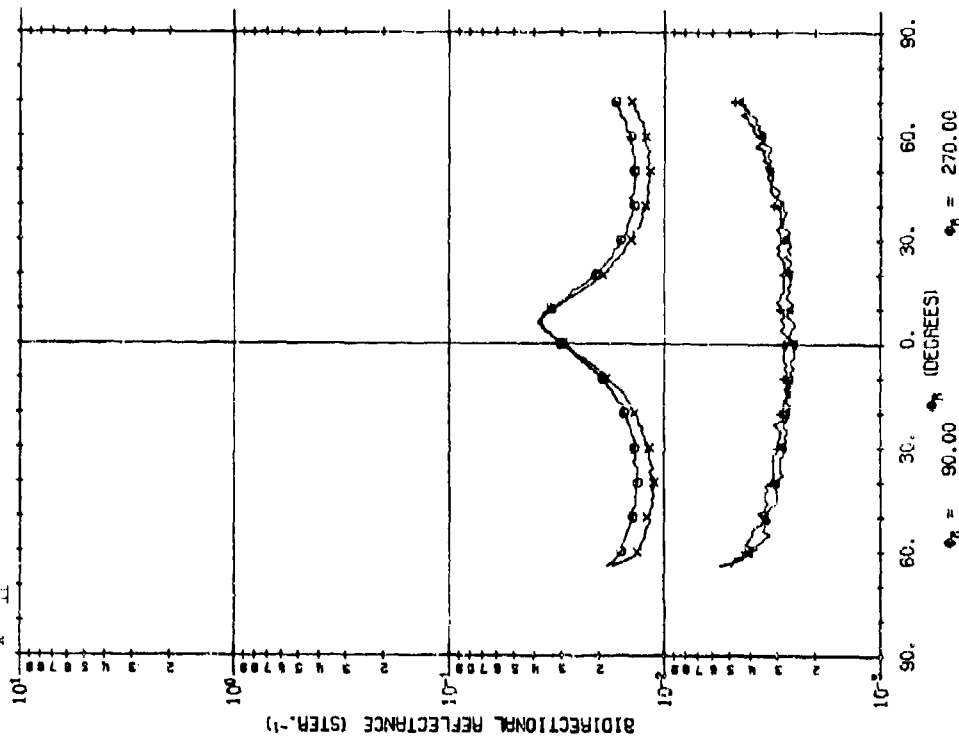


PAINT

A01848 301

OLIVE DRAB AND WHITE PAINT ON METAL

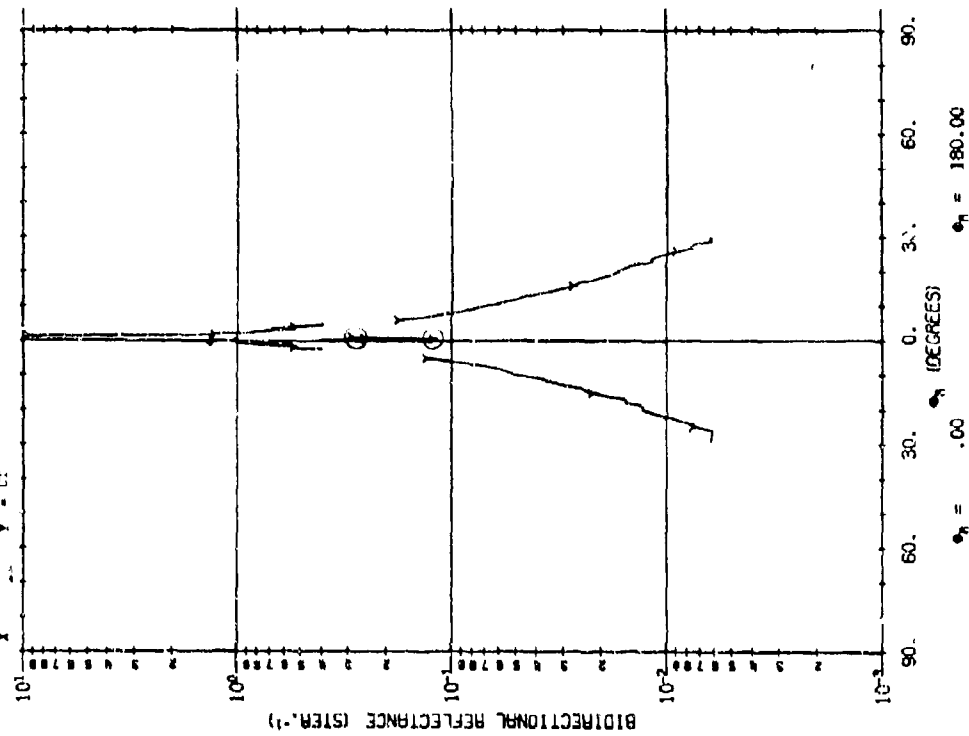
$2\theta = 10.0$   
 $\lambda = 1.06$   
 $\phi = 90.00$   
 $\phi_h = 270.00$



A01879 201

GREEN PAINT ON METAL

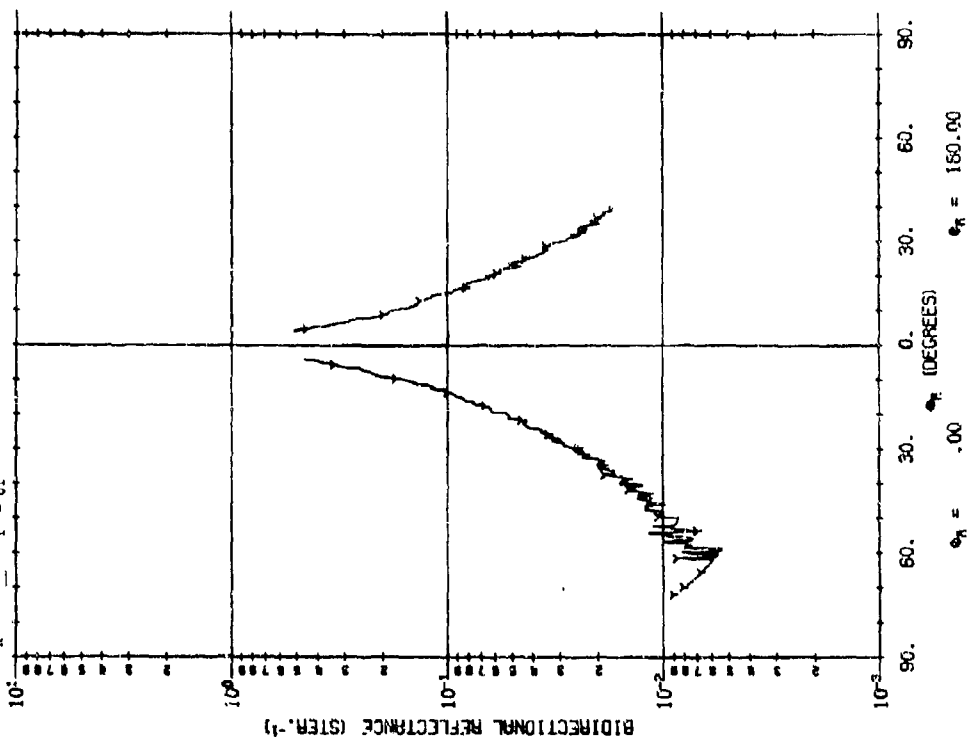
$2\theta = 2.0$   
 $\lambda = 10.6$   
 $\phi = 180.00$   
 $\phi_h = 180.00$



A01879 201  
0 11 22 - 2.0  
+ 11 11  
2 11 11  
X 11 11

Green Paint on Metal

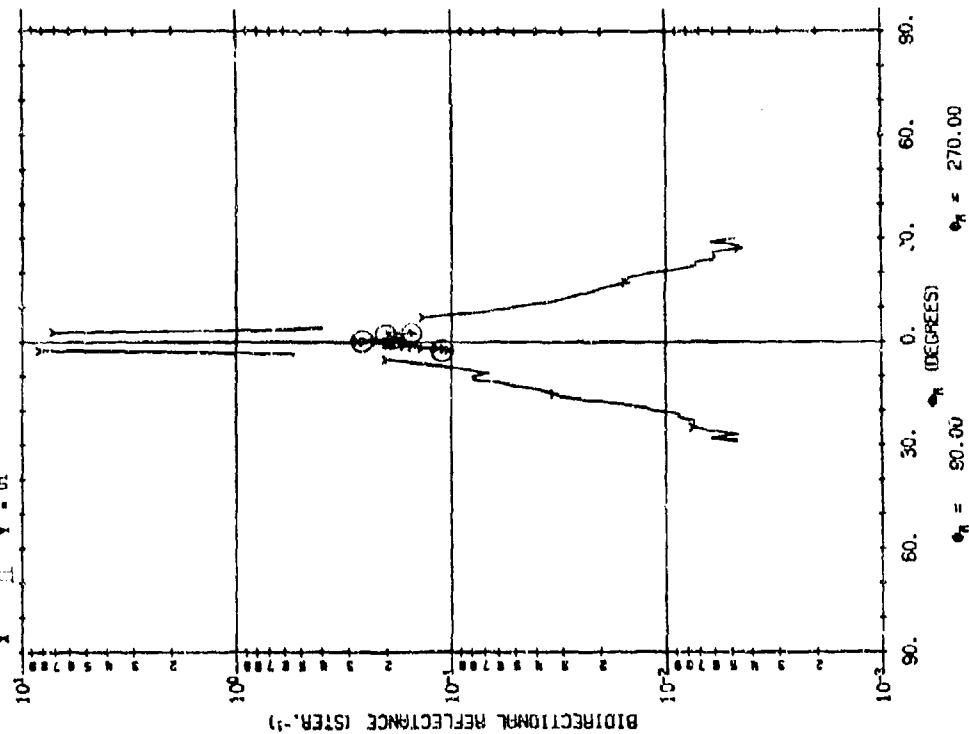
$\theta_1 = 0.0$   
 $\theta_2 = 180.0$   
 $\lambda = 10.6$   
Y = UT



A01879 201  
0 11 22 - 2.0  
+ 11 11  
2 11 11  
X 11 11

Green Paint on Metal

$\theta_1 = 0$   
 $\theta_2 = 180.0$   
 $\lambda = 10.6$   
Y = UT

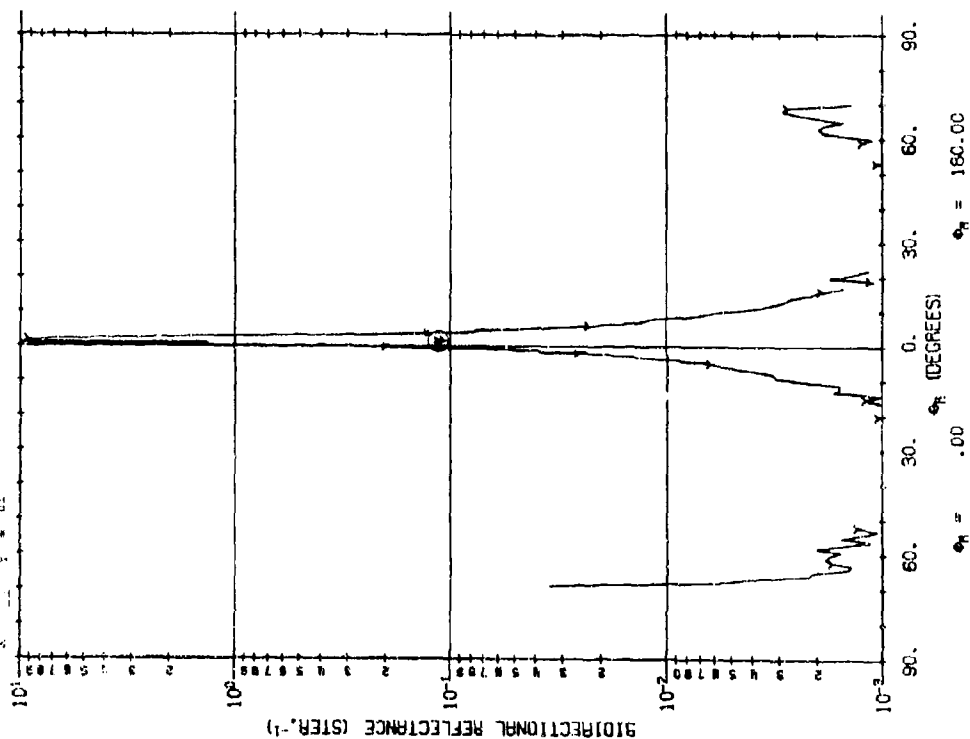


PAINT

A01880 201

Green Paint on Metal

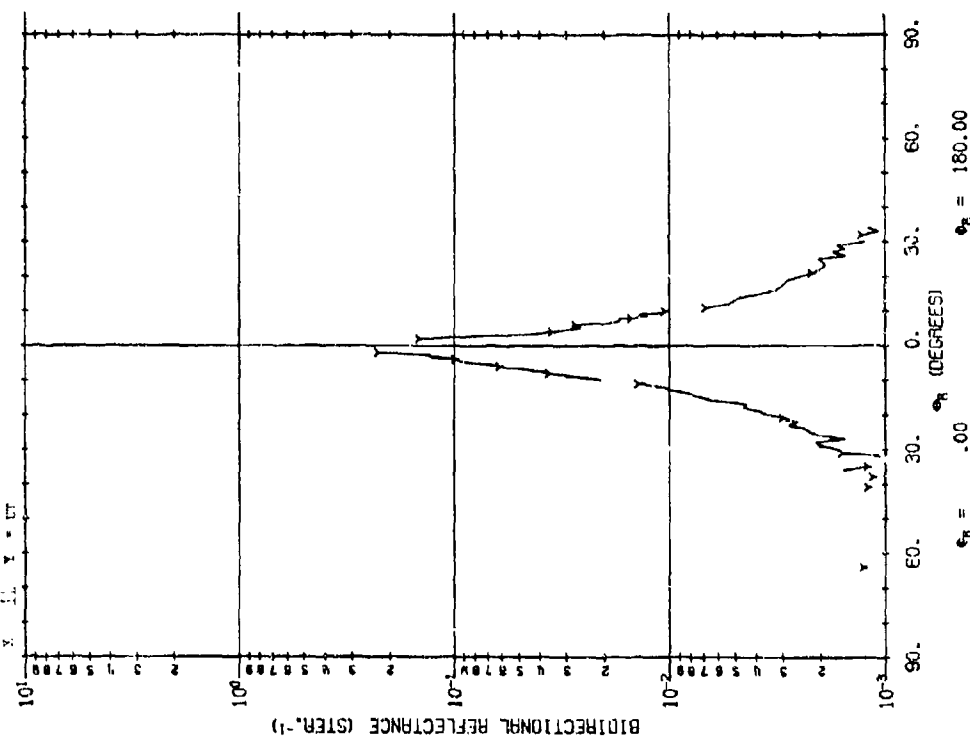
0  $\theta_i = 2.0$   
 +  $\theta_r = 4.0$   
 -  $\theta_t = 10.6$   
 X  $\theta = 10.6$   
 Y  $\theta = 10.6$



A01880 201

Green Paint on Metal

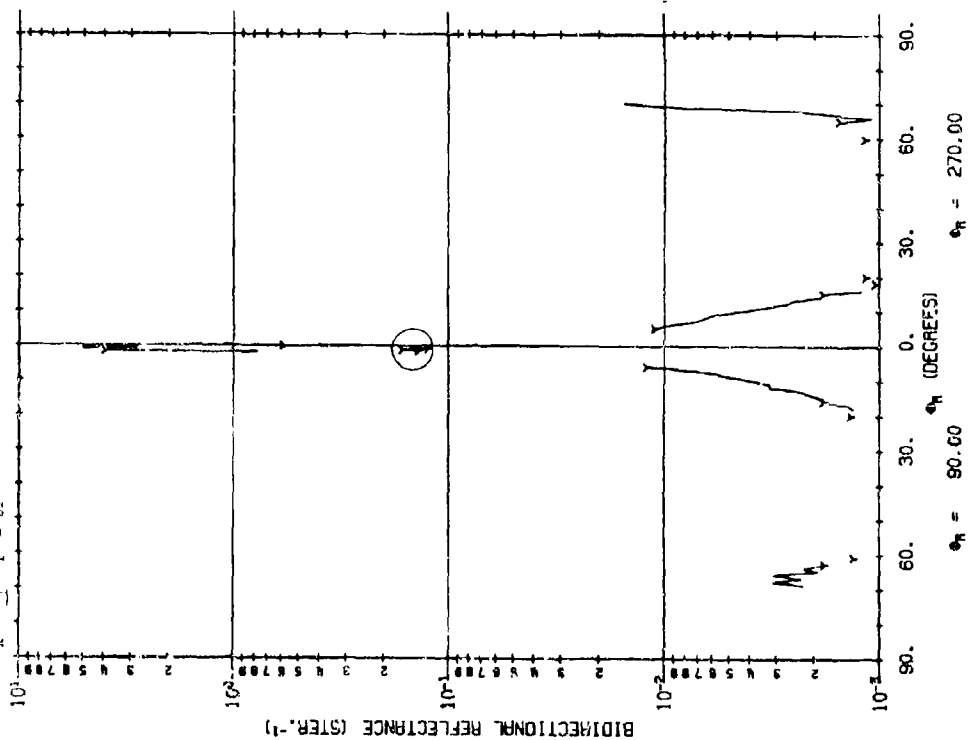
0  $\theta_i = 0.0$   
 +  $\theta_r = 180.0$   
 -  $\theta_t = 10.6$   
 X  $\theta = 10.6$   
 Y  $\theta = 10.6$



A01880 2C1

Green Paint on Metal

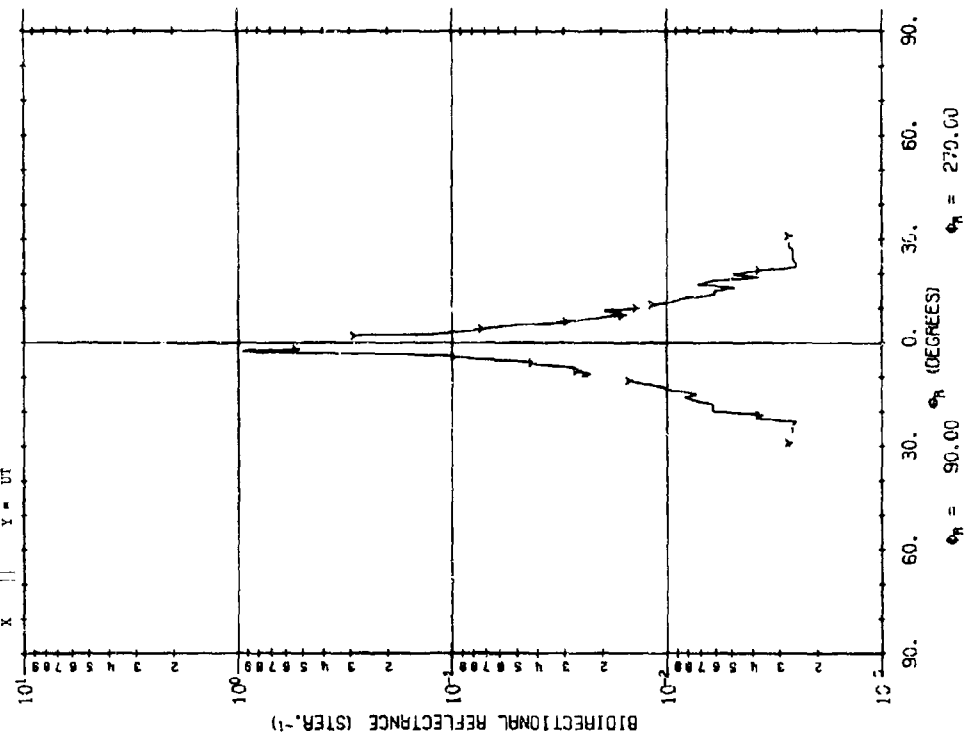
0 11 2.0  
- 11 2.0  
- 11 2.0  
X 11 2.0



A01880 201

GREEN PAINT ON METAL

0 11 0.0  
+ 11 0.0  
- 11 0.0  
X 11 0.0

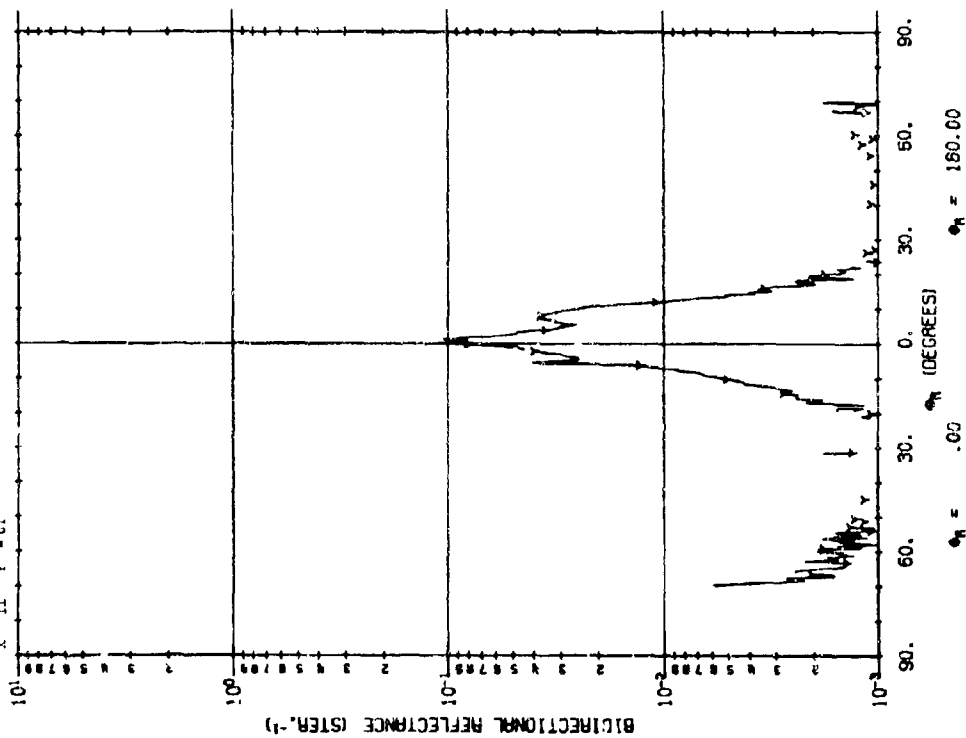


PAINT

A01881 301

Black Paint on Metal

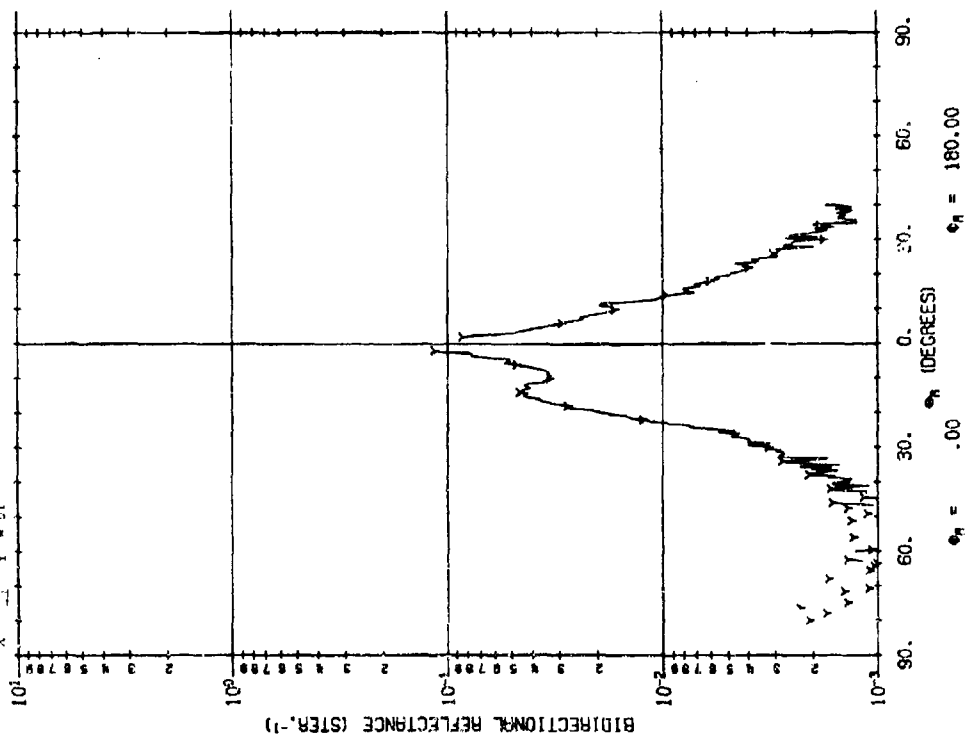
0 1 2 3 = 2.0  
+ 1 2 3 = 4.0  
- 1 2 3 = 10.6  
X 11 Y = UT



A01881 301

Black Paint on Metal

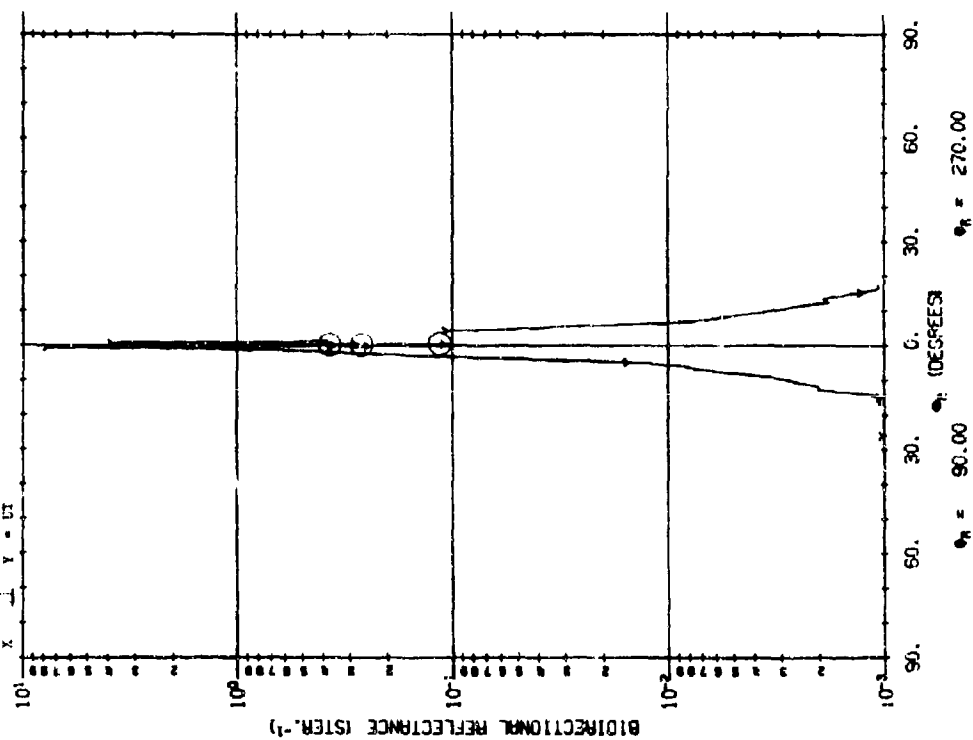
0 1 2 3 = 0.0  
+ 1 2 3 = 180.0  
- 1 2 3 = 10.6  
X 11 Y = UT



A01881 301

Black Paint on Metal

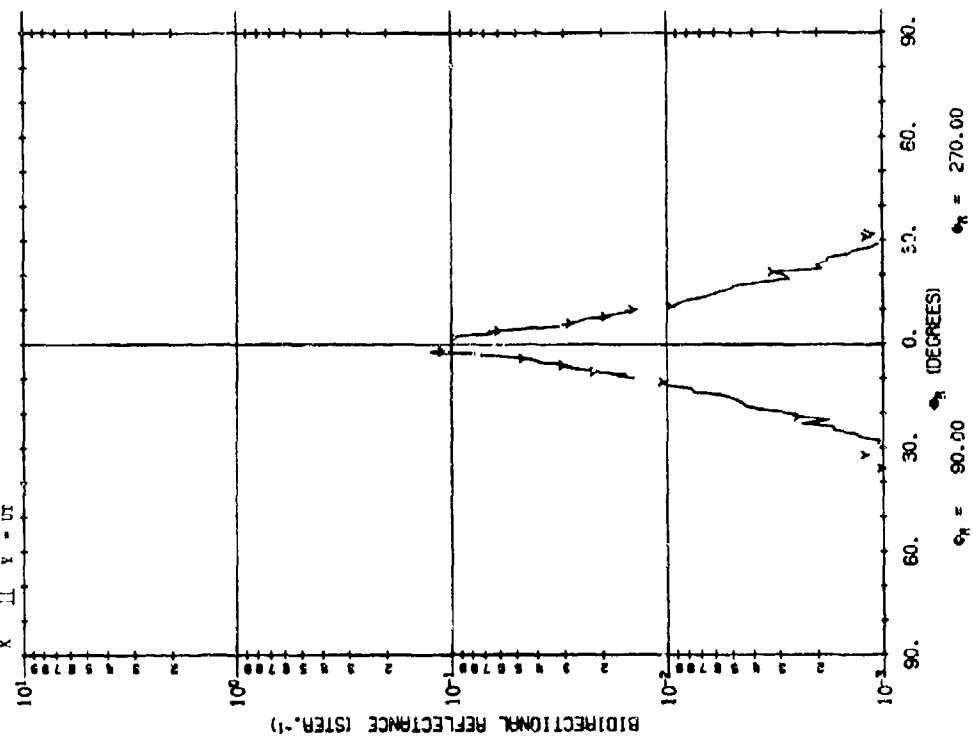
0 11 20 = 2.0  
+ 11 11 11 = 11  
- 11 11 11 = 11  
X 11 11 11 = 11  
Y = DT



A01881 301

Black Paint on Metal

0 11 0.0  
+ 11 11 11 = 11  
- 11 11 11 = 11  
X 11 11 11 = 11  
Y = DT



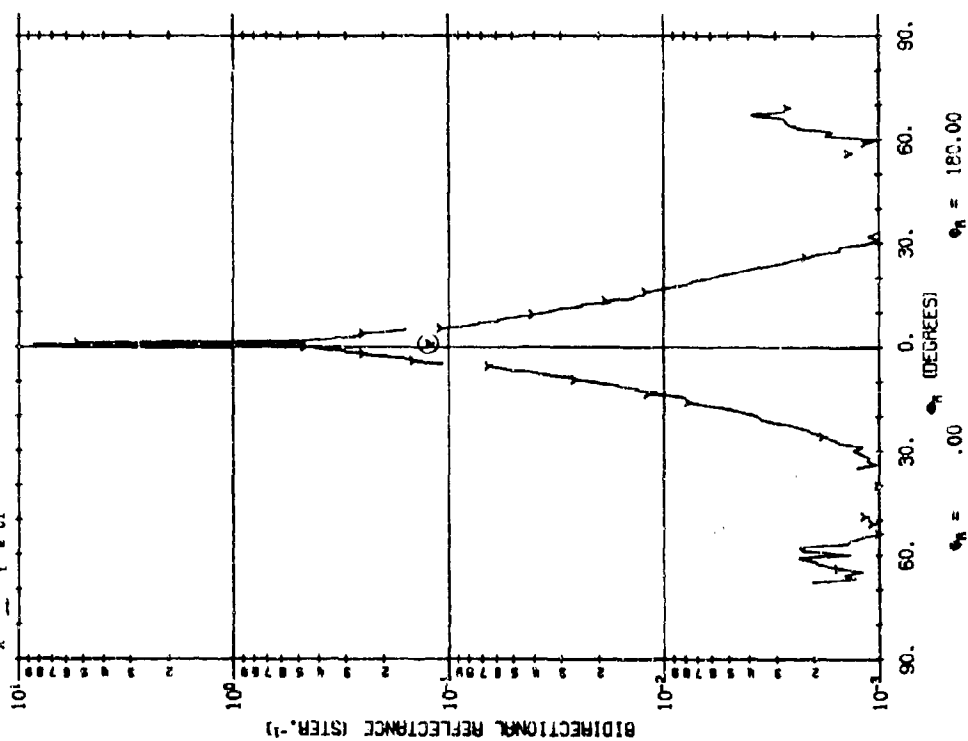
PAINT



R01882 201

Orange Paint on Metal

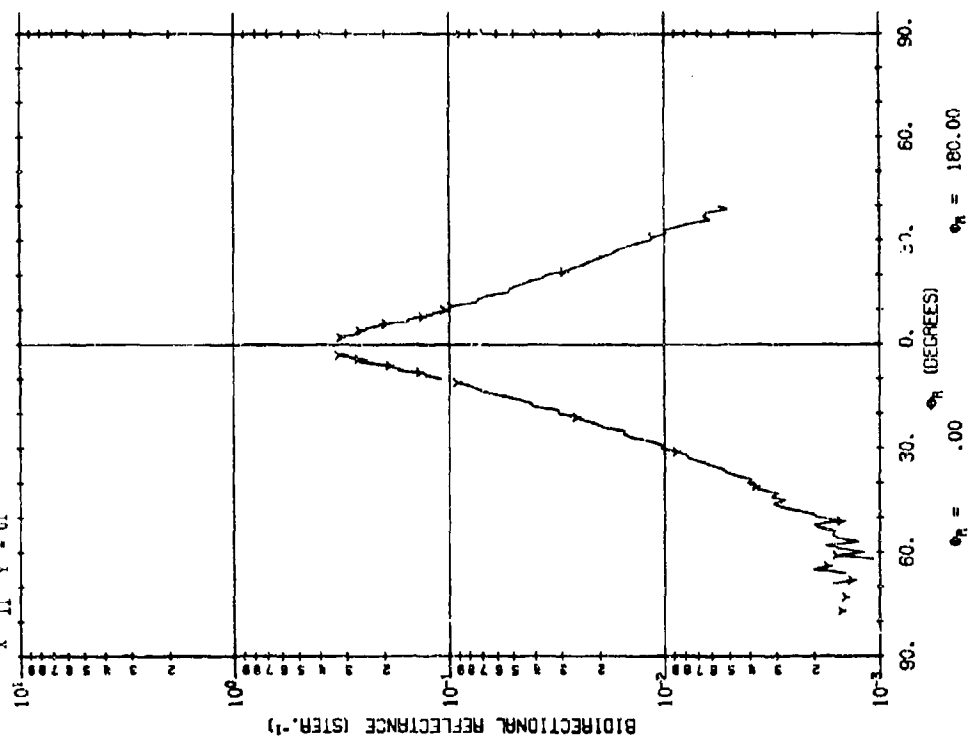
0  $\theta_1 = 2.0$   
 +  $\theta_2 = 3.0$   
 x  $\theta_3 = 10.6$   
 x  $\theta_4 = 51$



R01882 201

Orange Paint on Metal

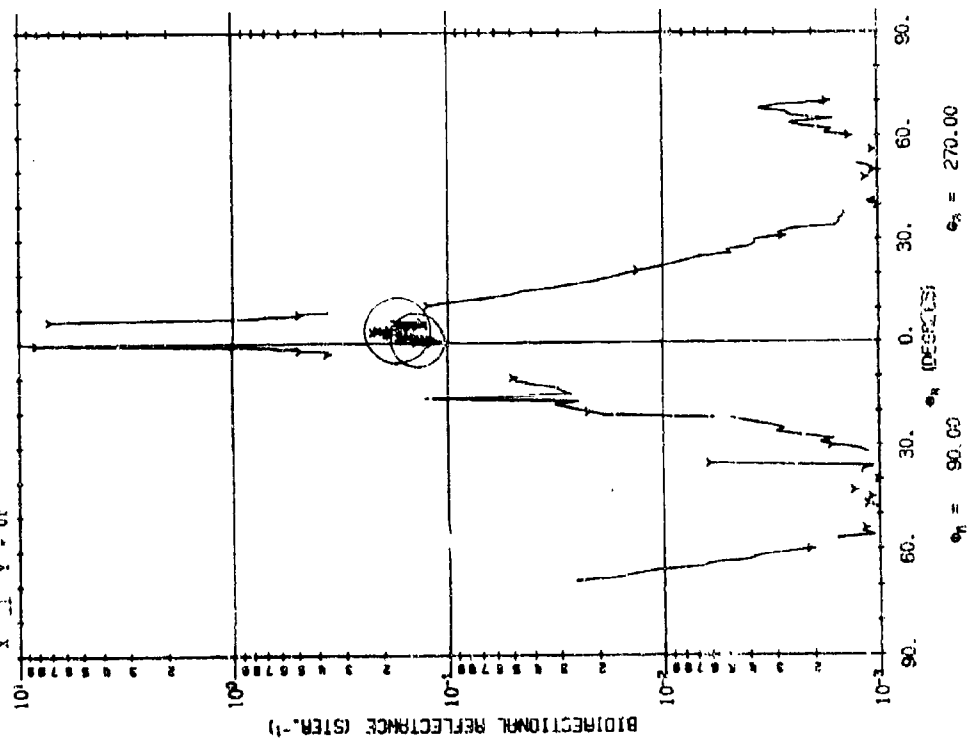
0  $\theta_1 = 0.0$   
 +  $\theta_2 = 180.0$   
 x  $\theta_3 = 10.6$   
 x  $\theta_4 = 51$



R01882 201

Orange Paint on Metal

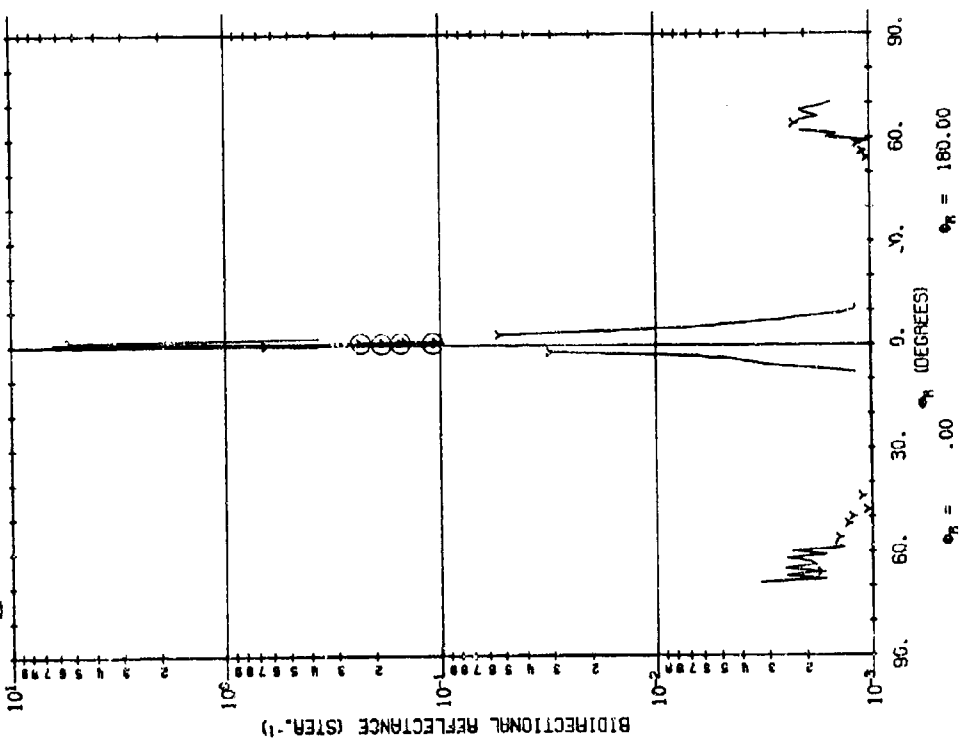
0 11 22 = 2.0  
+ 11 21 =  $\phi_r$   
- 11 21 = 10.6  
X 11 Y = UT



R01883 101

Olive Drab Paint on Metal

0 11 22 = 2.0  
+ 11 21 =  $\phi_r$   
- 11 21 = 10.6  
X 11 Y = UT

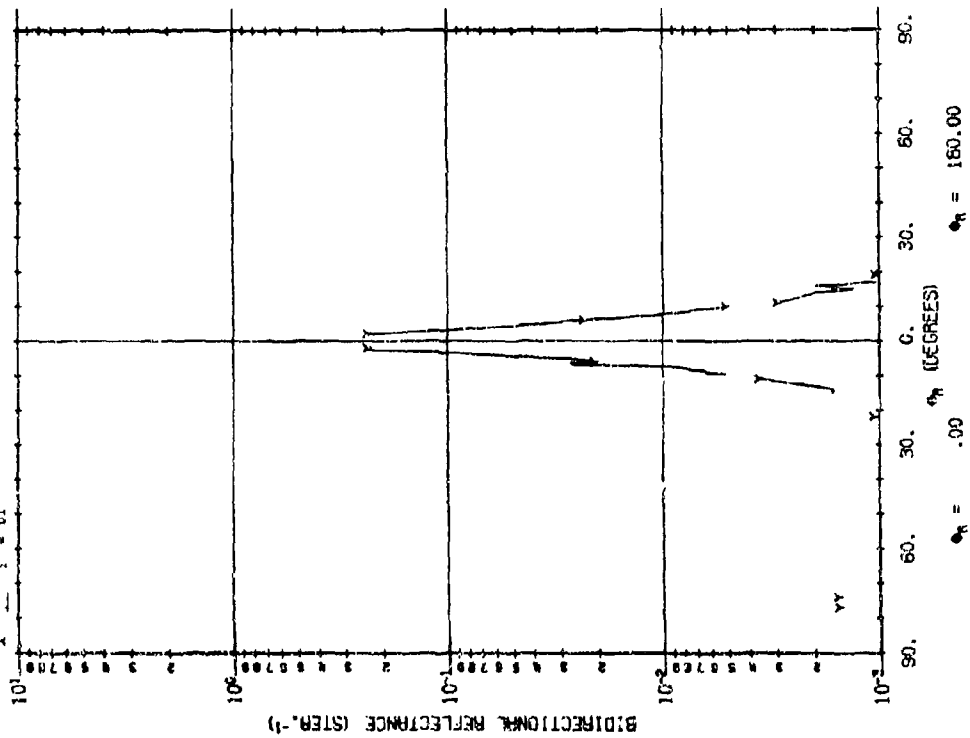


PAINT

A01883 101

Olive Drab Paint on Metal

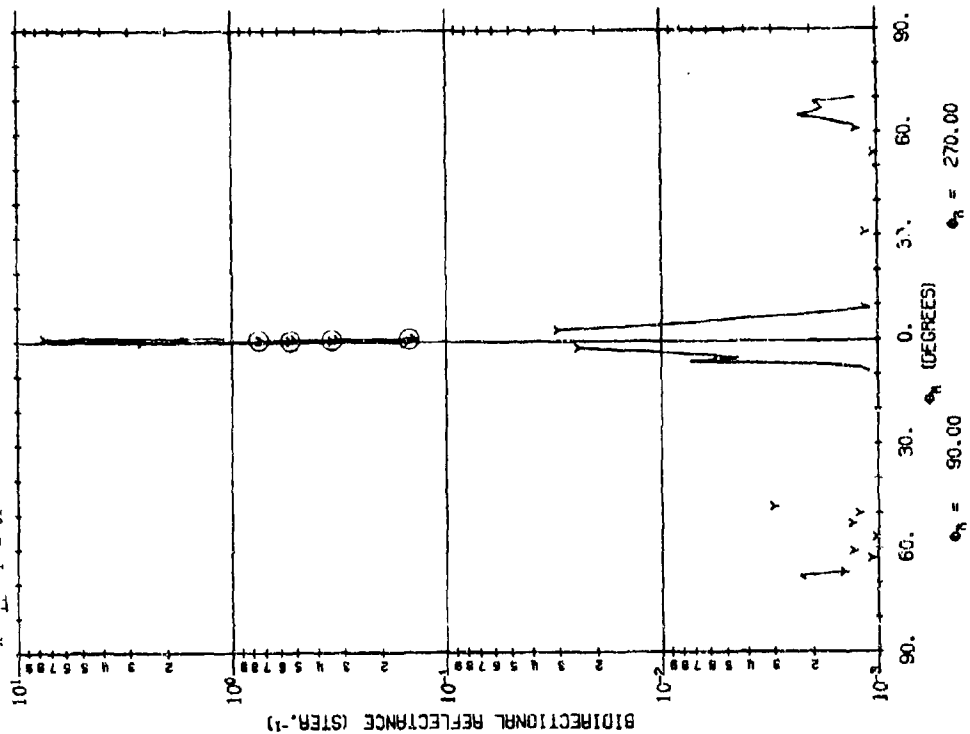
0 11  $\phi_i = 0.0$   
 + 11  $\phi_i = 180.0$   
 - 11  $\lambda = 10.6$   
 X 11 Y = UT



A01883 101

Olive Drab Paint on Metal

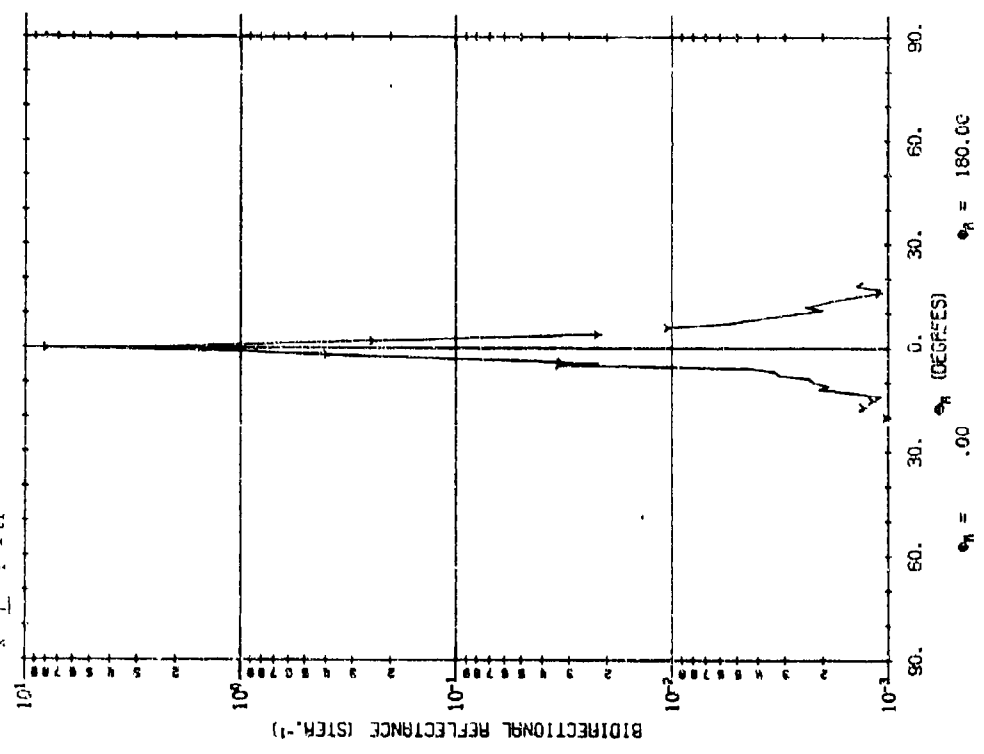
0 11  $\phi_i = 2.0$   
 + 11  $\phi_i = 4$   
 - 11  $\lambda = 10.6$   
 X 11 Y = UT



CO1887 201

Blue Paint on Metal

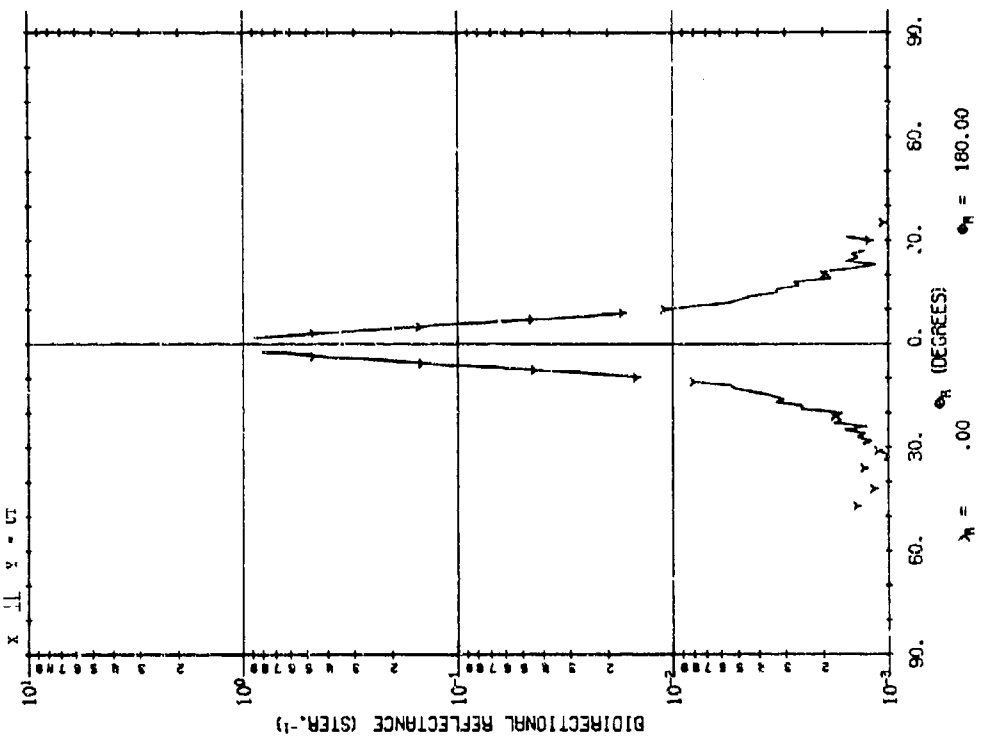
0  $\theta_1 = 2.0$   
 +  $\theta_2 = 0.0$   
 x  $\theta_3 = 10.6$   
 y  $\theta_4 = 180.0$



CO1887 201

Blue Paint on Metal

0  $\theta_1 = 0.0$   
 +  $\theta_2 = 180.0$   
 x  $\theta_3 = 10.6$   
 y  $\theta_4 = 180.0$

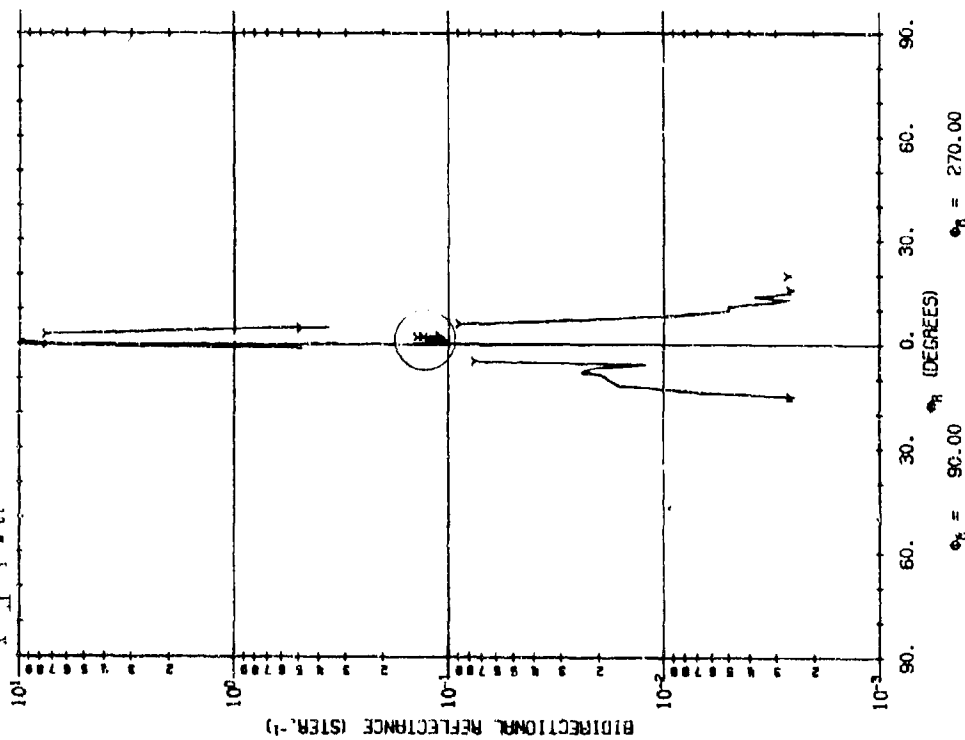


PAIN

R01887 201

Blue Paint on Metal

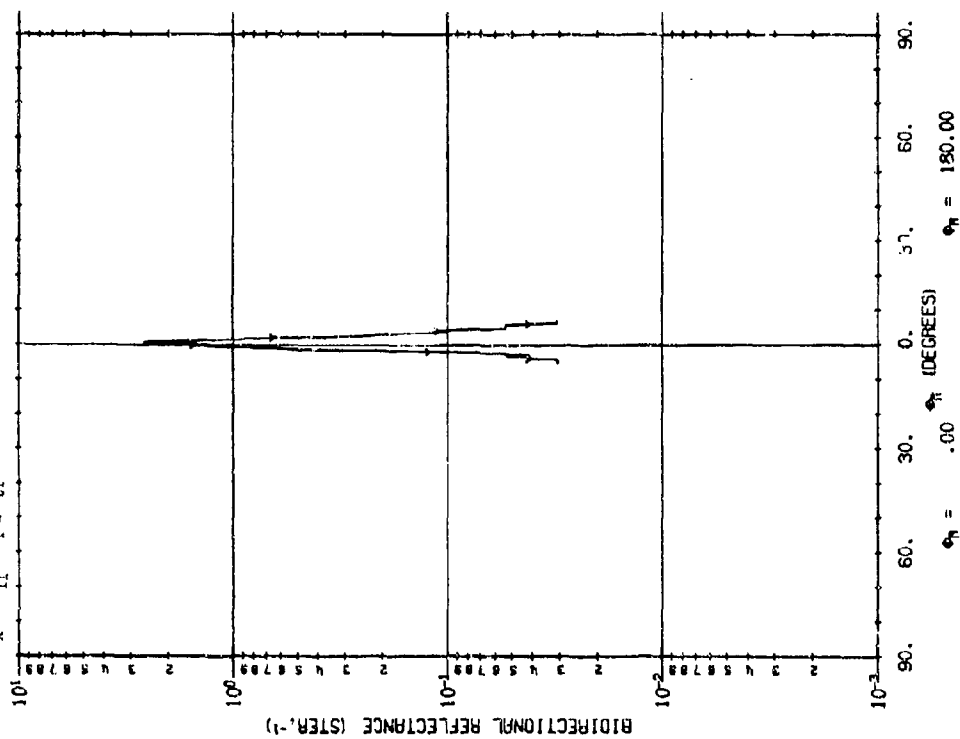
0 11 25 = 2.0  
+ 11  $\phi_1 = \phi_r$   
- 11  $\lambda = 10.6$   
x 11  $\gamma = \gamma_t$



R01888 201

OLIVE DRAB PAINT ON BLUE PAINTED METAL

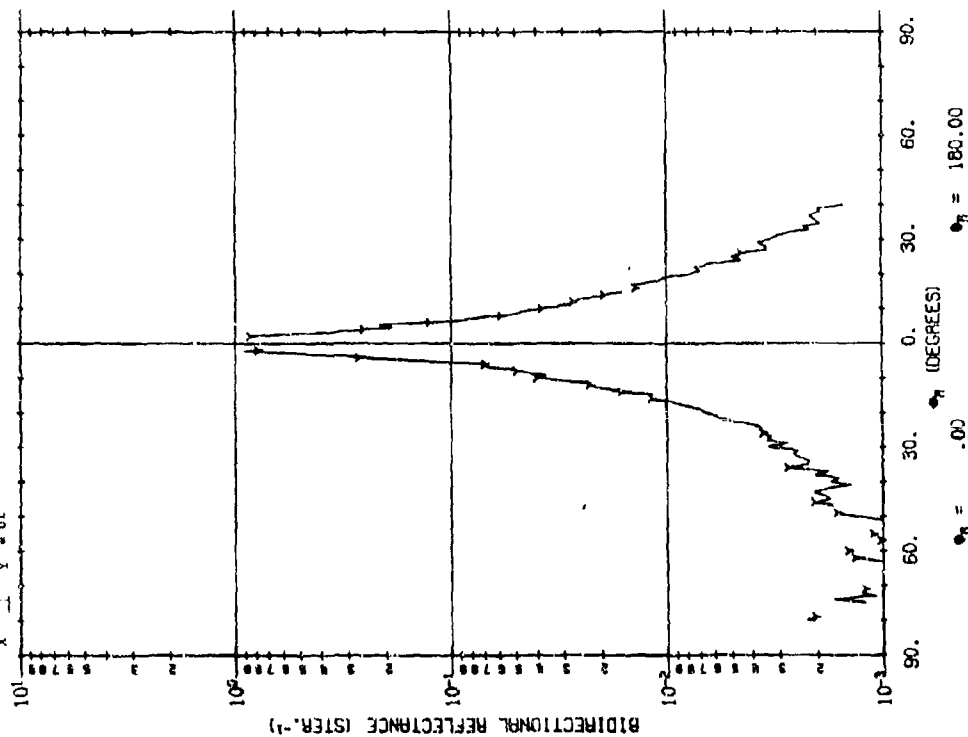
0 11 25 = 2.0  
+ 11  $\phi_1 = \phi_r$   
- 11  $\lambda = 10.6$   
x 11  $\gamma = \gamma_t$



A01888 201

Olive Drab Paint on Blue Painted Metal

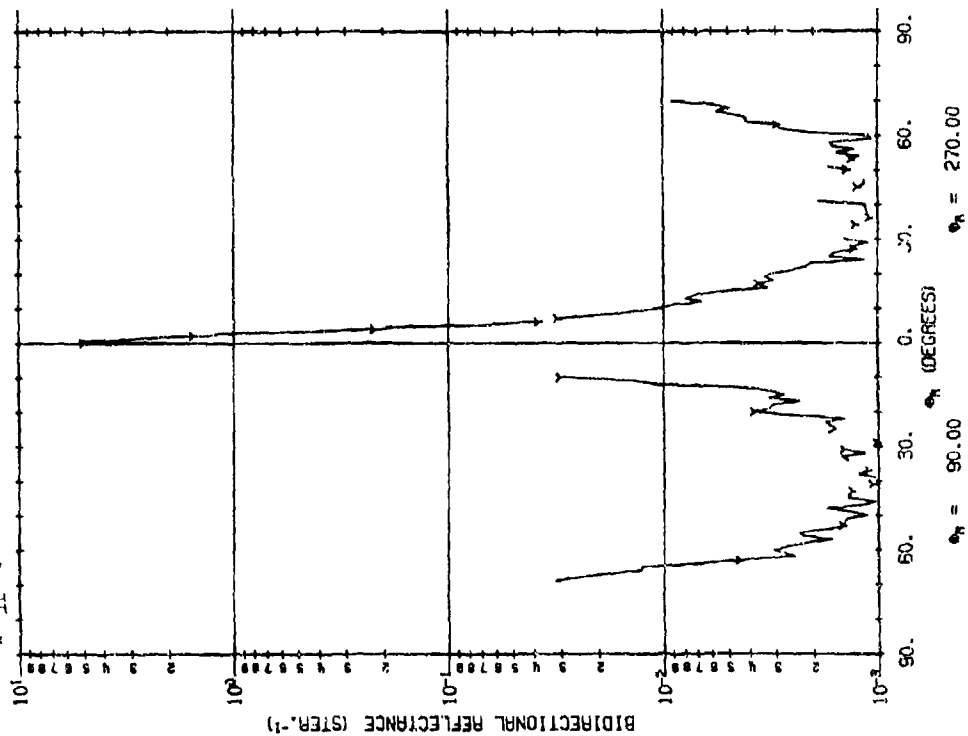
0 11  $\theta_1 = 0.0$   
 + 11  $\theta_1 = 180.0$   
 x 11  $\theta_1 = 19.6$   
 x 11  $\theta_1 = 19.6$



A01888 201

Olive Drab Paint on Blue Painted Metal

0 11  $\theta_1 = 2.0$   
 + 11  $\theta_1 = 6.0$   
 x 11  $\theta_1 = 10.6$   
 x 11  $\theta_1 = 10.6$



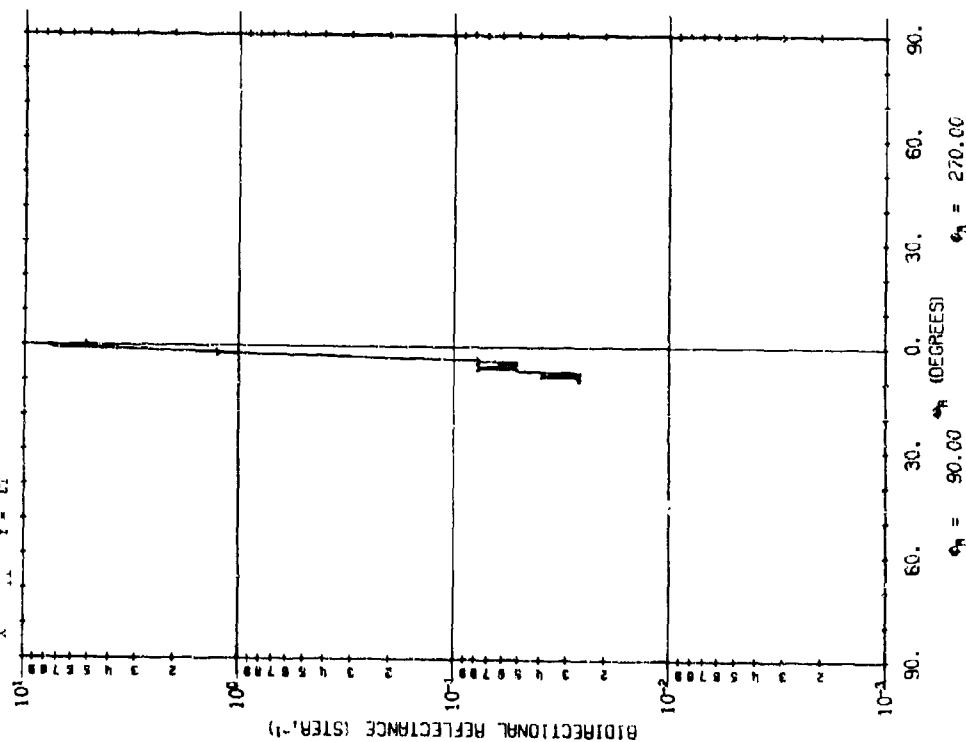
PAINT

R01888 201

OLIVE DRAB PAINT ON BLUE PAINTED METAL

0 1 2 3 4 5 6 7 8 9  
+ 11 12 13 14 15 16 17 18 19  
- 1 2 3 4 5 6 7 8 9  
X 1 2 3 4 5 6 7 8 9

$\phi_1 = 0.0$   
 $\phi_2 = 0.0$   
 $\phi_3 = 10.6$   
 $\phi_4 = 0.0$

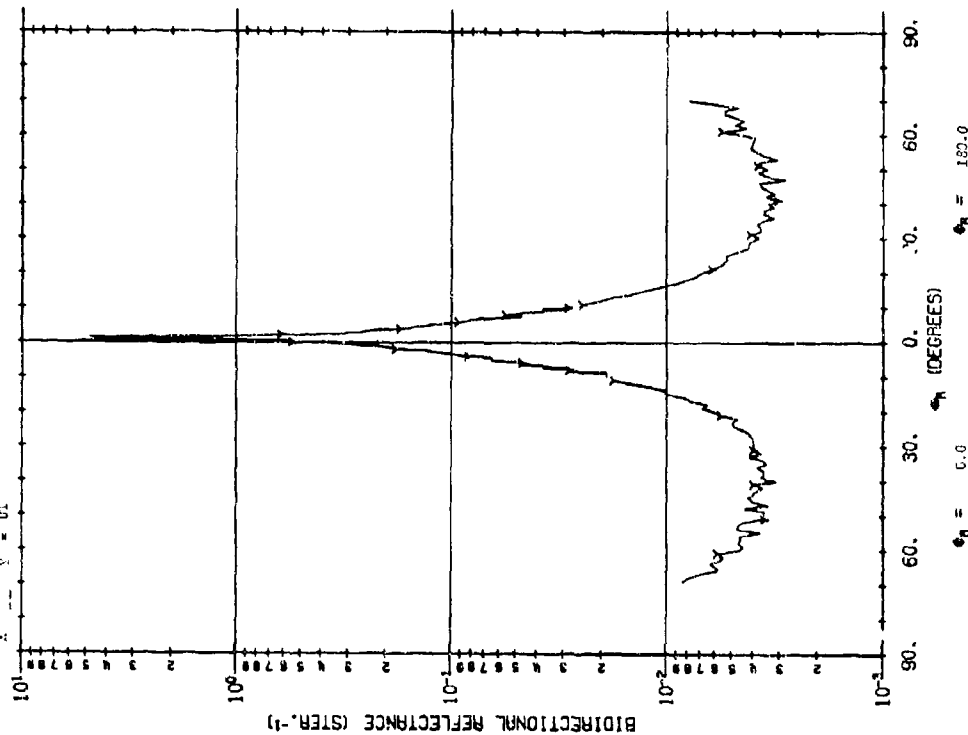


R01889 101

OLIVE DRAB PAINT ON GREEN PRIMER ON ALUMINUM

0 1 2 3 4 5 6 7 8 9  
+ 11 12 13 14 15 16 17 18 19  
- 1 2 3 4 5 6 7 8 9  
X 1 2 3 4 5 6 7 8 9

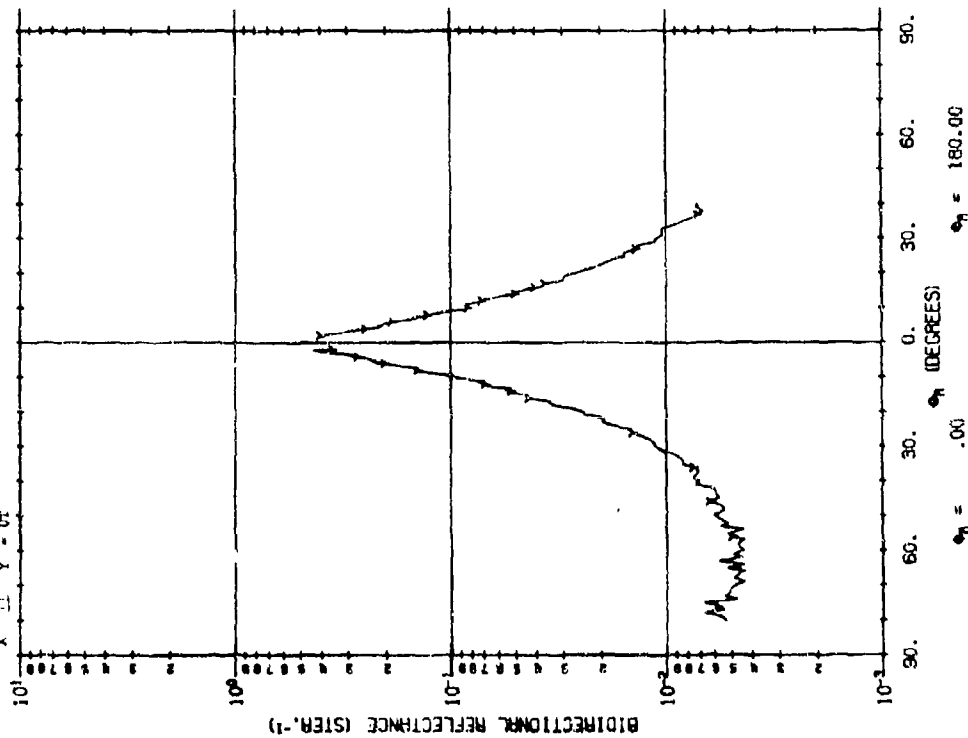
$\phi_1 = 2.0$   
 $\phi_2 = 0.0$   
 $\phi_3 = 10.6$   
 $\phi_4 = 0.0$



A01889 101

Olive Drab Paint on Green Primer on  
Aluminum

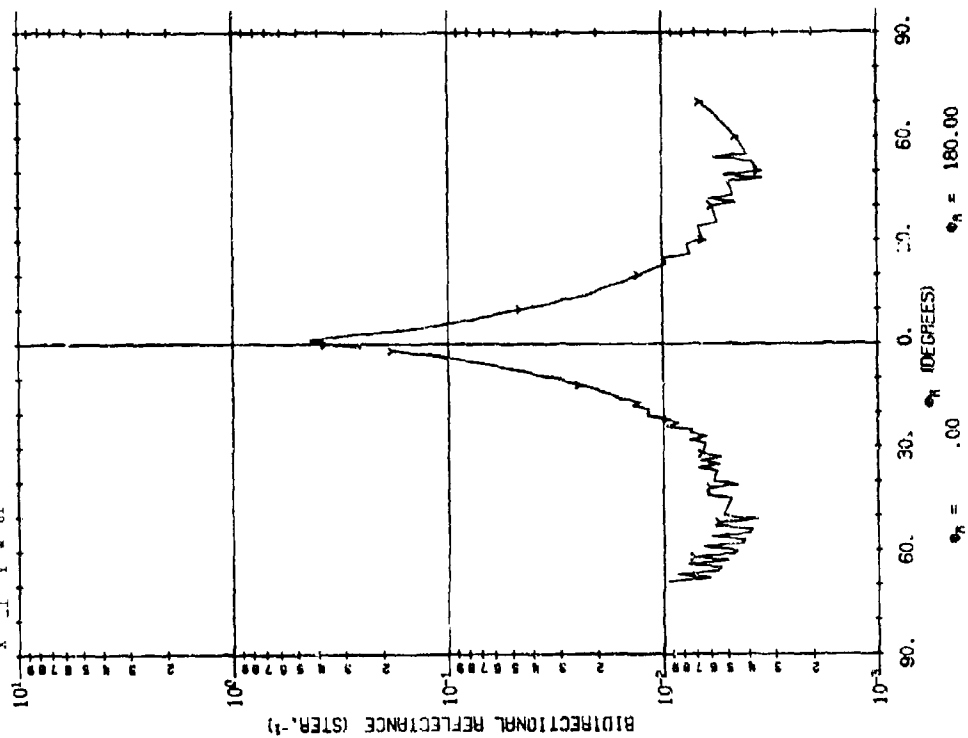
$\theta_i = 0.0$   
 $\theta_r = 180.0$   
 $\lambda = 10.6$   
X Y Z



A01892 301

Olive Drab Paint on Aluminum

$\theta_i = 2.0$   
 $\theta_r = 180.0$   
 $\lambda = 10.6$   
X Y Z



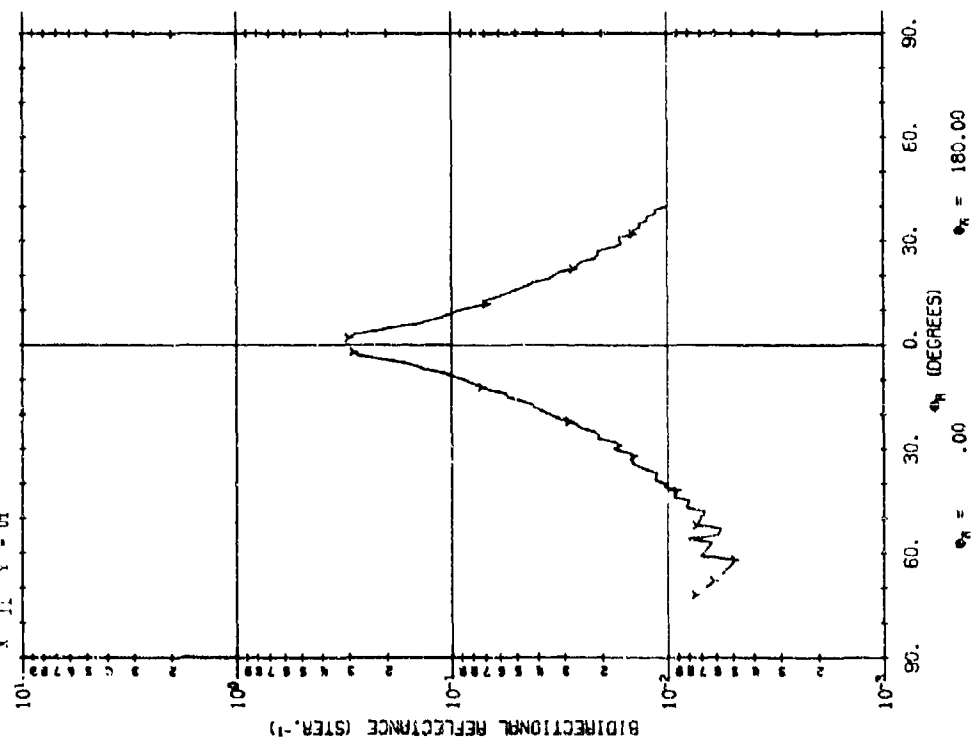
PAINT



R01892 301

Olive Drab Paint on Aluminum

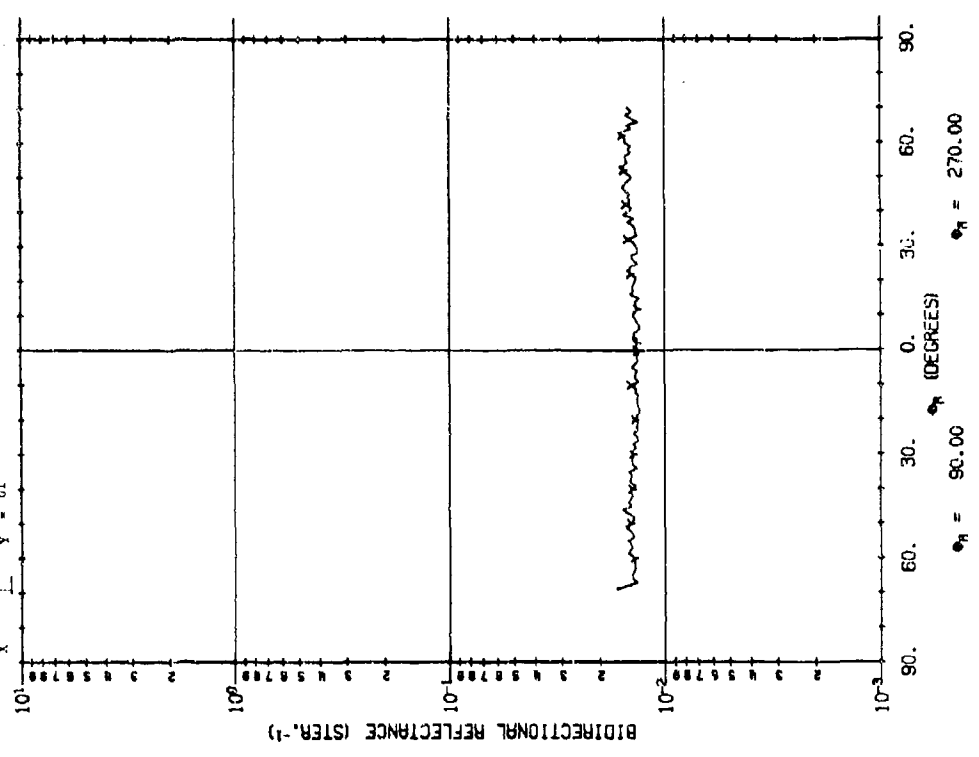
$\theta_i = 0.0$   
 $\theta_r = 180.0$   
 $\phi_i = 10.6$   
 $\phi_r = 10.6$   
 $\phi_h = 180.00$   
 $\phi_h = 180.00$

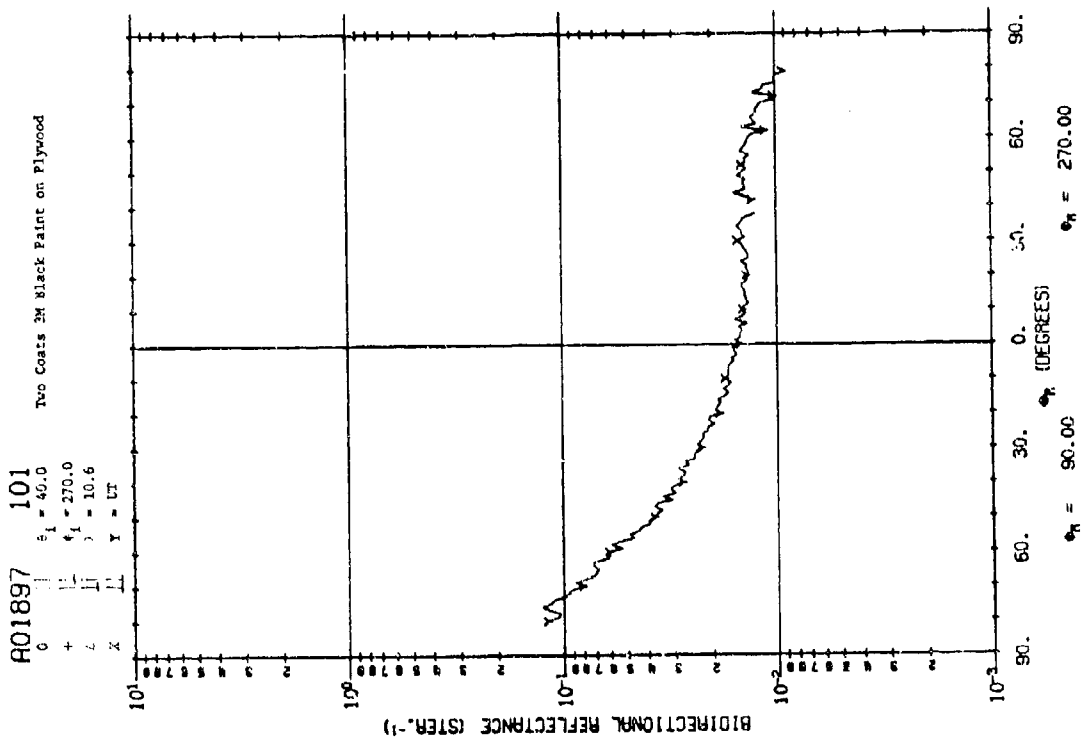
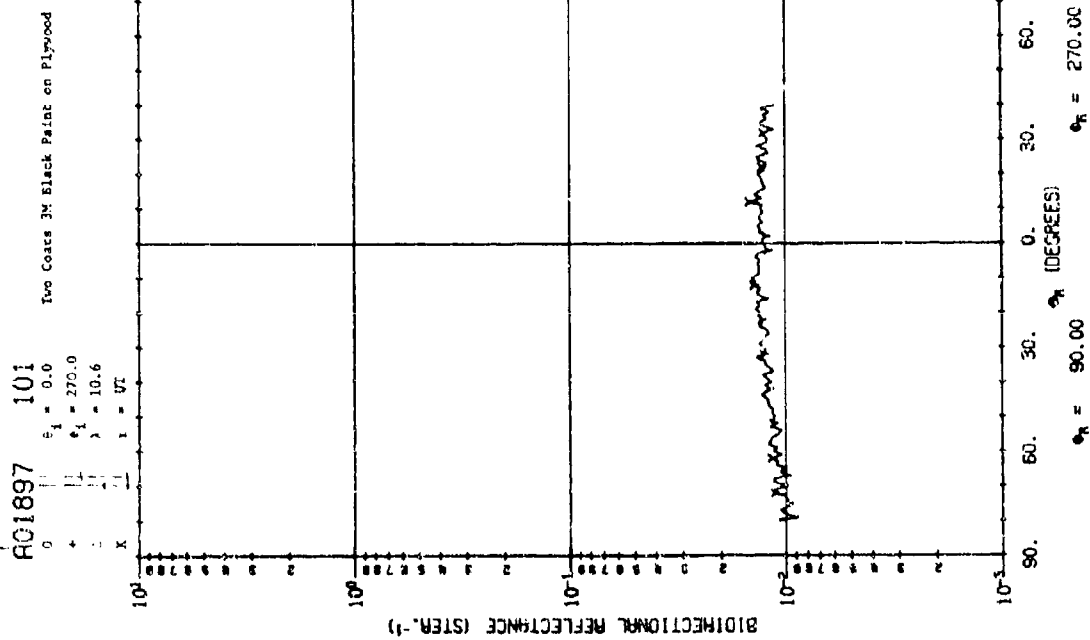


R01897 101

Two Coats 3M Black Paint on Plywood

$\theta_i = 2.0$   
 $\theta_r = 180.0$   
 $\phi_i = 10.6$   
 $\phi_r = 10.6$   
 $\phi_h = 270.00$   
 $\phi_h = 270.00$



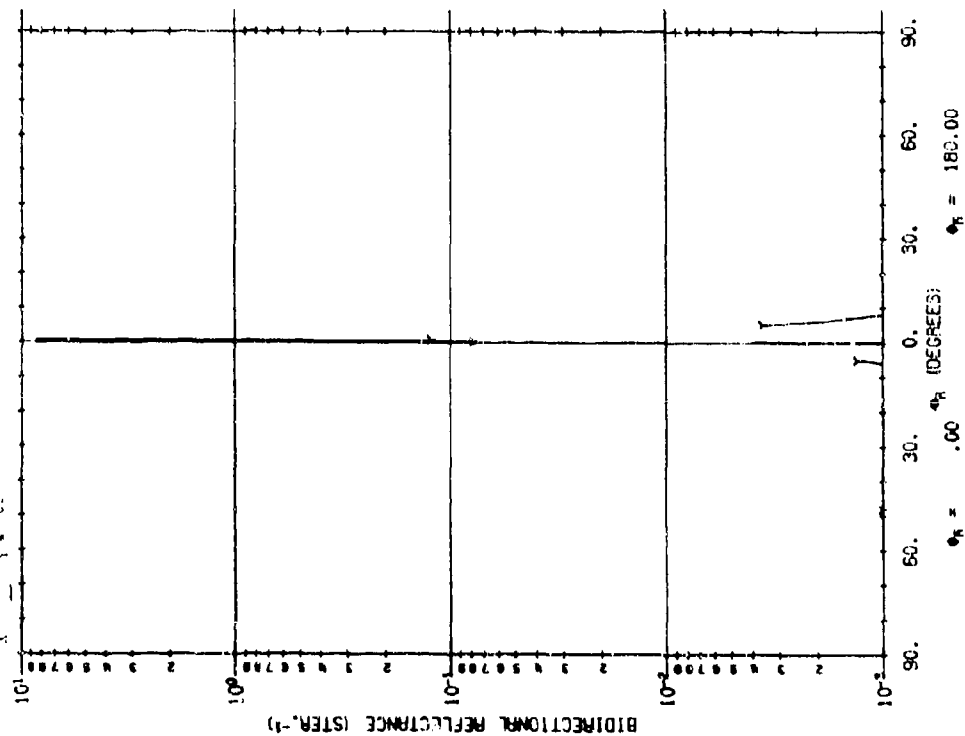


PAINT

R01917 101

OLIVE DRAB KEYLON PAINT ON ALUMINUM

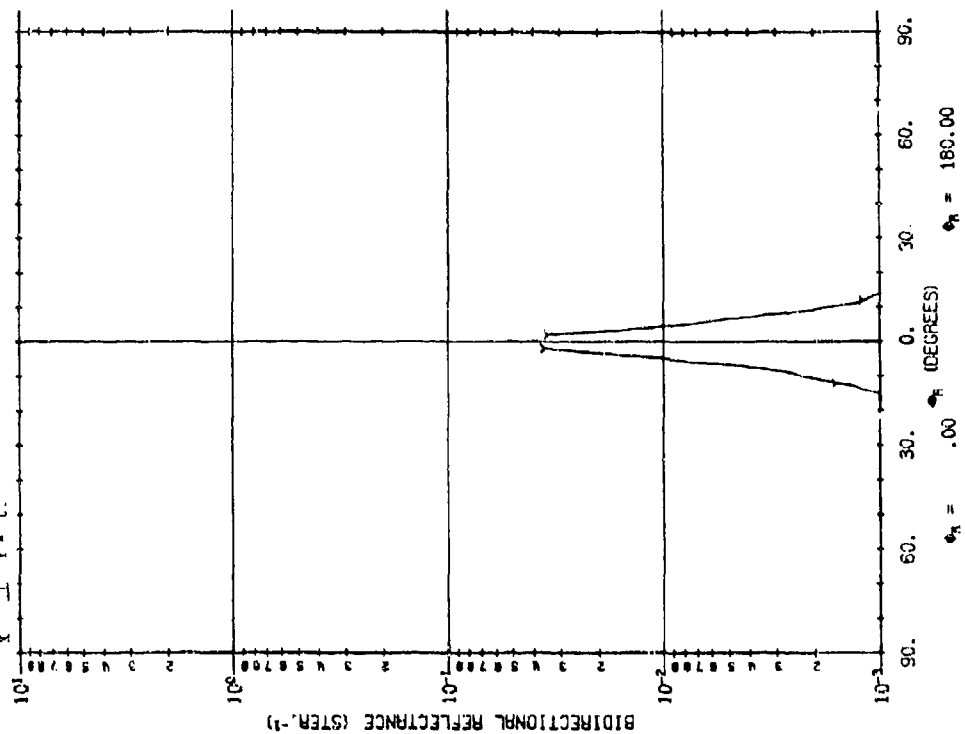
0  $\theta_i = 2.0$   
 +  $\theta_r = 183.0$   
 -  $\lambda = 10.6$   
 x  $\gamma = 0$



R01917 101

OLIVE DRAB KEYLON PAINT ON ALUMINUM

0  $\theta_i = 0.0$   
 +  $\theta_r = 183.0$   
 -  $\lambda = 10.6$   
 x  $\gamma = 0$

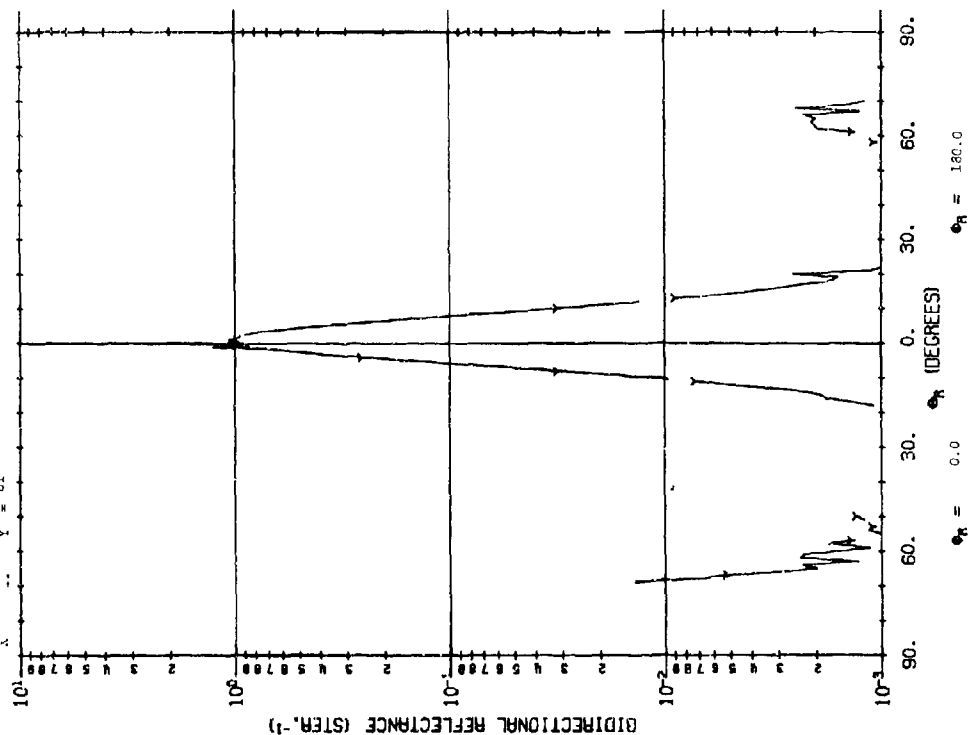




A01922 101

Olive Drab Krylon Paint on  
White Posterboard

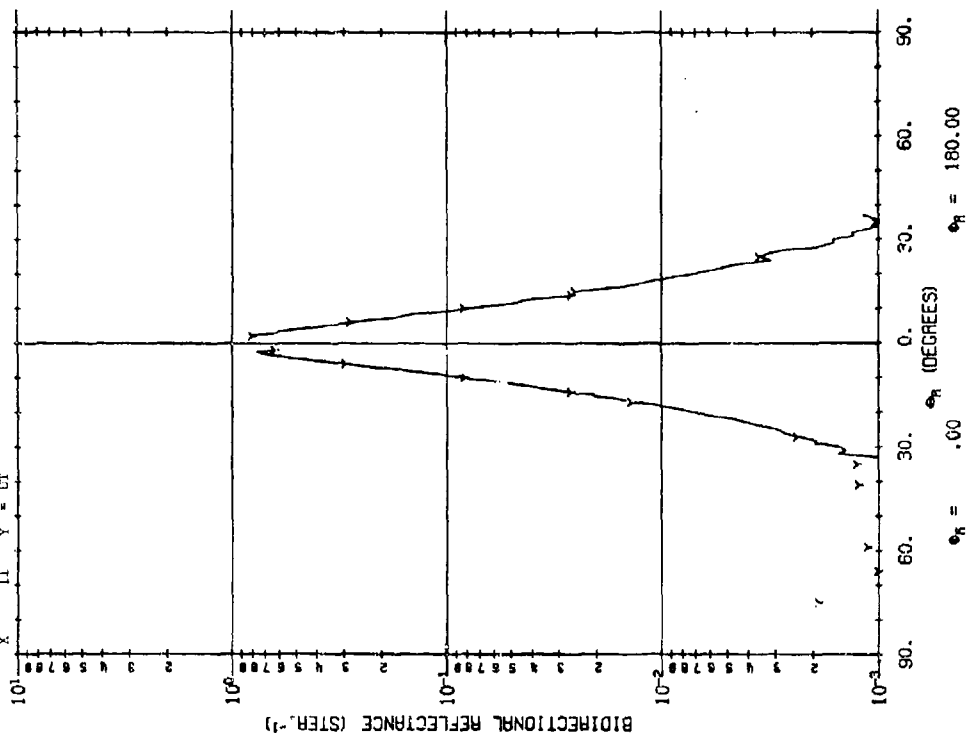
0  $\theta_i = 2.0$   
+  $\theta_i = \phi_r$   
-  $\theta_i = 10.6$   
X Y = UT



A01922 101

Olive Drab Krylon Paint on  
White Posterboard

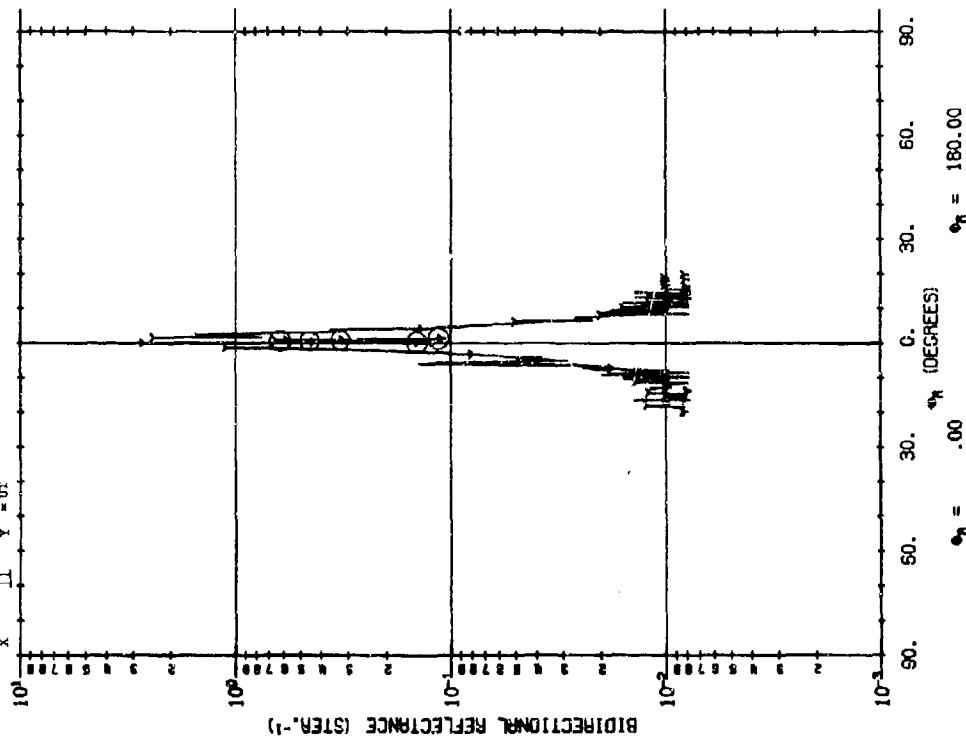
0  $\theta_i = 0.0$   
+  $\theta_i = 180.0$   
-  $\theta_i = 10.6$   
X Y = UT



A01924 101

Olive Drab Krylon Paint on  
Acrylic Plexiglass

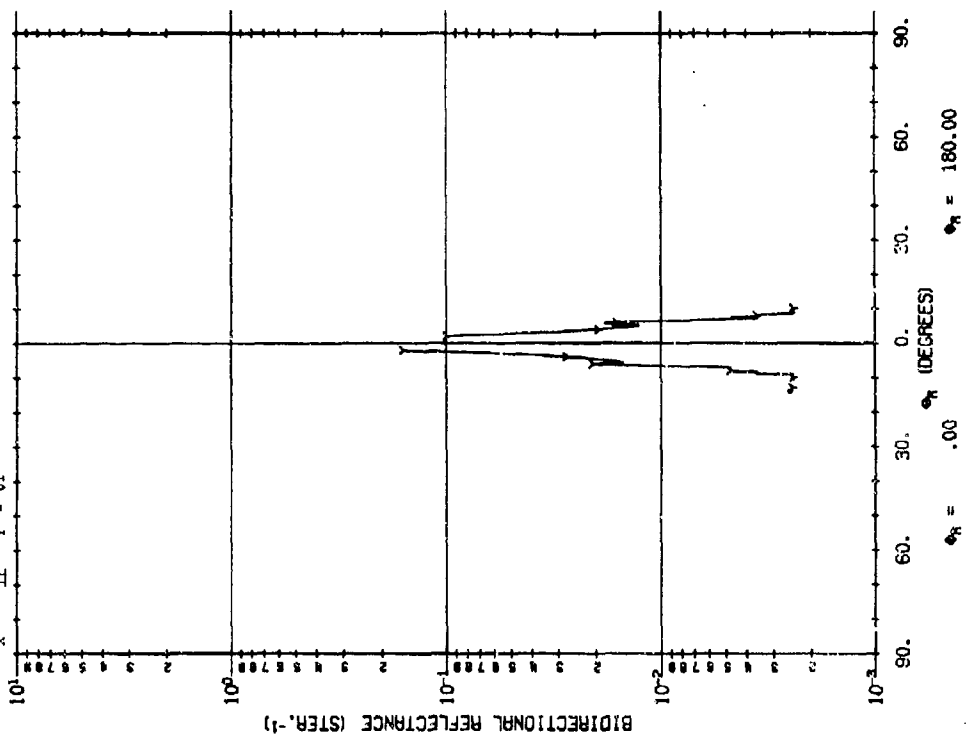
0 28 = 2.0  
+  $\phi_1 = \phi_r$   
 $\lambda = 10.6$   
X Y = UT



A01924 101

Olive Drab Krylon Paint on  
Acrylic Plexiglass

0  $\phi_1 = 0.0$   
+  $\phi_1 = 180.0$   
 $\lambda = 10.6$   
X Y = UT

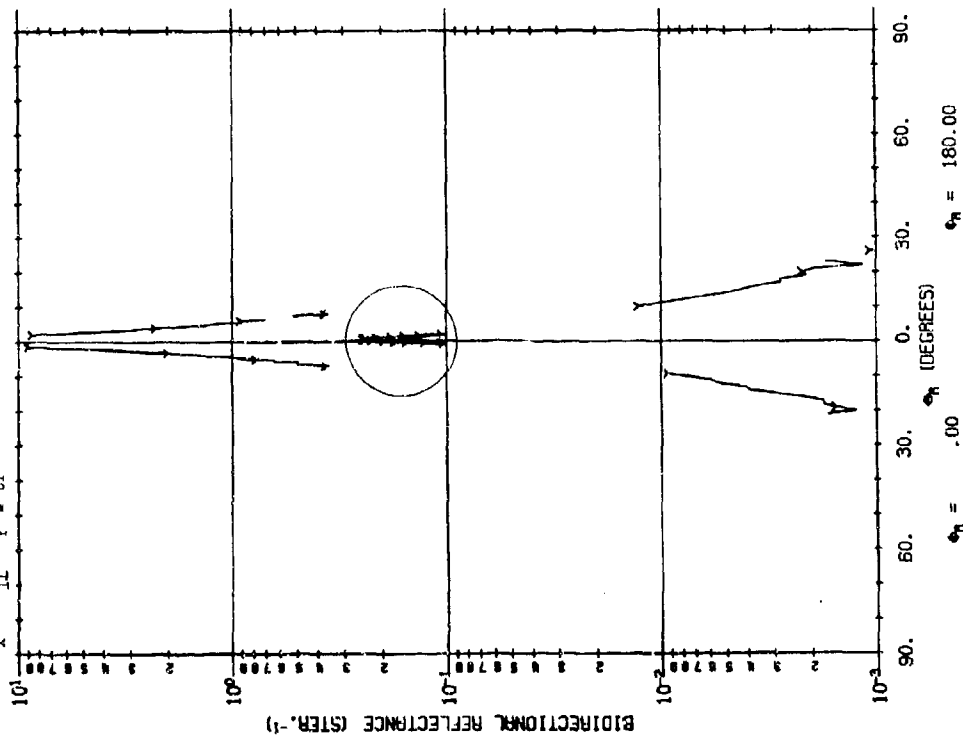


PAINT

A01926 101

Olive Drab Krylon Paint on Brown  
Corrugated Cardboard

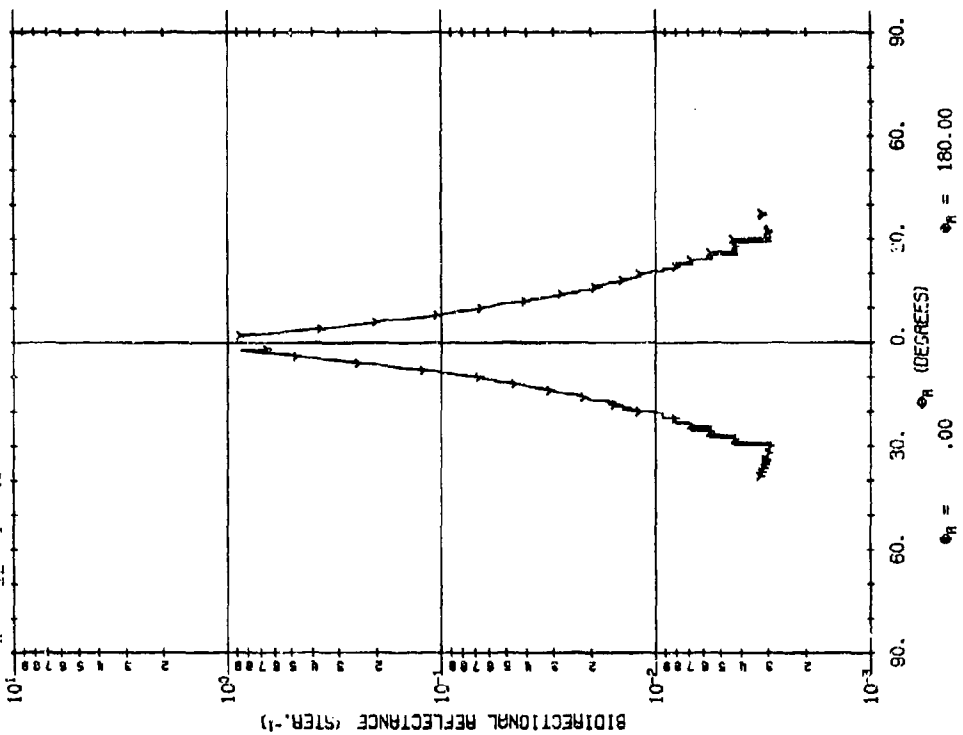
0 25 = 2.0  
+ 11 21 = 10  
2 11 11 = 10.6  
X Y = UT

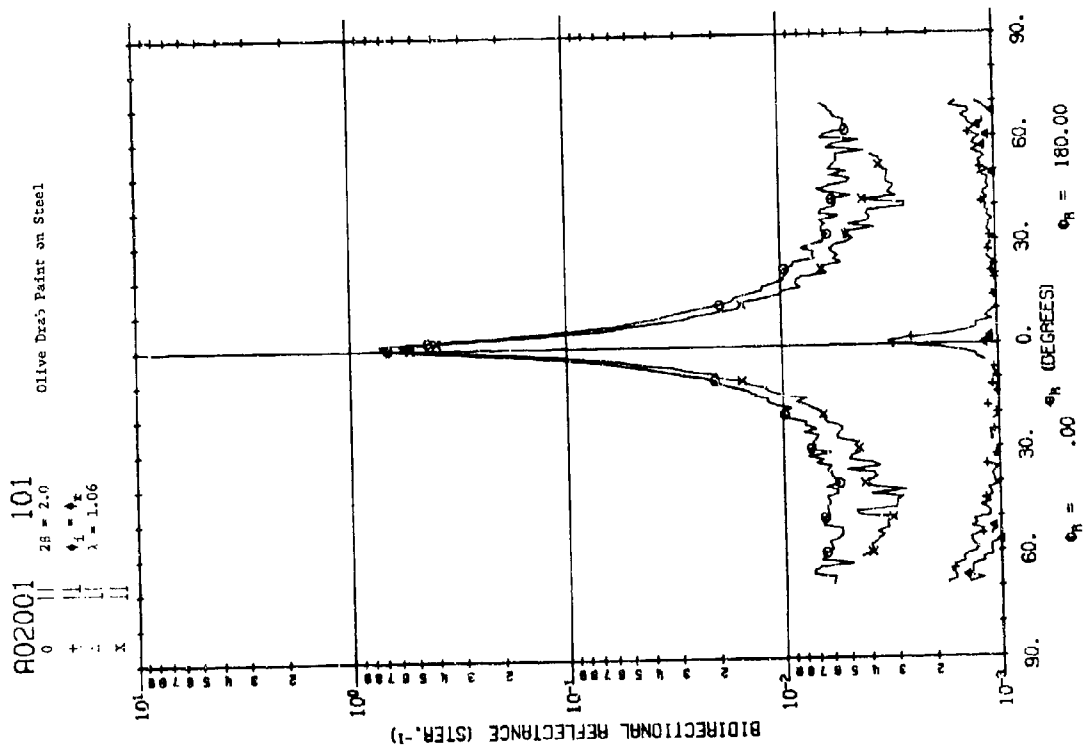
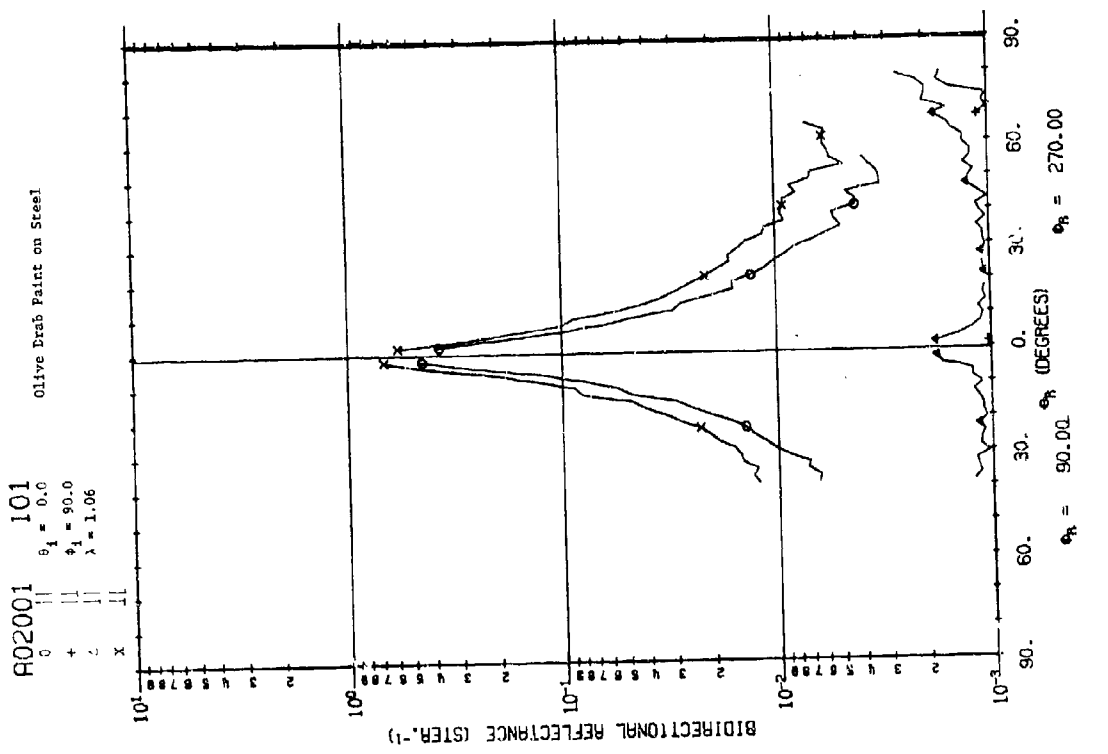


A01926 101

Olive Drab Krylon Paint on Brown  
Corrugated Cardboard

0 25 = 0.0  
+ 11 21 = 180.0  
2 11 11 = 10.6  
X Y = UT





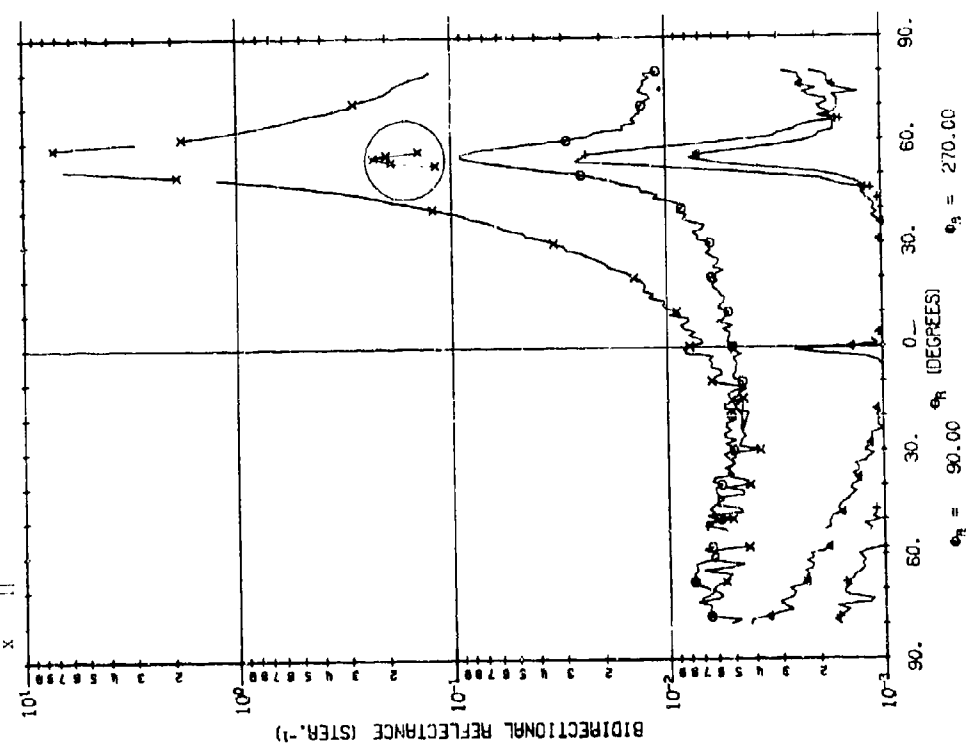
PAINT



A02001 101

Olive Drab Paint on Steel

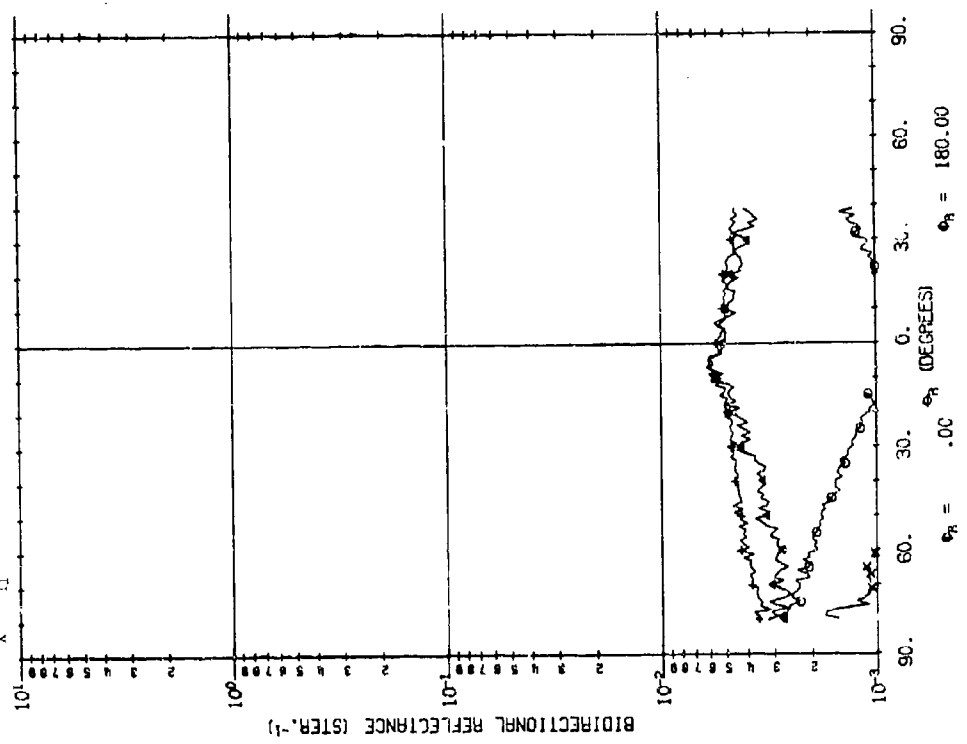
$\theta_i = 56.0$   
 $\theta_r = 90.0$   
 $\lambda = 1.06$



A02001 101

Olive Drab Paint on Steel

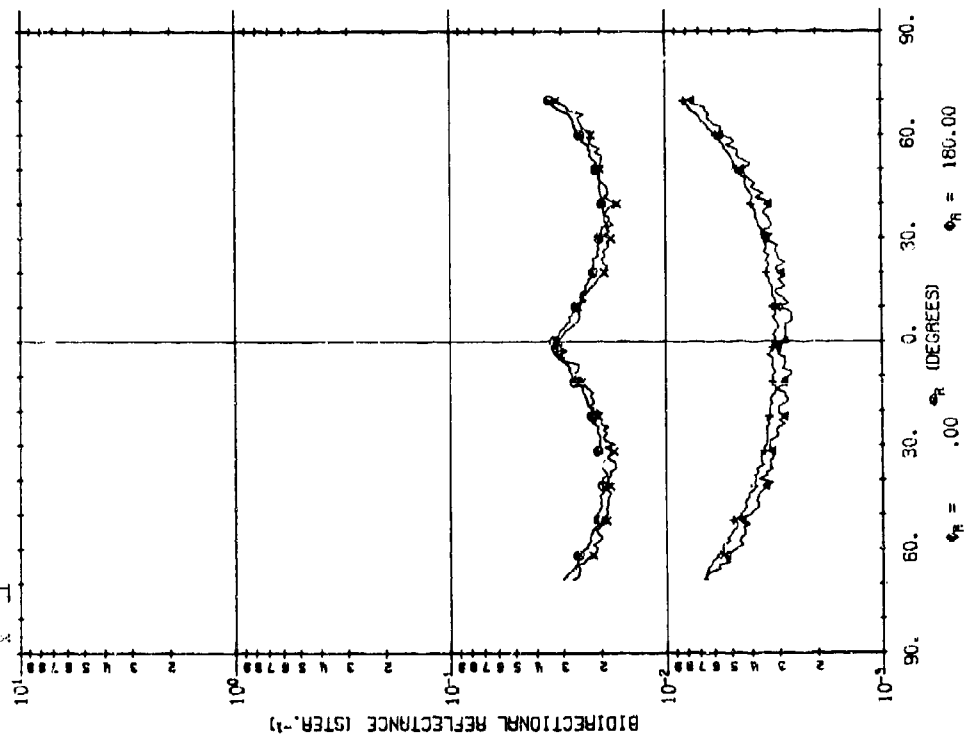
$\theta_i = 56.0$   
 $\theta_r = 90.0$   
 $\lambda = 1.06$



R02004 101

CLIVE DRAB PAINT ON STEEL

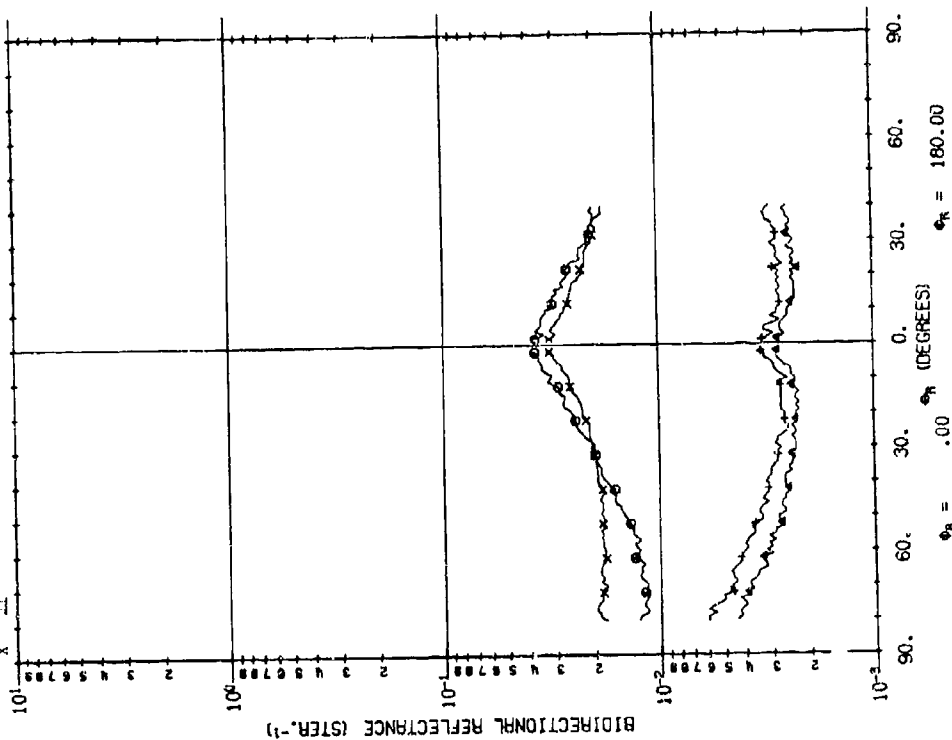
0 || 25 = 2.0  
+ ||  $\phi_t = \phi_r$   
2 || 1 = 1.06



R02004 101

OLIVE DRAB PAINT ON STEEL

0 ||  $\phi_t = 0.0$   
+ ||  $\phi_t = 180.0$   
2 || 1 = 1.06

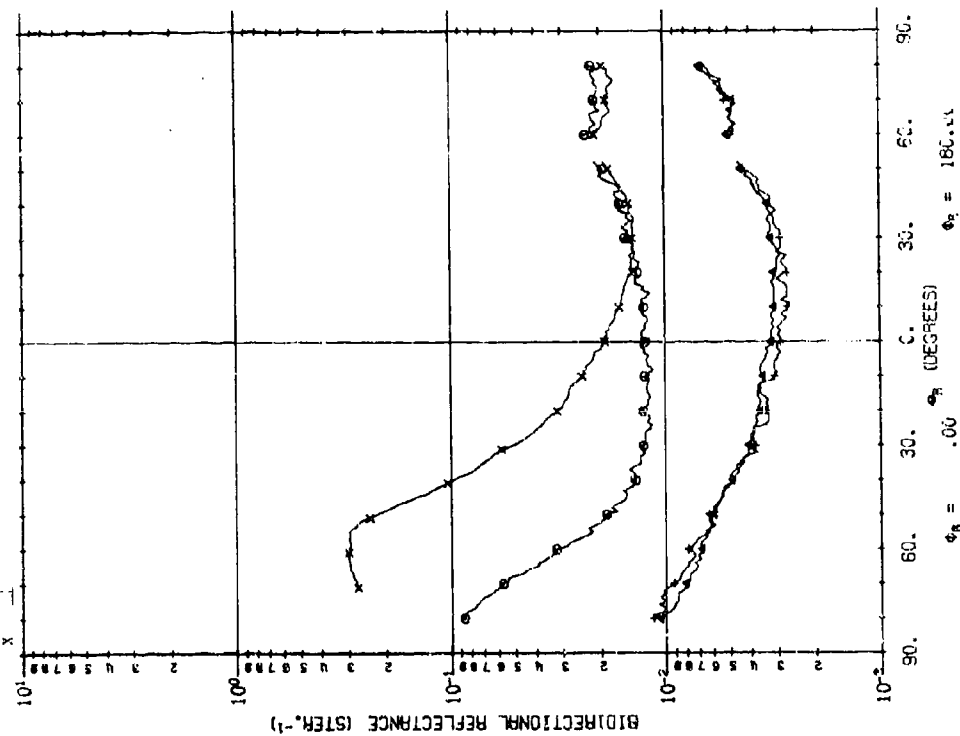


PAINT

R02004 101

OLIVE DRAB PAINT ON STEEL

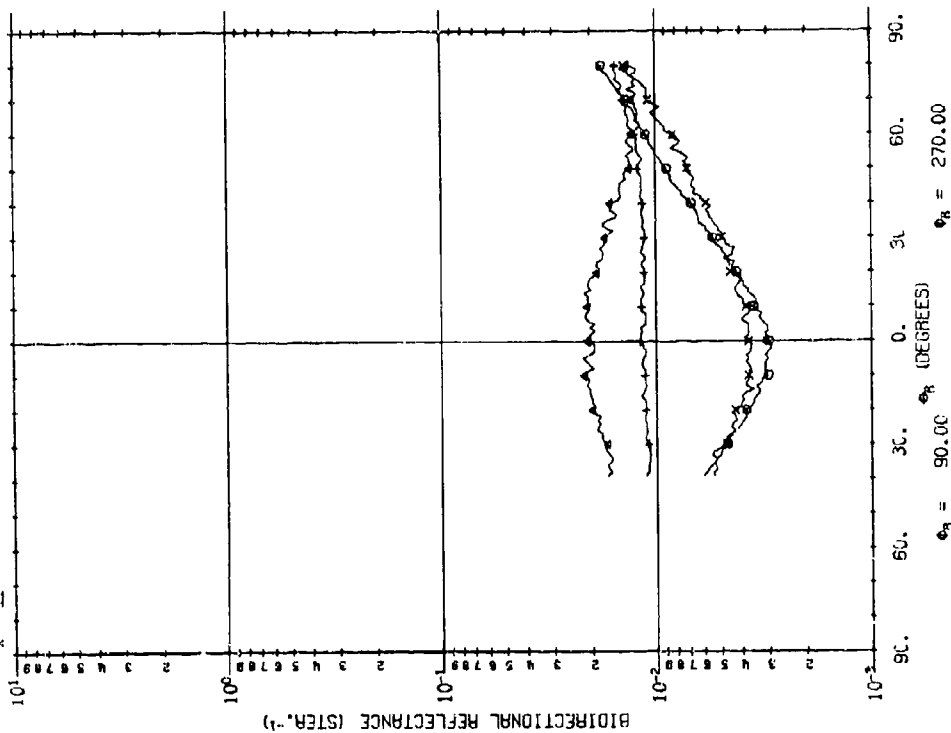
0  $\epsilon_1 = 56.0$   
 +  $\epsilon_2 = 180.0$   
 -  $\epsilon_3 = 1.06$



R02004 101

OLIVE DRAB PAINT ON STEEL

0  $\epsilon_1 = 56.0$   
 +  $\epsilon_2 = 180.0$   
 -  $\epsilon_3 = 1.06$

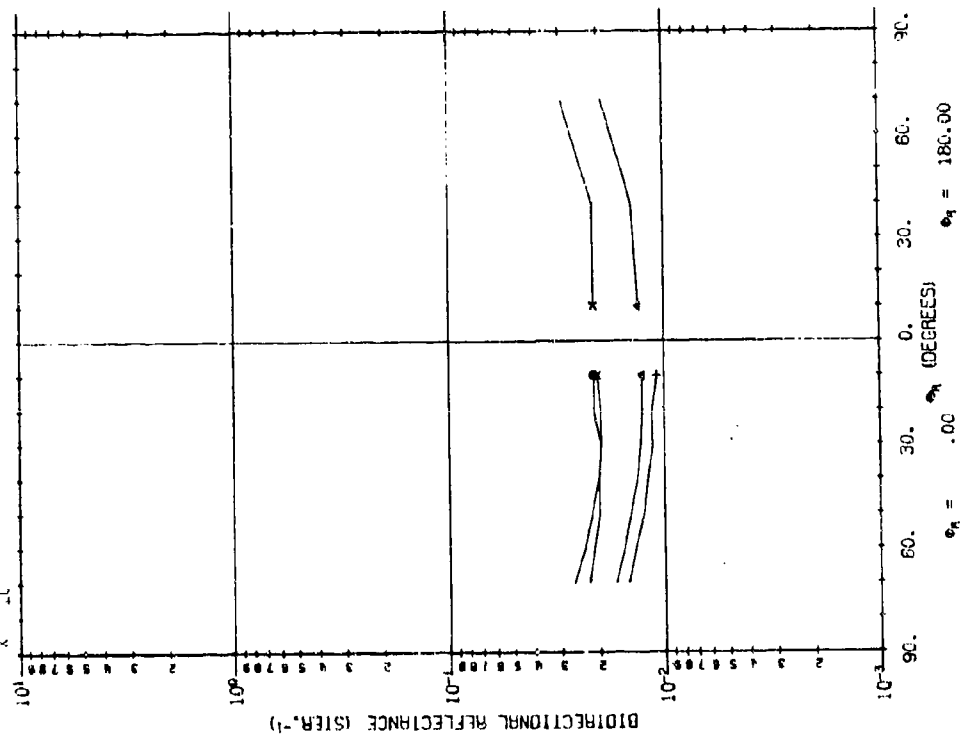


# CLOTH AND CANVAS

R01013 007

BLUE GRAY COTTON

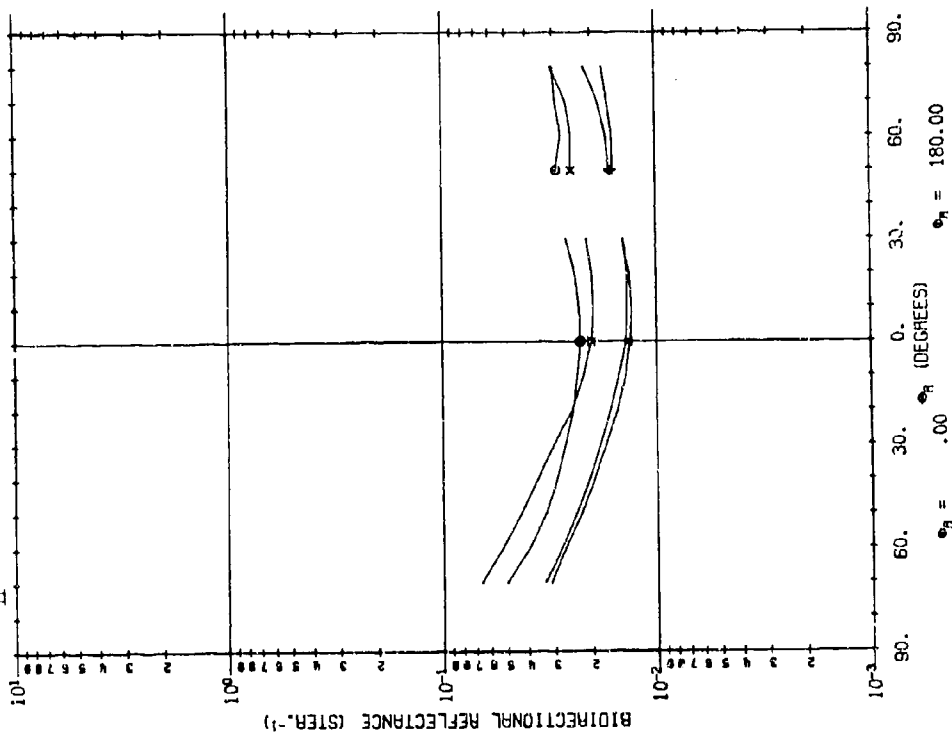
0  $\theta_1 = 0.0$   
 +  $\theta_1 = 180.0$   
 x  $\theta_1 = 0.63$



R01013 007

BLUE GRAY COTTON

0  $\theta_1 = 40.0$   
 +  $\theta_1 = 180.0$   
 x  $\theta_1 = 0.63$

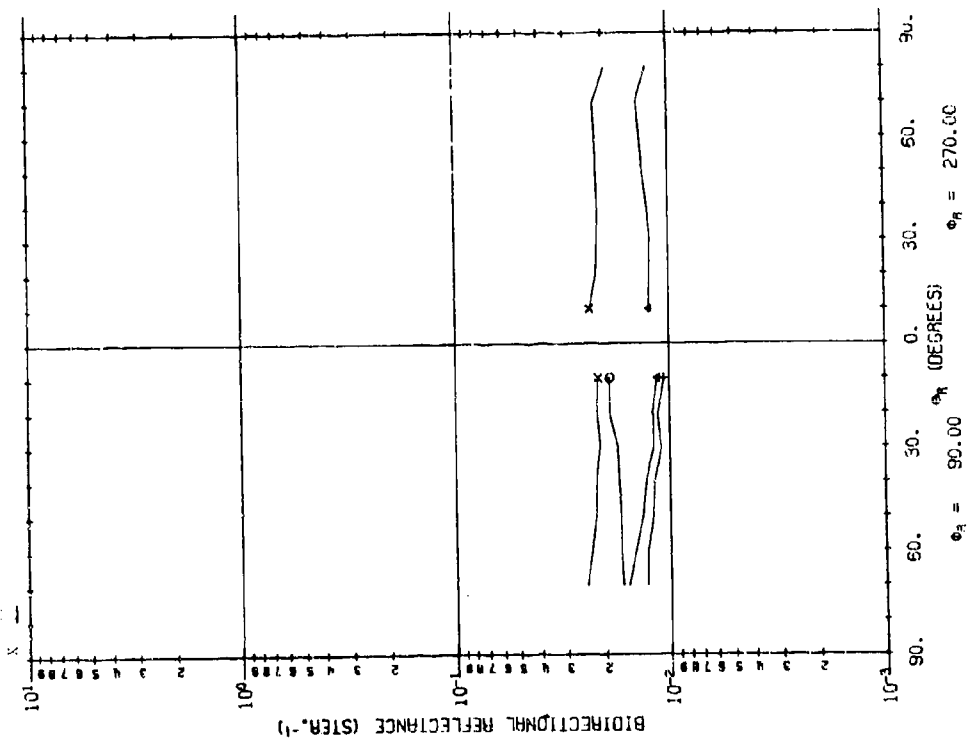


CLOTH AND CANVAS

RG1013 007

BLUE GRAY COTTON

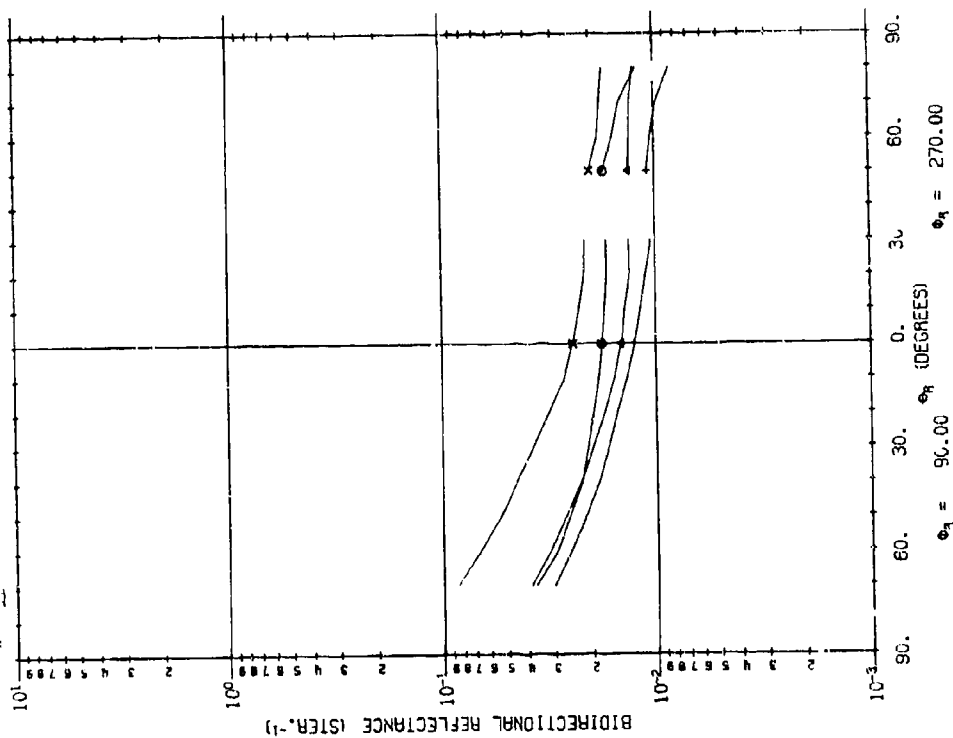
0  $\lambda_1 = 0.0$   
 +  $\lambda_2 = 270.0$   
 -  $\lambda_3 = 0.53$   
 x



RG1013 007

BLUE GRAY COTTON

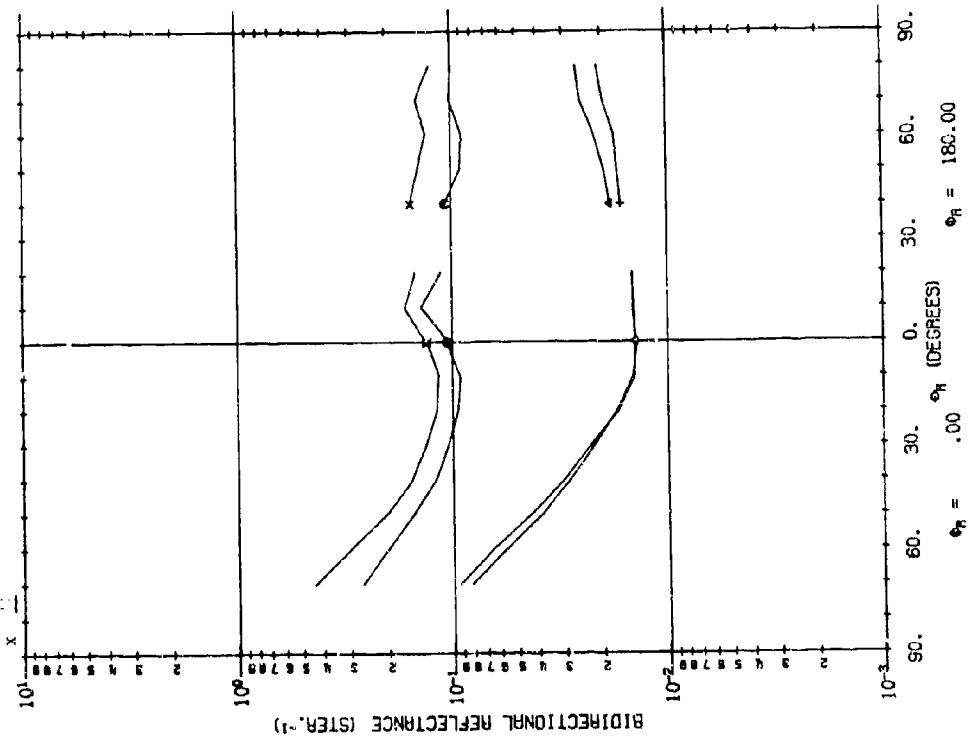
0  $\lambda_1 = 40.0$   
 +  $\lambda_2 = 270.0$   
 -  $\lambda_3 = 0.53$   
 x



R01057 014

WHITE NYLON, PLAIN WEAVE, RIB STOP PATTERN

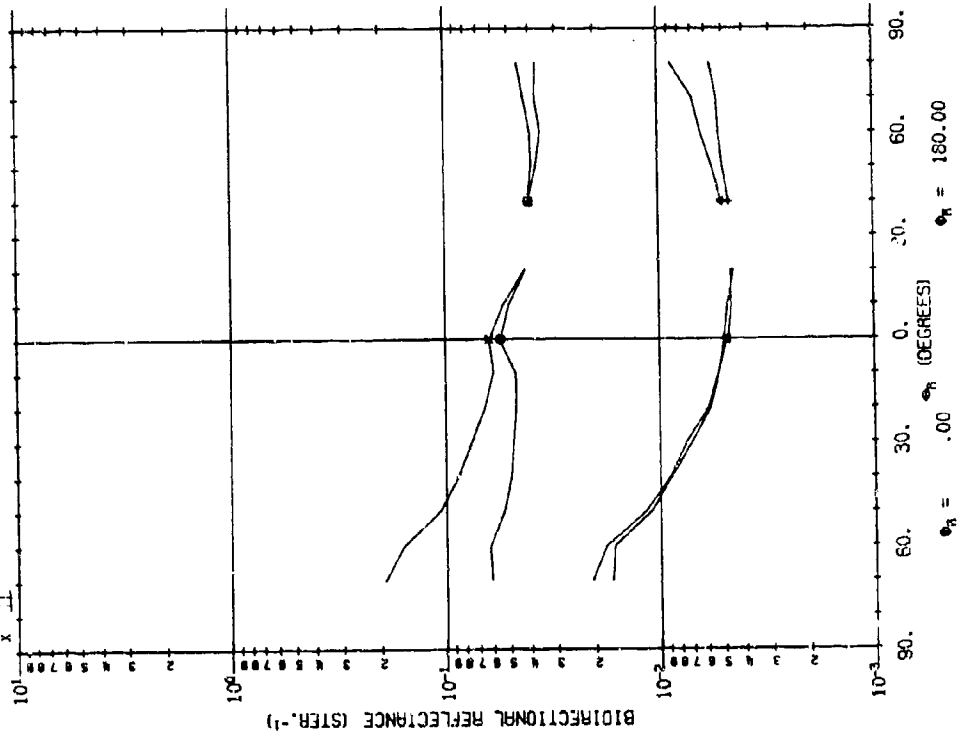
$\theta_i = 30.0$   
 $\theta_r = 180.0$   
 $\phi = 0.63$



R01058 014

OLIVE GREEN NYLON, PLAIN WEAVE, RIB STOP PATTERN

$\theta_i = 30.0$   
 $\theta_r = 180.0$   
 $\phi = 0.63$

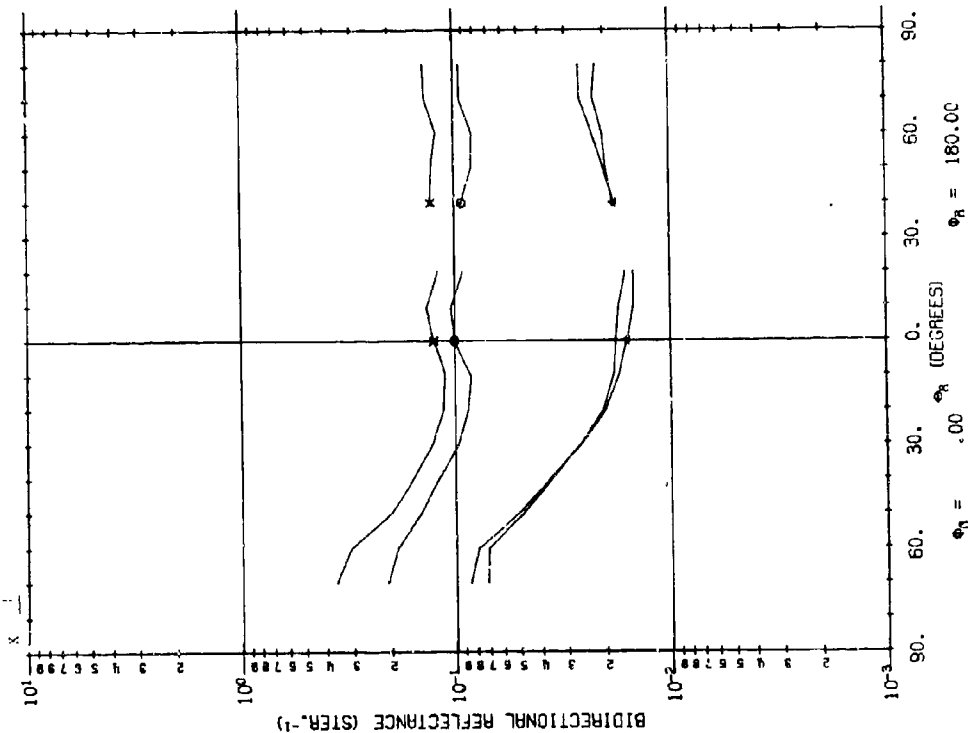


## CLOTH AND CANVAS

A01059 014

ORANGE NYLON, PLAIN WEAVE, RIB STOP  
PATTERN

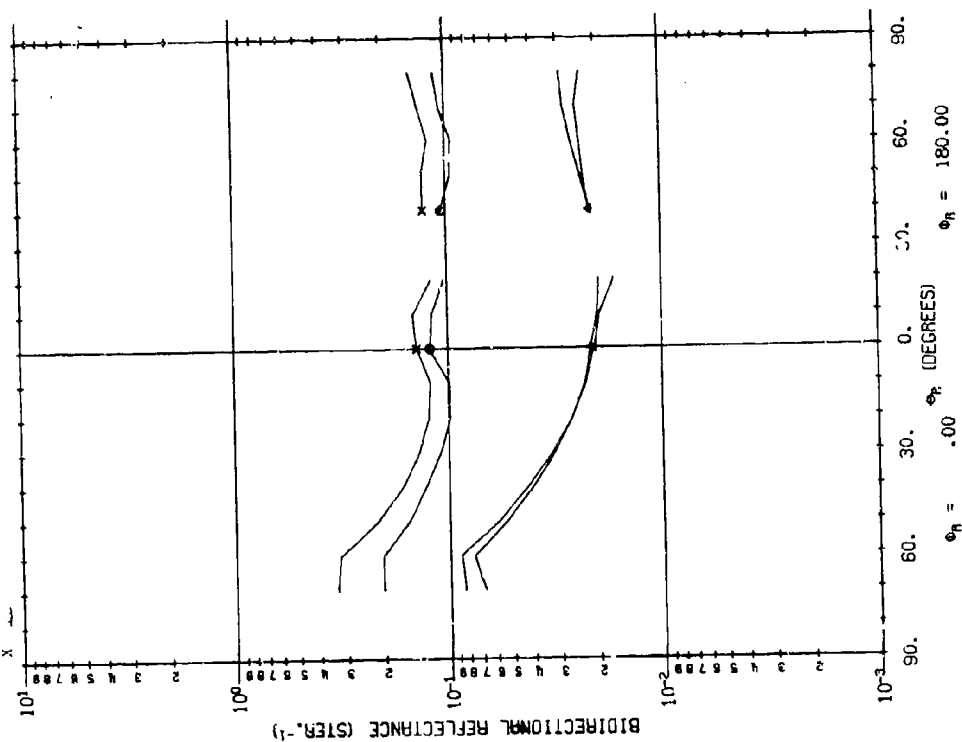
$\lambda = 50.0$   
 $\lambda = 180.0$   
 $\lambda = 0.63$



A01059 015

ORANGE NYLON, PLAIN WEAVE, RIB STOP  
PATTERN, FOUR LAYERS OVER SYCAMORE  
LEAVES

$\lambda = 50.0$   
 $\lambda = 180.0$   
 $\lambda = 0.63$

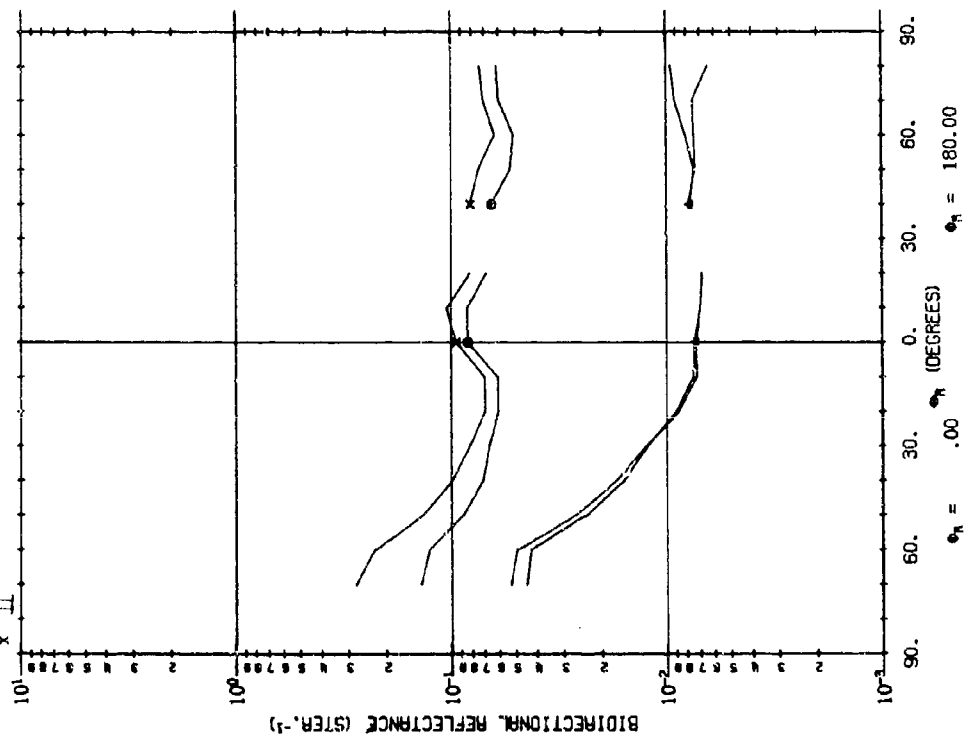




A01060 014

SAND (BEIGE) NYLON, PLAIN WEAVE, RIB  
STOP PATTERN

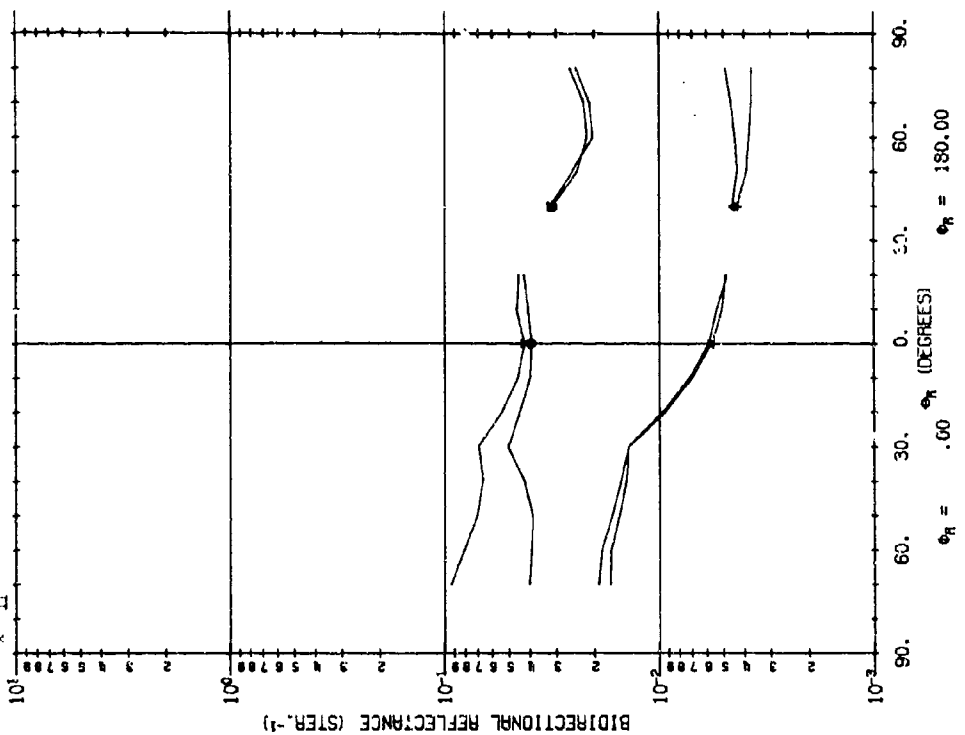
0 ||  $\theta_1 = 30.0$   
+ ||  $\phi_1 = 180.0$   
Δ ||  $\lambda = 0.63$   
x ||



A01061 014

OLIVE GREEN NYLON, DOBBY WEAVE

0 ||  $\theta_1 = 30.0$   
+ ||  $\phi_1 = 180.0$   
Δ ||  $\lambda = 0.63$   
x ||

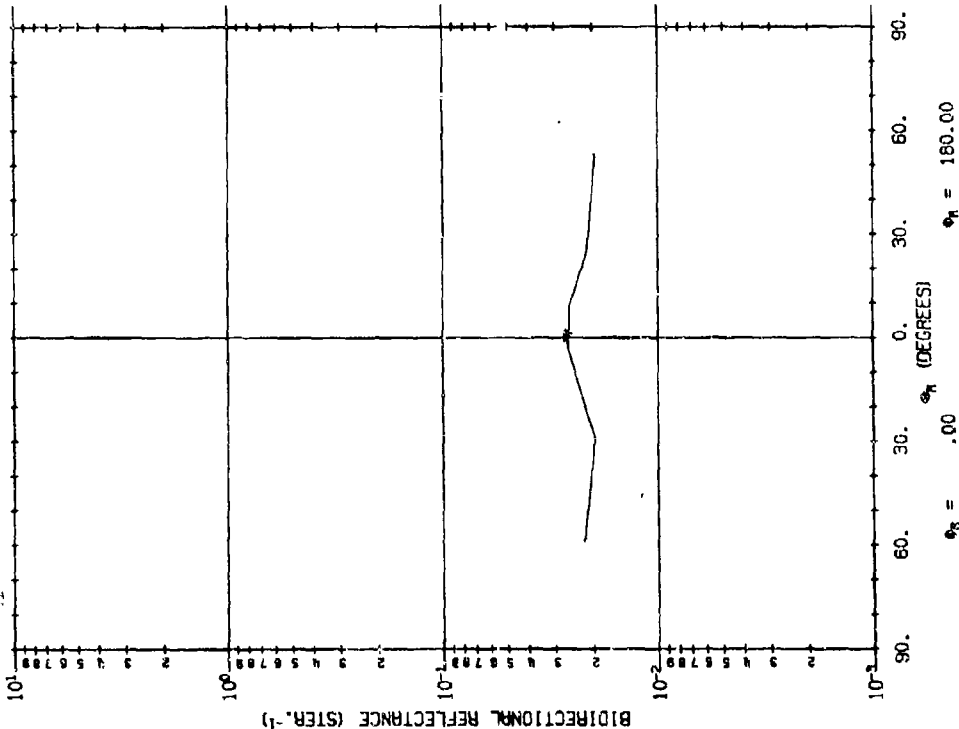


# CLOTH AND CANVAS

R01095 72 Green Canvas

0 1 2 3 4 5 6 7 8 9  
+ 1 2 3 4 5 6 7 8 9  
- 1 2 3 4 5 6 7 8 9  
X 1 2 3 4 5 6 7 8 9

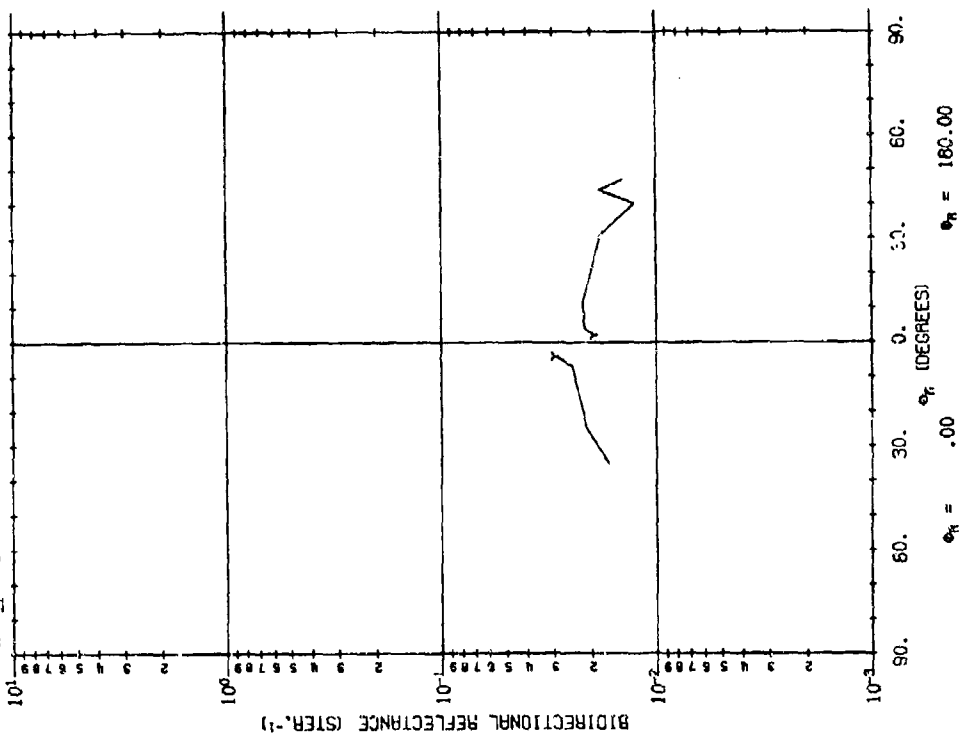
$\phi_1 = 1.10$   
 $\phi_2 = \phi_3$   
 $\lambda = 10.6$   
 $Y = 5T$



R01096 002 Green Canvas

0 1 2 3 4 5 6 7 8 9  
+ 1 2 3 4 5 6 7 8 9  
- 1 2 3 4 5 6 7 8 9  
X 1 2 3 4 5 6 7 8 9

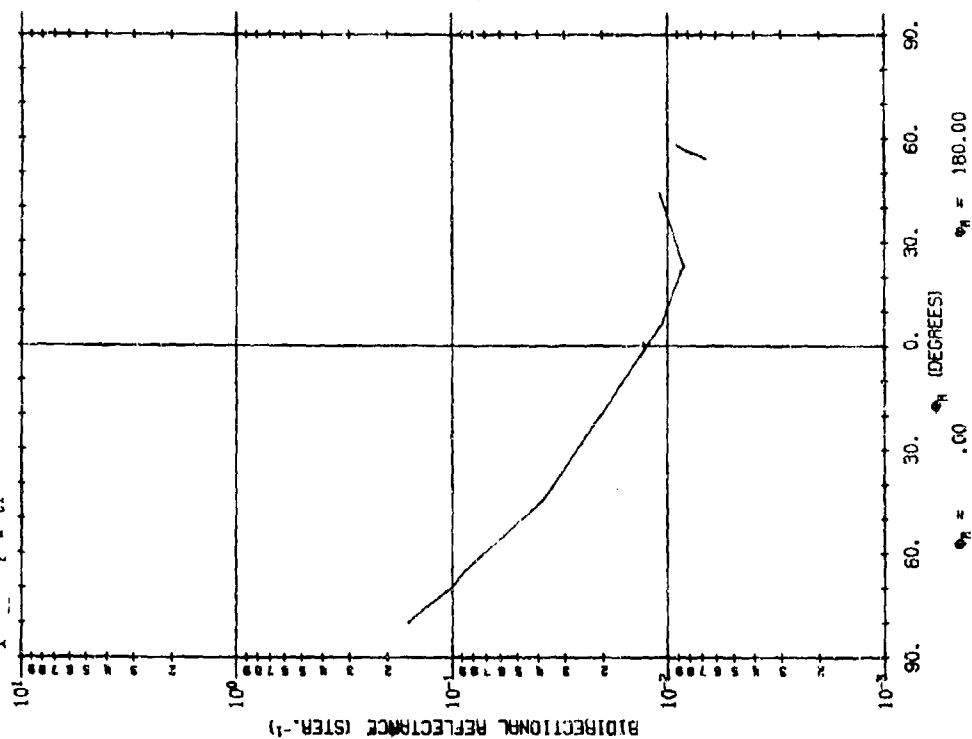
$\phi_1 = 0.0$   
 $\phi_2 = 180.0$   
 $\lambda = 10.6$   
 $Y = 5T$



A01096 002

Green Canvas

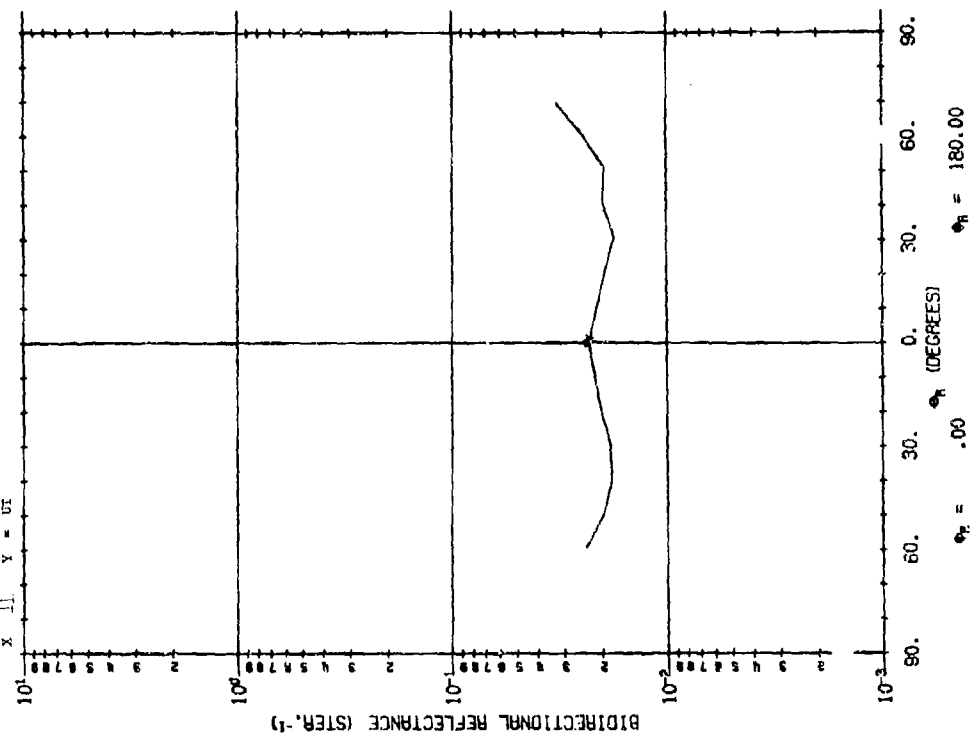
0 ||  $g_1 = 50.00$   
 + ||  $\phi_1 = 180.0$   
 - ||  $\lambda = 10.6$   
 X ||  $Y = 5T$



A01099 002

White Canvas

0 ||  $2\theta = 1.10$   
 + ||  $\phi_1 = 4T$   
 - ||  $\lambda = 10.6$   
 X ||  $Y = 5T$

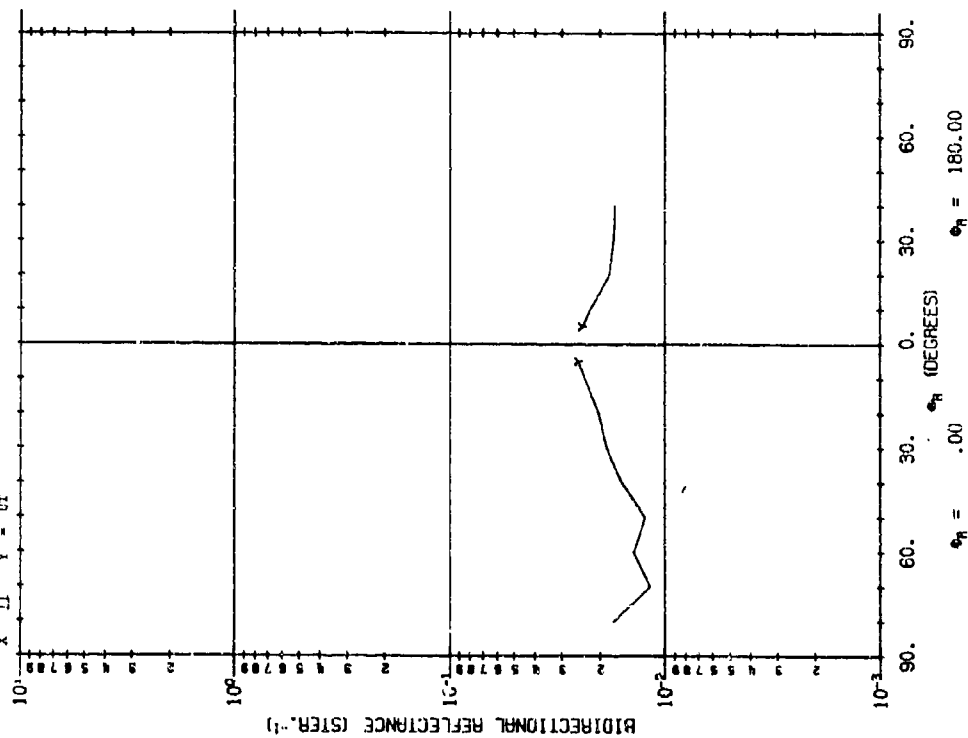


CLOTH AND CANVAS

R01099 002

White Canvas

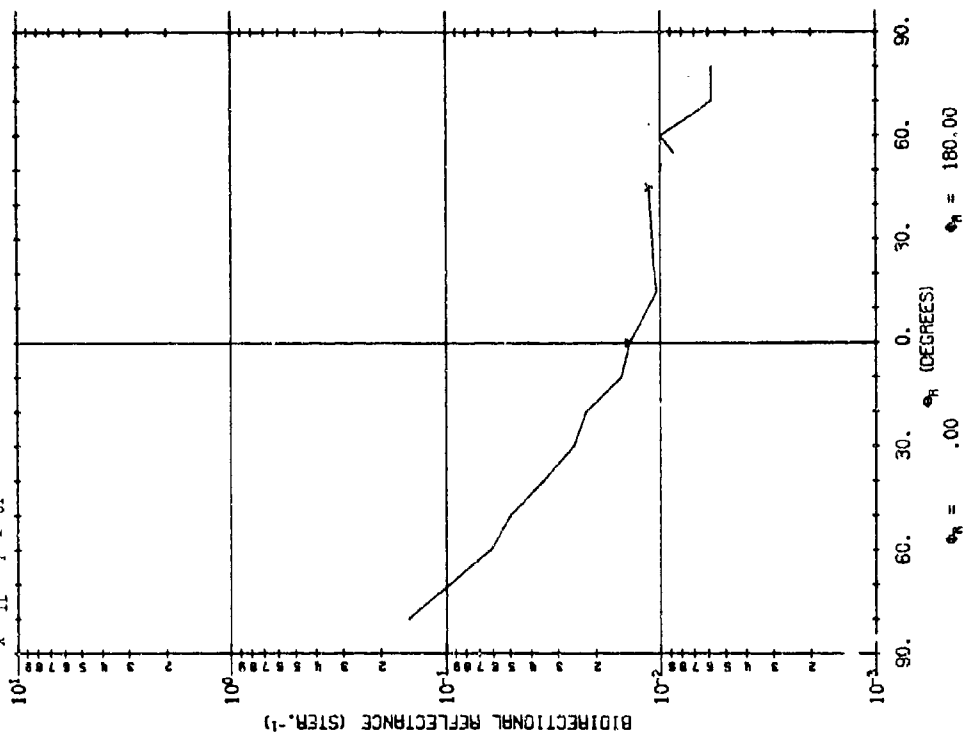
0 ||  $\phi_1 = 0.0$   
 + ||  $\phi_1 = 180.0$   
 2 ||  $\lambda = 10.6$   
 X || Y = UT



R01099 002

White Canvas

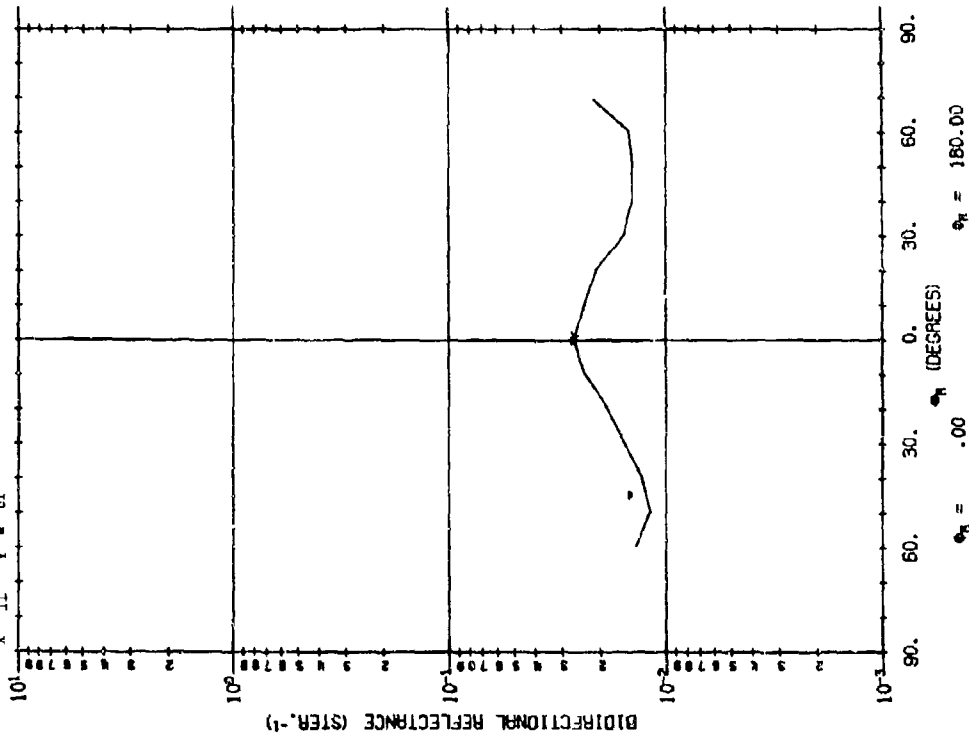
0 ||  $\phi_1 = 50.0$   
 + ||  $\phi_1 = 180.0$   
 2 ||  $\lambda = 10.6$   
 X || Y = UT



R01103 002

Black Canvas

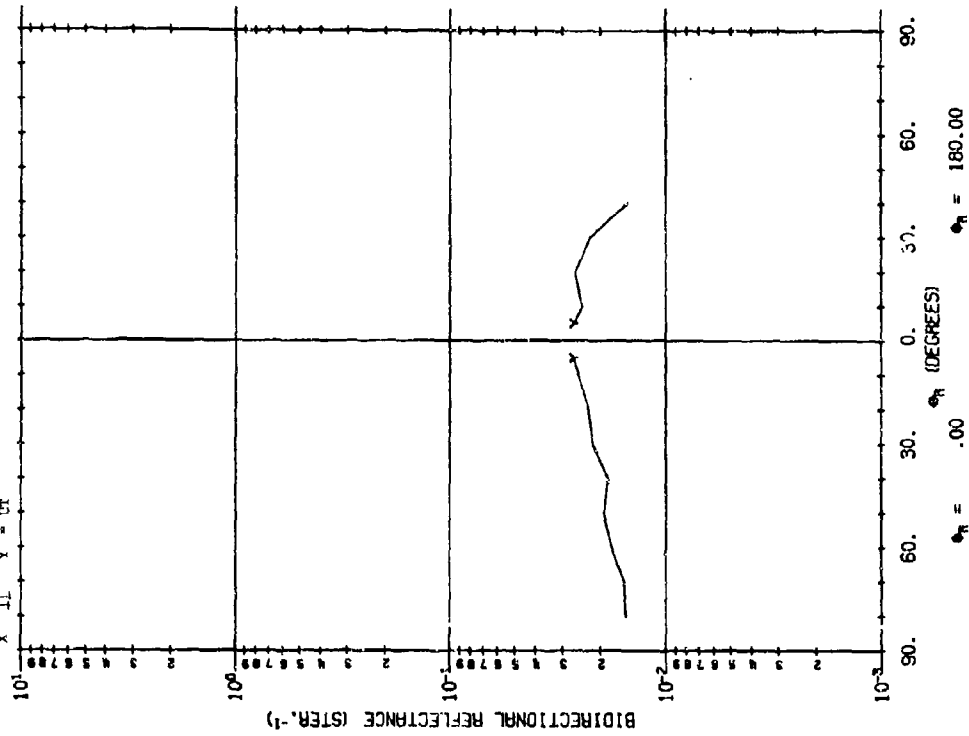
0 //  $\theta_1 = 1.10$   
 + //  $\phi_1 = \phi_2$   
 $\Delta$  //  $\lambda = 10.6$   
 X // Y = UT



R01103 002

Black Canvas

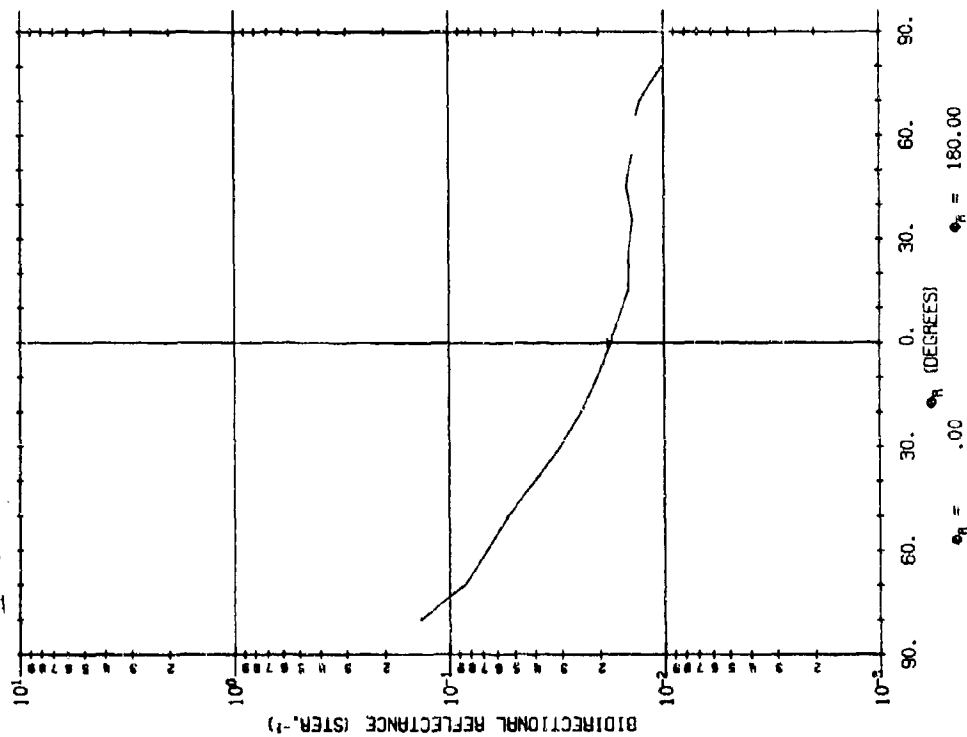
0 //  $\theta_1 = 0.0$   
 + //  $\phi_1 = 180.3$   
 $\Delta$  //  $\lambda = 10.6$   
 X // Y = UT



CLOTH AND CANVAS

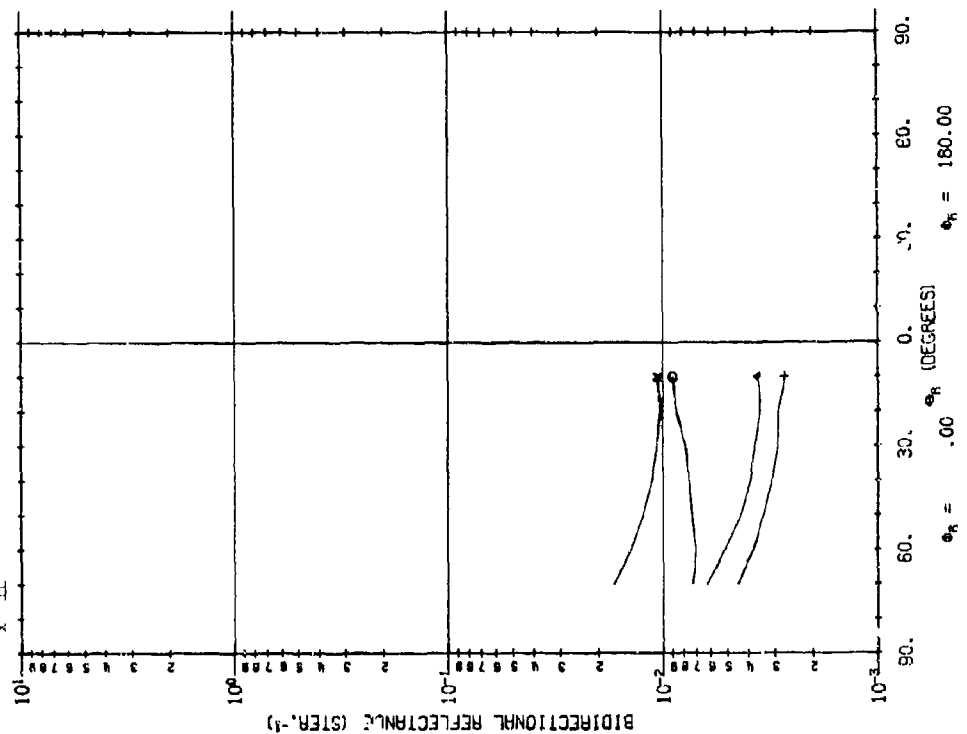
A01103 002  
 0 ||  $\theta_i = 50.0$   
 + ||  $\theta_i = 180.0$   
 - ||  $\theta_i = 10.6$   
 x ||  $\theta_i = 0.0$

Black Canvas



A01188 007  
 0 ||  $\theta_i = 0.0$   
 + ||  $\theta_i = 180.0$   
 - ||  $\theta_i = 0.63$   
 x ||  $\theta_i = 0.0$

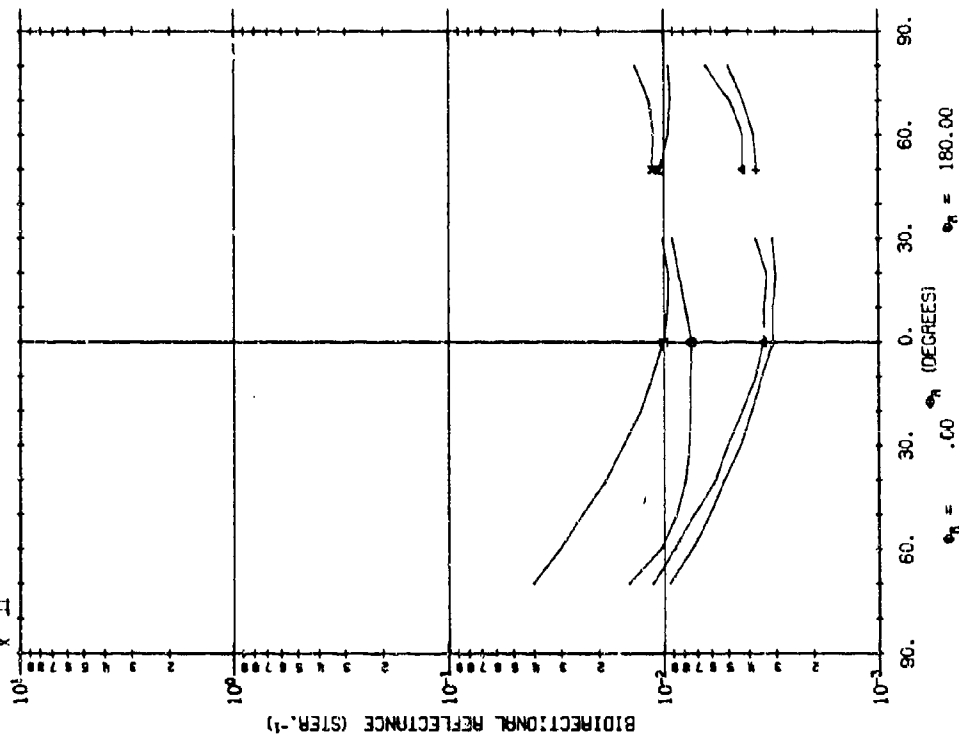
FADED BLACK COTTON



A01188 007

FADED BLACK COTTON

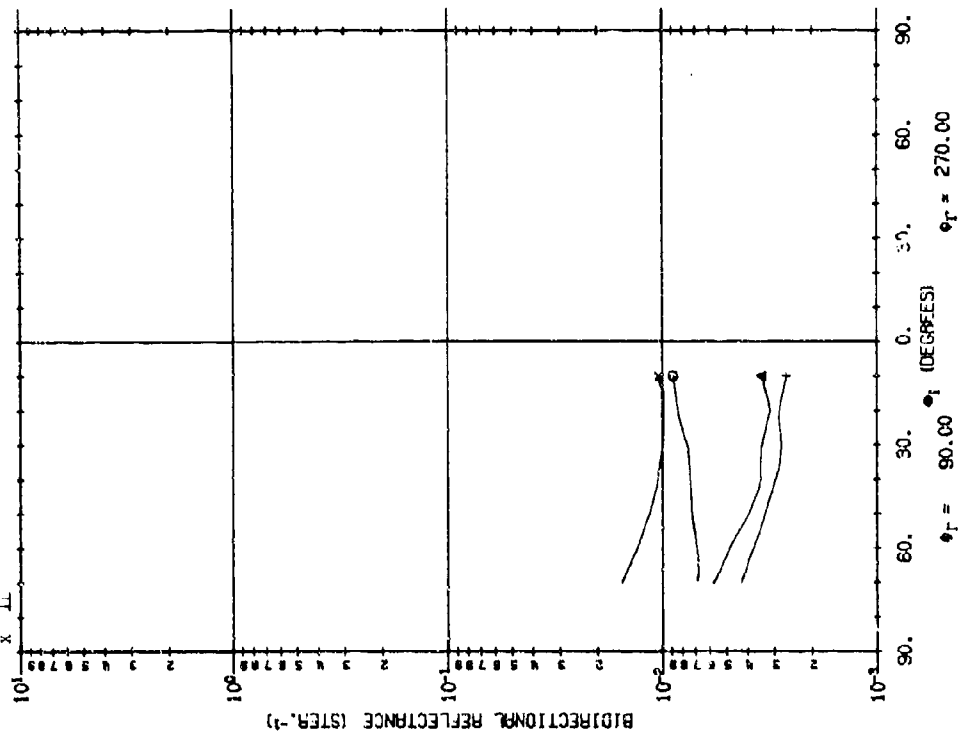
$\theta_1 = 40.0$   
 $\phi_1 = 180.0$   
 $\lambda = 0.63$



A01188 007

FADED BLACK COTTON

$\theta_1 = 0.0$   
 $\phi_1 = 270.0$   
 $\lambda = 0.63$

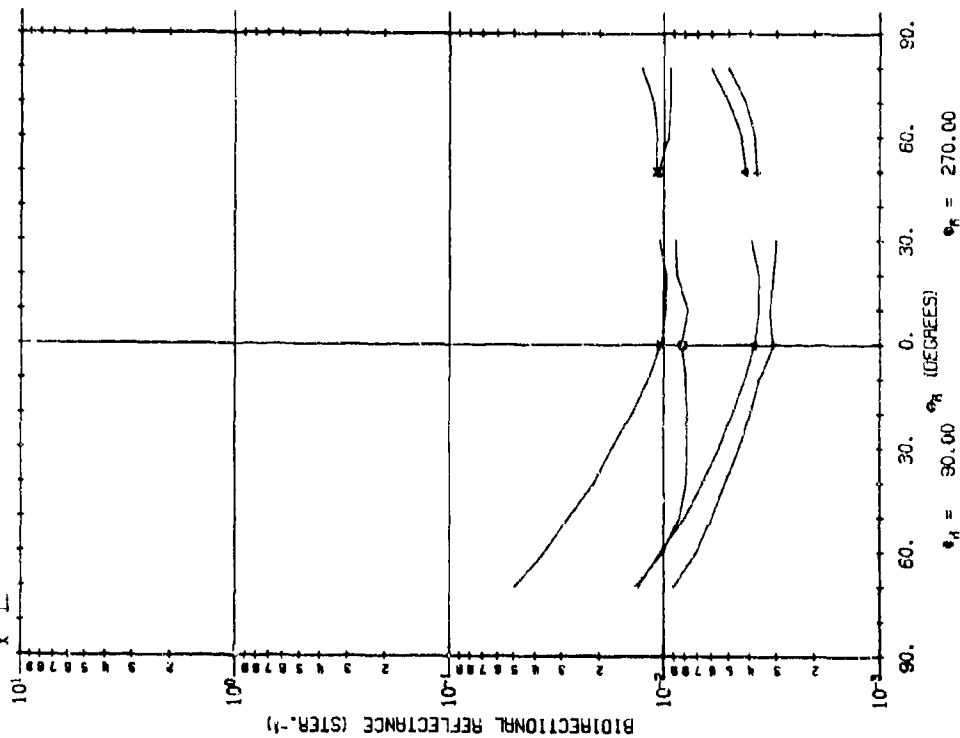


CLOTH AND CANVAS

R01188 007

FADED BLACK COTTON

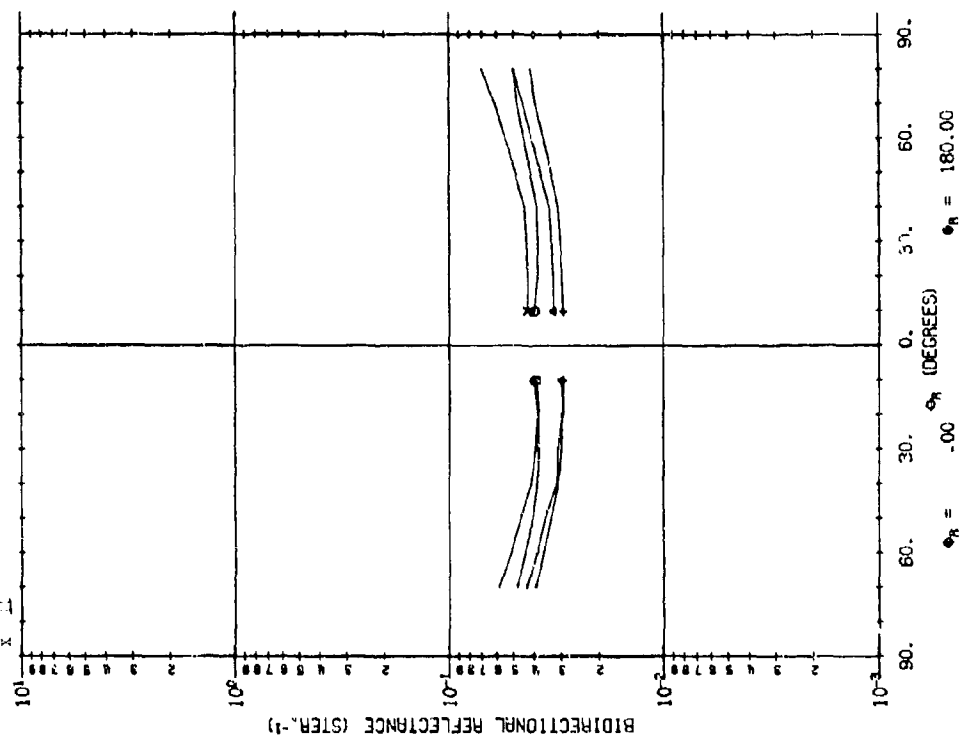
0 11  $\phi_1 = 40.0$   
 + 11  $\phi_1 = 270.0$   
 4 11  $\lambda = 0.63$



R01189 008

GRAY-GREEN HEAVY COTTON DRILL

0 11  $\phi_1 = 0.0$   
 + 11  $\phi_1 = 180.0$   
 1 11  $\lambda = 0.63$

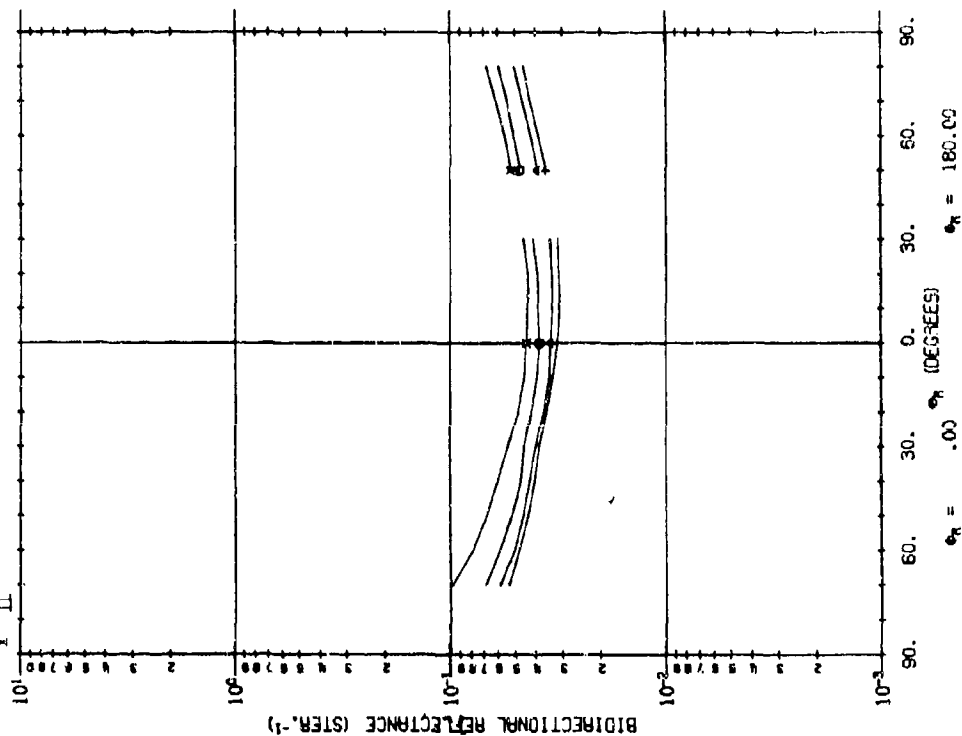




A01189 008

GRAY-GREEN HEAVY COTTON DRILL

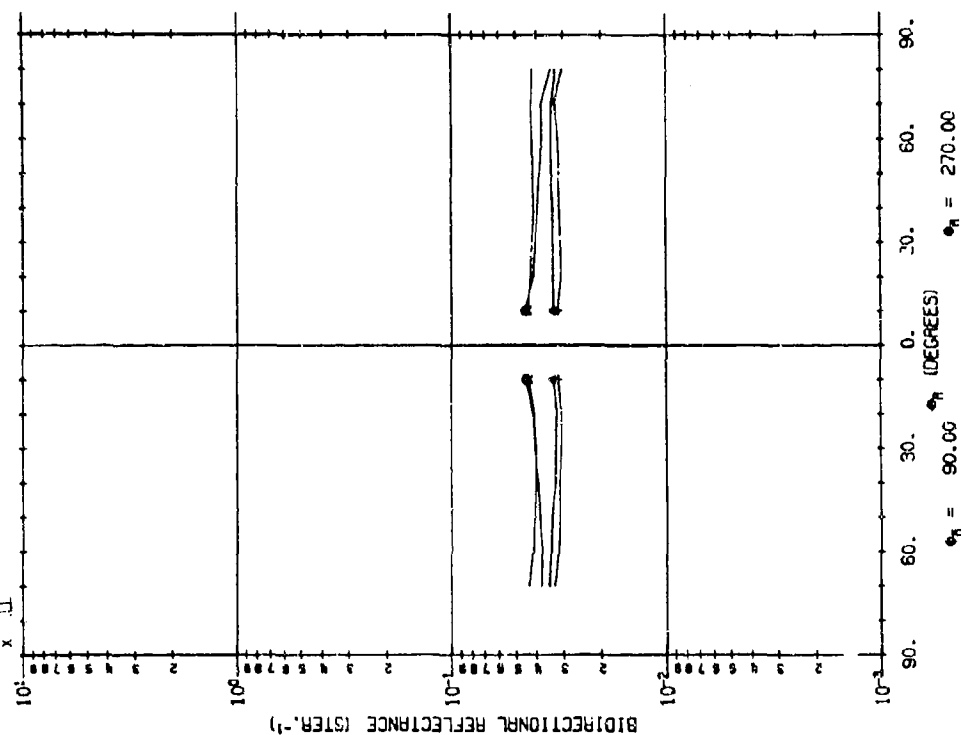
0 ||  $\theta_1 = 40.0$   
 + ||  $\theta_2 = 180.0$   
 x ||  $\lambda = 0.63$



A01189 008

GRAY-GREEN HEAVY COTTON DRILL

0 ||  $\theta_1 = 0.0$   
 + ||  $\theta_2 = 270.0$   
 x ||  $\lambda = 0.63$

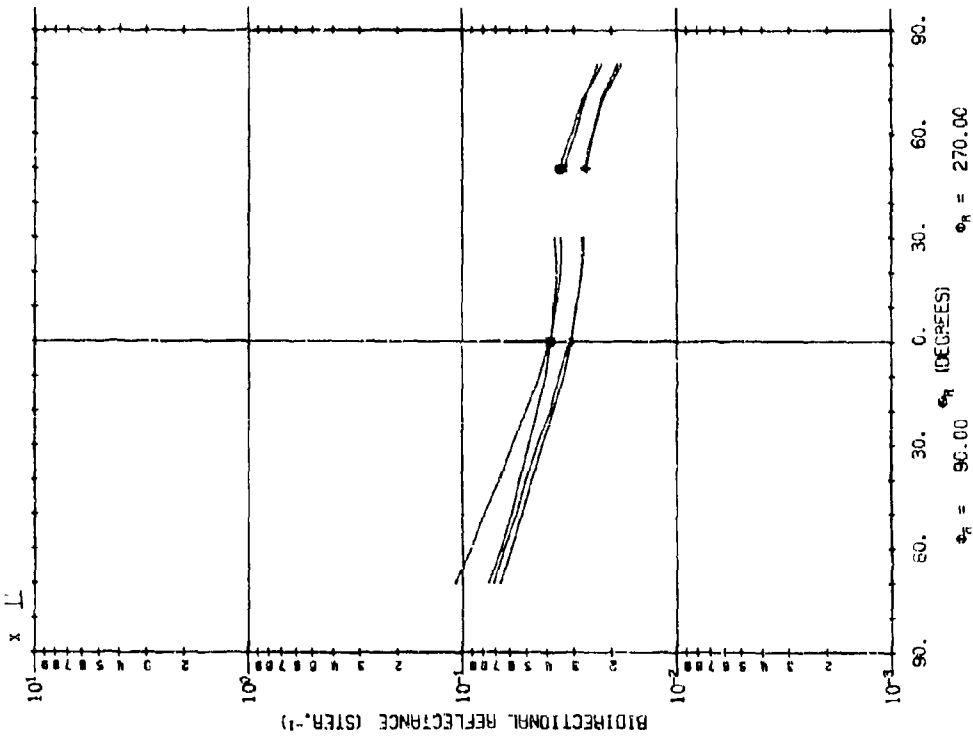


CLOTH AND CANVAS

R01189 008

GRAY-GREEN HEAVY COTTON DRILL

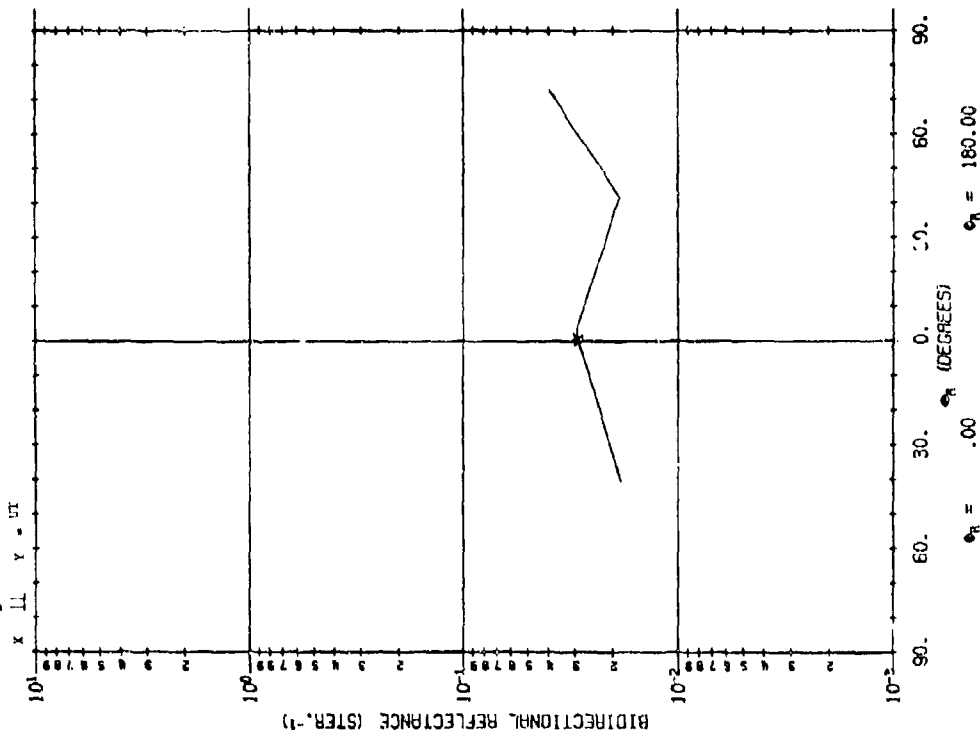
$\phi_1 = 40.0$   
 $\phi_2 = 270.0$   
 $\lambda = 0.63$



R01466 002

Black Paint on Canvas, 4% Reflectance

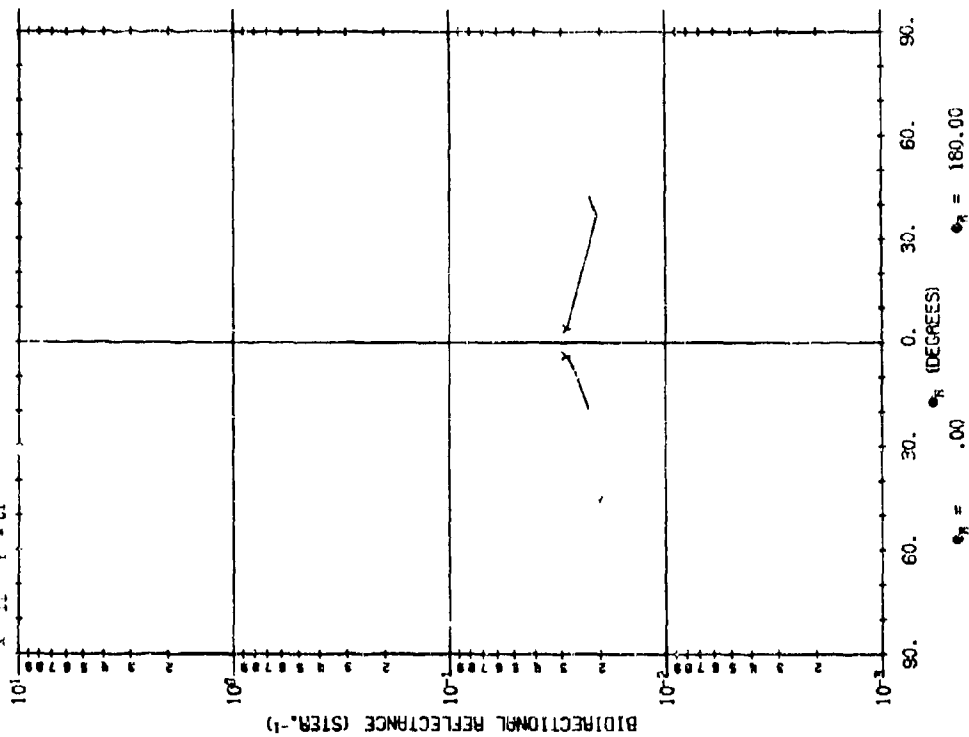
$\phi_1 = 1.10$   
 $\phi_2 = 4\pi$   
 $\lambda = 10.6$



R01466 002

Black Paint on Canvas, 4% Reflectance

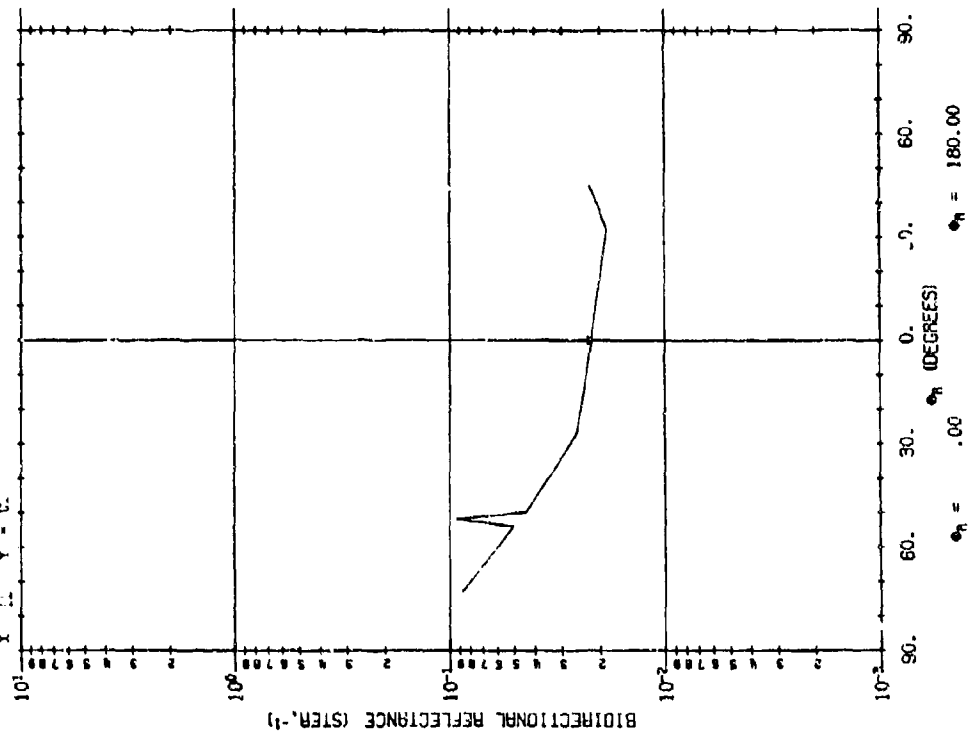
0 //  $\phi_1 = 0.0$   
 + //  $\phi_2 = 180.0$   
 - //  $\phi_3 = 10.6$   
 X // Y = U



R01466 002

Black Paint on Canvas, 4% Reflectance

0 //  $\phi_1 = 50.0$   
 + //  $\phi_2 = 180.0$   
 - //  $\phi_3 = 10.6$   
 X // Y = U

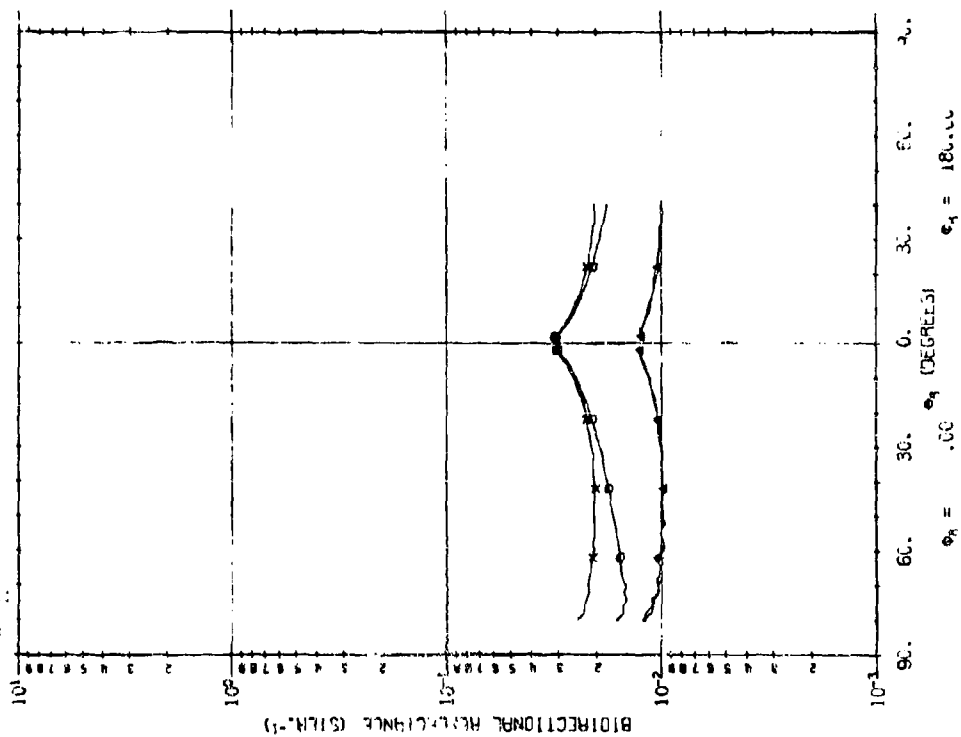


CLOTH AND CANVAS

901470 101

MEDIUM GRAY PAINT ON CANVAS,  
16 PERCENT REFLECTANCE

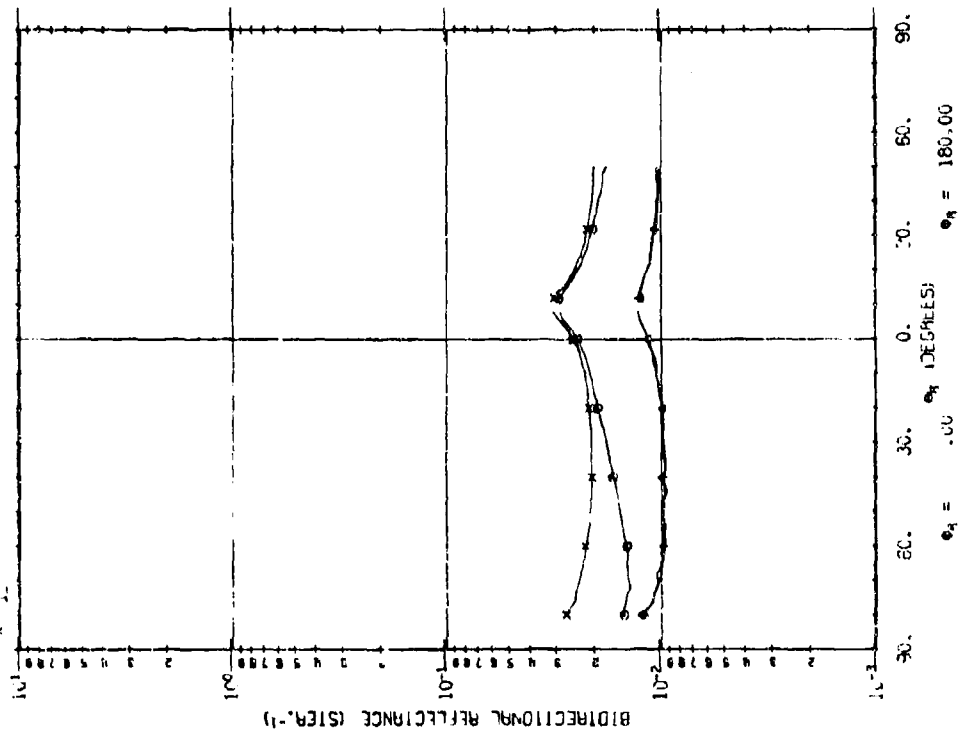
0 1  $\phi_1 = 0.0$   
+ 1  $\phi_1 = 180.0$   
x 1  $\phi_1 = 0.63$



901470 101

MEDIUM GRAY PAINT ON CANVAS,  
16 PERCENT REFLECTANCE

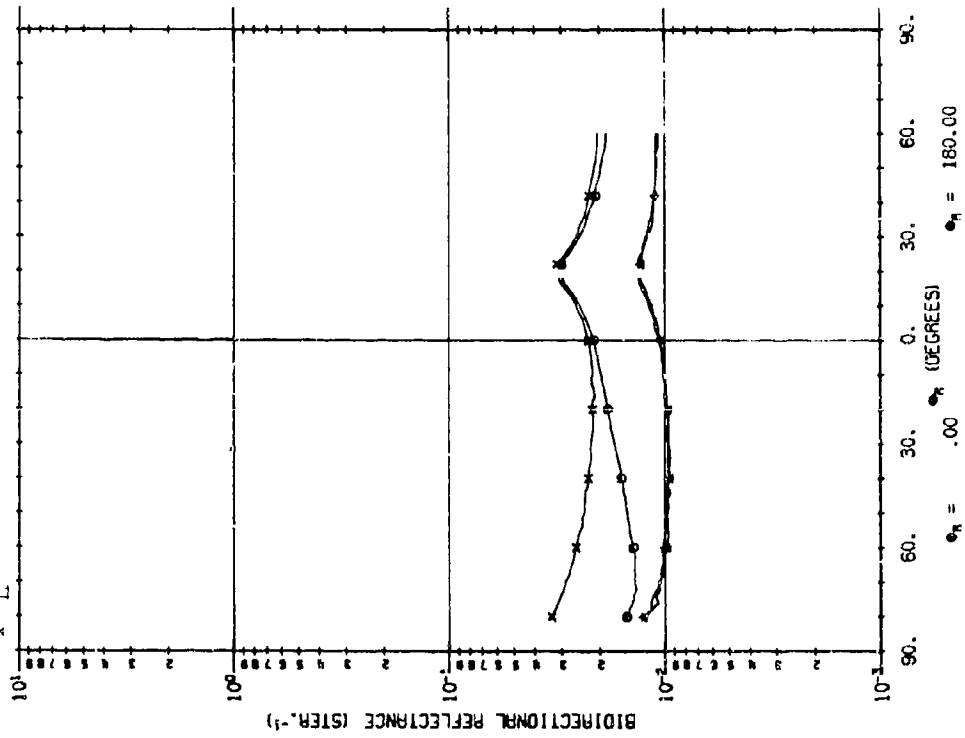
0 1  $\phi_1 = 0.0$   
+ 1  $\phi_1 = 180.0$   
x 1  $\phi_1 = 0.63$



A01470 101

MEDIUM GRAY PAINT ON CANVAS,  
16 PERCENT REFLECTANCE

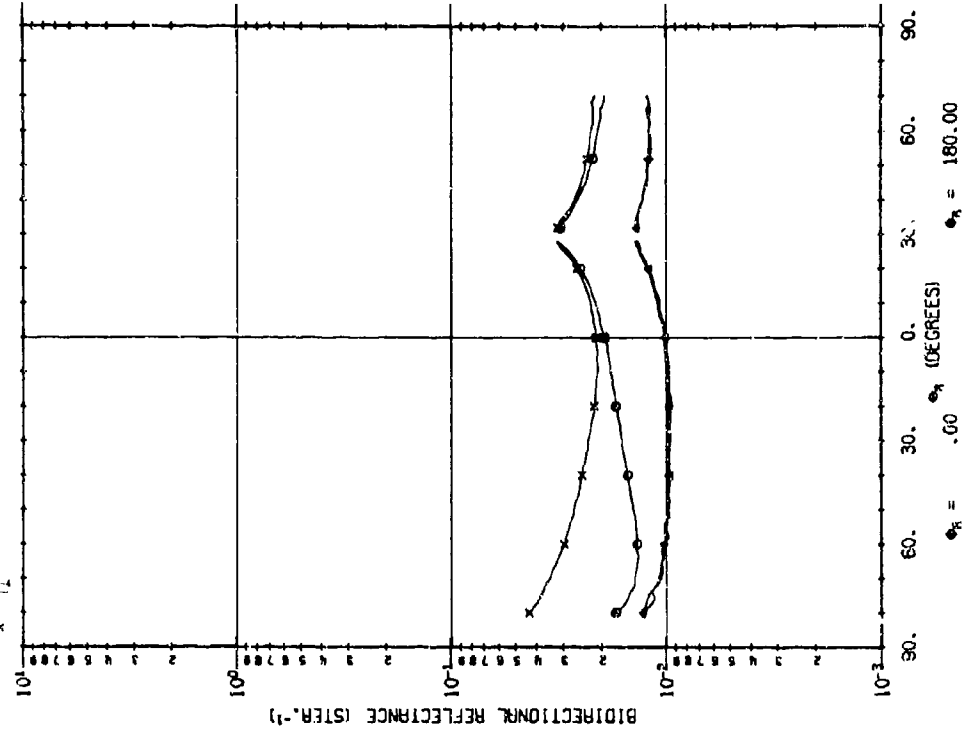
$\phi_1 = 20.0$   
 $\phi_2 = 180.0$   
 $\lambda = 0.63$



A01470 101

MEDIUM GRAY PAINT ON CANVAS,  
16 PERCENT REFLECTANCE

$\phi_1 = 30.0$   
 $\phi_2 = 180.0$   
 $\lambda = 0.63$



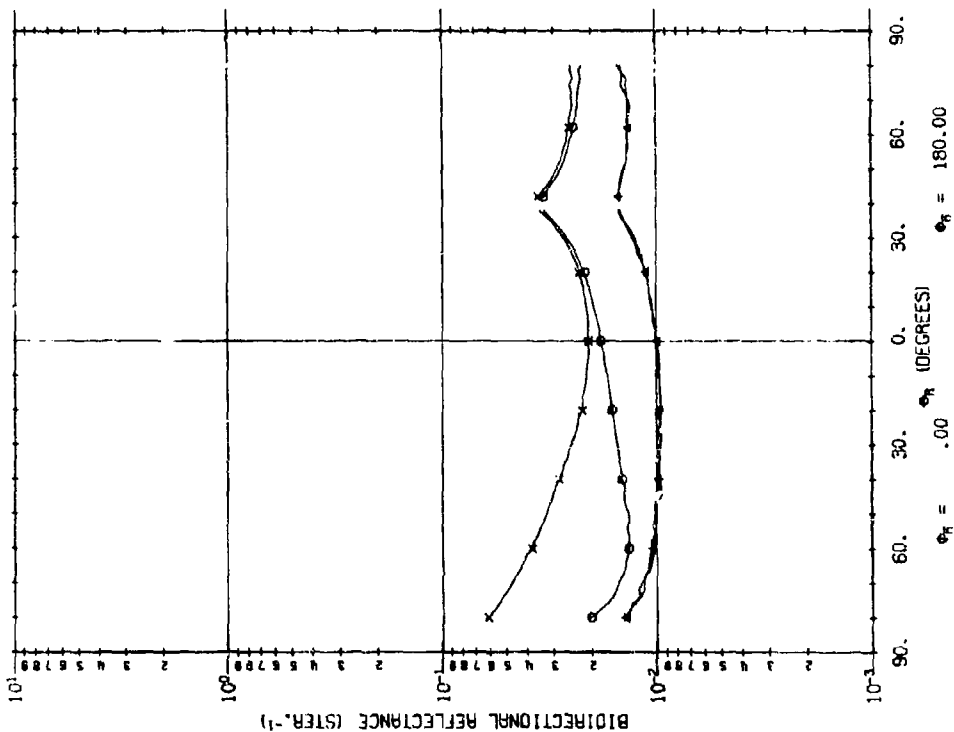
## CLOTH AND CANVAS

A01470 101

MEDIUM GRAY PAINT ON CANVAS,  
16 PERCENT REFLECTANCE

$\frac{1}{2} \lambda = 40.0$   
 $t_1 = 180.0$   
 $\lambda = 0.63$

0  
+  
x  
x

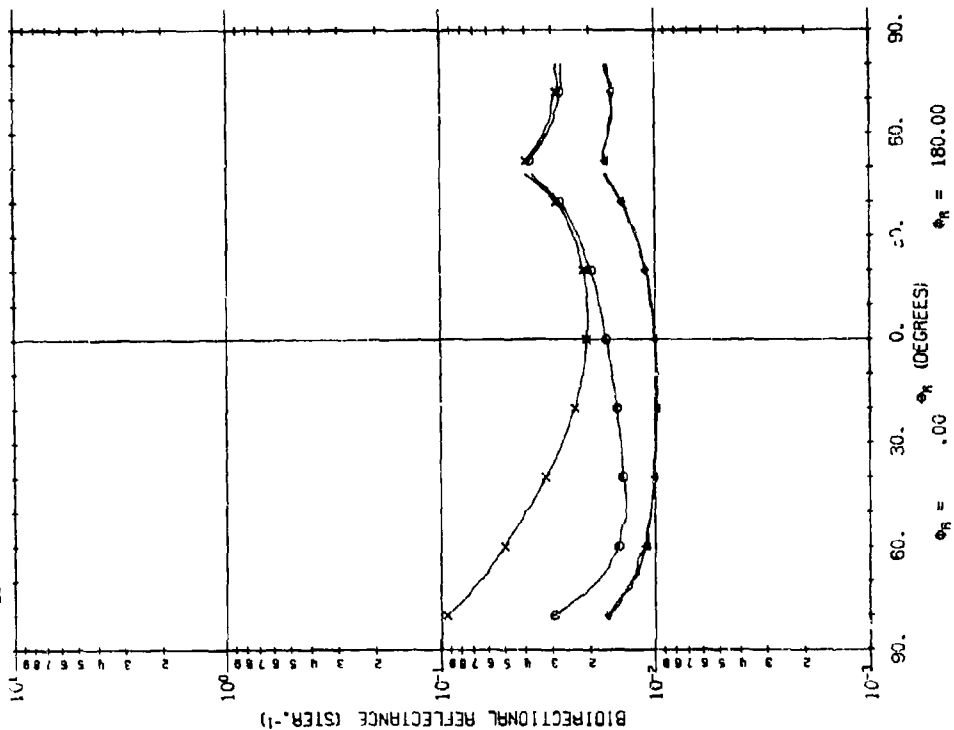


A01470 101

MEDIUM GRAY PAINT ON CANVAS,  
16 PERCENT REFLECTANCE

$\frac{1}{2} \lambda = 50.0$   
 $t_1 = 180.0$   
 $\lambda = 0.63$

0  
+  
x  
x

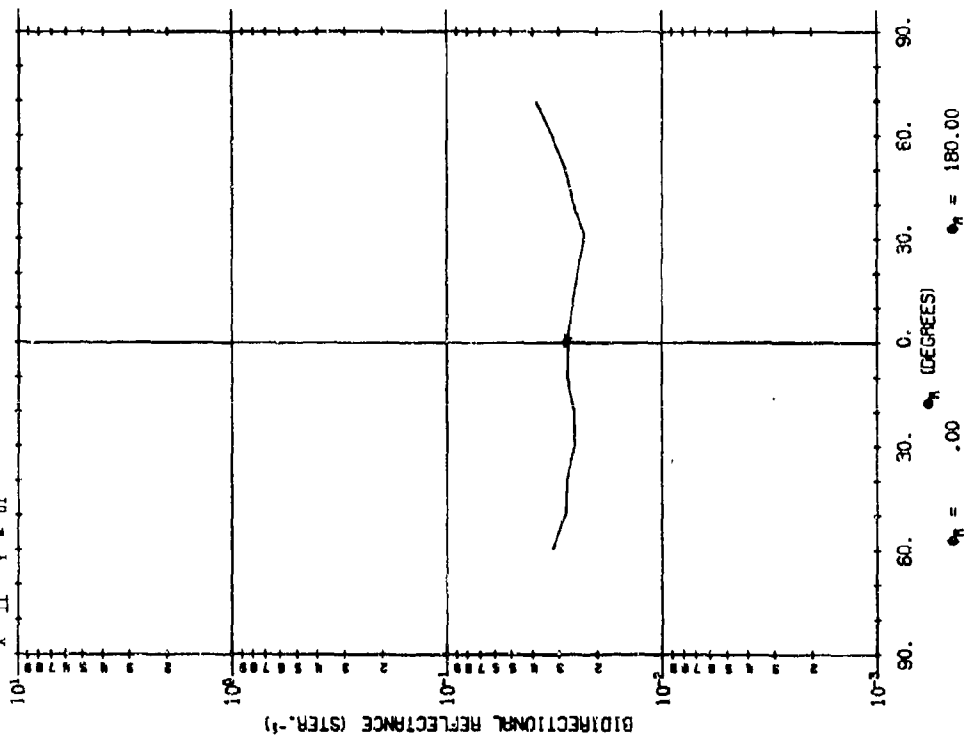




A01470 002

Medium Gray Paint on Canvas, 16% Reflectance

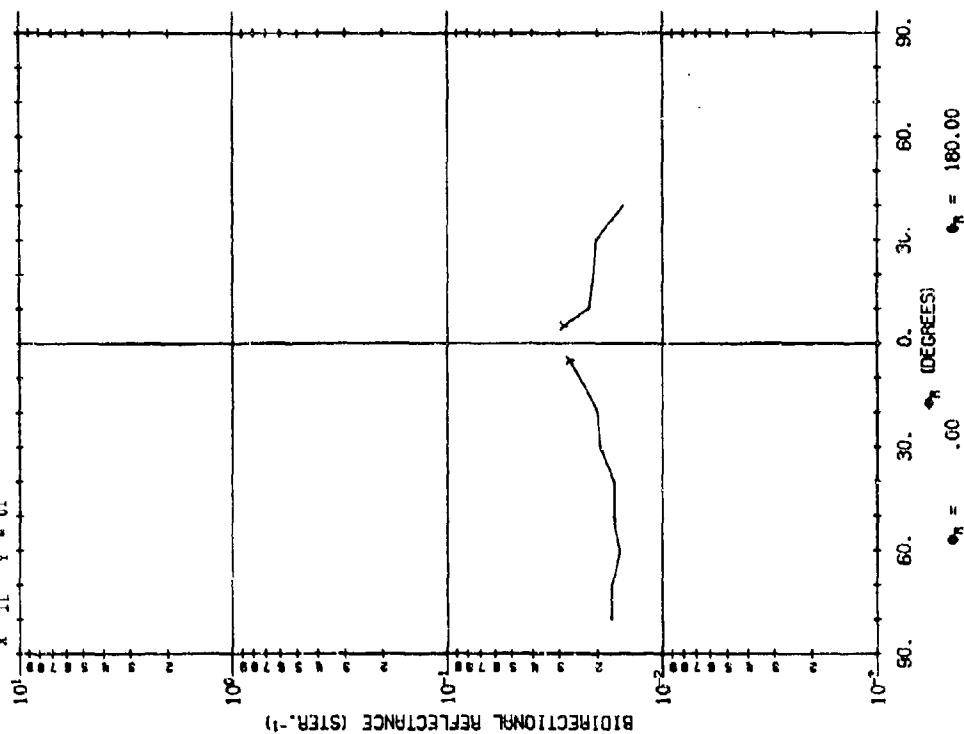
0 11 23 = 1.10  
+ 11  $\phi_1 = \phi_r$   
Δ 11  $\lambda = 10.6$   
X 11 Y = UT



A01470 002

Medium Gray Paint on Canvas, 16% Reflectance

0 11  $\phi_1 = 0.0$   
+ 11  $\phi_1 = 180.0$   
Δ 11  $\lambda = 10.6$   
X 11 Y = UT

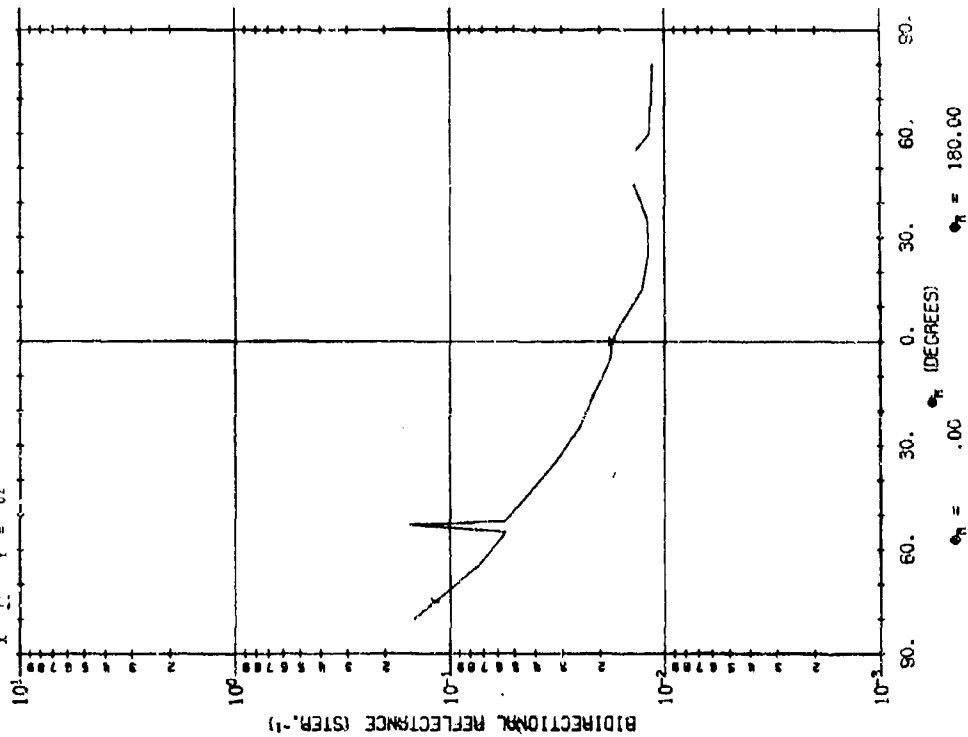




R01470 002

Medium Gray Paint on Canvas, 16% Reflectance

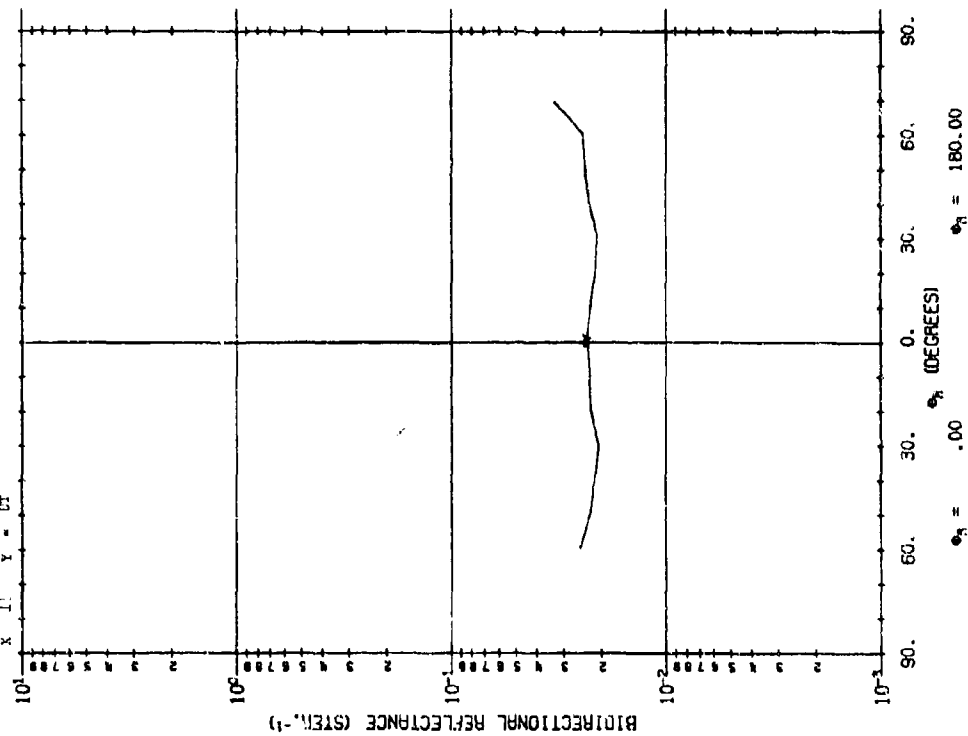
0 11  $\theta_1 = 50.0$   
+ 11  $\theta_2 = 180.0$   
2 11  $\lambda = 10.6$   
X 11 Y = UT



R01471 002

Medium Gray Paint on Canvas, 16% Reflectance

0 11  $\theta_1 = 1.10$   
+ 11  $\theta_2 = 0$   
2 11  $\lambda = 10.6$   
X 11 Y = UT

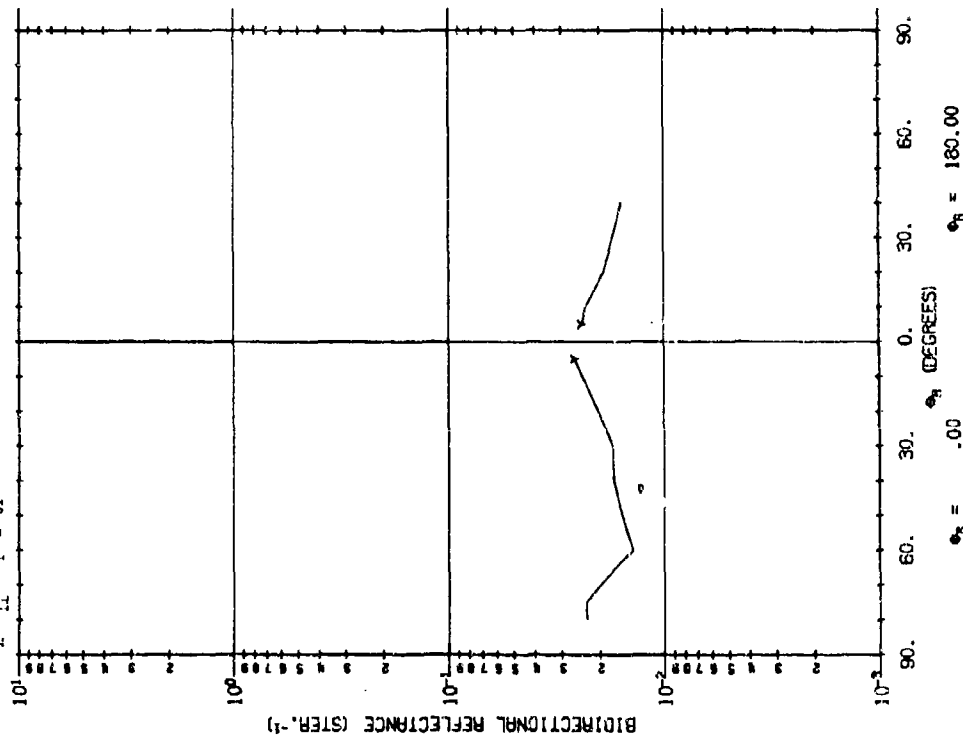


CLOTH AND CANVAS

A01471 002

Medium Gray Paint on Canvas, 16% Reflectance

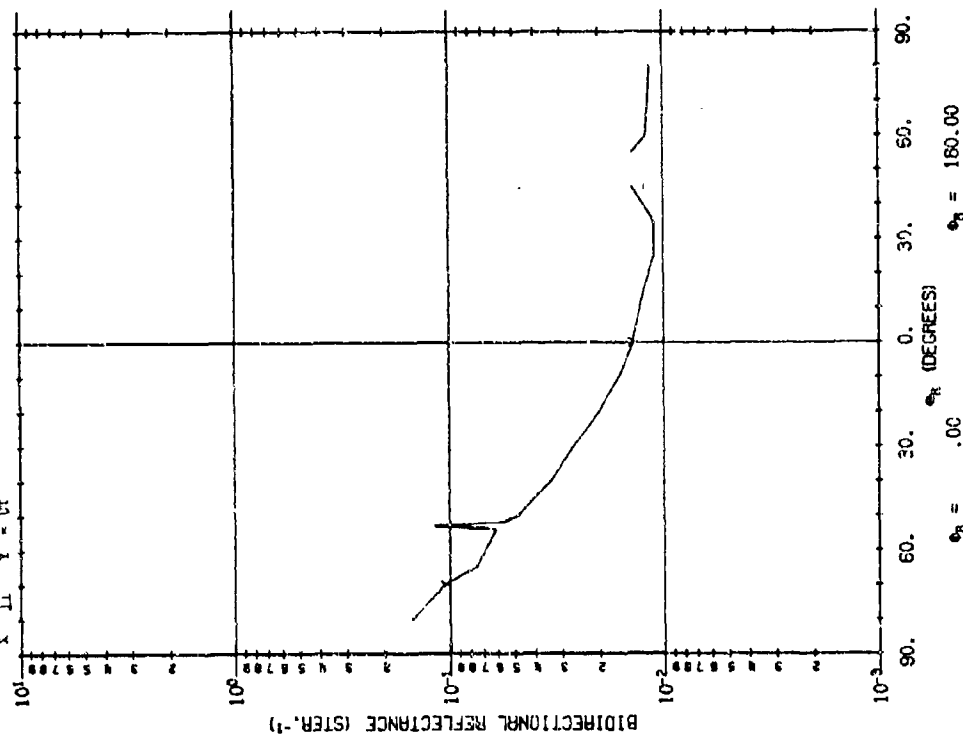
0 11  $\theta_1 = 0.0$   
 + 11  $\theta_2 = 180.0$   
 A 11  $\lambda = 10.6$   
 X 11  $\gamma = 0^\circ$



A01471 002

Medium Gray Paint on Canvas, 16% Reflectance

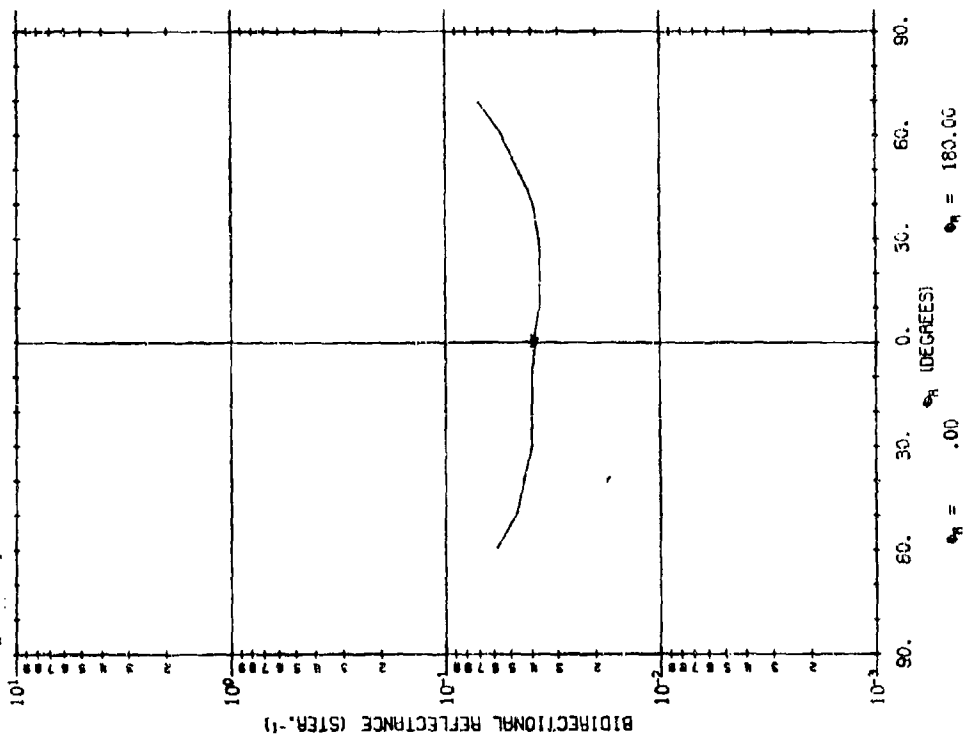
0 11  $\theta_1 = 50.0$   
 + 11  $\theta_2 = 180.0$   
 A 11  $\lambda = 10.6$   
 X 11  $\gamma = 0^\circ$



AC1474 .002

Grayish-White Paint on Canvas, 64% Reflectance

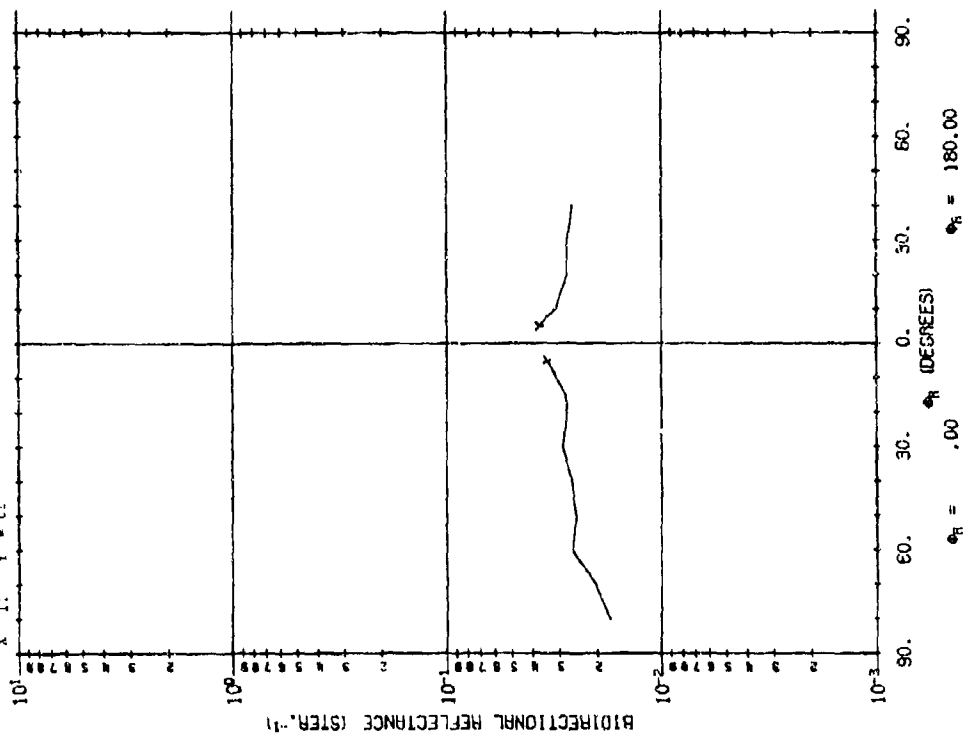
0 11 21 = 1.10  
+ 11 21 = 10  
- 11 21 = 10.6  
X 11 Y = 11



AC1474 .002

Grayish-White Paint on Canvas, 64% Reflectance

0 11 21 = 0.0  
+ 11 21 = 180.0  
- 11 21 = 10.6  
X 11 Y = 11

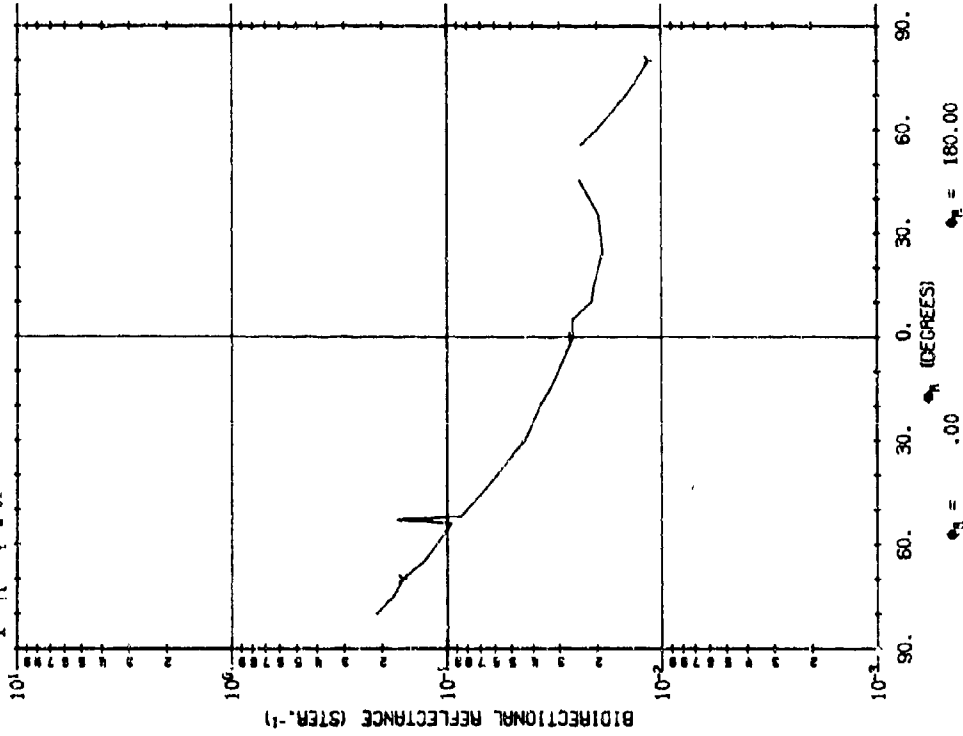


CLOTH AND CANVAS

A01474 002

Grayish-White Paint on Canvas, 64% Reflectance

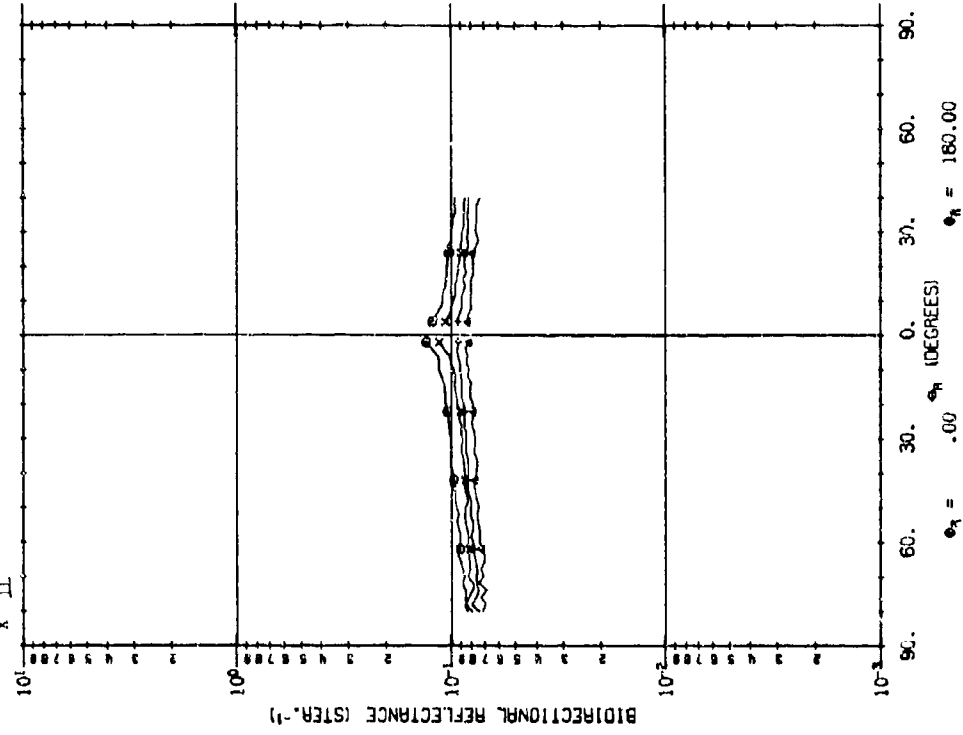
0 ||  $\epsilon_1 = 50.0$   
 + ||  $\epsilon_2 = 180.0$   
 x ||  $\lambda = 10.6$   
 x ||  $\gamma = \text{VT}$



A01475 101

GRAYISH-WHITE PAINT ON CANVAS,  
 64 PERCENT REFLECTANCE

0 ||  $\epsilon_1 = 0.0$   
 + ||  $\epsilon_2 = 180.0$   
 x ||  $\lambda = 0.63$   
 x ||  $\gamma = \text{VT}$

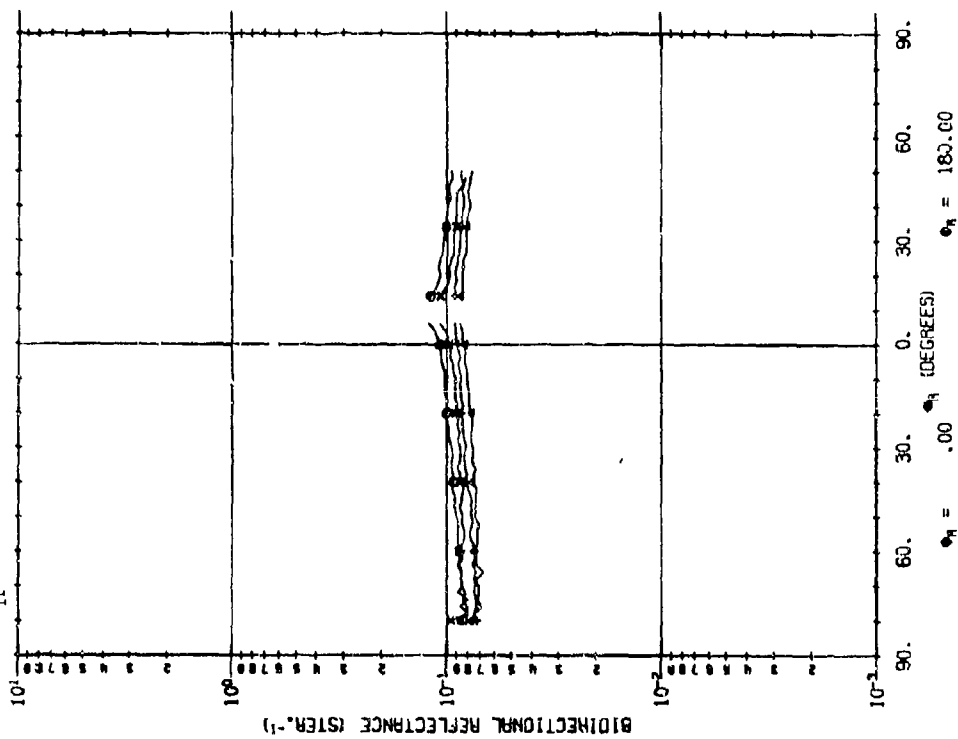


A01475 101

GRAYISH-WHITE PAINT ON CANVAS,  
64 PERCENT REFLECTANCE

$\theta_i = 10.0$   
 $\phi_i = 180.0$   
 $\lambda = 0.63$

X II

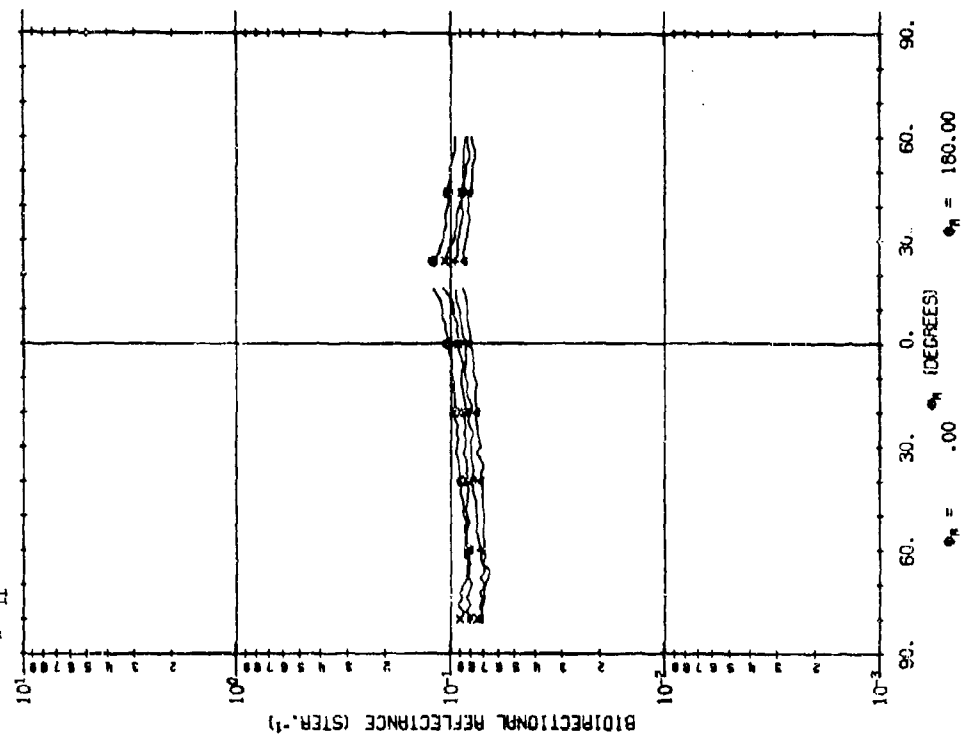


A01475 101

GRAYISH-WHITE PAINT ON CANVAS,  
64 PERCENT REFLECTANCE

$\theta_i = 20.0$   
 $\phi_i = 180.0$   
 $\lambda = 0.63$

X II

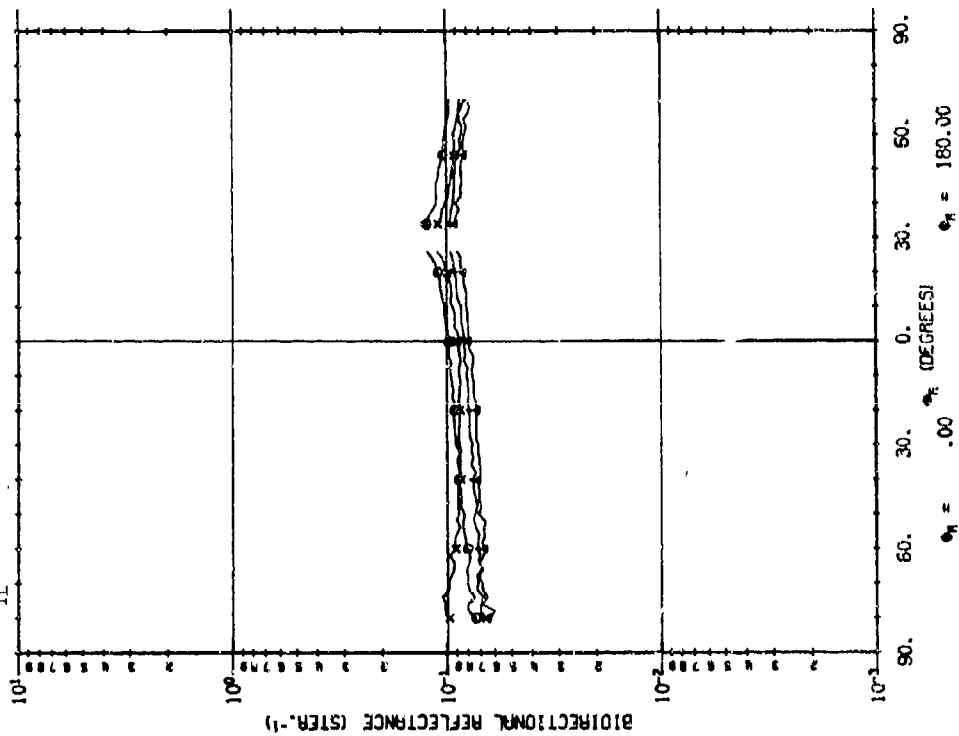


CLOTH AND CANVAS

A01475 101

GRAYISH-WHITE PAINT ON CANVAS,  
64 PERCENT REFLECTANCE

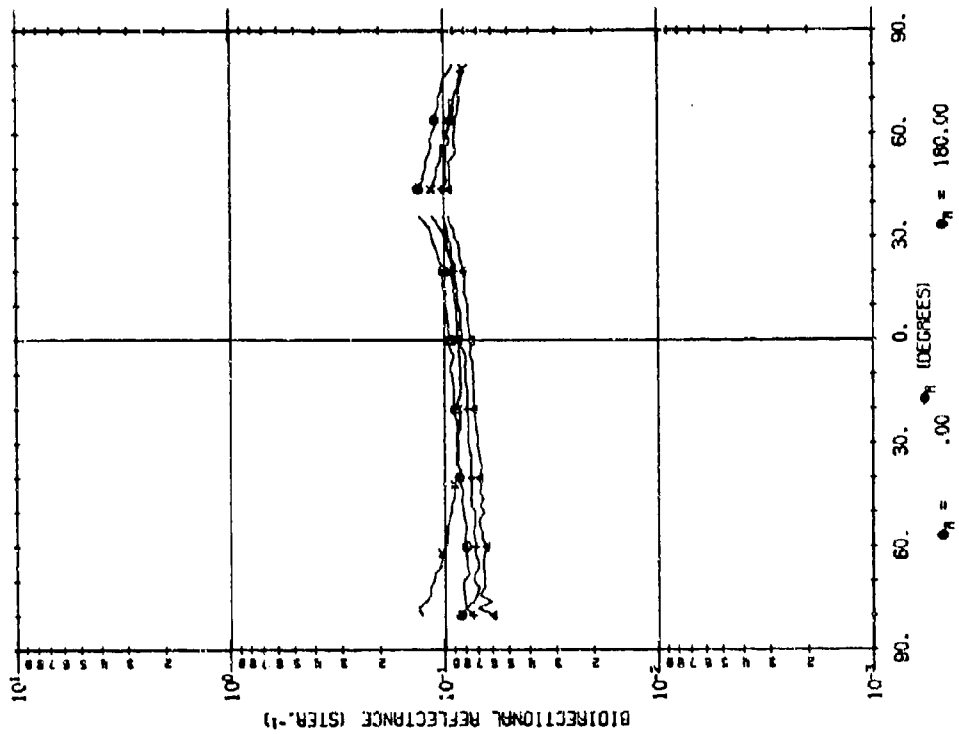
0 ||  $\phi_1 = 30.0$   
+ ||  $\phi_1 = 180.0$   
x ||  $\lambda = 0.63$



A01475 101

GRAYISH-WHITE PAINT ON CANVAS,  
64 PERCENT REFLECTANCE

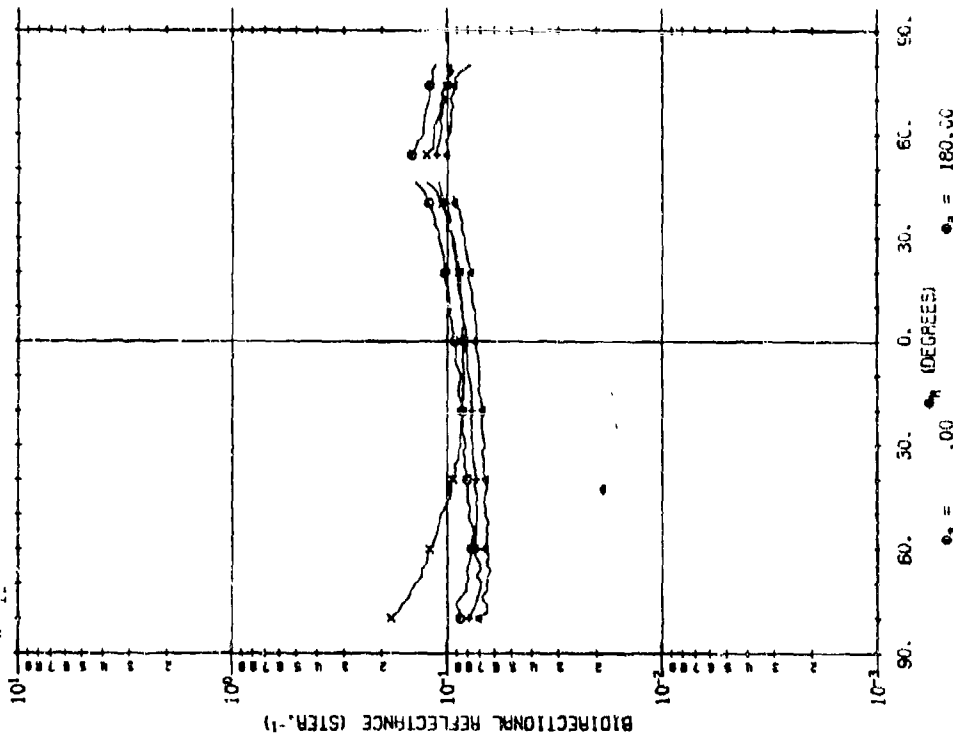
0 ||  $\phi_1 = 40.0$   
+ ||  $\phi_1 = 180.0$   
x ||  $\lambda = 0.63$



R01475 101

GRAYISH-WHITE PAINT ON CANVAS,  
64 PERCENT REFLECTANCE

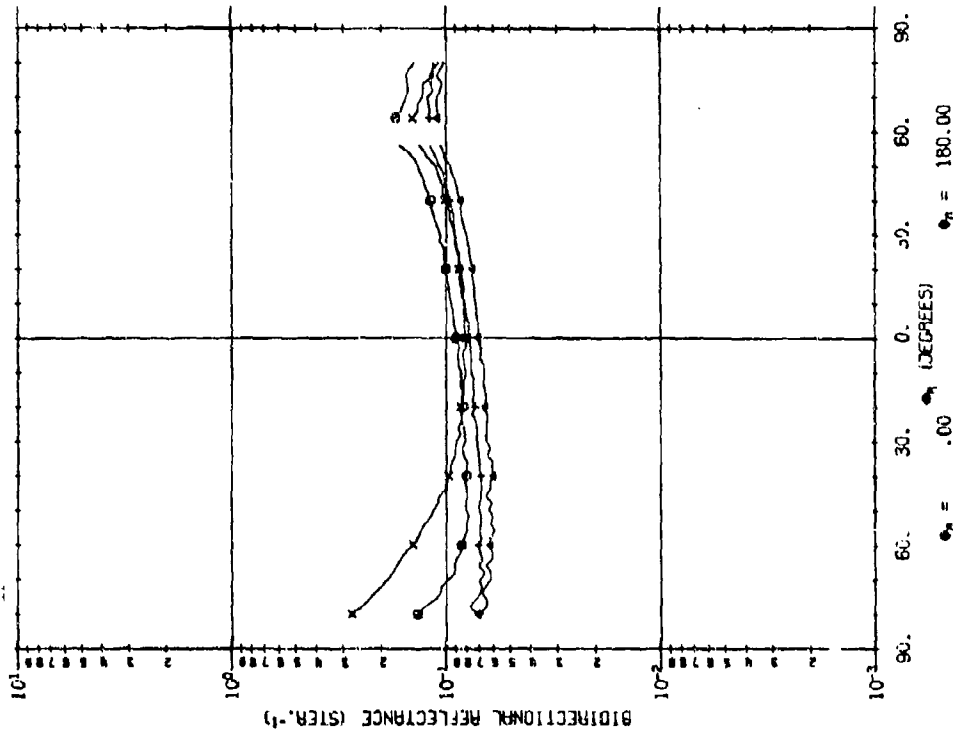
$\theta_1 = 50.0$   
 $\theta_2 = 180.0$   
 $\lambda = 0.53$



R01475 101

GRAYISH-WHITE PAINT ON CANVAS,  
64 PERCENT REFLECTANCE

$\theta_1 = 60.0$   
 $\theta_2 = 180.0$   
 $\lambda = 0.63$

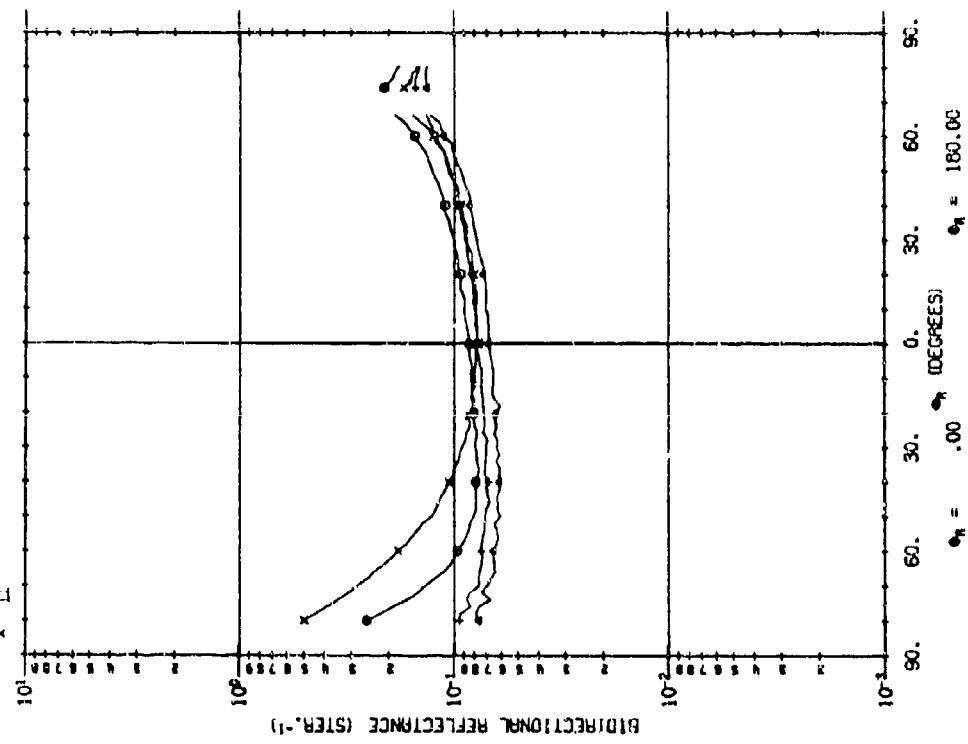


CLOTH AND CANVAS

A01475 101

GRAYISH-WHITE PAINT ON CANVAS.  
64 PERCENT REFLECTANCE

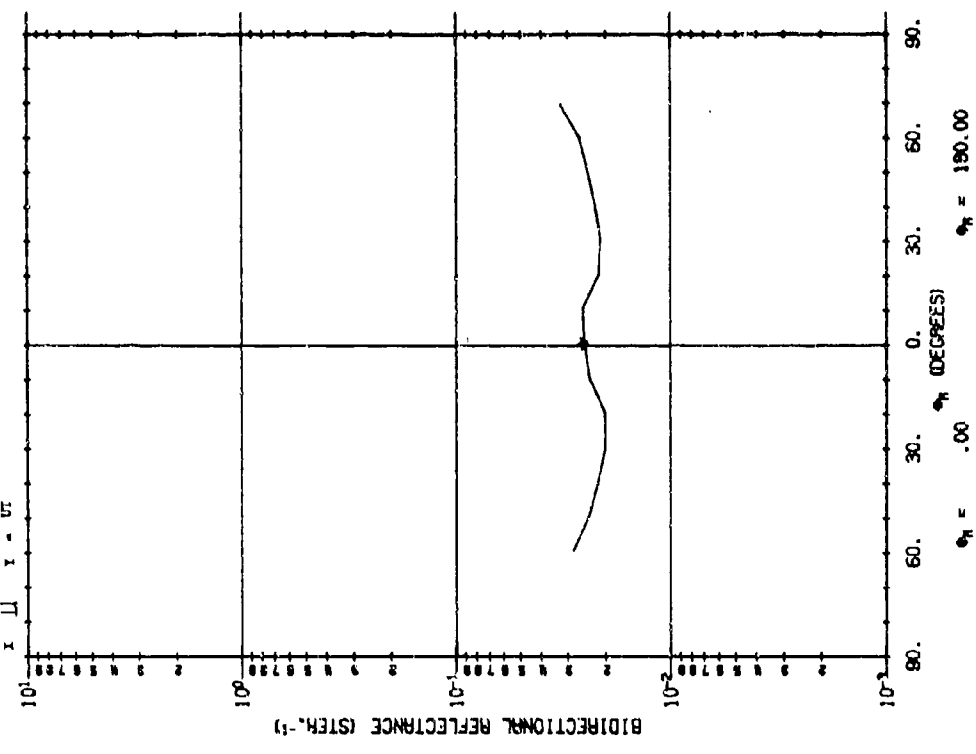
0 || 5" 70.6  
+ || 1" 180.0  
x || 1" 0.63



A01478 002

Green Paint on Canvas

0 || 23" 1.10  
+ || 1" 4.7  
x || 1" 10.6

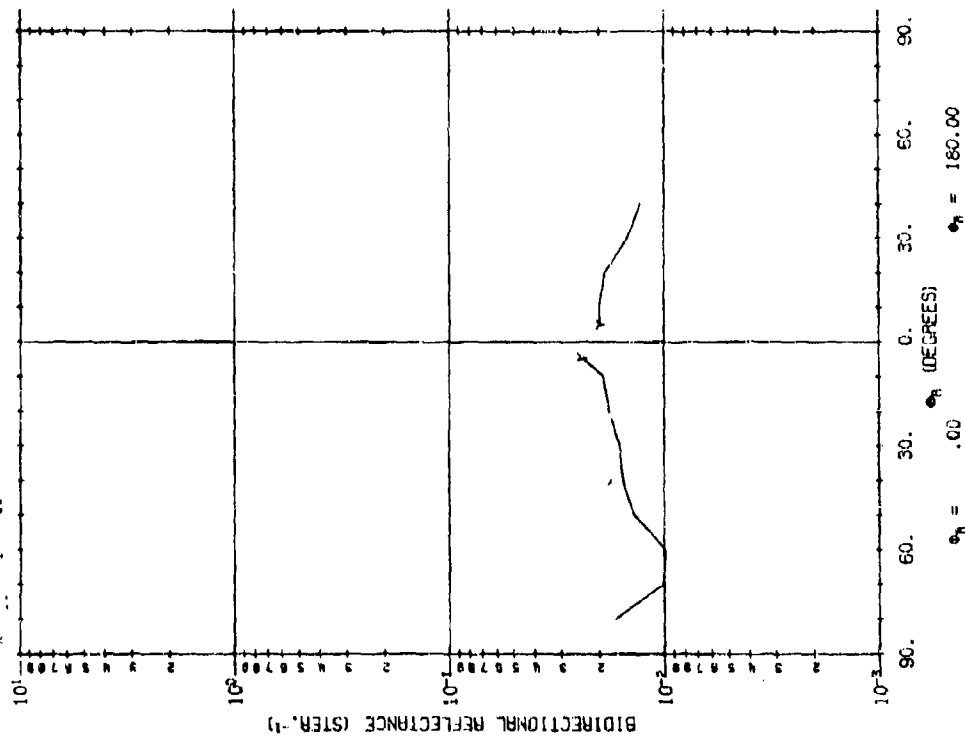




A01478 002

Green Paint on Canvas

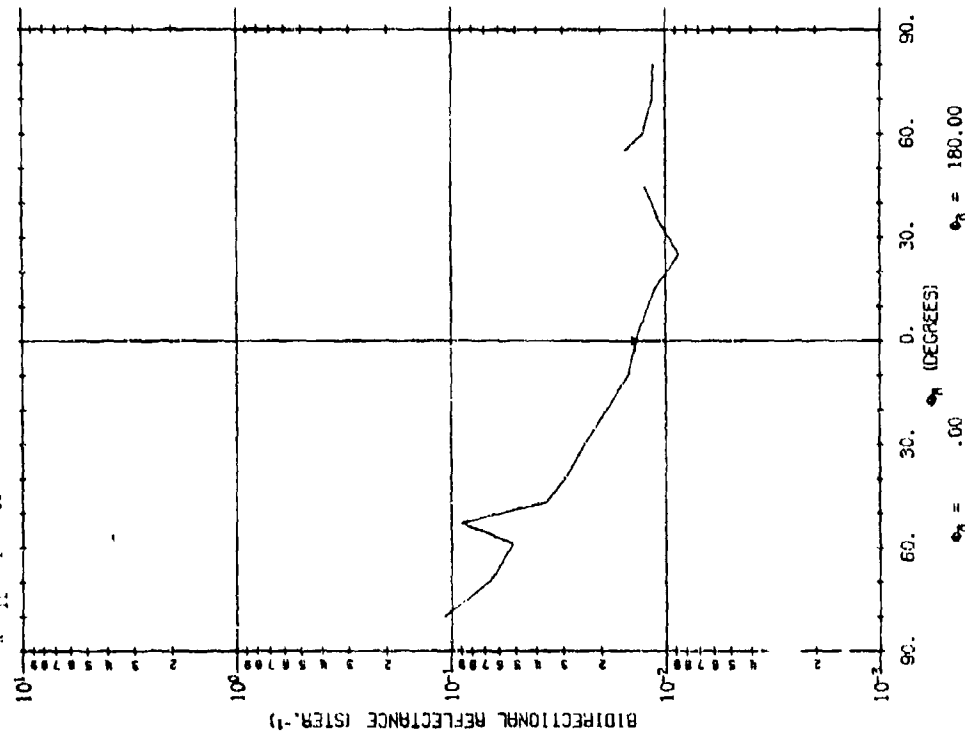
$\theta_i = 0.0$   
 $\theta_r = 180.0$   
 $\lambda = 10.6$   
 $\mu = 1.0$



A01478 002

Green Paint on Canvas

$\theta_i = 53.6$   
 $\theta_r = 180.0$   
 $\lambda = 10.6$   
 $\mu = 1.0$



CLOTH AND CANVAS

R01480 002

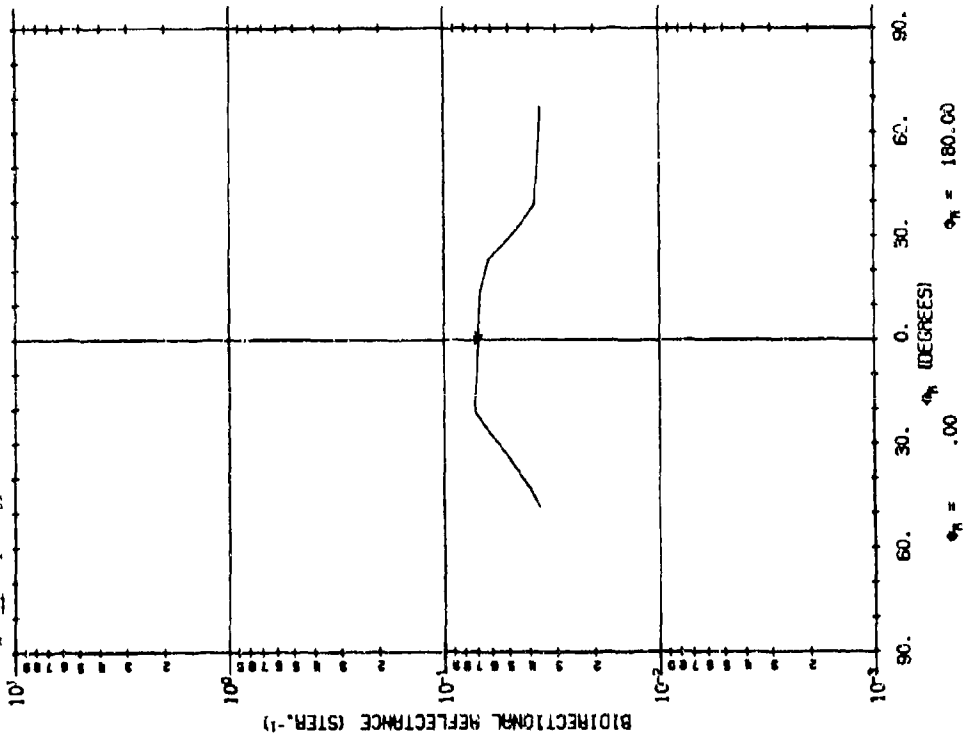
Undyed Cotton, Mercerized Medium

$2\theta = 1.10$

$\phi_1 = \phi_2$

$\lambda = 13.6$

$\gamma = 0^\circ$



R01480 002

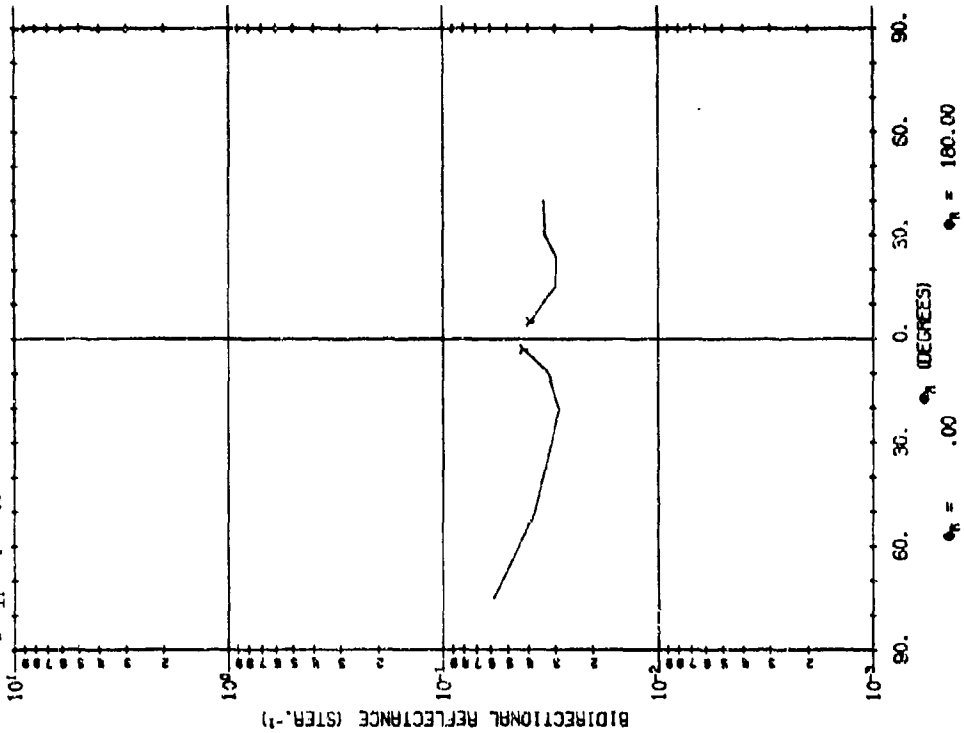
Undyed Cotton, Mercerized Medium

$2\theta = 0.0$

$\phi_1 = \phi_2$

$\lambda = 10.6$

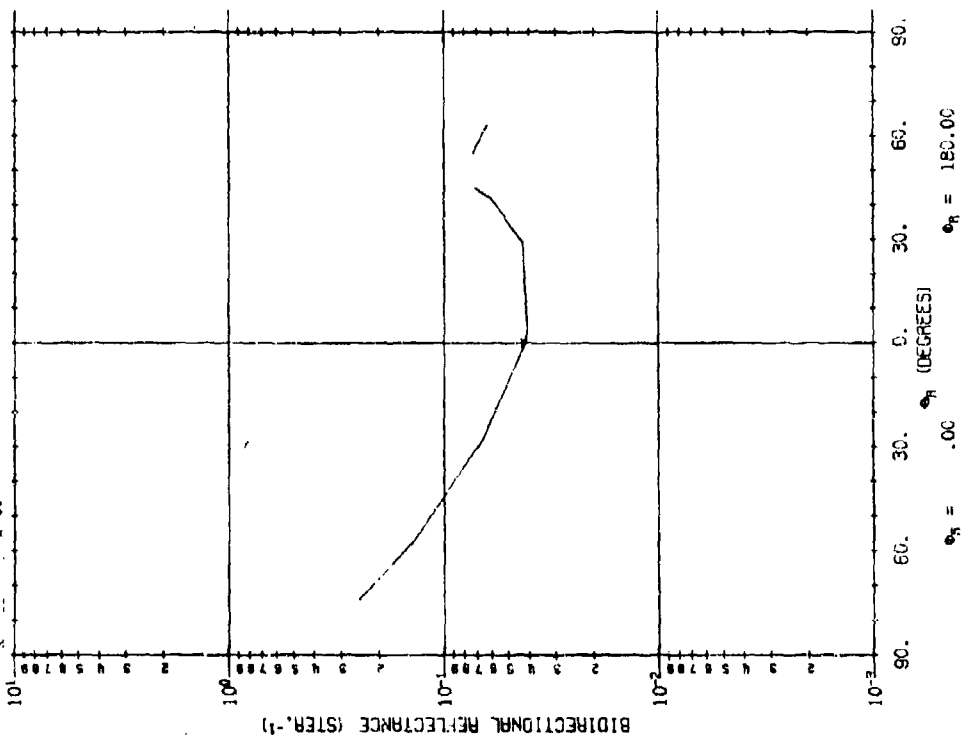
$\gamma = 0^\circ$



A01480 002

Indyed Cotton, Mercerized Medium

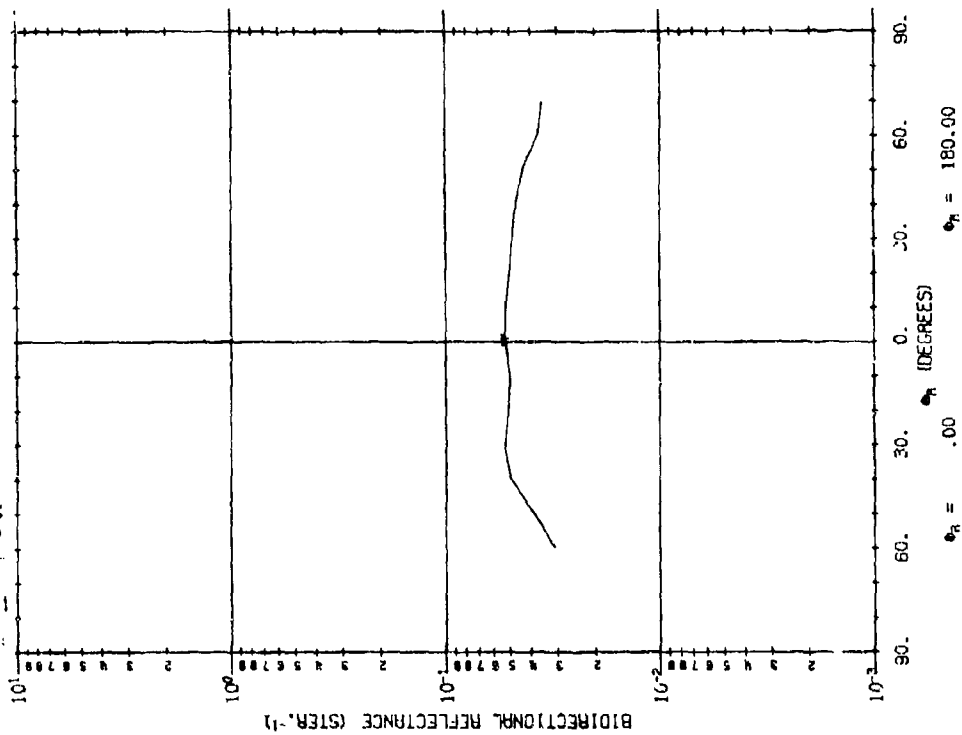
$\theta_i = 50.0$   
 $\theta_r = 180.0$   
 $\theta_t = 10.6$   
 $\theta_n = 0.0$



A01483 002

Vat Dyed Cotton, Mercerized Medium

$\theta_i = 1.10$   
 $\theta_r = 180.0$   
 $\theta_t = 10.6$   
 $\theta_n = 0.0$

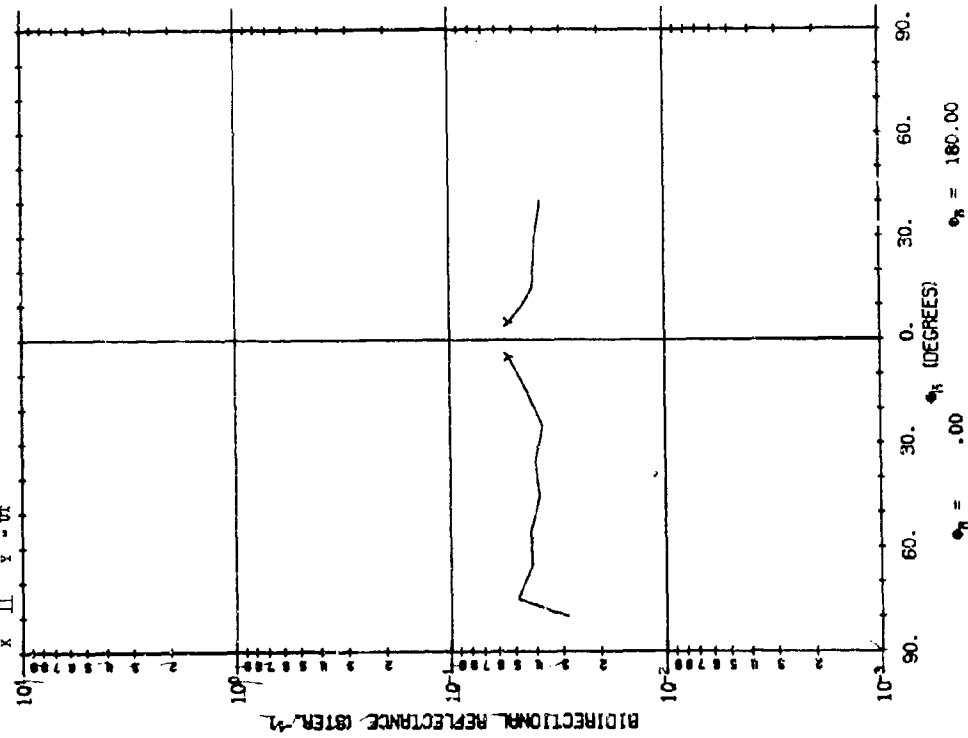


CLOTH AND CANVAS

AG1483 002

Vat Dyed Cotton, Mercerized Medium

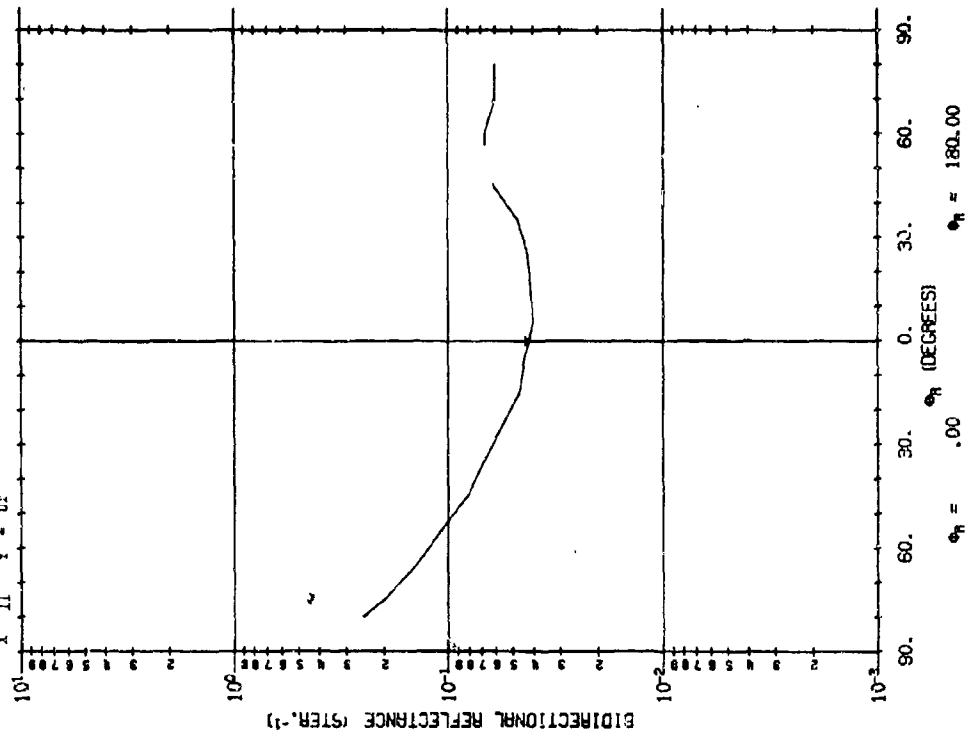
0 ||  $\theta_1 = 0.0$   
 + ||  $\phi_1 = 180.0$   
 Δ ||  $\lambda = 10.6$   
 X || Y = VT



AG1483 002

Vat Dyed Cotton, Mercerized Medium

0 ||  $\theta_1 = 50.0$   
 + ||  $\phi_1 = 180.0$   
 Δ ||  $\lambda = 10.6$   
 X || Y = VT

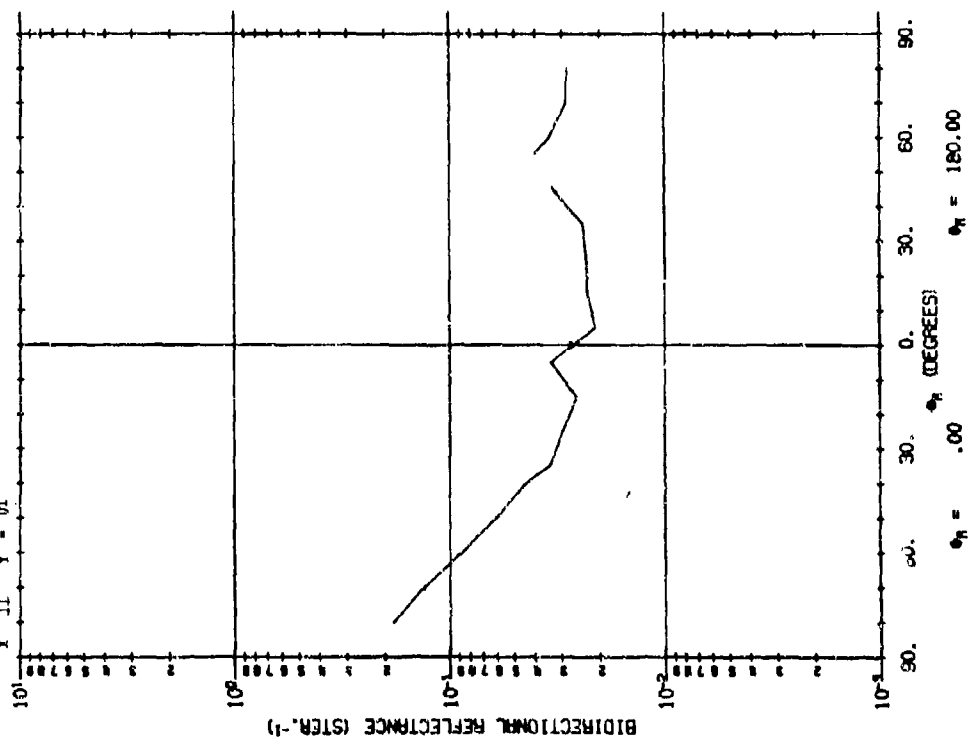




A01486 002

Cotton, Sulfur Dye, Mercerized Medium

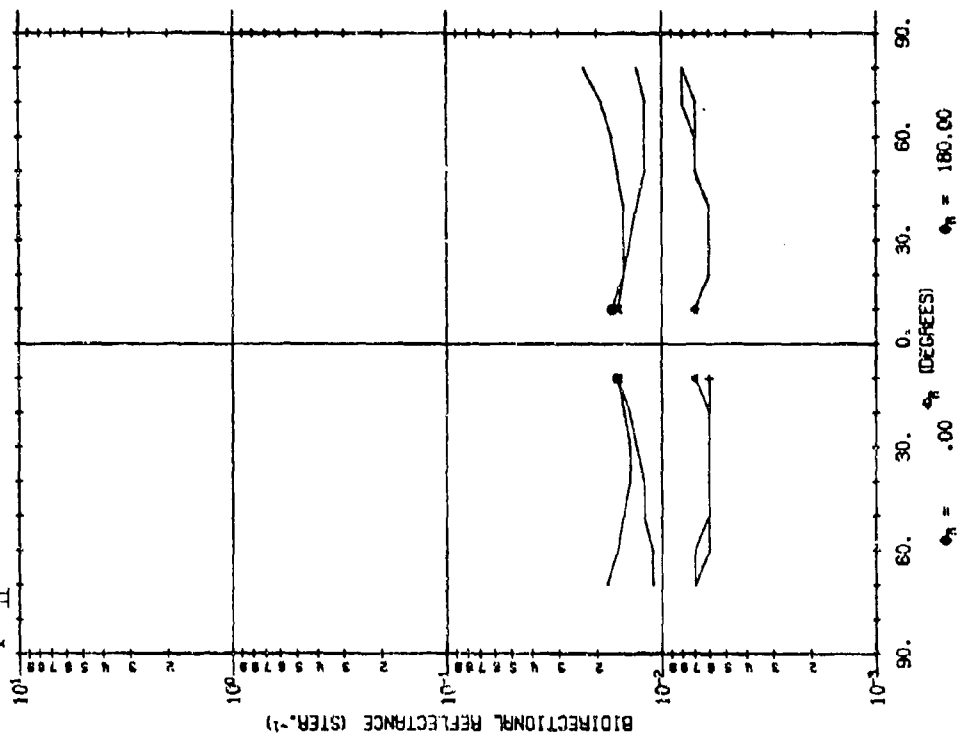
0 //  $\epsilon_1 = 50.0$   
 + //  $\epsilon_2 = 180.0$   
 Δ //  $\lambda = 10.6$   
 X //  $\gamma = \text{WT}$



A01510 001

OLIVE DRAB CANVAS TARPAILIN

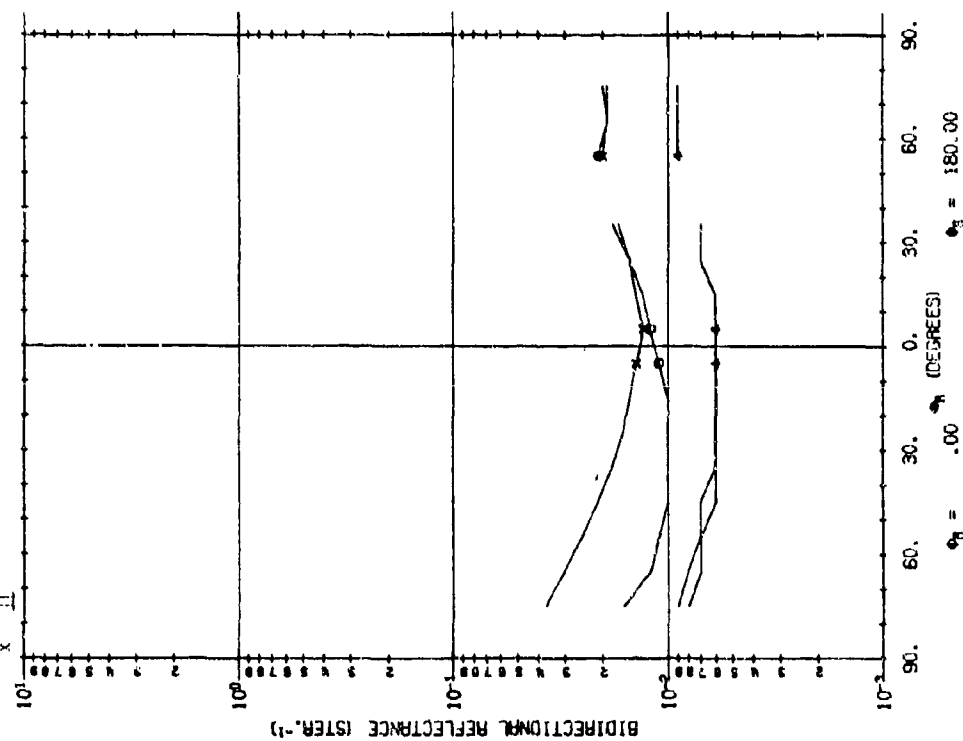
0 //  $\epsilon_1 = 0.0$   
 + //  $\epsilon_2 = 180.0$   
 Δ //  $\lambda = 0.63$   
 X //  $\gamma = \text{WT}$



A01510 001

OLIVE DRAB CANVAS TAREALIN

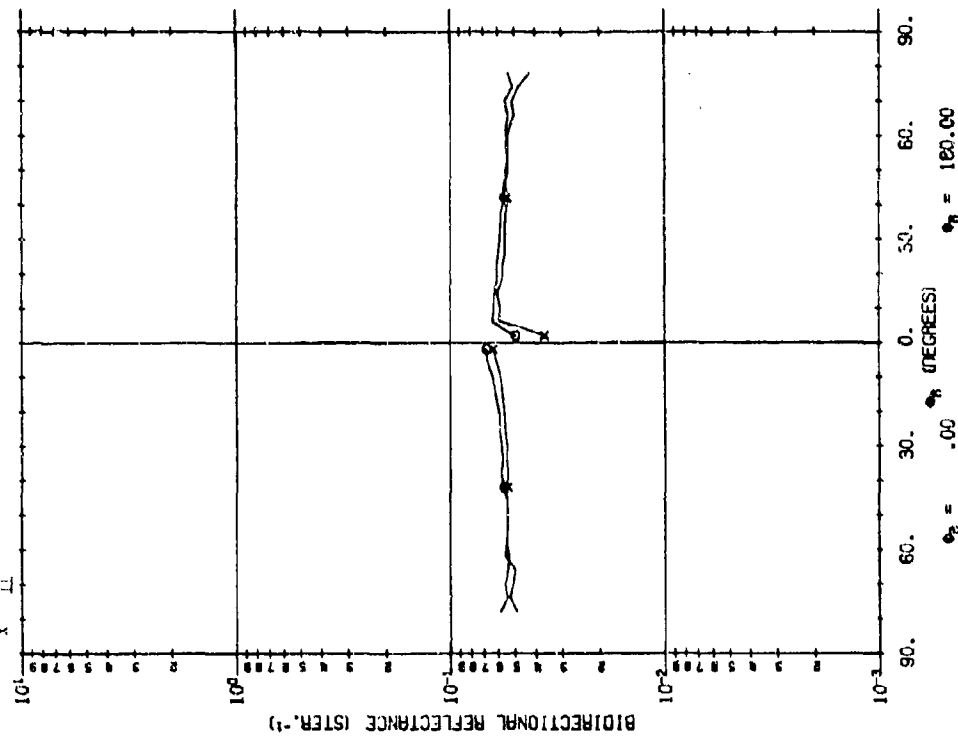
0  $\theta_1 = 45.0$   
 +  $\theta_1 = 180.0$   
 -  $\theta_1 = 0.0$   
 x  $\theta_1 = 0.63$



A01667 101

Red Canvas

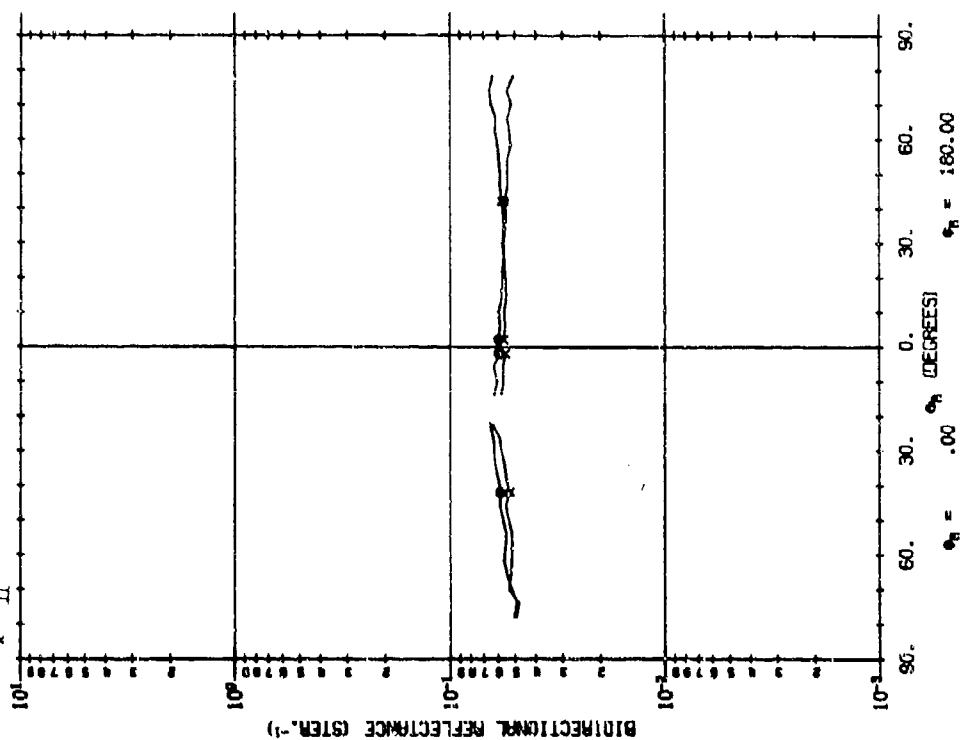
0  $\theta_1 = 0.0$   
 +  $\theta_1 = 0.0$   
 -  $\theta_1 = 0.0$   
 x  $\theta_1 = 0.63$



CLOTH AND CANVAS

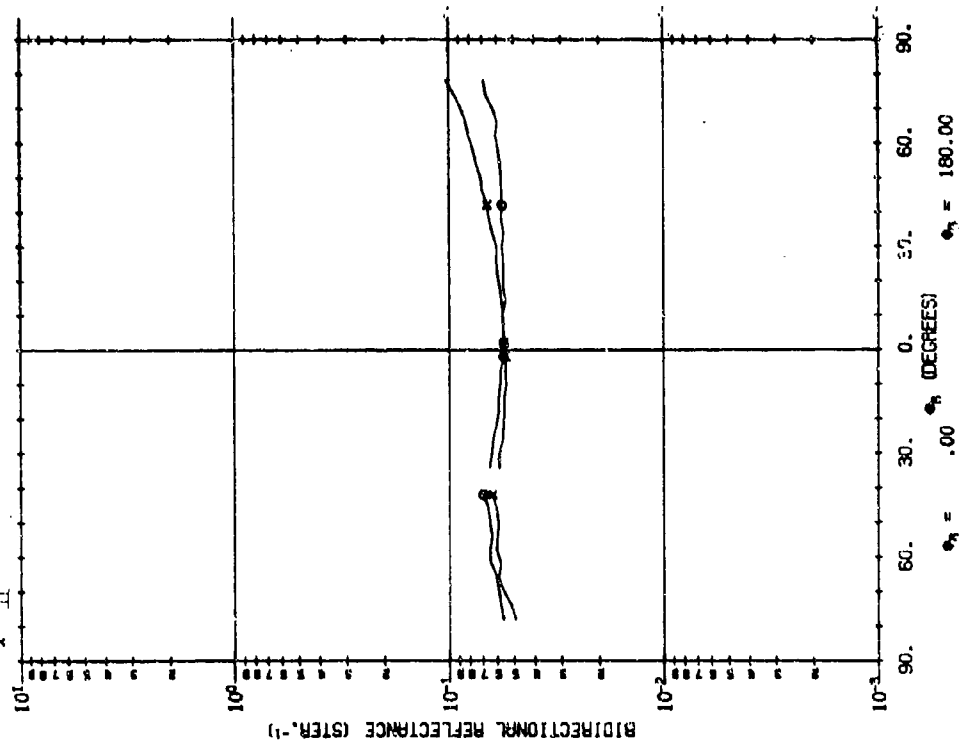
R01667 101  
 0 ||  $\theta_i = 20.0$   
 + ||  $\phi_i = 0.0$   
 A ||  $\lambda = 0.63$   
 X ||

Red Curves



R01667 101  
 0 ||  $\theta_i = 40.0$   
 + ||  $\phi_i = 0.0$   
 A ||  $\lambda = 0.63$   
 X ||

Red Curves

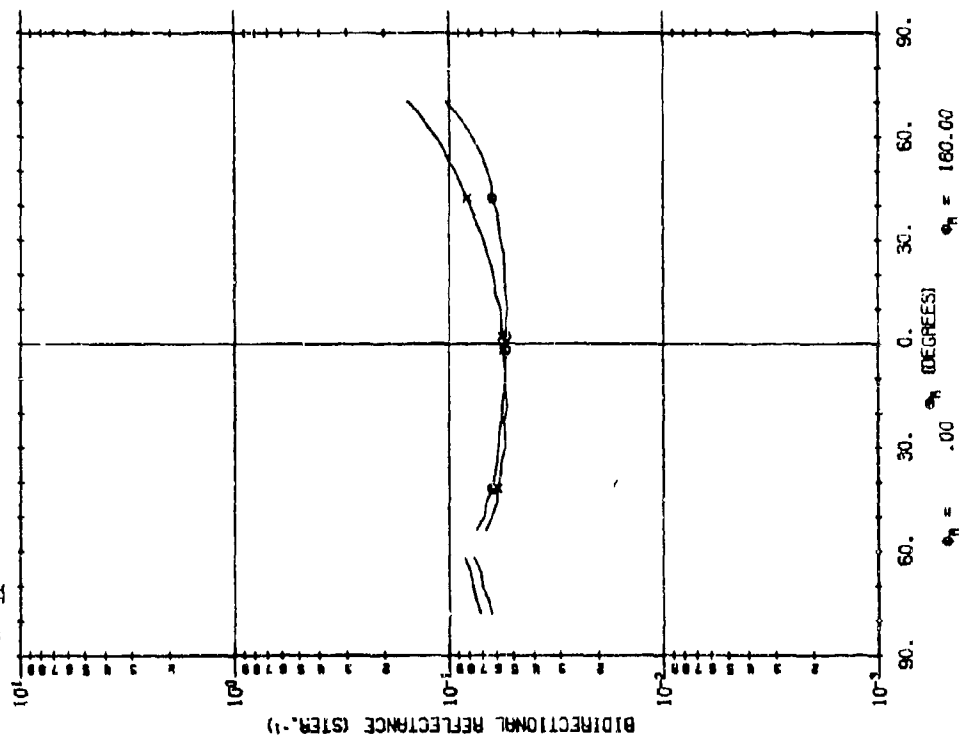




A01667 101  
 0  
 +  
 -  
 x

Ref Canvas

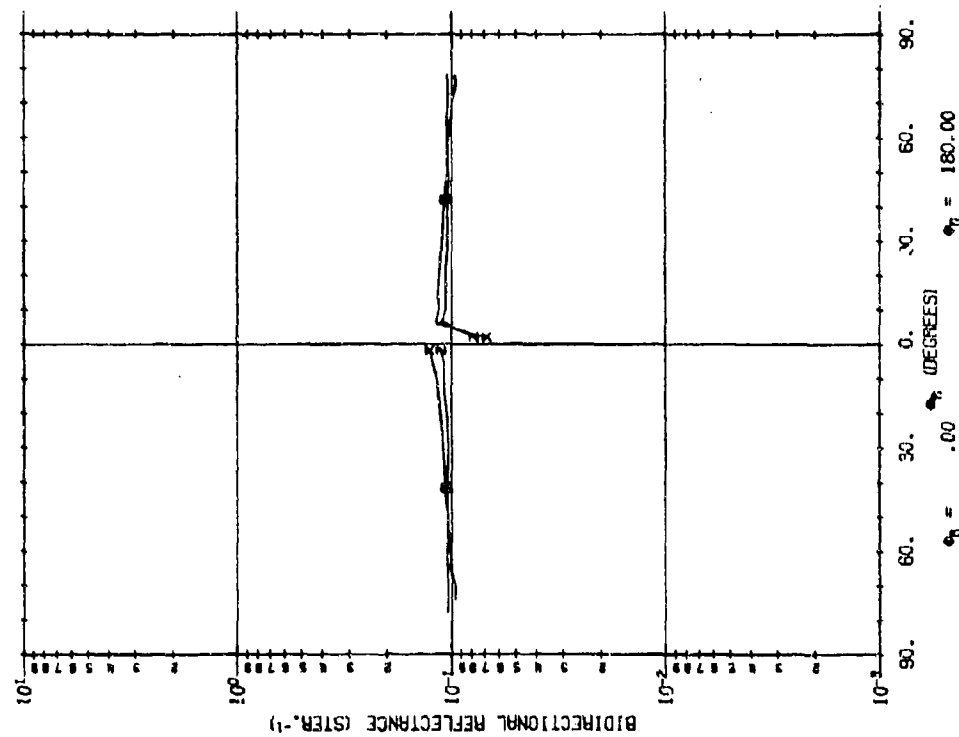
$\theta_1 = 60.0$   
 $\phi_1 = 0.0$   
 $\lambda = 0.63$



A01667 103  
 x  
 z

Ref Canvas

$\theta_1 = 0.0$   
 $\phi_1 = 0.0$   
 $\lambda = 0.63$



CLOTH AND CANVAS

A01667 103

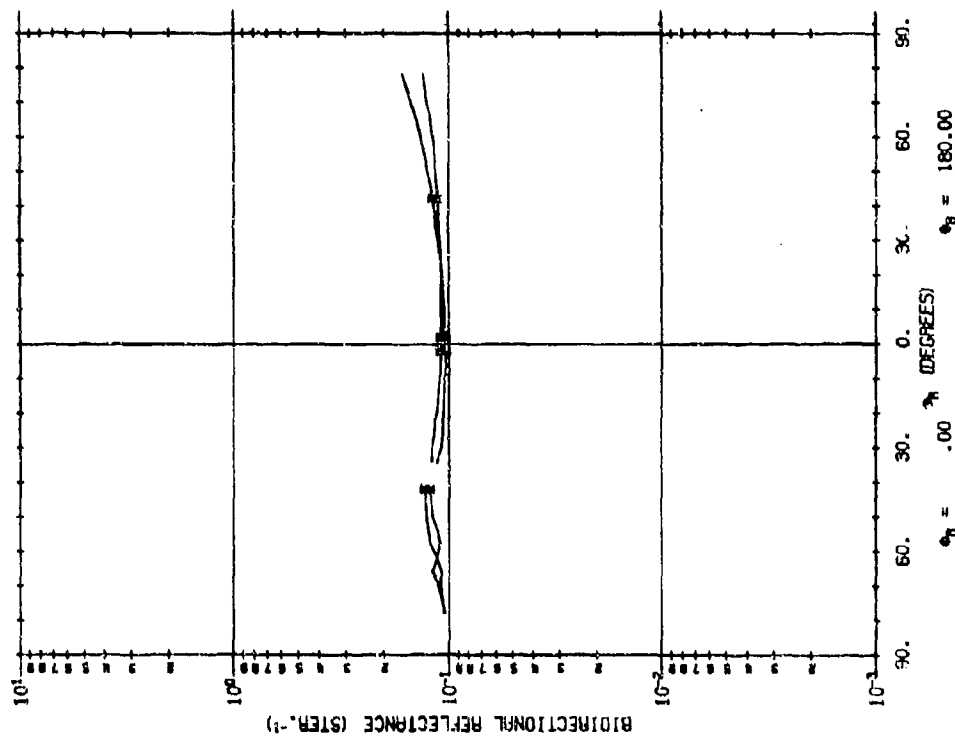
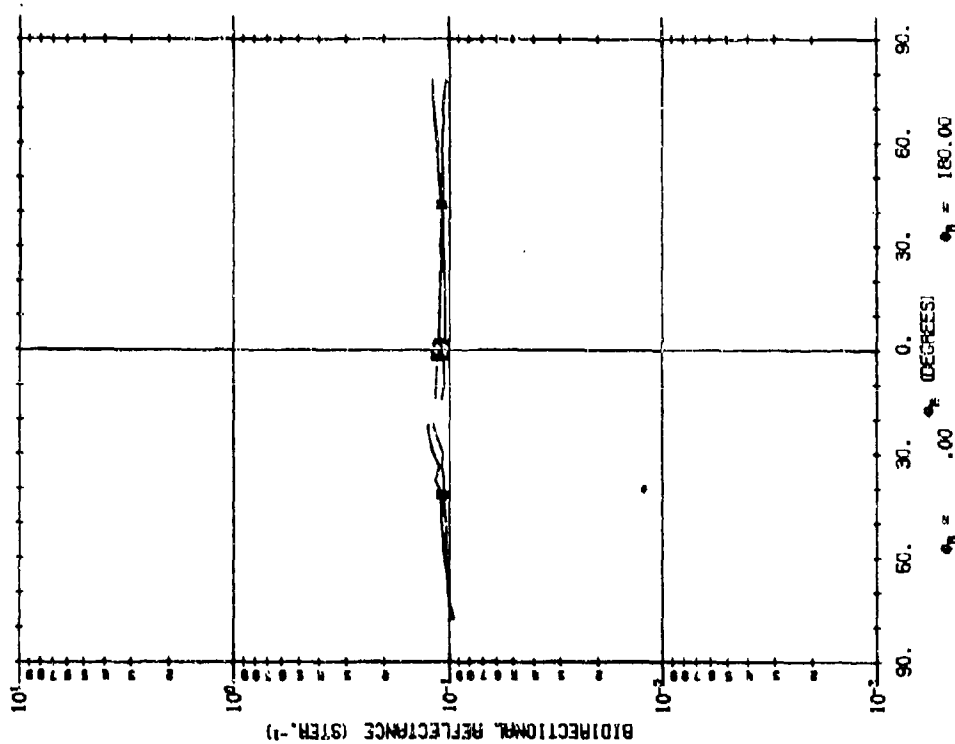
Ref Curves

$\theta_i = 20.0$   
 $\phi_i = 0.0$   
 $\lambda = 0.63$

A01667 103

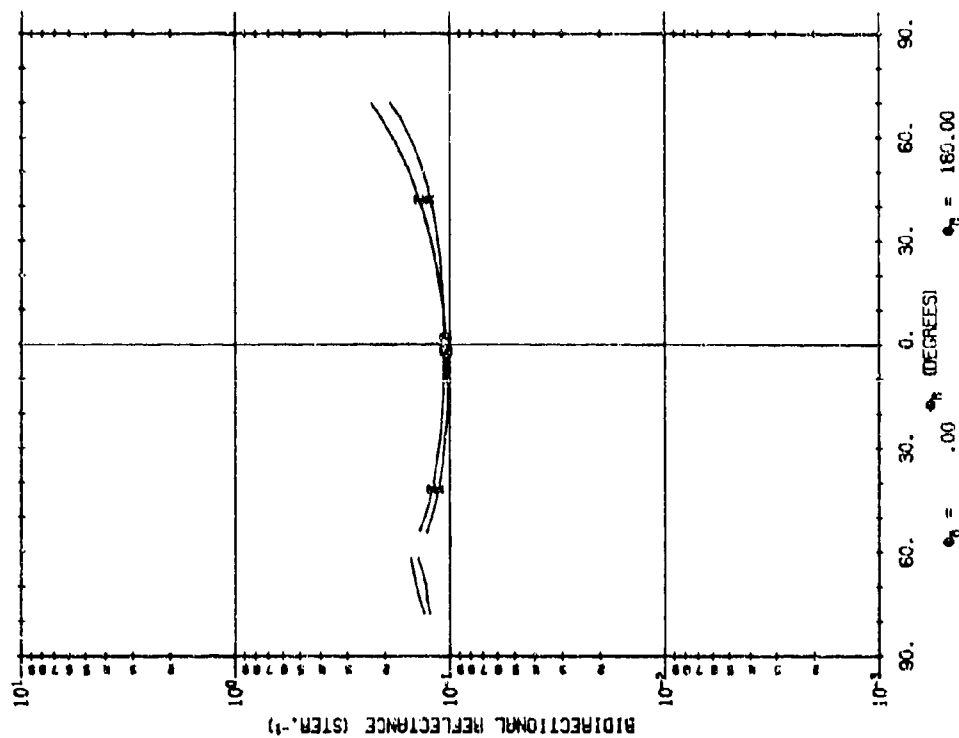
Ref Curves

$\theta_i = 40.0$   
 $\phi_i = 0.0$   
 $\lambda = 0.63$



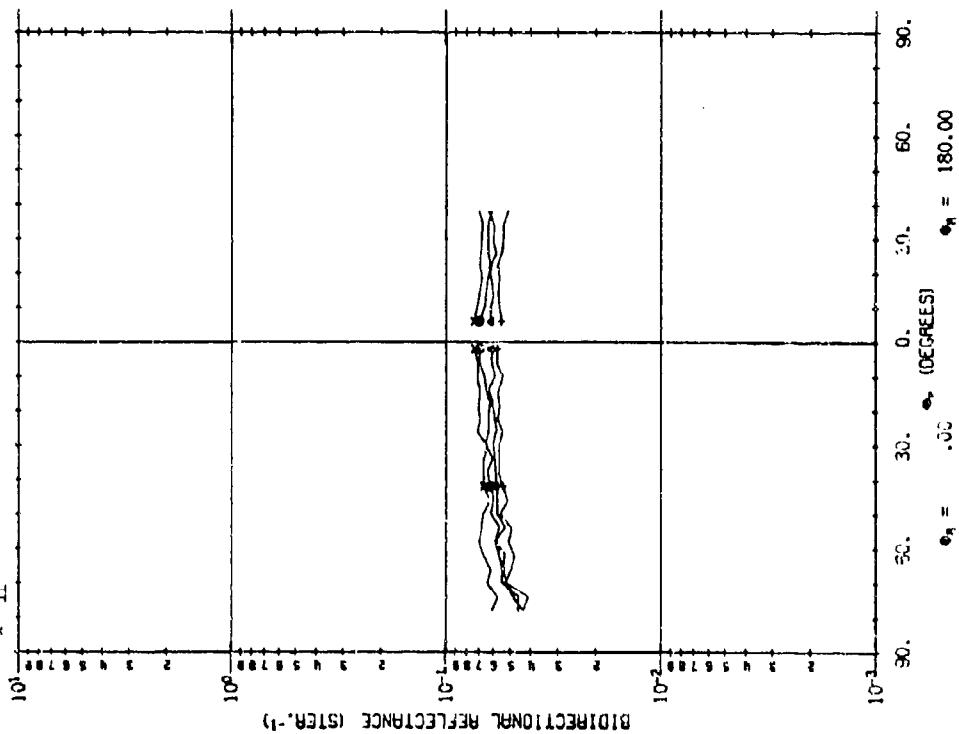
A01667 103  
 X 17  $\theta_1 = 60.0$   
 Z 17  $\theta_1 = 0.0$   
 17  $\lambda = 0.63$

Red Canvas



A01667 102  
 0 17  $\theta_1 = 0.0$   
 + 17  $\theta_1 = 180.0$   
 2 17  $\lambda = 1.15$   
 17

RED CANVAS

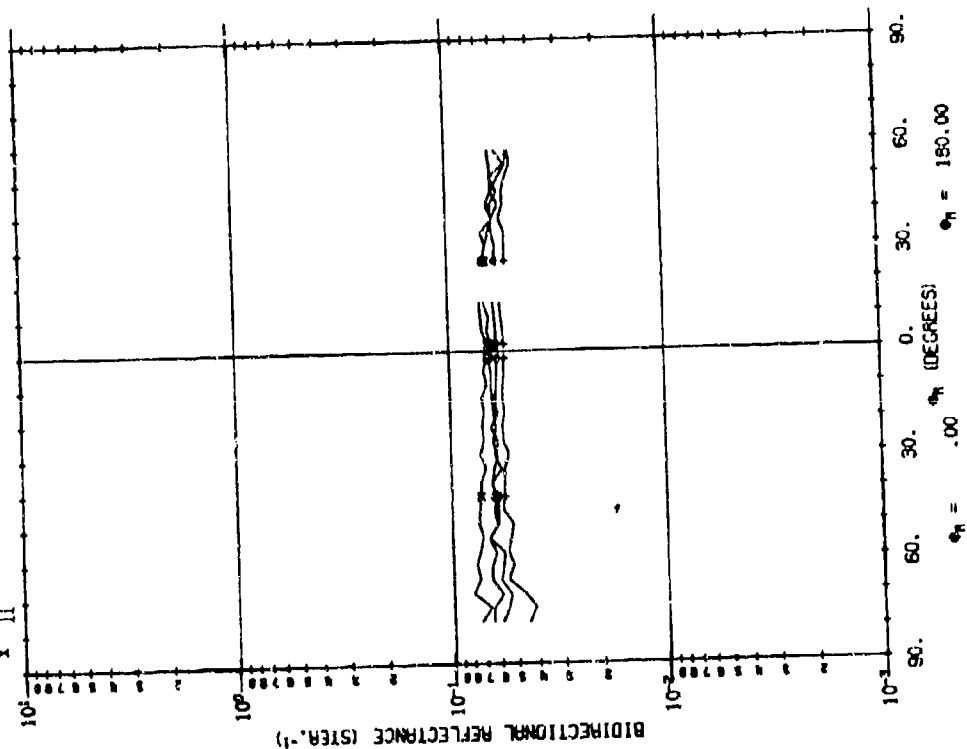


CLOTH AND CANVAS

R01667 102

KEY CURVES

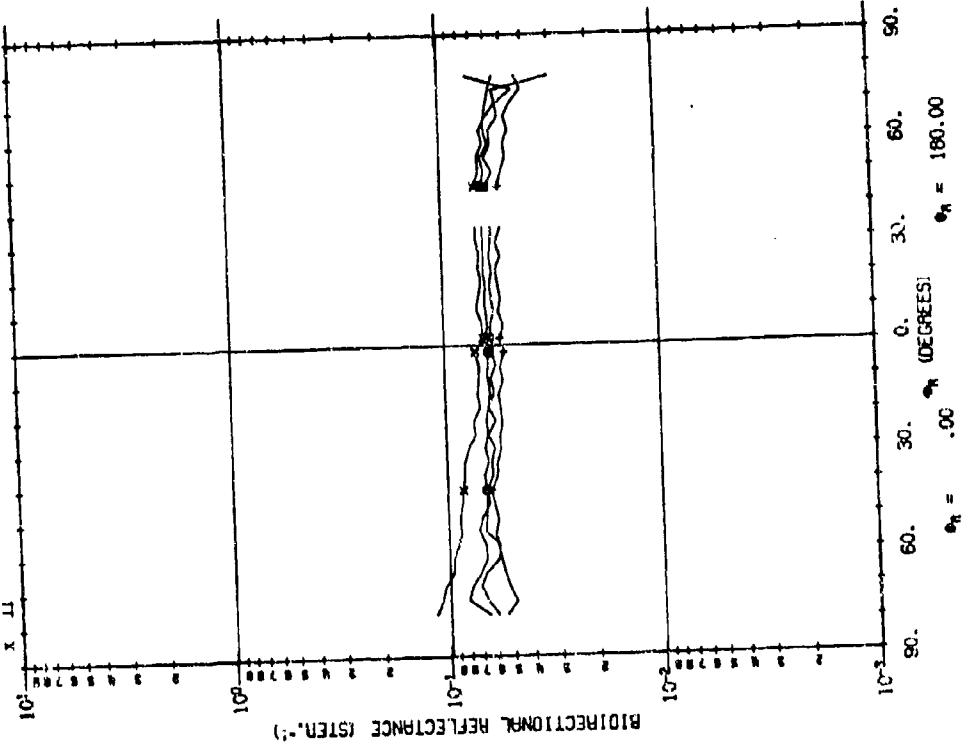
0 ||  $\epsilon_1 = 20.0$   
 + ||  $\epsilon_1 = 180.0$   
 x ||  $\lambda = 1.15$   
 ||



R01667 102

KEY CURVES

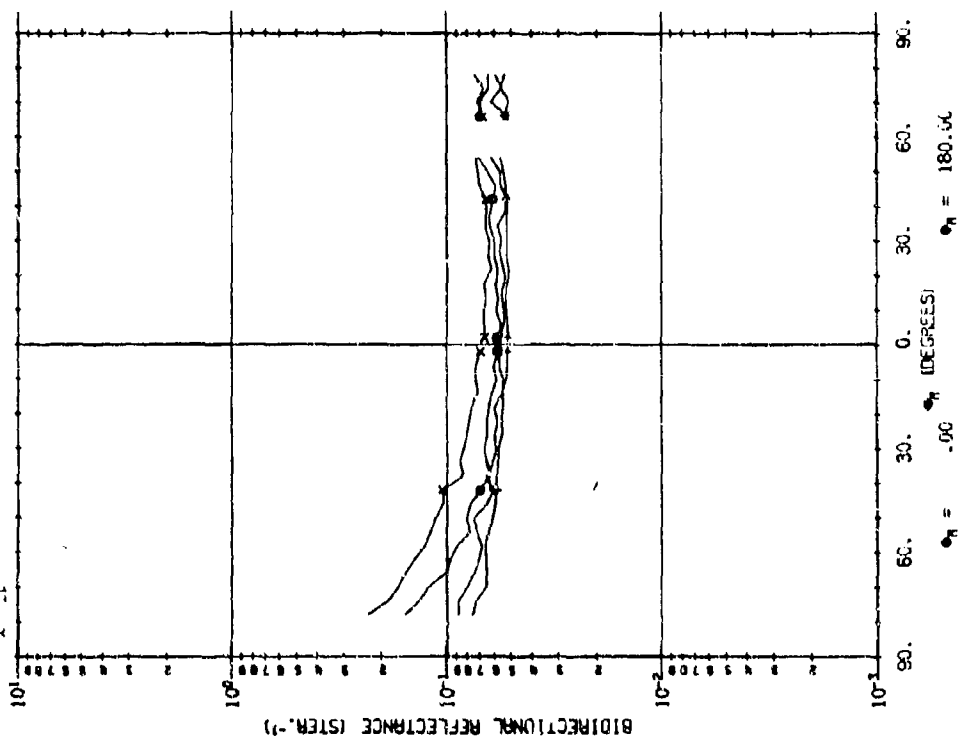
0 ||  $\epsilon_1 = 40.0$   
 + ||  $\epsilon_1 = 180.0$   
 x ||  $\lambda = 1.15$   
 ||



A01667 102

RED CANVAS

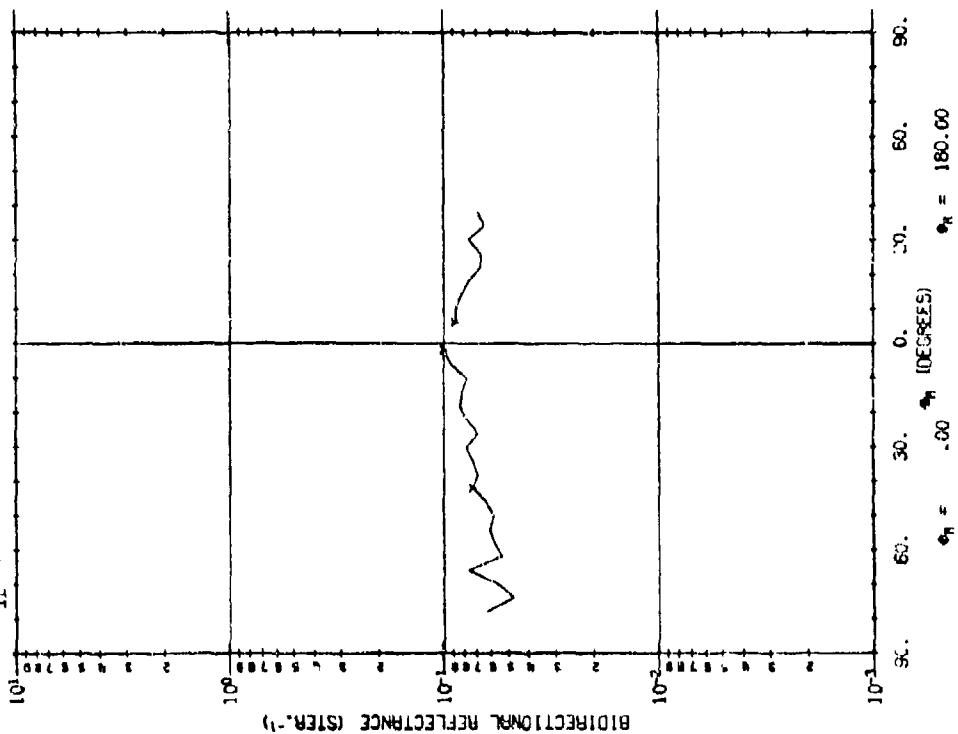
0 ||  $\epsilon_1 = 60.0$   
 + ||  $\epsilon_2 = 180.0$   
 Δ ||  $\lambda = 1.15$   
 x ||  $\gamma = \pi$



A01668 102

BLUE CANVAS

0 ||  $\epsilon_1 = 0.0$   
 + ||  $\epsilon_2 = 180.0$   
 Δ ||  $\lambda = 0.46$   
 x ||  $\gamma = \pi$

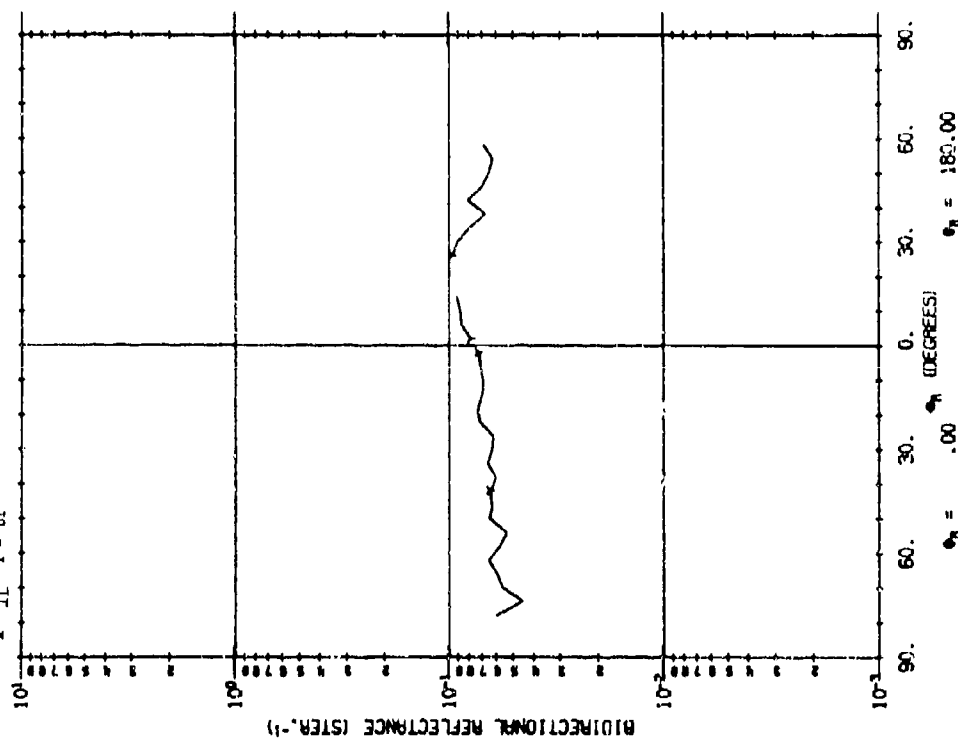


# CLOTH AND CANVAS

R01668 102

BLUE CANVAS

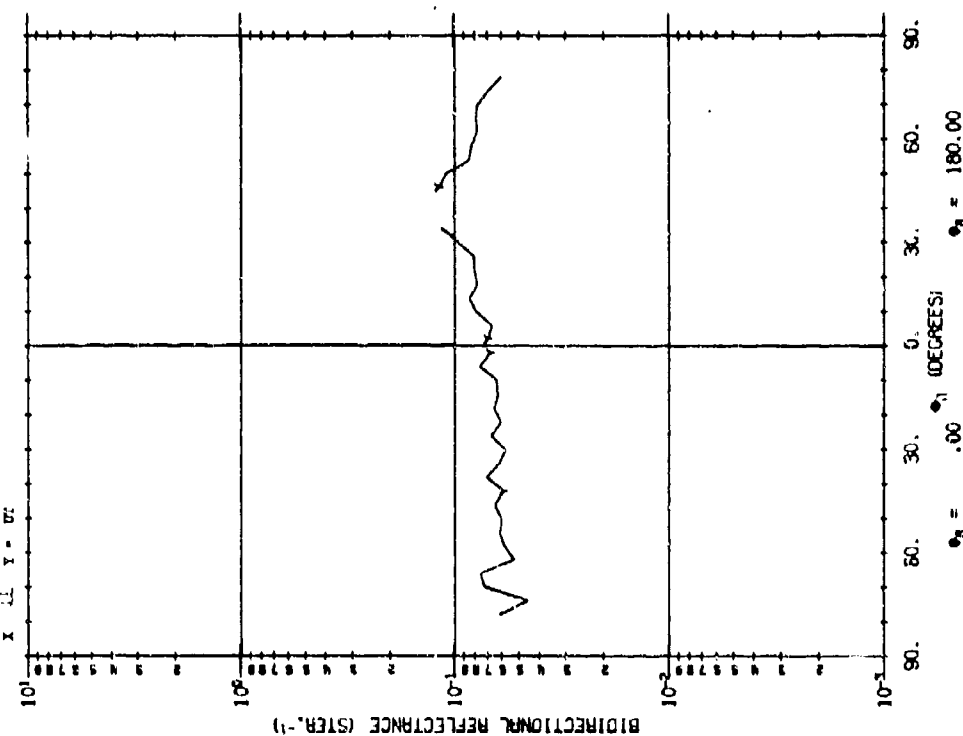
C ||  $\theta_1 = 20.0$   
 + ||  $\theta_2 = 180.0$   
 A ||  $\lambda = 0.46$   
 X || Y = UT



R01668 102

BLUE CANVAS

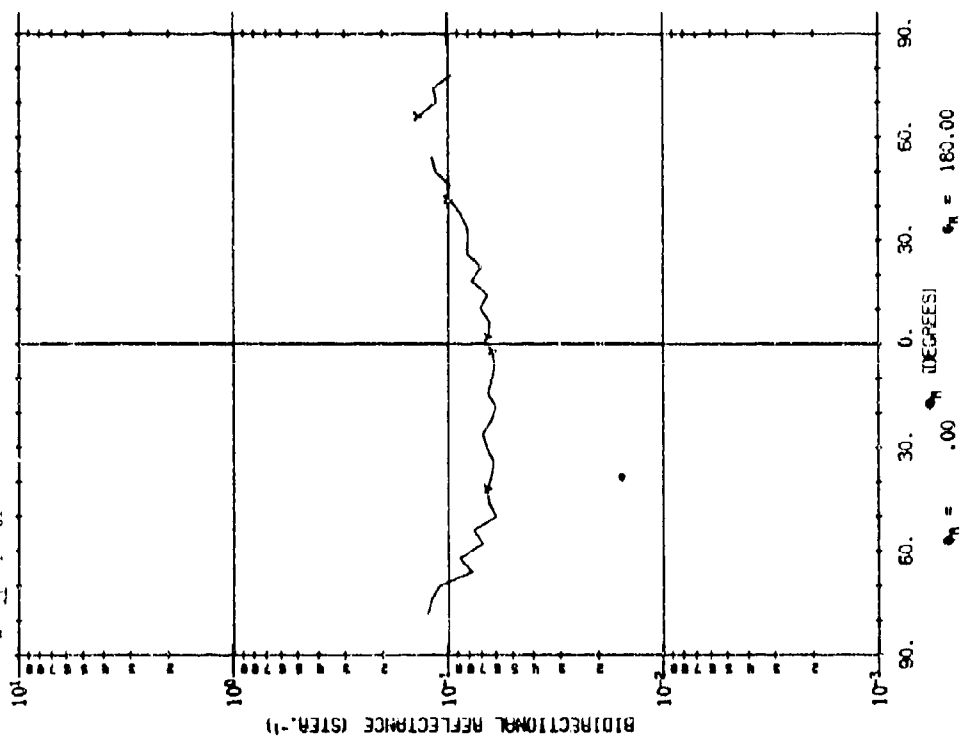
C ||  $\theta_1 = 40.0$   
 + ||  $\theta_2 = 180.0$   
 A ||  $\lambda = 0.45$   
 X || Y = UT



A01668 102

ELITE CANVAS

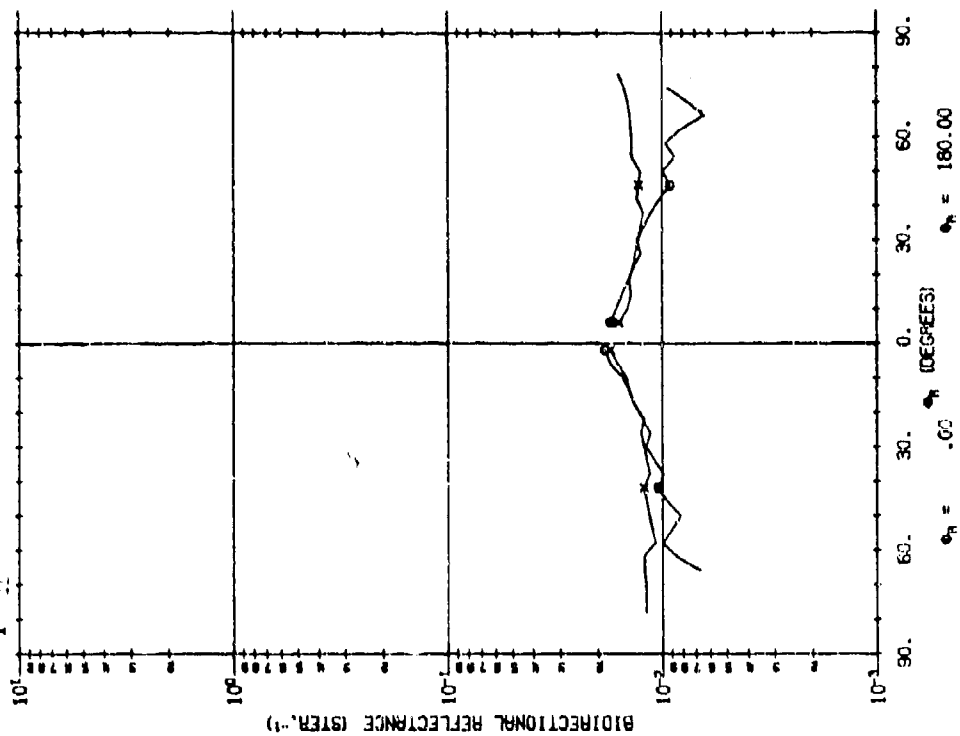
$\theta_1 = 60.0$   
 $\theta_2 = 180.0$   
 $\lambda = 0.66$   
 $\gamma = 0.0$



A01668 101

ELITE CANVAS

$\theta_1 = 60.0$   
 $\theta_2 = 180.0$   
 $\lambda = 0.63$   
 $\gamma = 0.0$

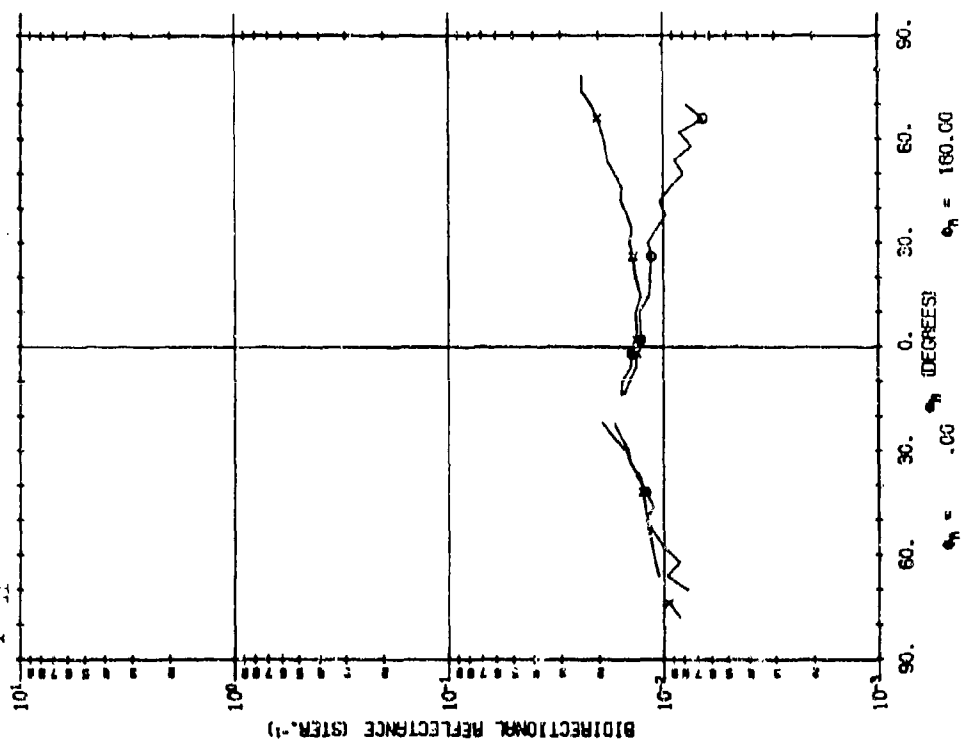


CLOTH AND CANVAS

R01658 101

Blue Canvas

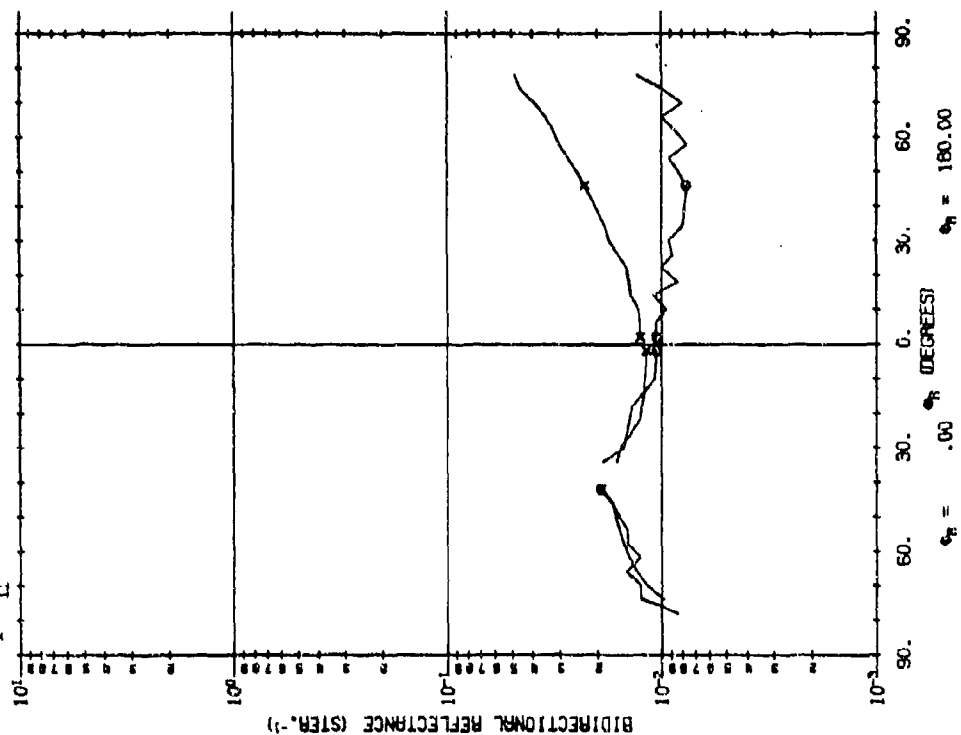
$\theta_1 = 23.0$   
 $\phi_1 = 0.0$   
 $\lambda = 0.63$



R01658 101

Blue Canvas

$\theta_1 = 40.0$   
 $\phi_1 = 0.0$   
 $\lambda = 0.63$

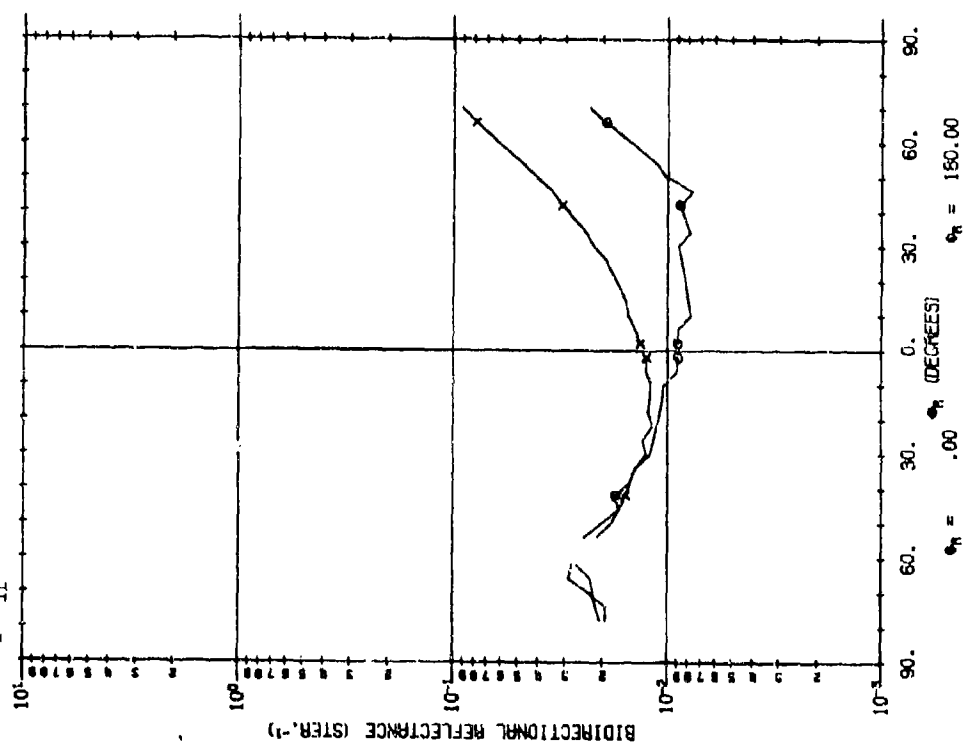




R01668 101  
 C || ||  
 + || ||  
 / || ||  
 x || ||

Blue Curves

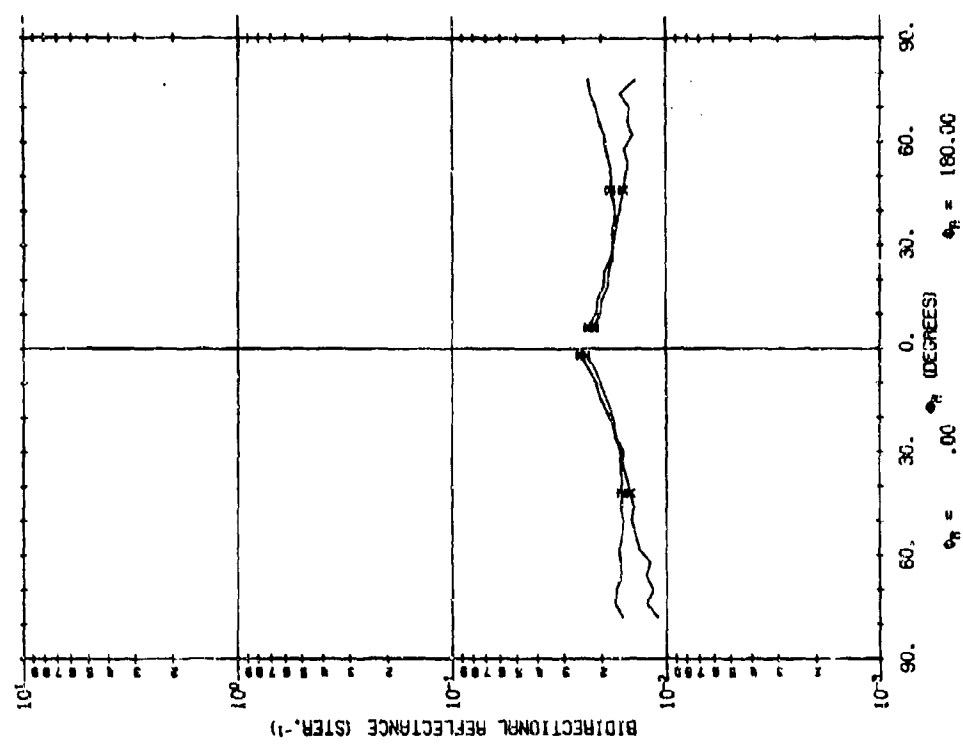
$\theta_i = 60.0$   
 $\phi_i = 0.0$   
 $\lambda = 0.63$



R01668 104  
 x || ||  
 z || ||

Blue Curves

$\theta_i = 0.0$   
 $\phi_i = 0.0$   
 $\lambda = 0.63$

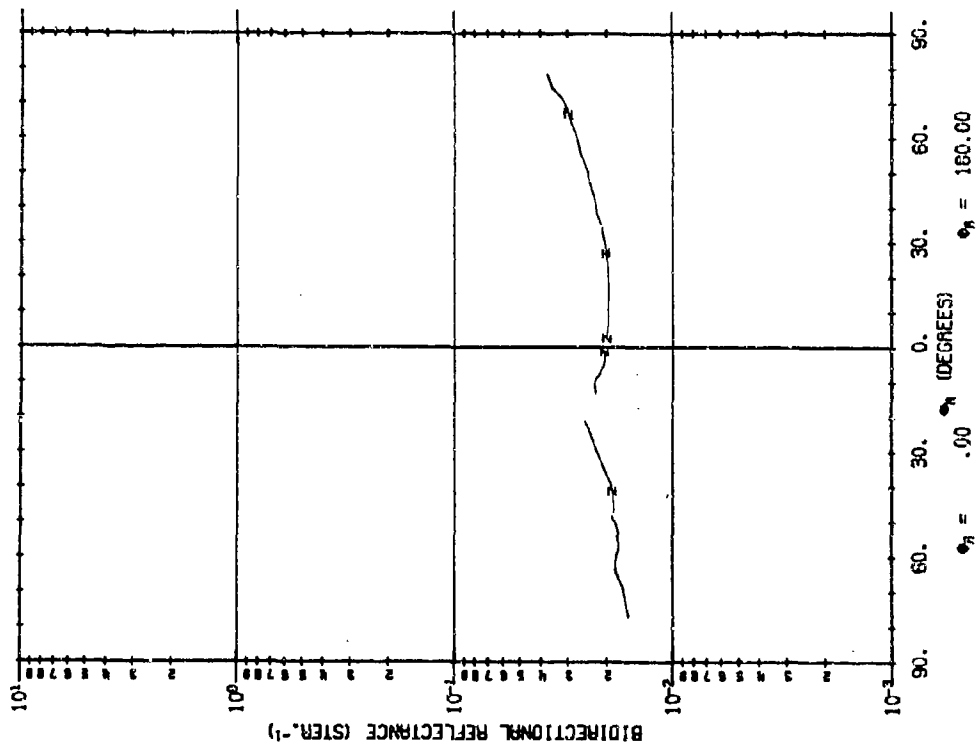


# CLOTH AND CANVAS

R01668 104

Blue Canvas

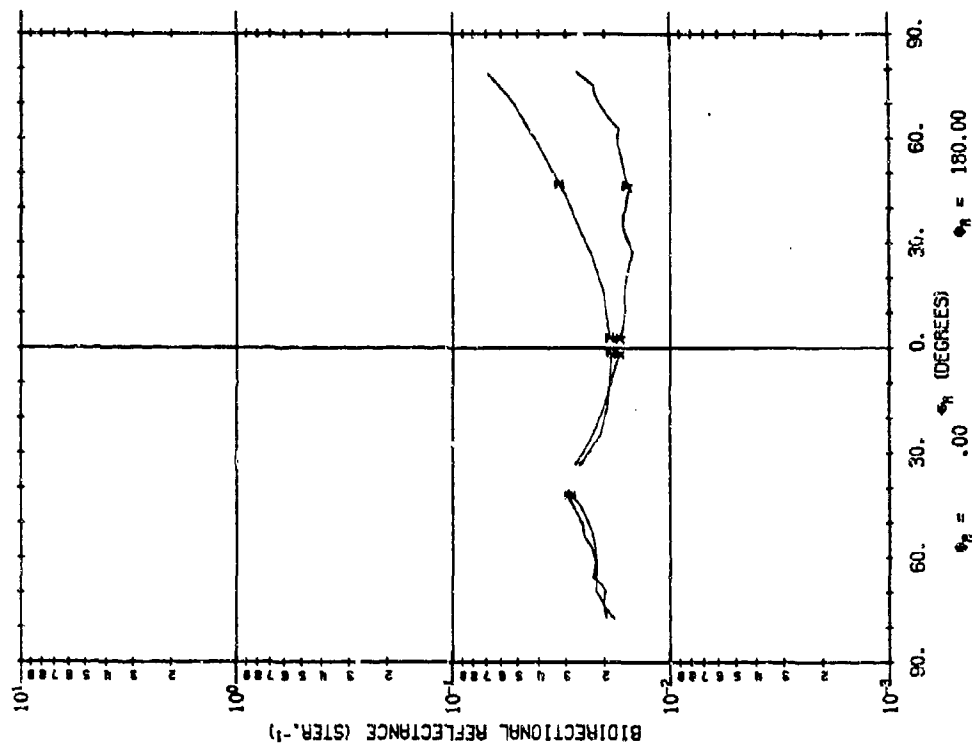
$\theta_1 = 20.0$   
 $\phi_1 = 0.0$   
 $\lambda = 0.63$



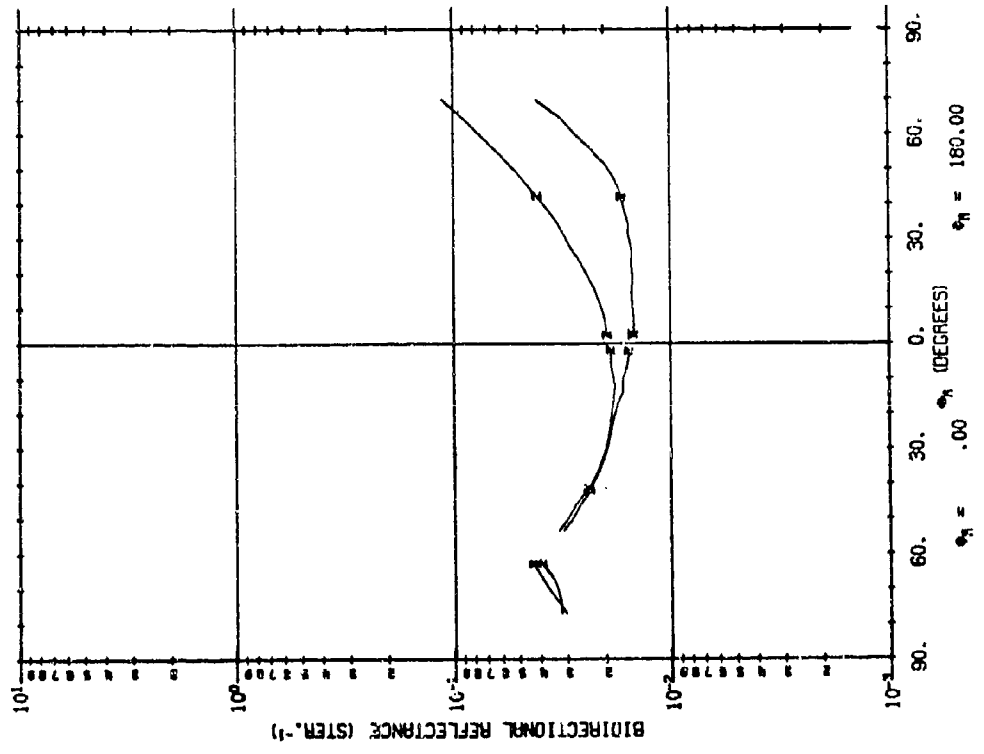
R01668 104

Blue Canvas

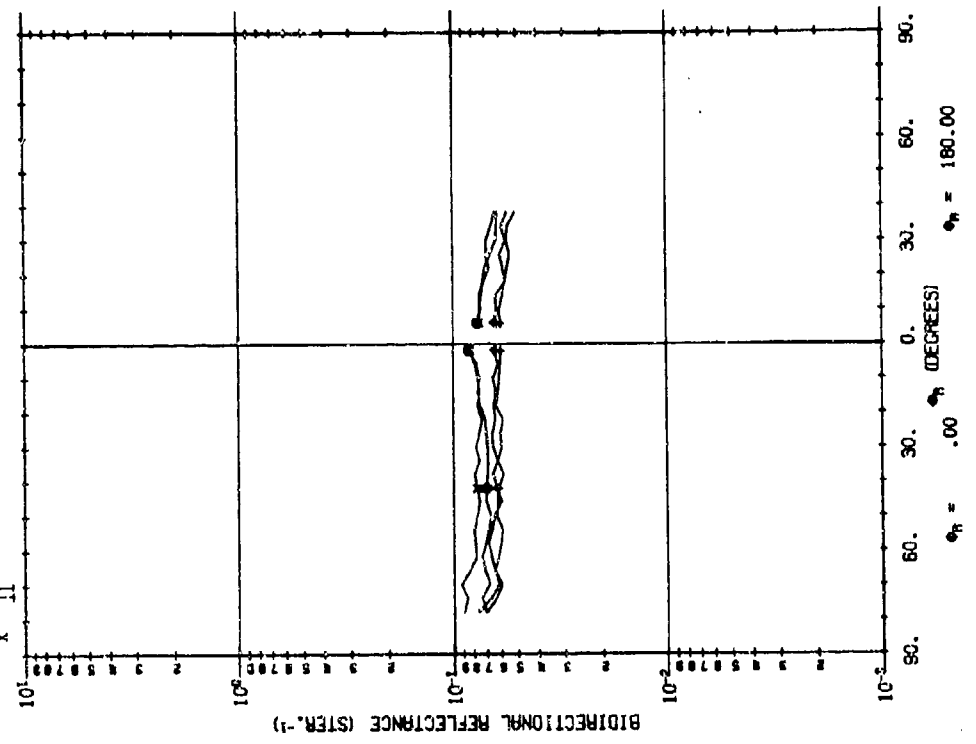
$\theta_1 = 40.0$   
 $\phi_1 = 0.0$   
 $\lambda = 0.63$



R01668 104  
 Blue Canvas  
 $\theta_1 = 60.0$   
 $\phi_1 = 0.0$   
 $\lambda = 0.63$



R01668 103  
 Blue Canvas  
 $\theta_1 = 0.0$   
 $\phi_1 = 180.0$   
 $\lambda = 1.15$

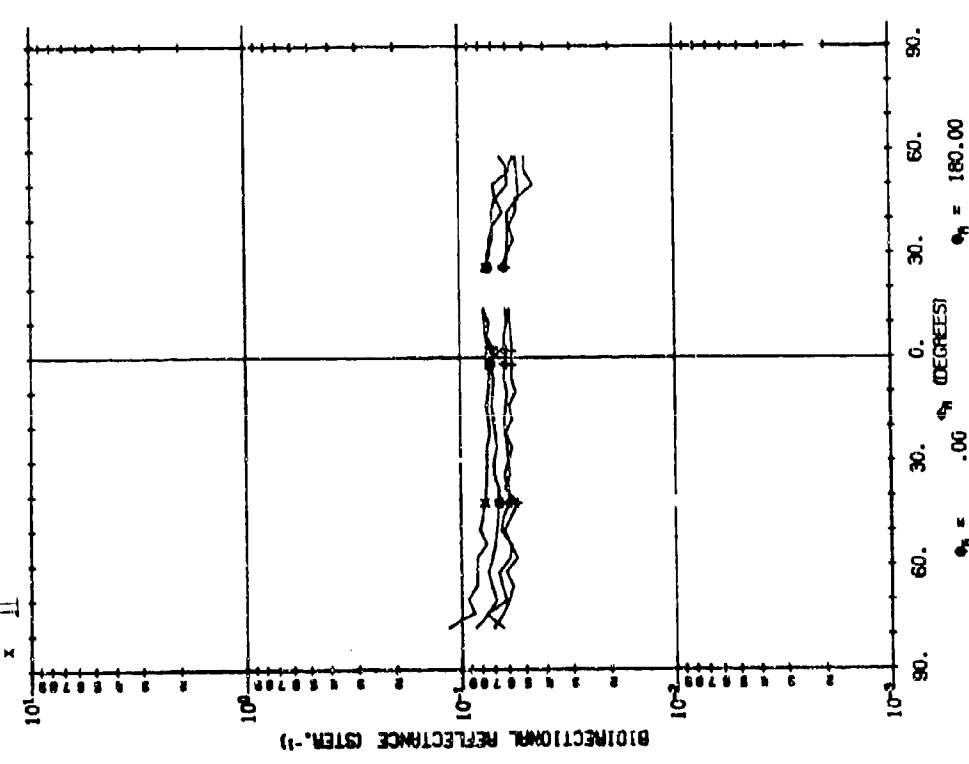


CLOTH AND CANVAS

R01668 103  
 0 11  
 + 11  
 x 11

Blue Canvas

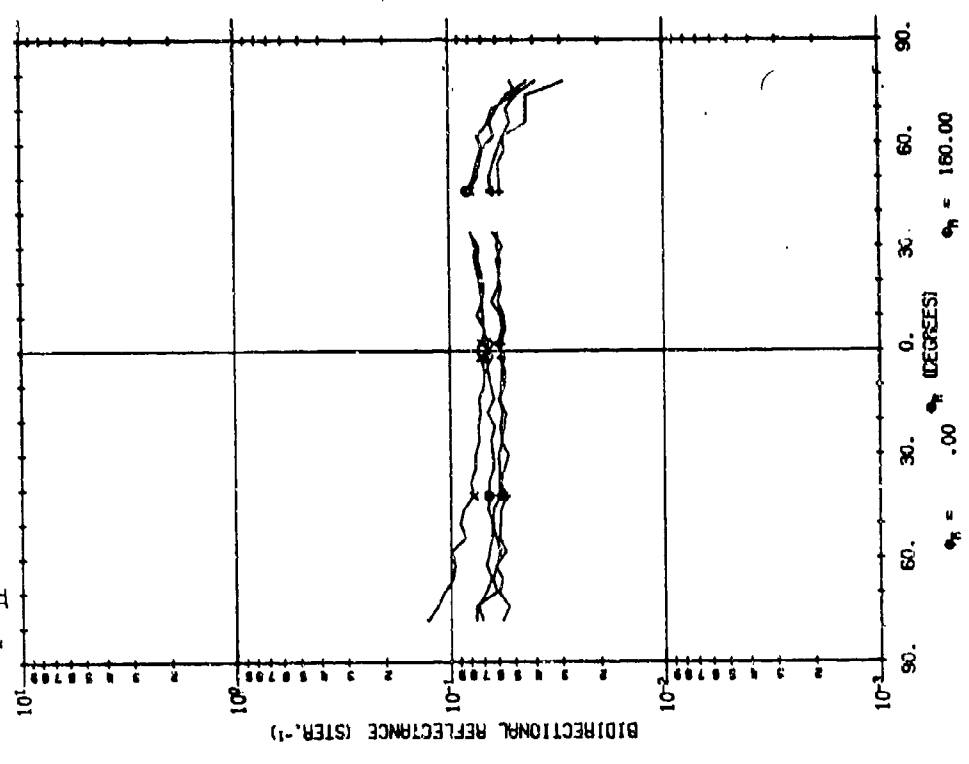
$\theta_1 = 20.0$   
 $\theta_2 = 180.0$   
 $\lambda = 1.15$



R01668 103  
 0 11  
 + 11  
 x 11

Blue Canvas

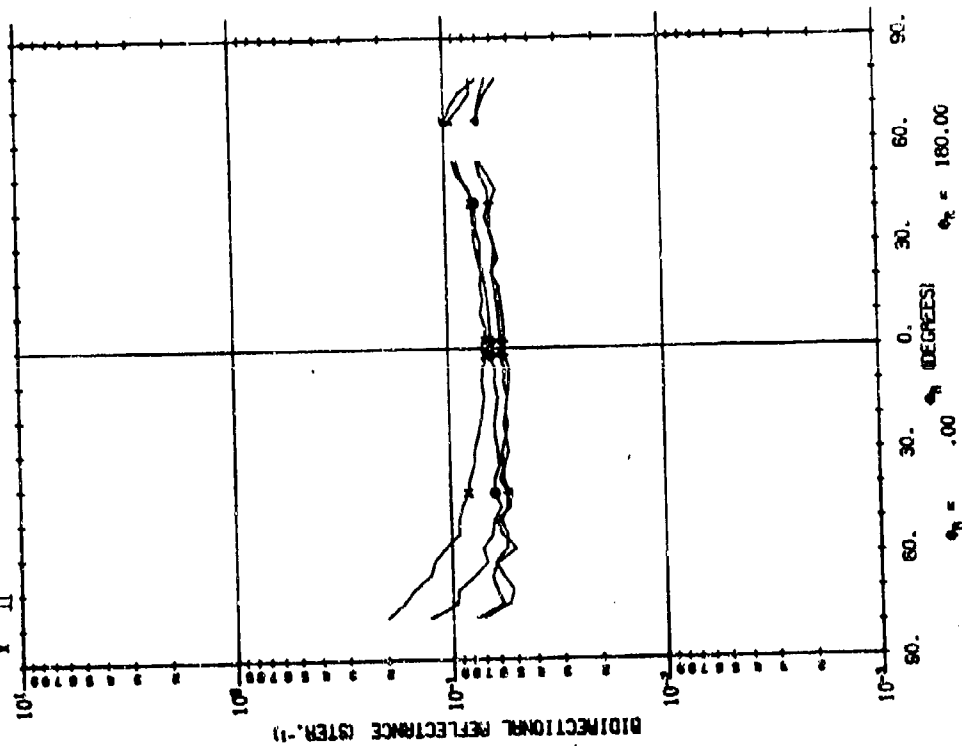
$\theta_1 = 40.0$   
 $\theta_2 = 180.0$   
 $\lambda = 1.15$



R01668 103

Blue Canvas

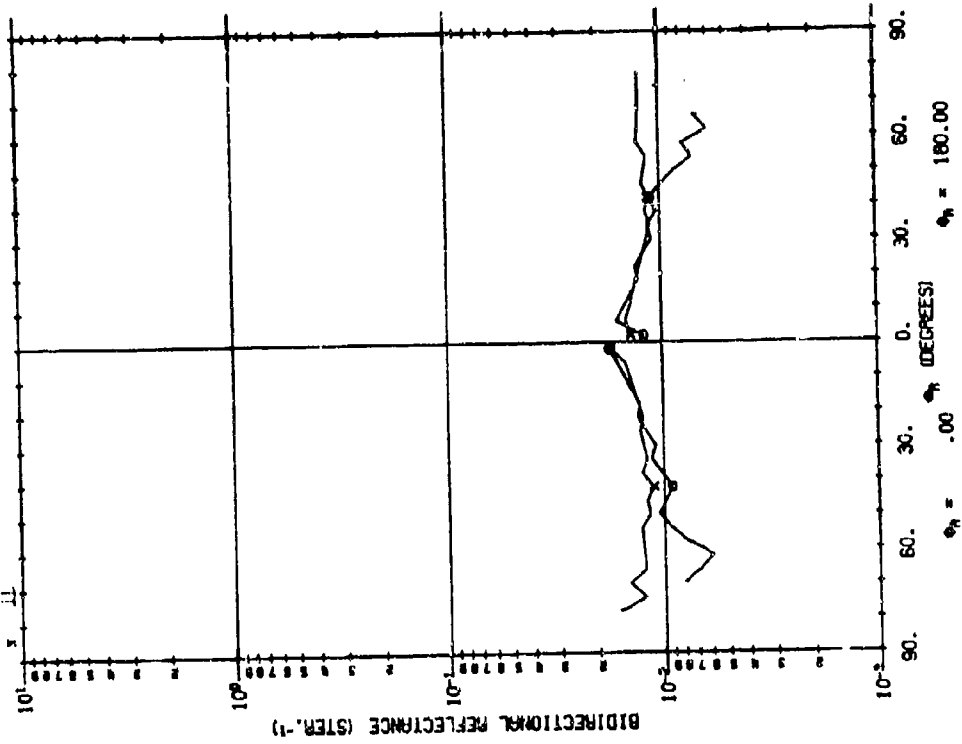
$\phi_1 = 60.0$   
 $\phi_2 = 180.0$   
 $\lambda = 1.15$



R01669 101

Green Canvas

$\phi_1 = 0.0$   
 $\phi_2 = 0.0$   
 $\lambda = 0.83$

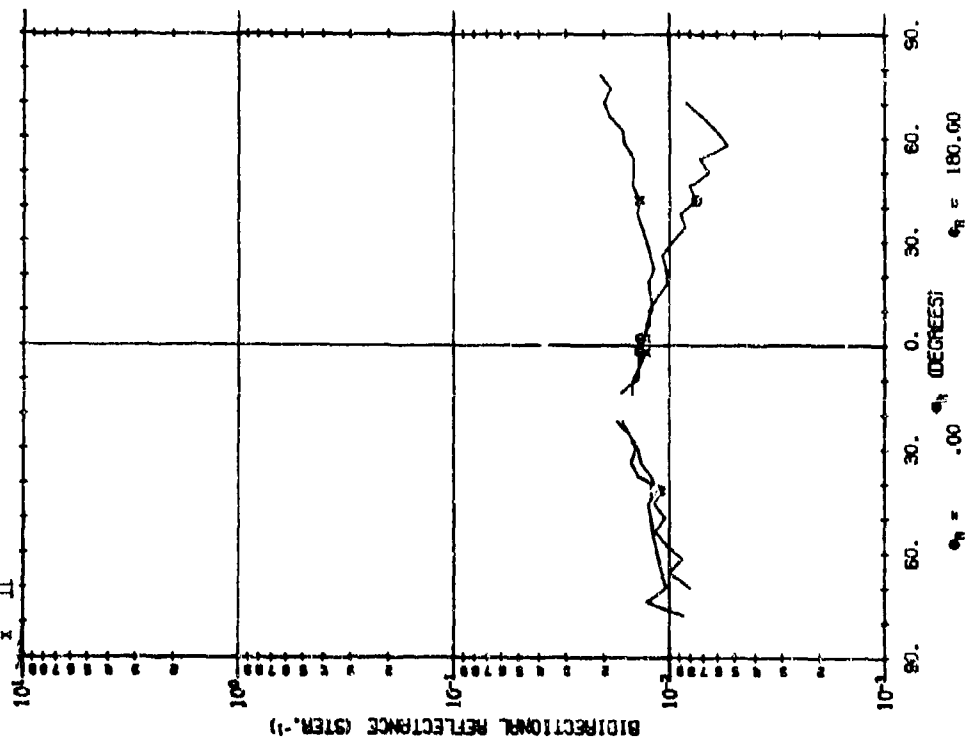


CLOTH AND CANVAS

R01669 101

Green Canvas

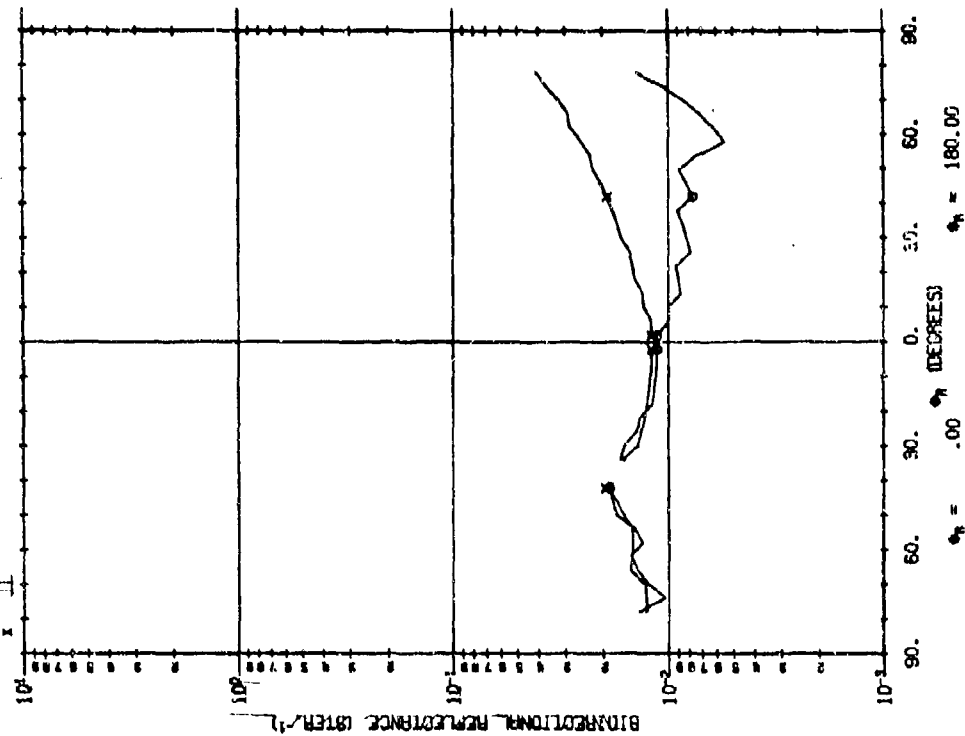
$\phi_1 = 20.0$   
 $\phi_2 = 0.0$   
 $\lambda = 0.63$

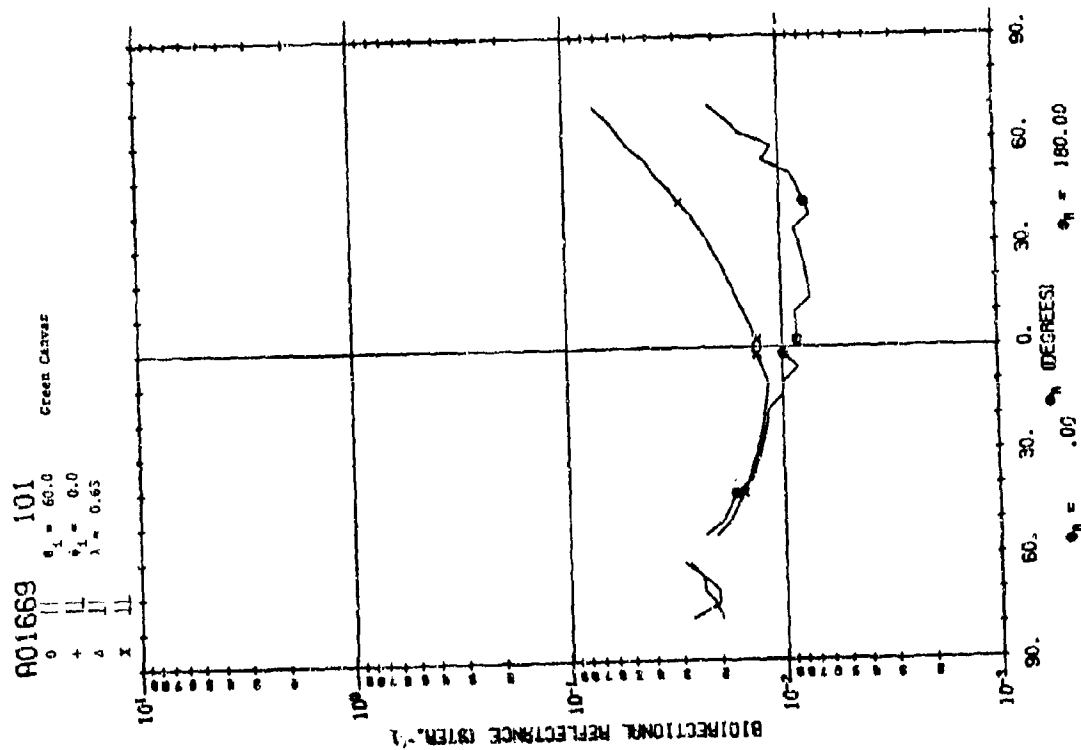
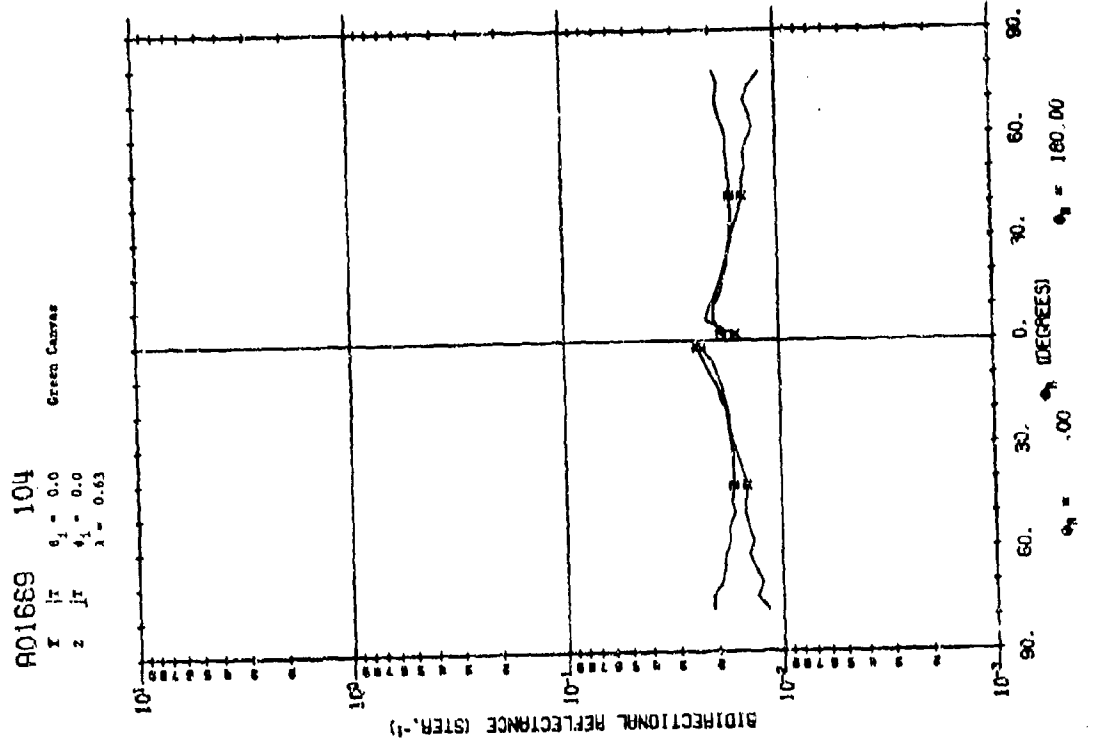


R01669 101

Green Canvas

$\phi_1 = 40.0$   
 $\phi_2 = 0.0$   
 $\lambda = 0.63$





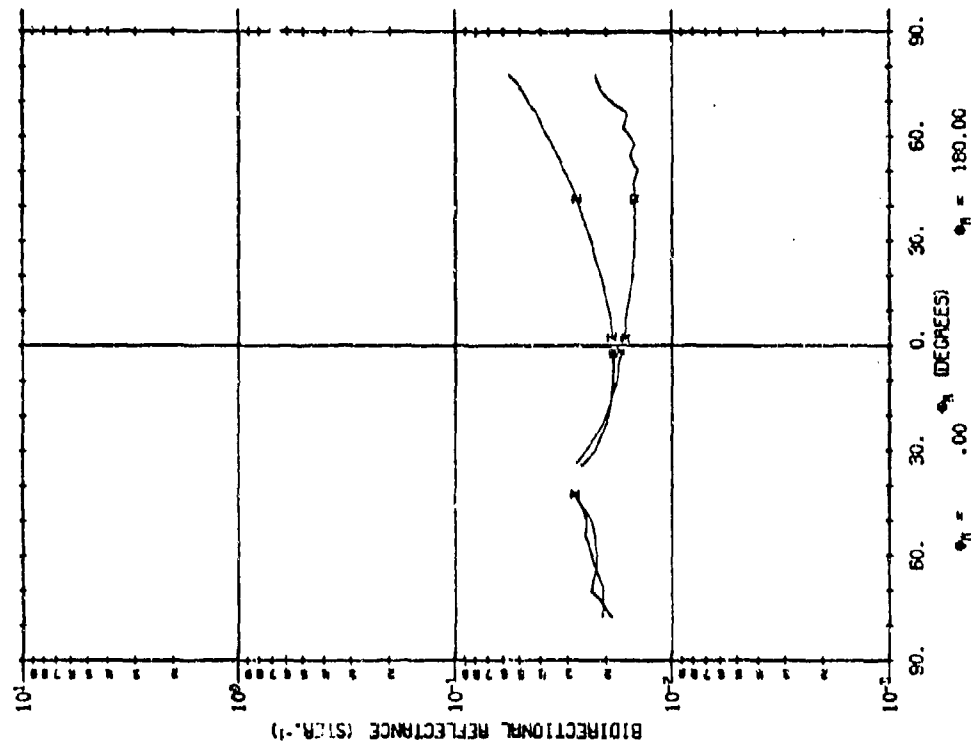
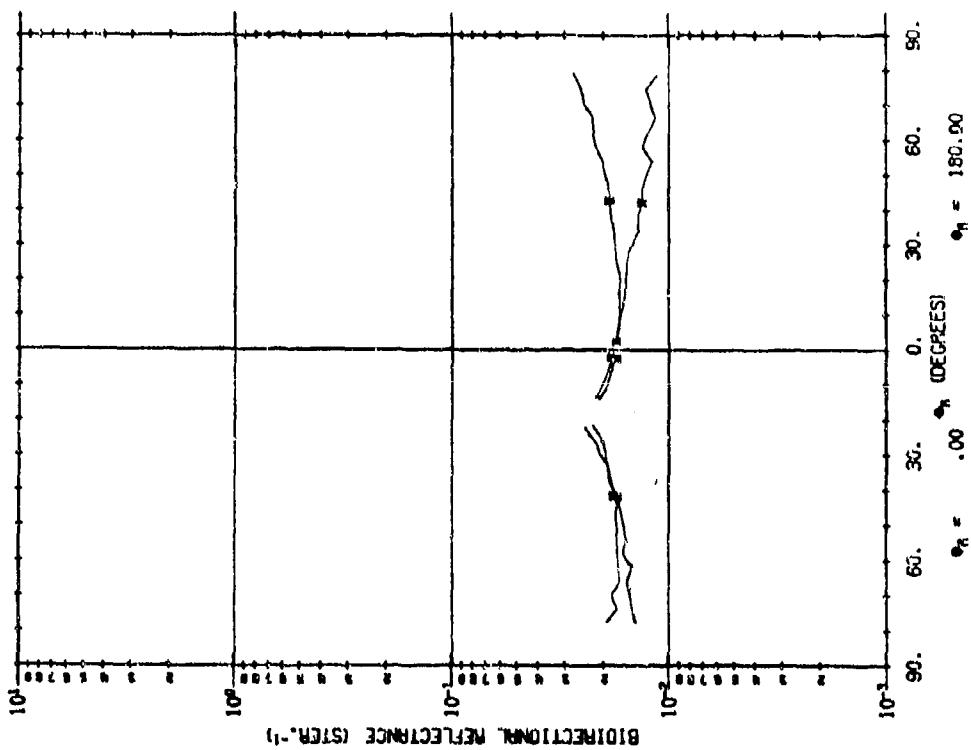
CLOTH AND CANVAS

R01669 104

Green Canvas

$\theta_1 = 20.0$   
 $\phi_1 = 0.0$   
 $\lambda = 0.63$

$\theta_1 = 40.0$   
 $\phi_1 = 0.0$   
 $\lambda = 0.63$

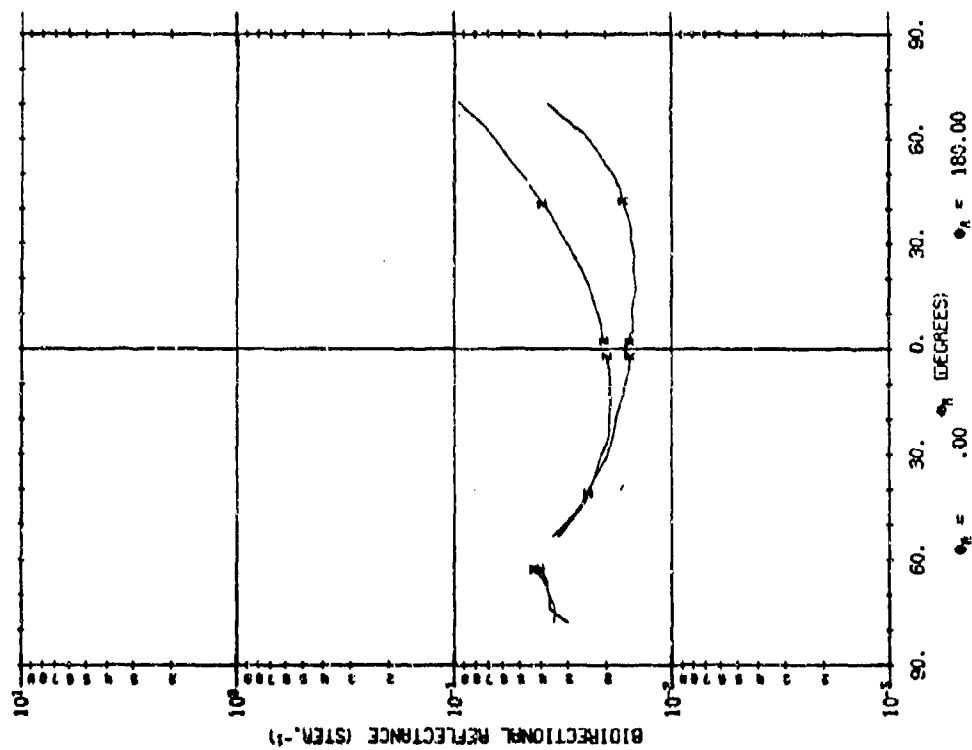




A01659 104

X	15	$\theta_1 = 60.0$
Z	15	$\phi_1 = 0.0$
		$\lambda = 0.63$

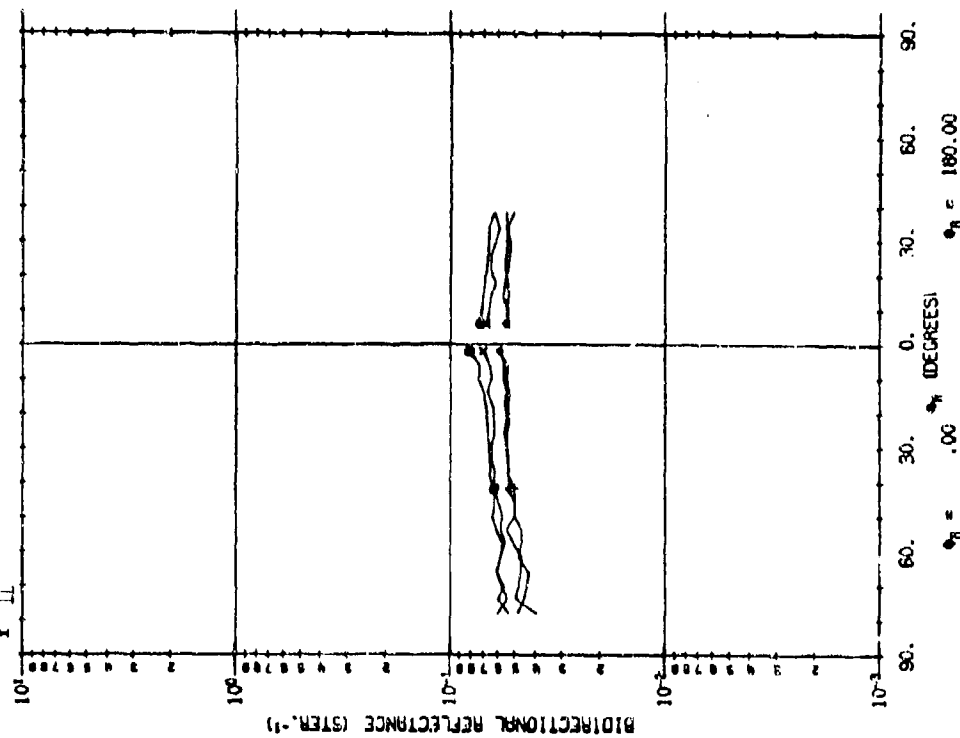
Cloth Canvas



A01669 103

X	15	$\theta_1 = 60.0$
Z	15	$\phi_1 = 180.0$
		$\lambda = 1.15$

Cloth Canvas



CLOTH AND CANVAS

901669 103

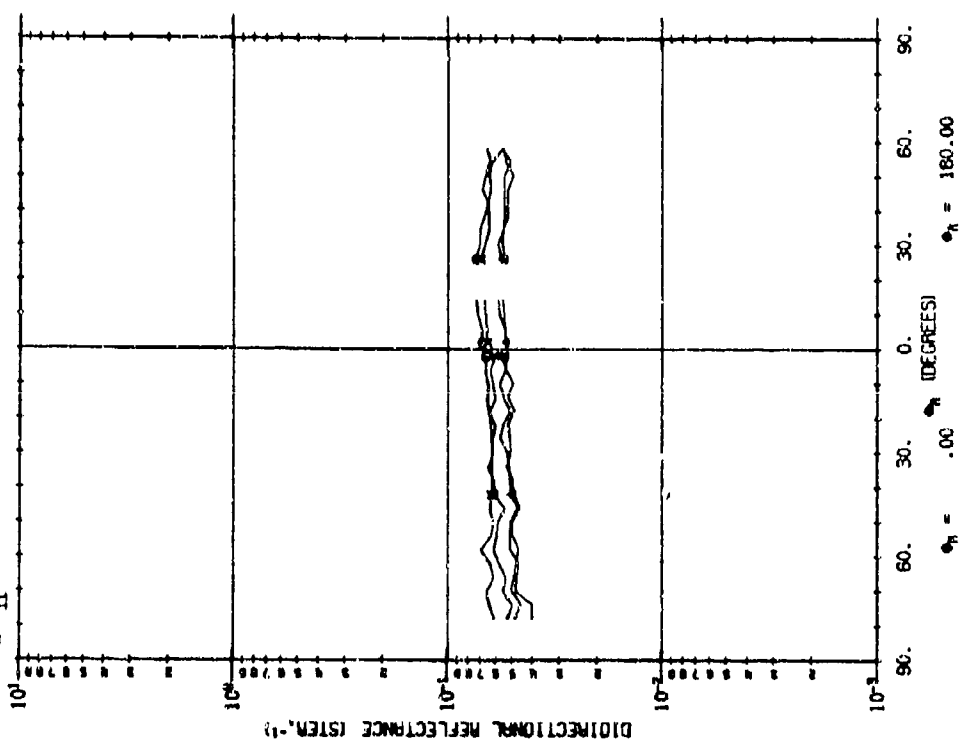
**STANLEY CANTAS**

$\alpha_1 = 20.0$

$$k_1 = 180.0$$

A • 1.15

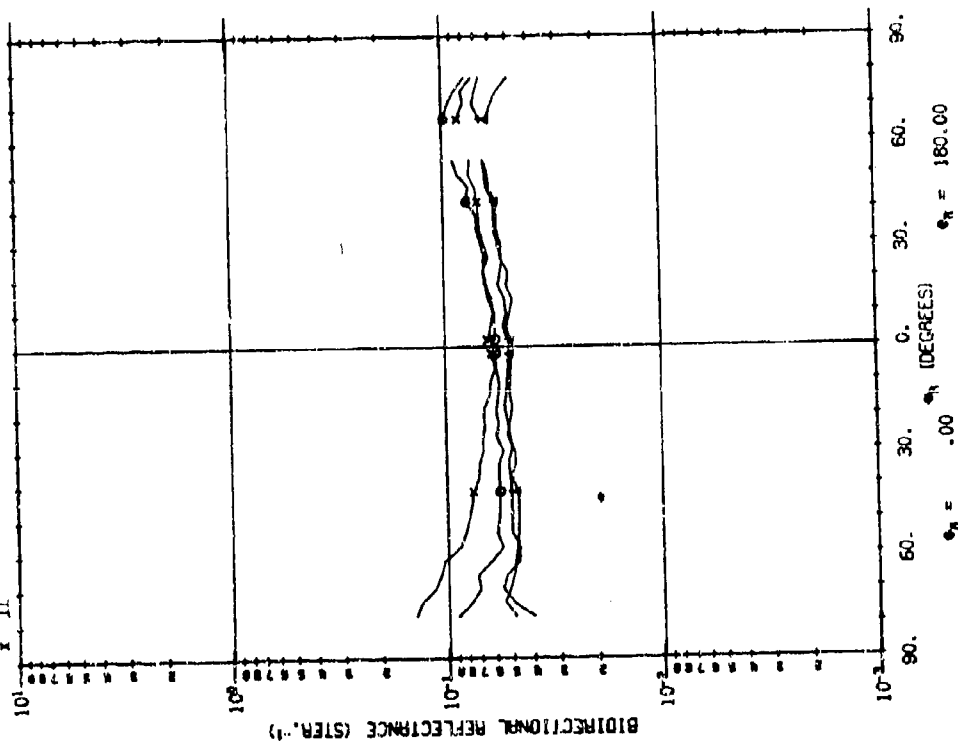
II



R01689 103

GREEN CANVAS

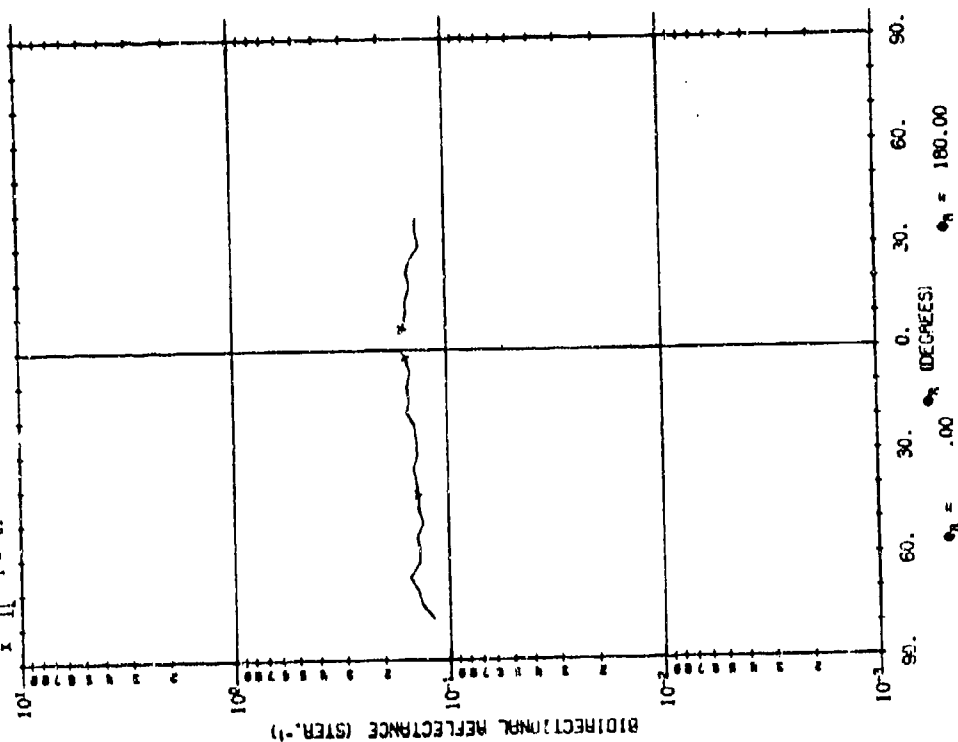
0 ||  $\phi_1 = 60.0$   
 + ||  $\phi_1 = 180.0$   
 Δ ||  $\lambda = 1.15$   
 x ||



R01670 102

GRAY TREATED CANVAS, 64  
 PERCENT REFLECTANCE

0 ||  $\phi_1 = 0.0$   
 + ||  $\phi_1 = 180.0$   
 Δ ||  $\lambda = 0.46$   
 x ||

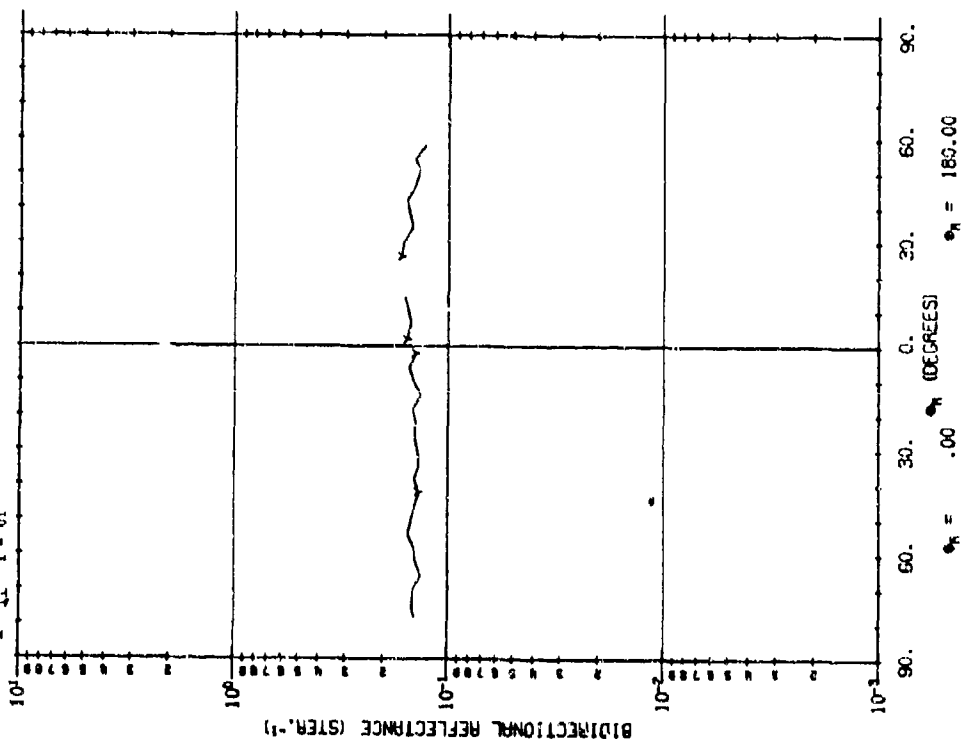


CLOTH AND CANVAS

R01670 102

GRAY TREATED CANVAS, 64  
PERCENT REFLECTANCE

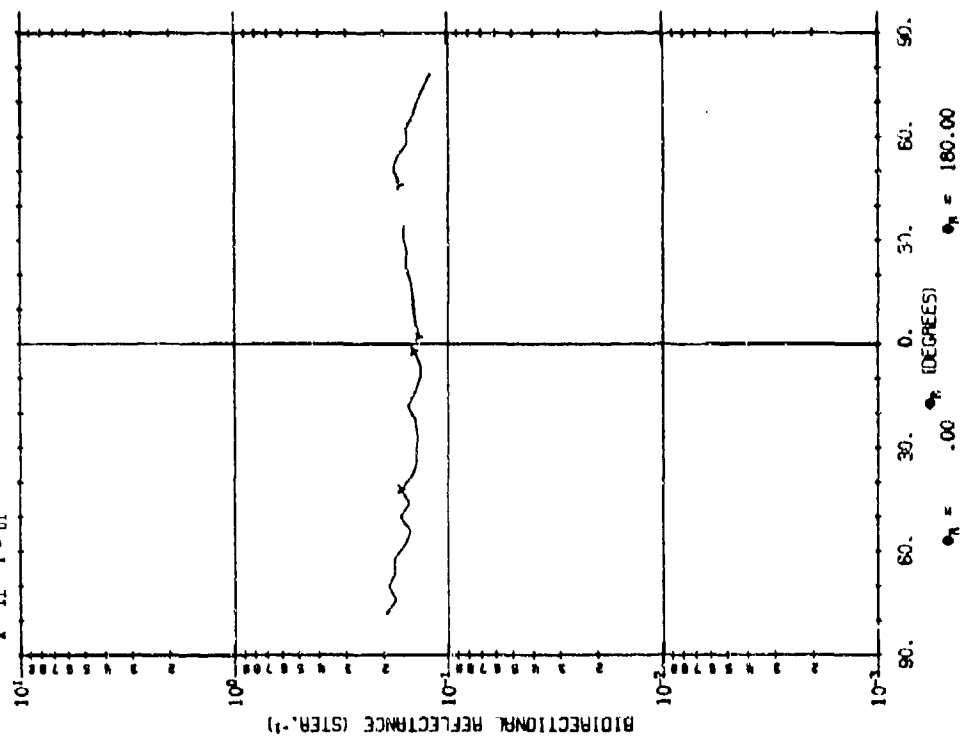
0 ||  $\theta_1 = 20.0$   
+ ||  $\phi_1 = 180.0$   
A ||  $\lambda = 0.45$   
X || Y = UT



R01670 102

GRAY TREATED CANVAS, 64  
PERCENT REFLECTANCE

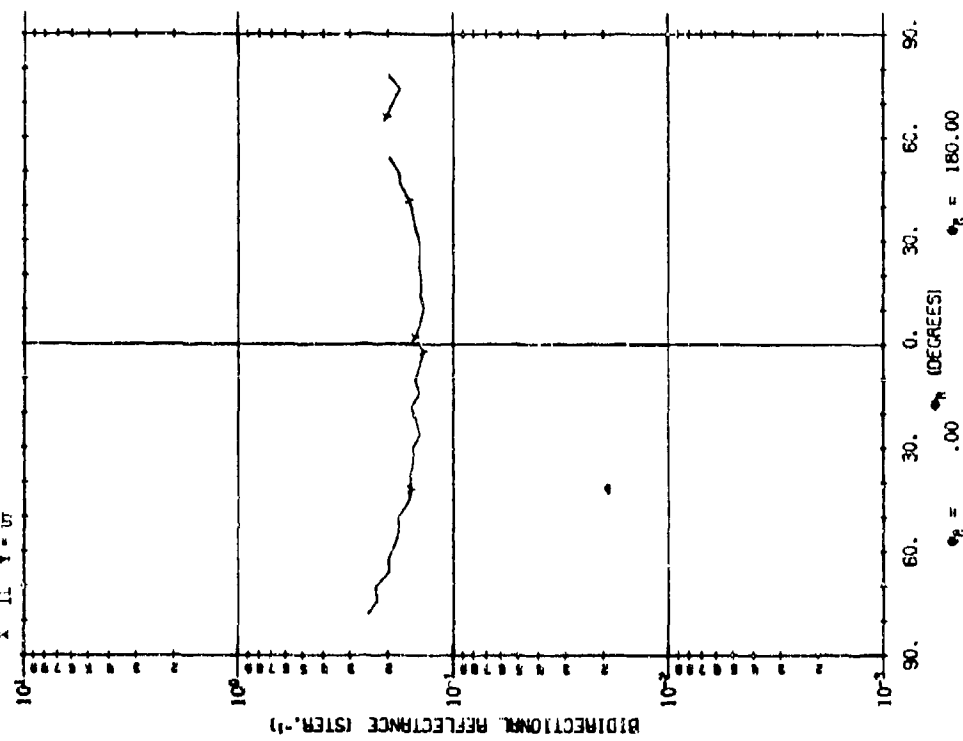
0 ||  $\theta_1 = 40.0$   
+ ||  $\phi_1 = 180.0$   
A ||  $\lambda = 0.45$   
X || Y = UT



R01670 102

GRAY TREATED CANVAS, 64  
PERCENT REFLECTANCE

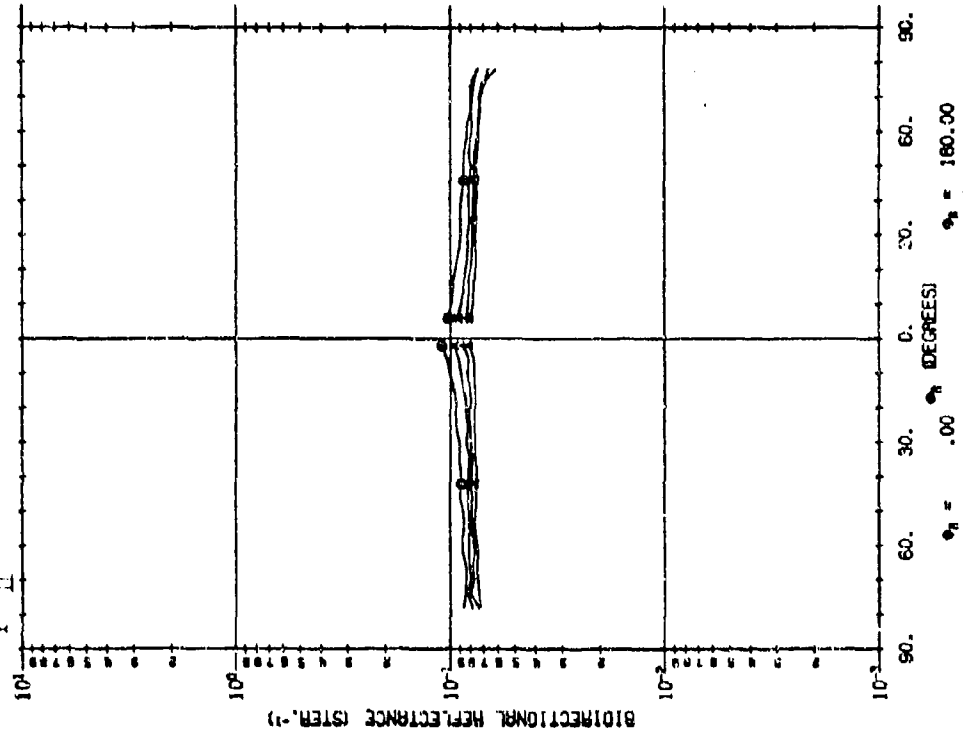
$\theta_i = 60.0$   
 $\phi_i = 180.0$   
 $\lambda = 0.46$   
 $\gamma = .07$



R01670 101

GRAY TREATED CANVAS, 64 PERCENT REFLECTANCE

$\theta_i = 0.0$   
 $\phi_i = 0.0$   
 $\lambda = 0.63$   
 $\gamma = .07$

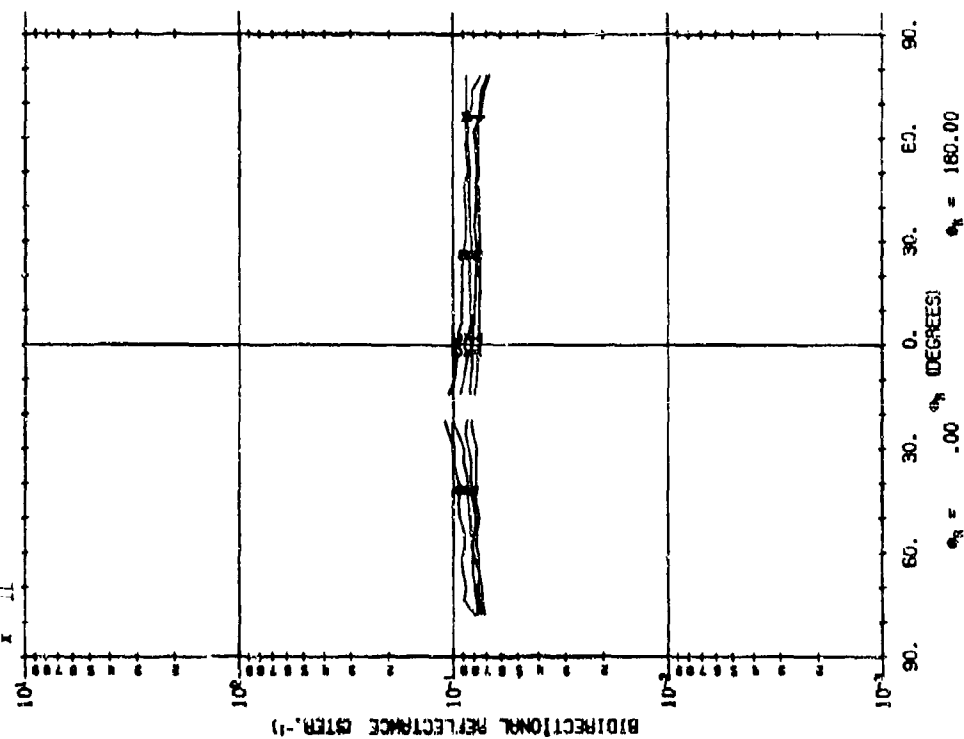


CLOTH AND CANVAS

R01670 101

Gray Treated Canvas, 64 Percent Reflectance

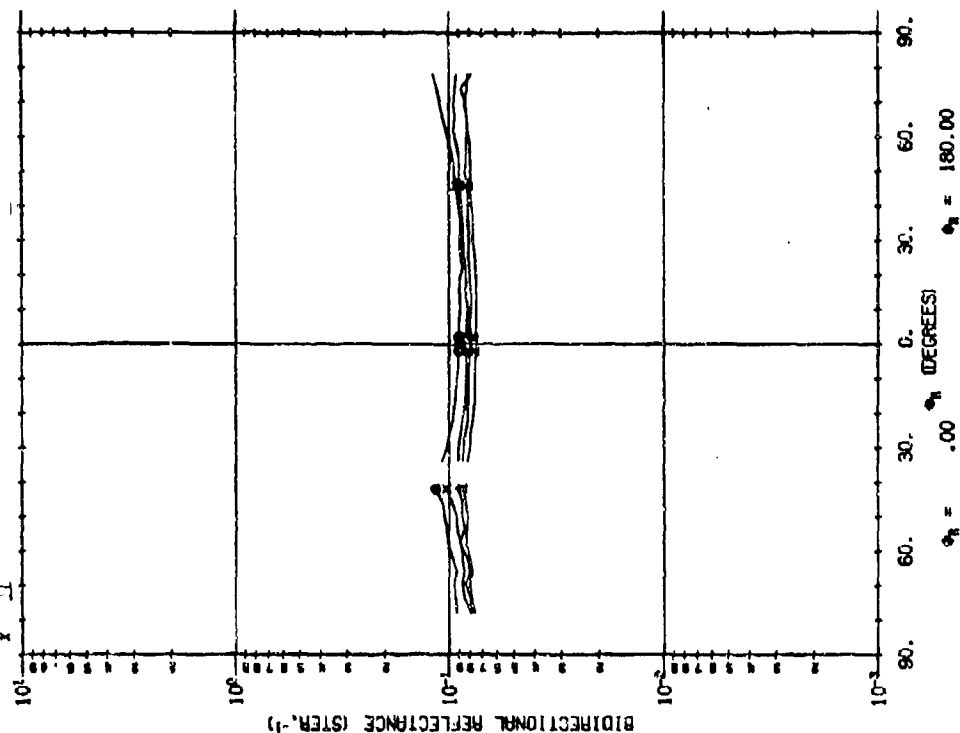
$\phi_1 = 20.0$   
 $\phi_2 = 0.6$   
 $\lambda = 0.63$



R01670 101

Gray Treated Canvas, 64 Percent Reflectance

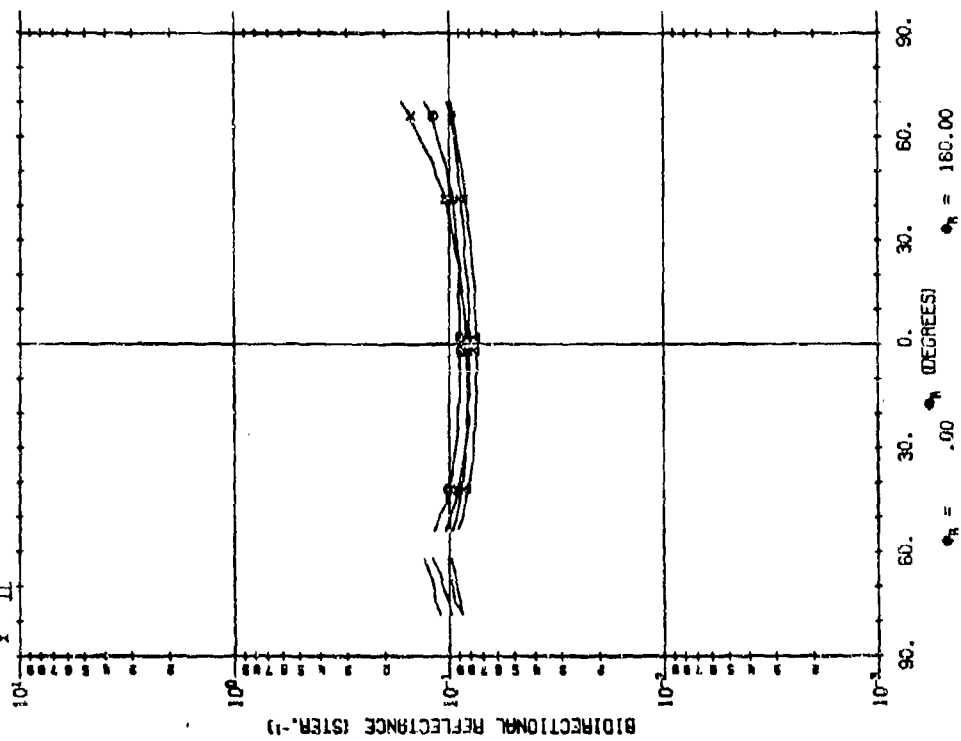
$\phi_1 = 40.0$   
 $\phi_2 = 0.6$   
 $\lambda = 0.63$



R01670 101

Gray treated Canvas, 64 Percent Reflectance

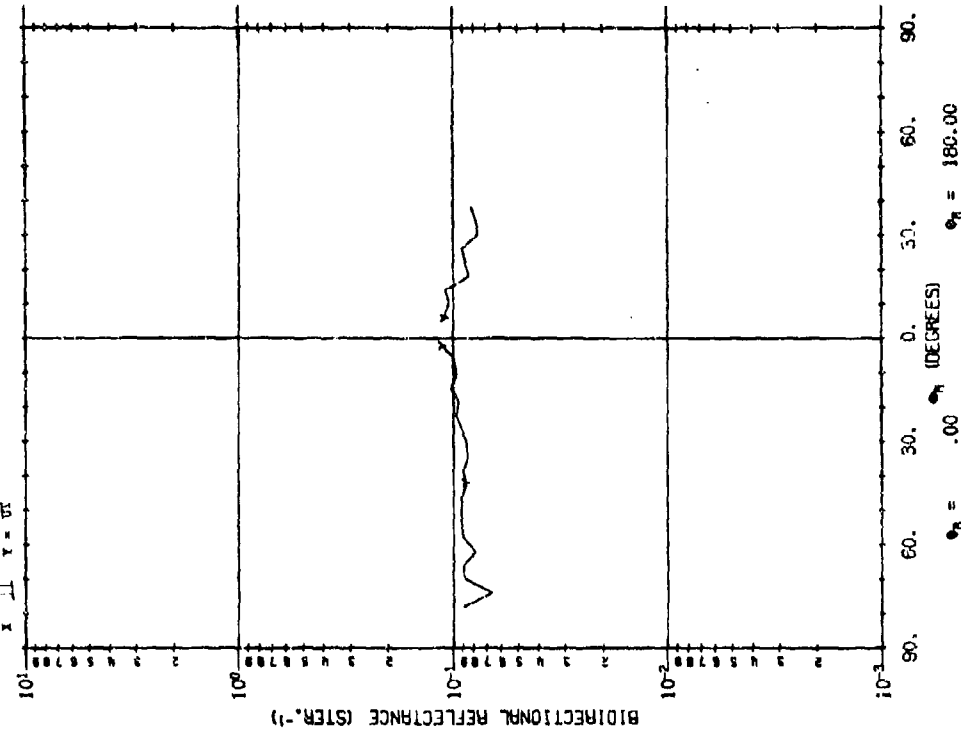
0 //  $\phi_1 = 60.0$   
 + //  $\phi_2 = 0.0$   
 Δ //  $\lambda = 0.63$



R01671 102

GRAY TREATED CANVAS, 32 PERCENT REFLECTANCE

0 //  $\phi_1 = 0.0$   
 + //  $\phi_2 = 130.0$   
 Δ //  $\lambda = 0.46$

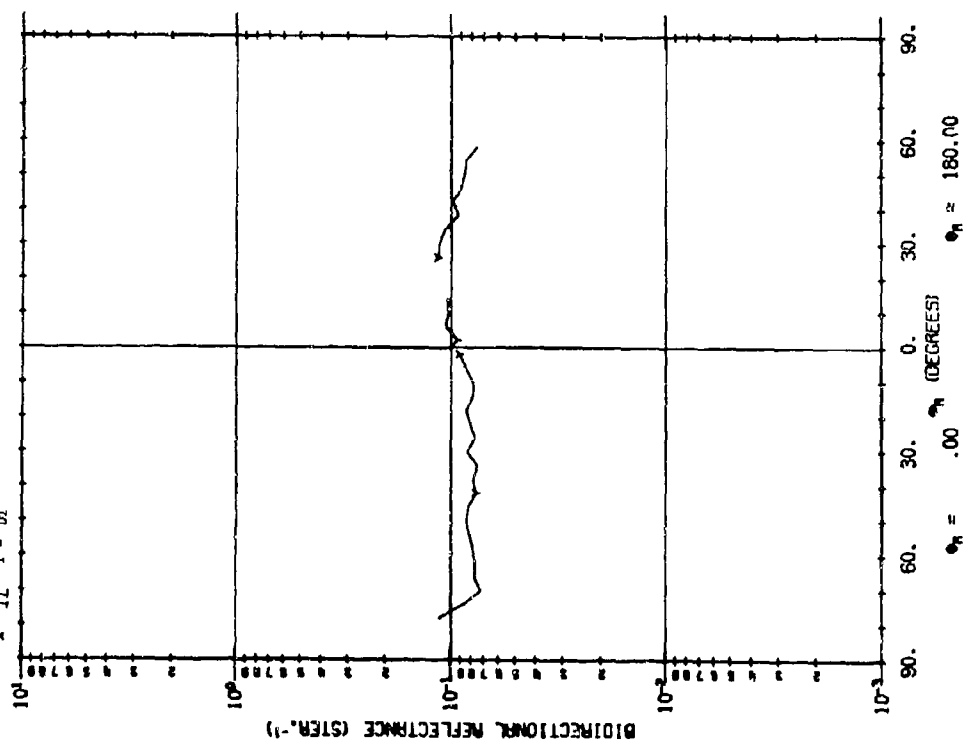


## CLOTH AND CANVAS

R01671 102

GRAY TREATED CANVAS, 32  
PERCENT REFLECTANCE

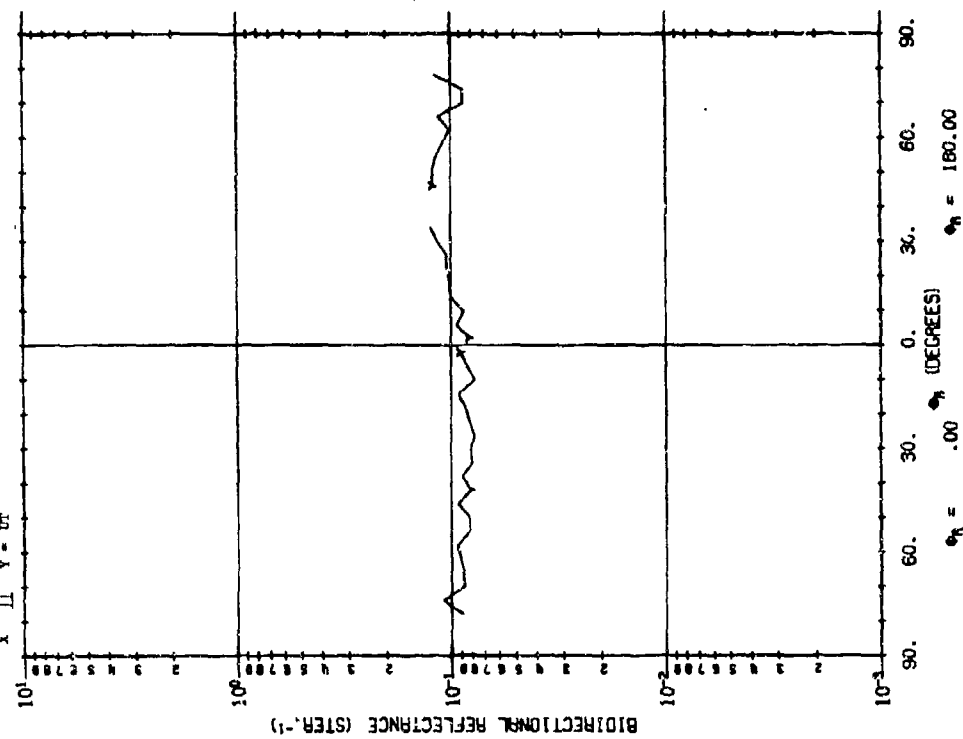
0 //  $\theta_1 = 20.0$   
+ //  $\theta_2 = 180.0$   
 $\Delta$  //  $\lambda = 0.46$   
x //  $\gamma = 0$



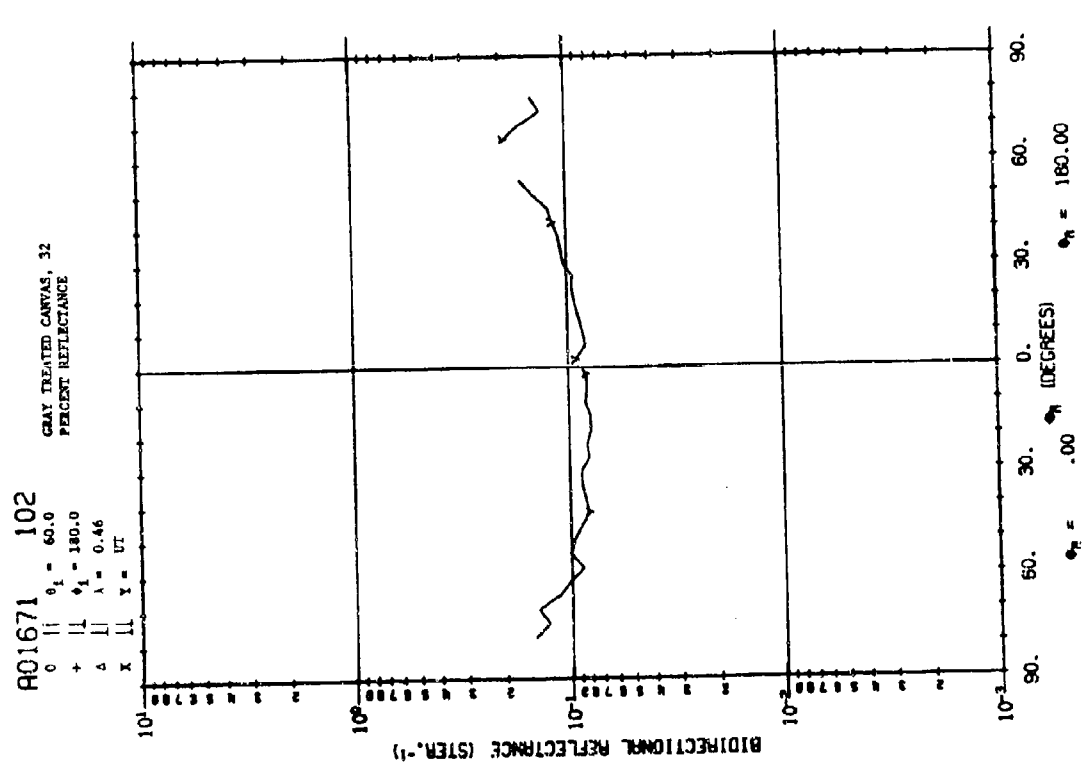
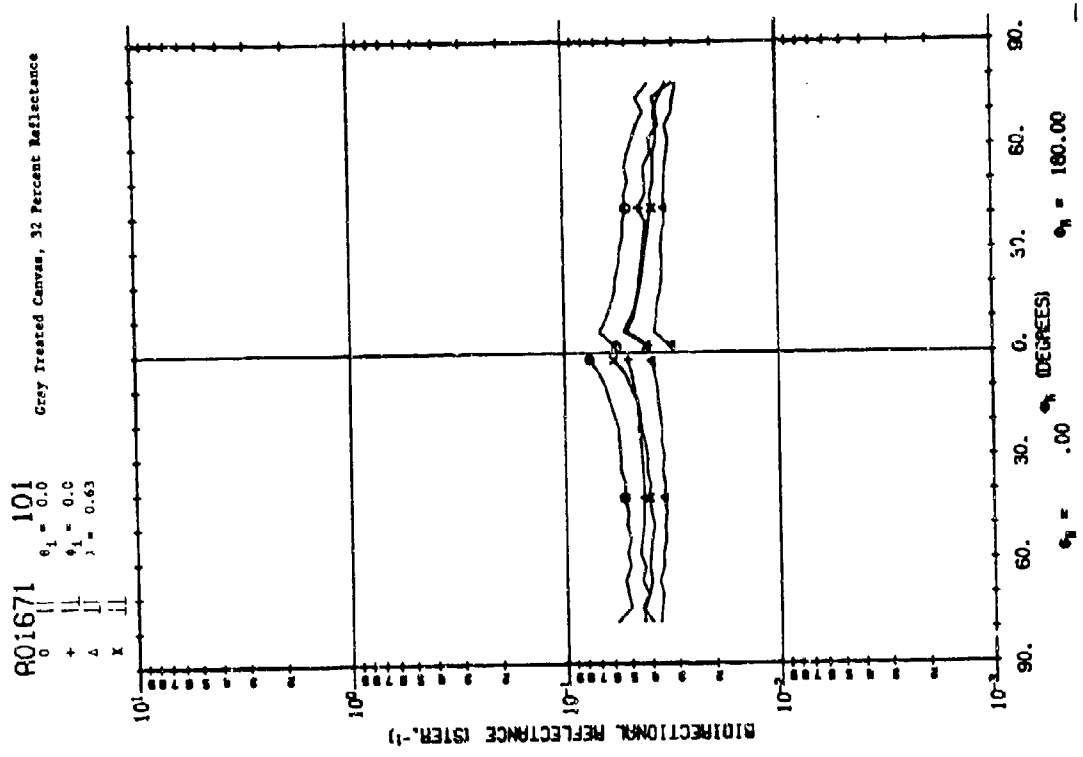
R01671 102

GRAY TREATED CANVAS, 32  
PERCENT REFLECTANCE

0 //  $\theta_1 = 40.0$   
+ //  $\theta_2 = 180.0$   
 $\Delta$  //  $\lambda = 0.46$   
x //  $\gamma = 0$



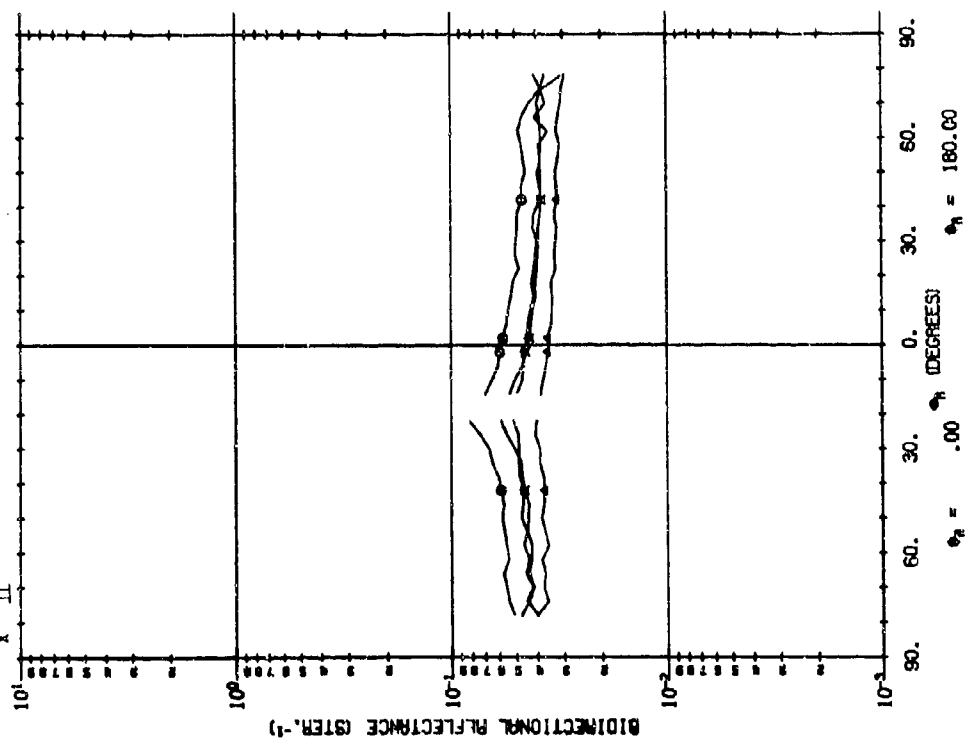




# CLOTH AND CANVAS

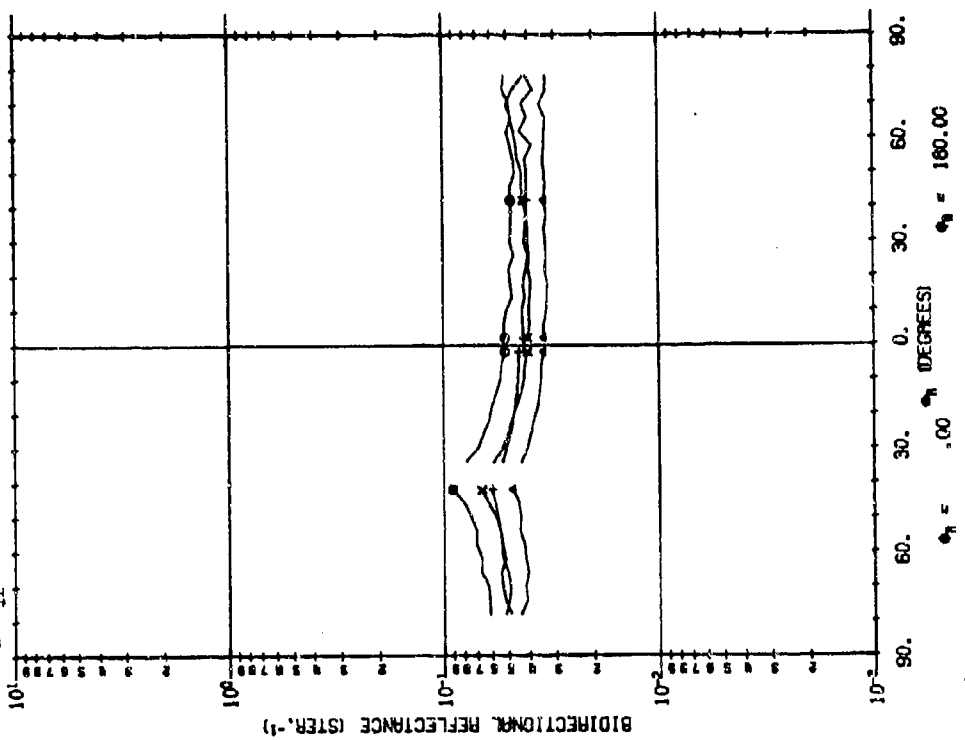
A01671 101  
 0 ||  $\theta_1 = 20.0$   
 + ||  $\phi_1 = 0.0$   
 Δ ||  $\lambda = 0.63$   
 x ||

Gray Treated Canvas, 32 Percent Reflectance



A01671 101  
 0 ||  $\theta_1 = 40.0$   
 + ||  $\phi_1 = 0.0$   
 Δ ||  $\lambda = 0.63$   
 x ||

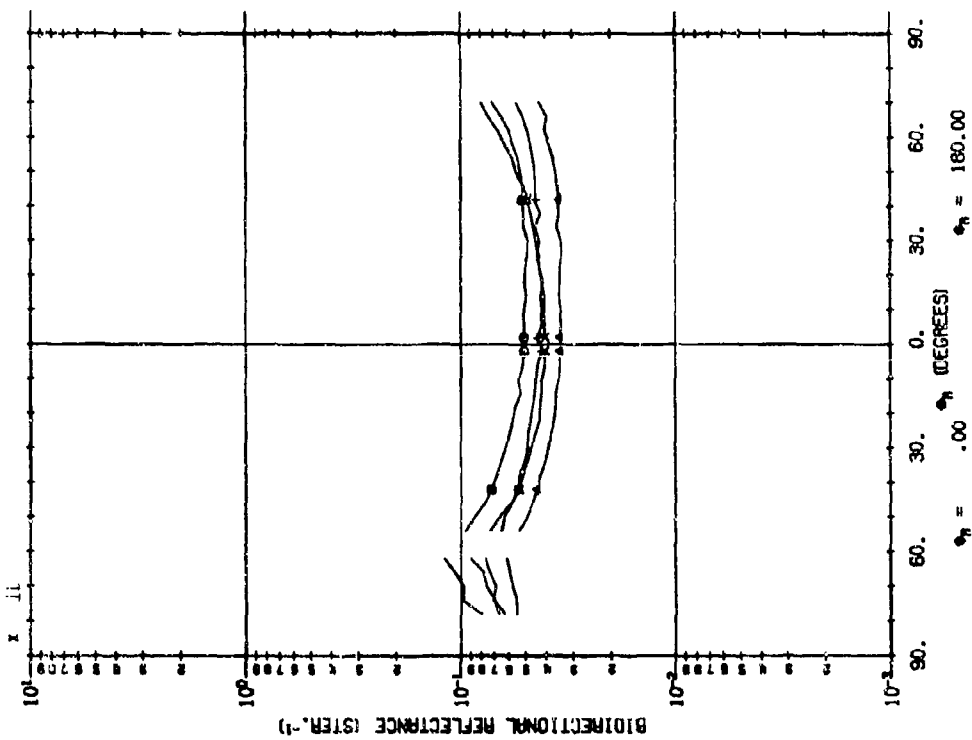
Gray Treated Canvas, 32 Percent Reflectance



R01671 101

Gray Treated Canvas, 32 Percent Reflectance

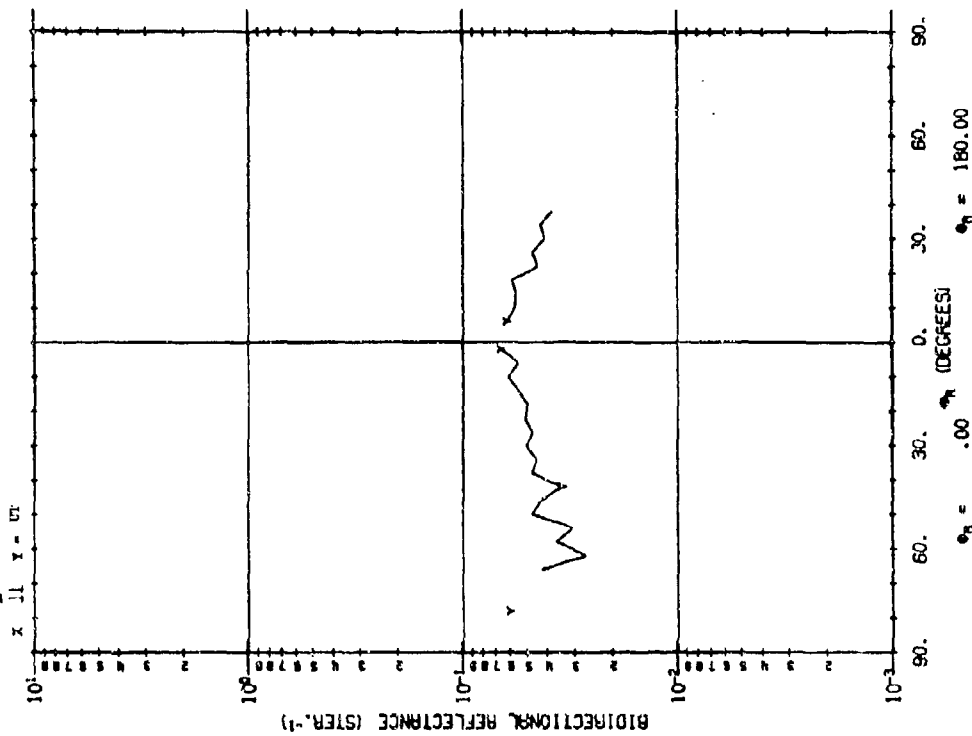
$\theta_i = 60.0$   
 $\phi_i = 0.0$   
 $\lambda = 0.63$



R01672 102

GRAY TREATED CANVAS, 16 PERCENT REFLECTANCE

$\theta_i = 0.0$   
 $\phi_i = 180.0$   
 $\lambda = 0.46$

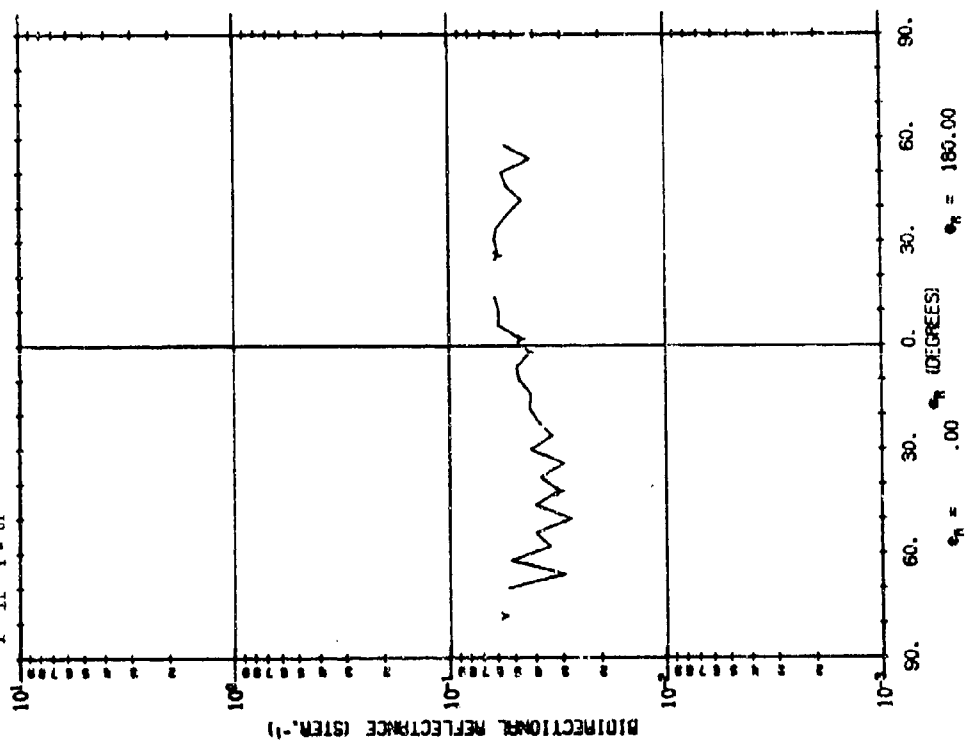


CLOTH AND CANVAS

R01672 102

GRAY TREATED CANVAS, 16  
PERCENT REFLECTANCE

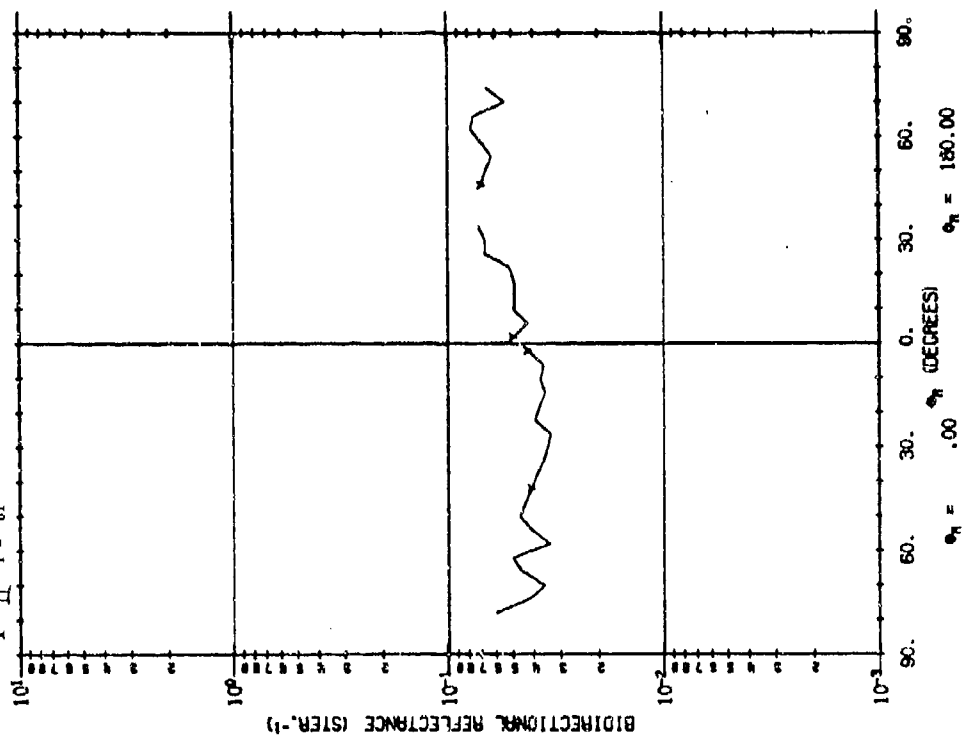
0 ||  $\theta_i = 20.0$   
+ ||  $\phi_i = 180.0$   
 $\Delta$  ||  $\lambda = 0.45$   
X || Y = UT



R01672 102

GRAY TREATED CANVAS, 16  
PERCENT REFLECTANCE

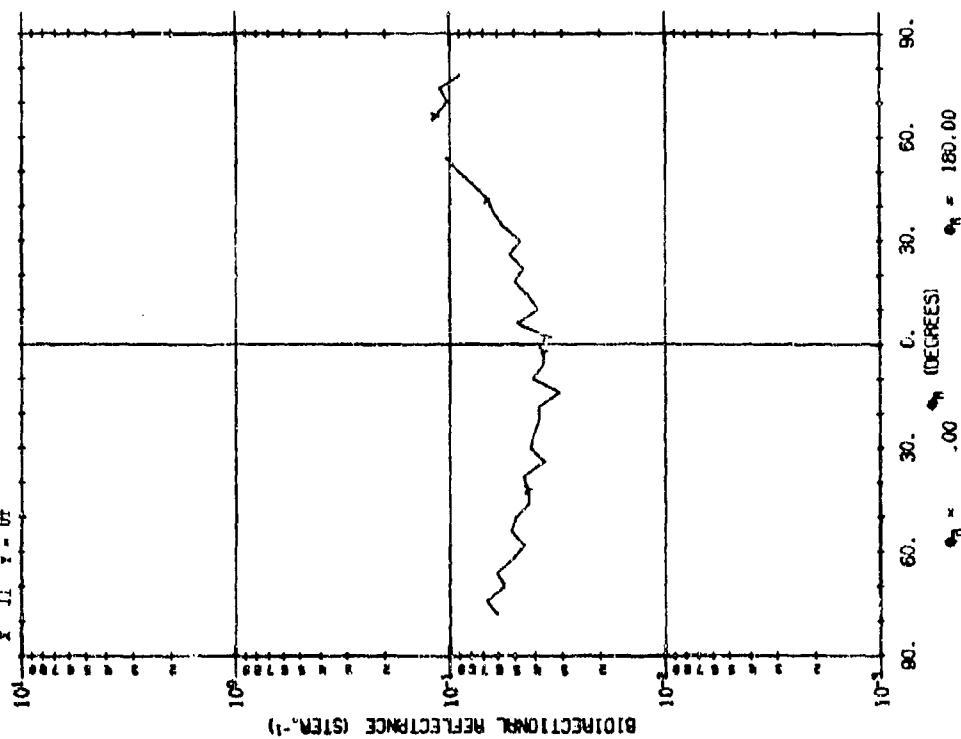
0 ||  $\theta_i = 40.0$   
+ ||  $\phi_i = 180.0$   
 $\Delta$  ||  $\lambda = 0.45$   
X || Y = UT



A01672 102

GRAY TREATED CANVAS, 16  
PERCENT REFLECTANCE

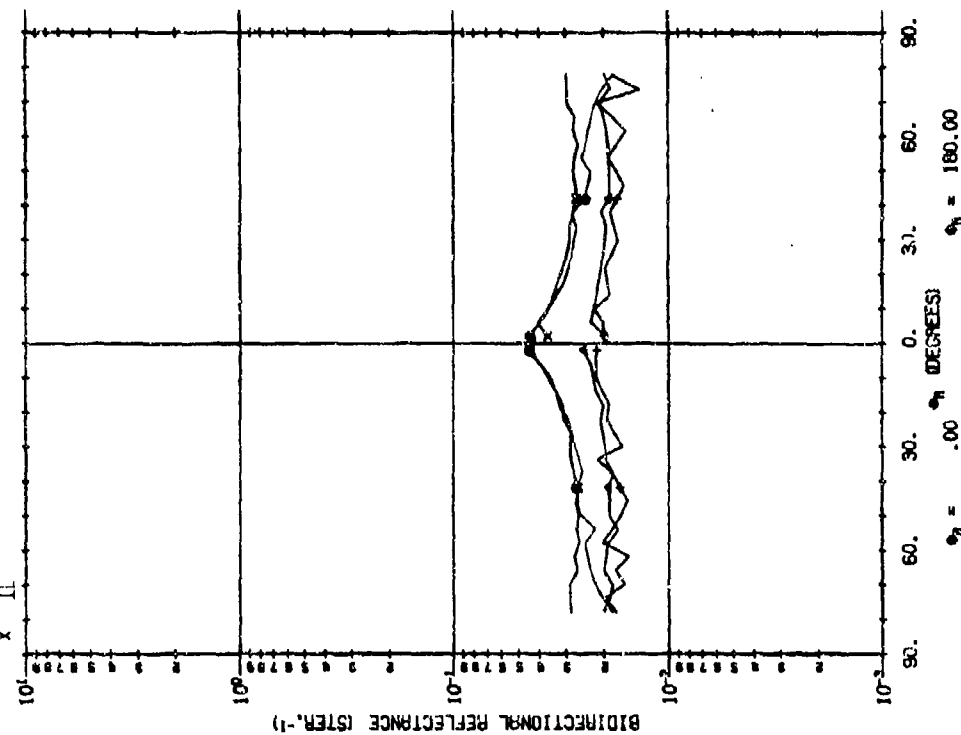
0 ||  $\theta_1 = 60.0$   
+ ||  $\theta_2 = 180.0$   
Δ ||  $\lambda = 0.46$   
x ||  $\gamma = 0.0$



A01672 101

Gray Treated Canvas, 16 Percent Reflectance

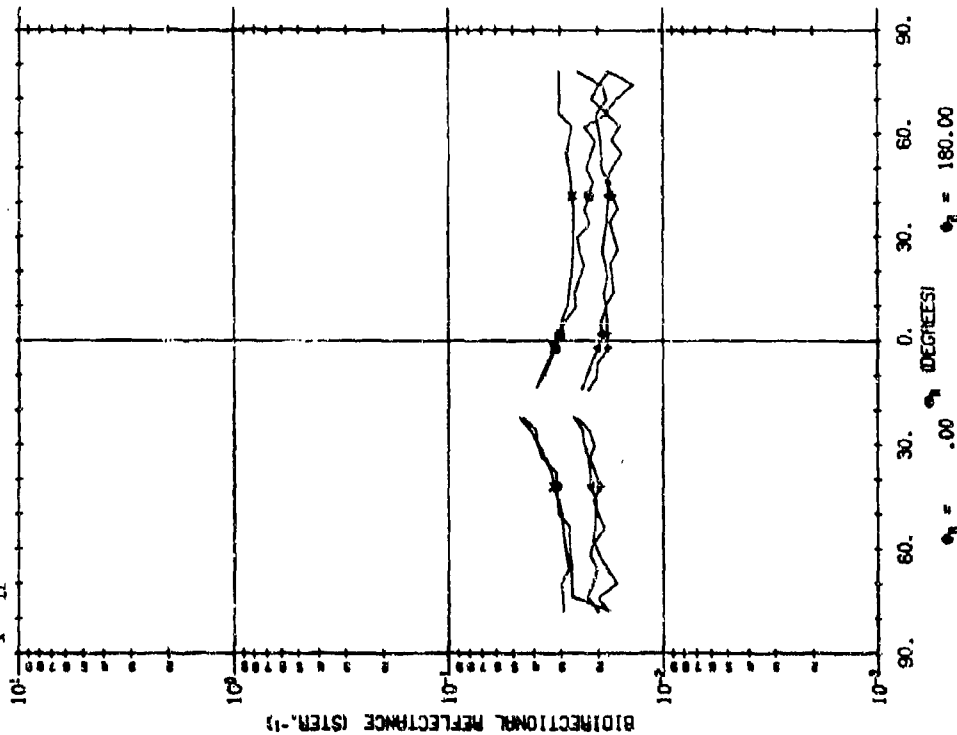
0 ||  $\theta_1 = 0.0$   
+ ||  $\theta_2 = 0.0$   
Δ ||  $\lambda = 0.63$   
x ||  $\gamma = 0.0$



CLOTH AND CANVAS

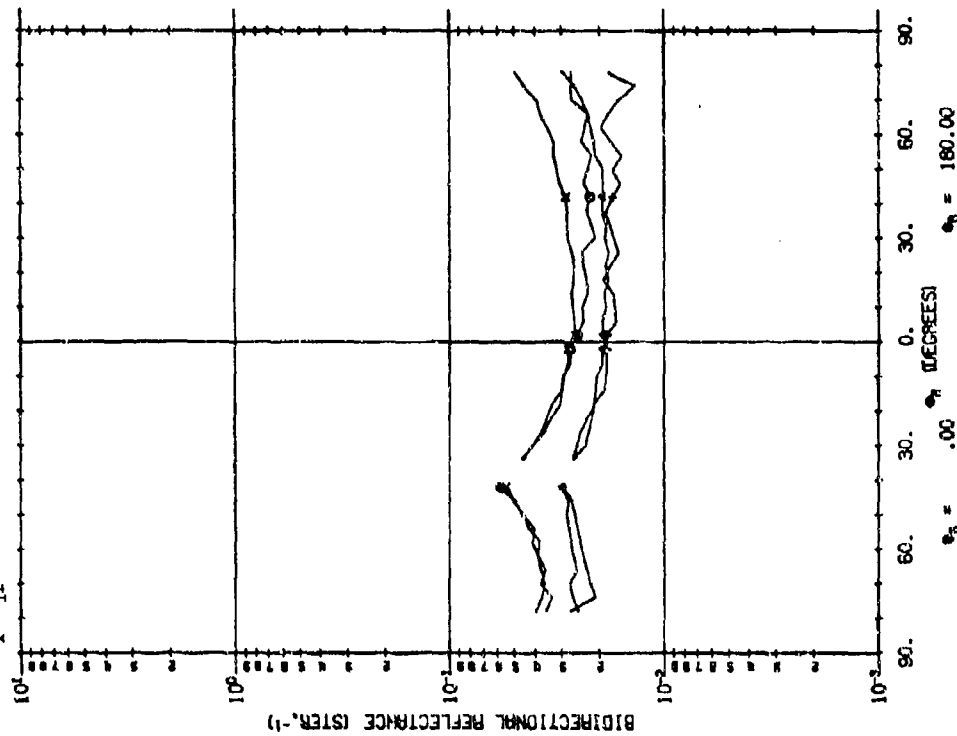
A01672 101  
 0 ||  $\theta_i = 20.0$   
 + ||  $\phi_i = 0.0$   
 x ||  $\lambda_i = 0.63$

Gray Treated Canvas, 16 Percent Reflectance



A01672 101  
 0 ||  $\theta_i = 40.0$   
 + ||  $\phi_i = 0.0$   
 x ||  $\lambda_i = 0.63$

Gray Treated Canvas, 16 Percent Reflectance

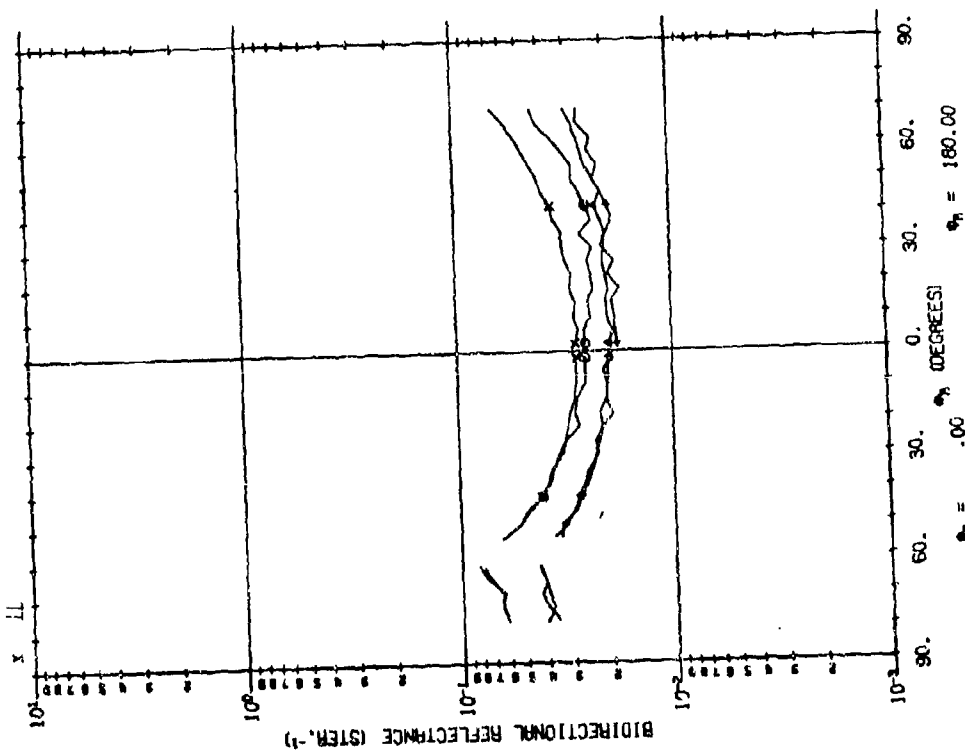


R01672 101

Gray Treated Canvas, 16 Percent Reflectance

$\theta_1 = 60.0$   
 $\theta_2 = 0.0$   
 $\lambda = 0.63$

0 II  
 + II  
 x II

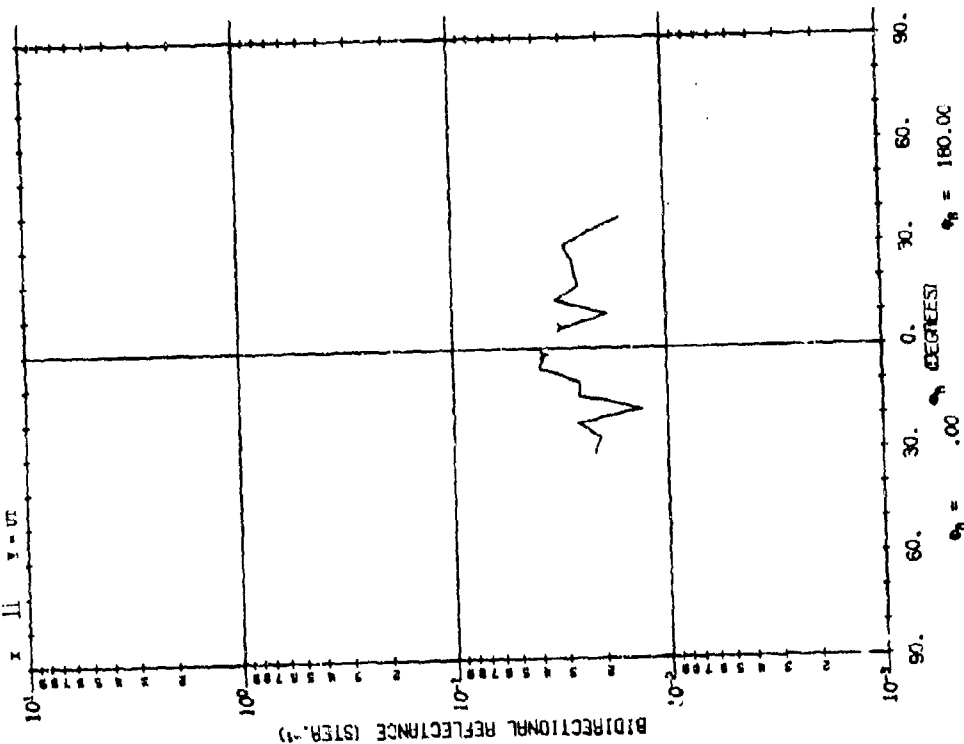


R01673 103

Gray Treated Canvas, 8 Percent Reflectance

$\theta_1 = 0.0$   
 $\theta_2 = 180.0$   
 $\lambda = 0.46$

0 II  
 + II  
 x II

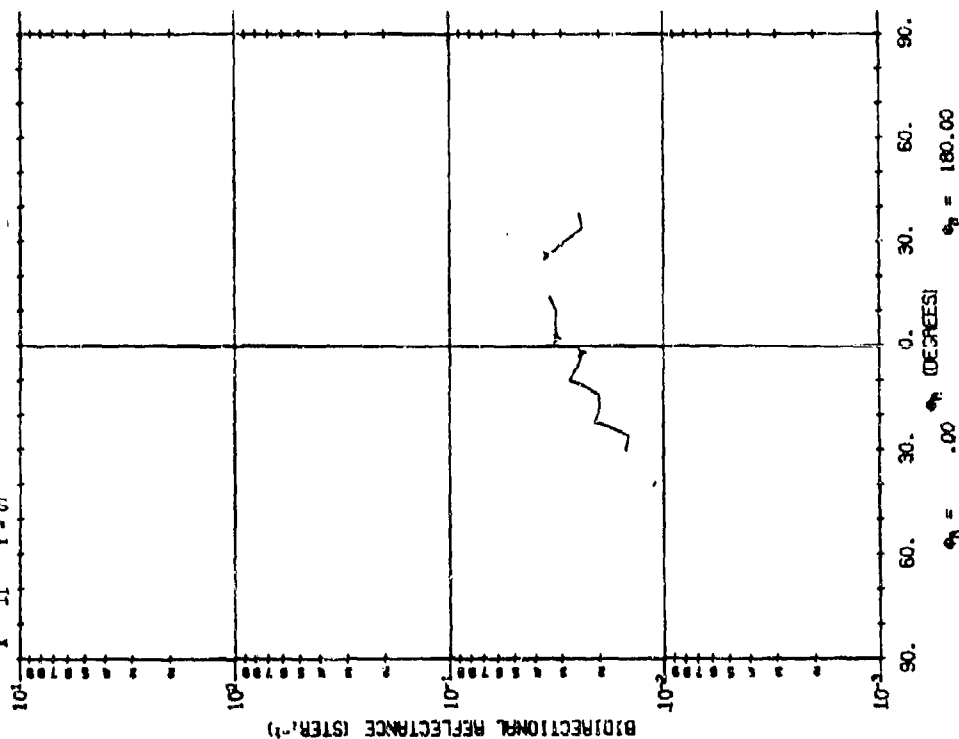


CLOTH AND CANVAS

A01673 103

Gray Treated Canvas, 8 Percent Reflectance

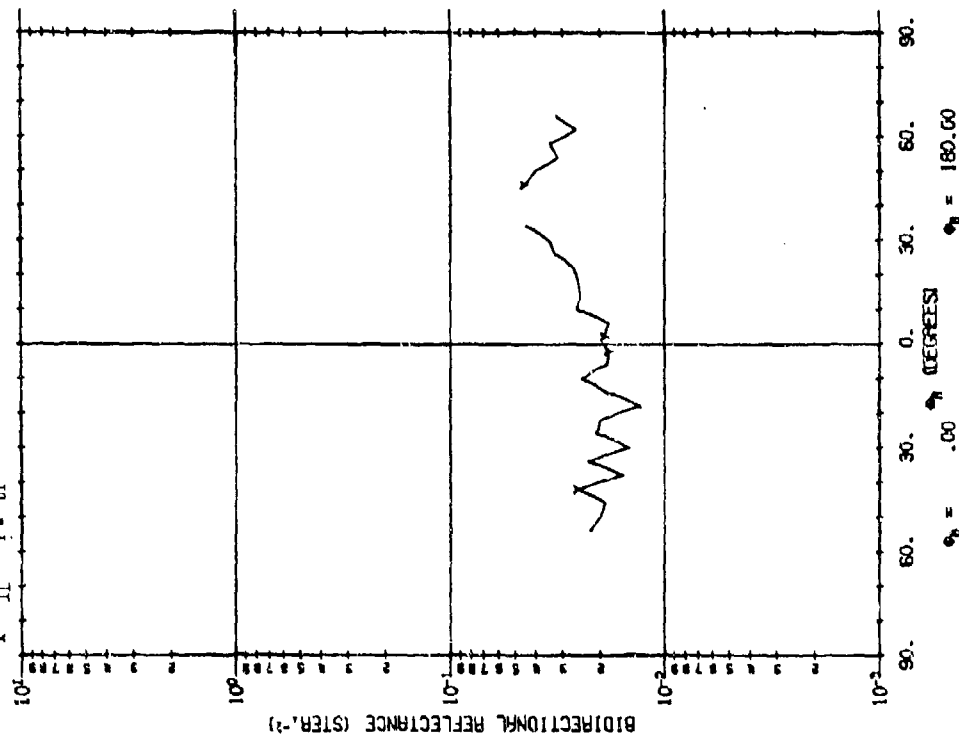
$\theta_1 = 20.0$   
 $\phi_1 = 180.0$   
 $\lambda = 0.46$   
 $Y = 07$



A01673 103

Gray Treated Canvas, 8 Percent Reflectance

$\theta_1 = 40.0$   
 $\phi_1 = 180.0$   
 $\lambda = 0.46$   
 $Y = 07$

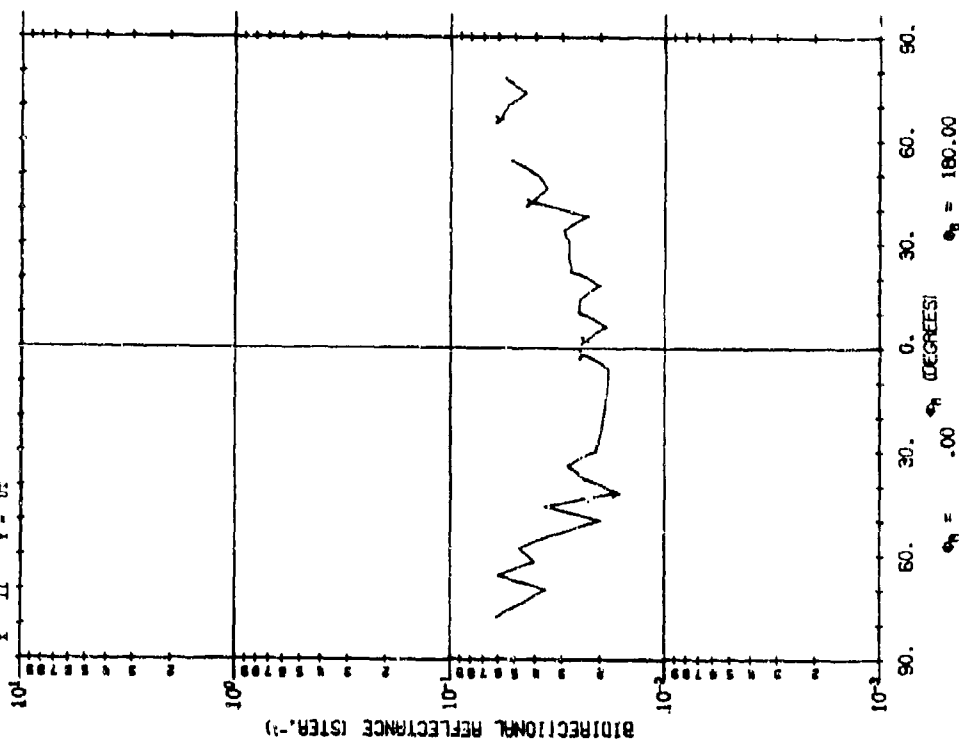




R01673 103

Gray Treated Canvas, 8 Percent Reflectance

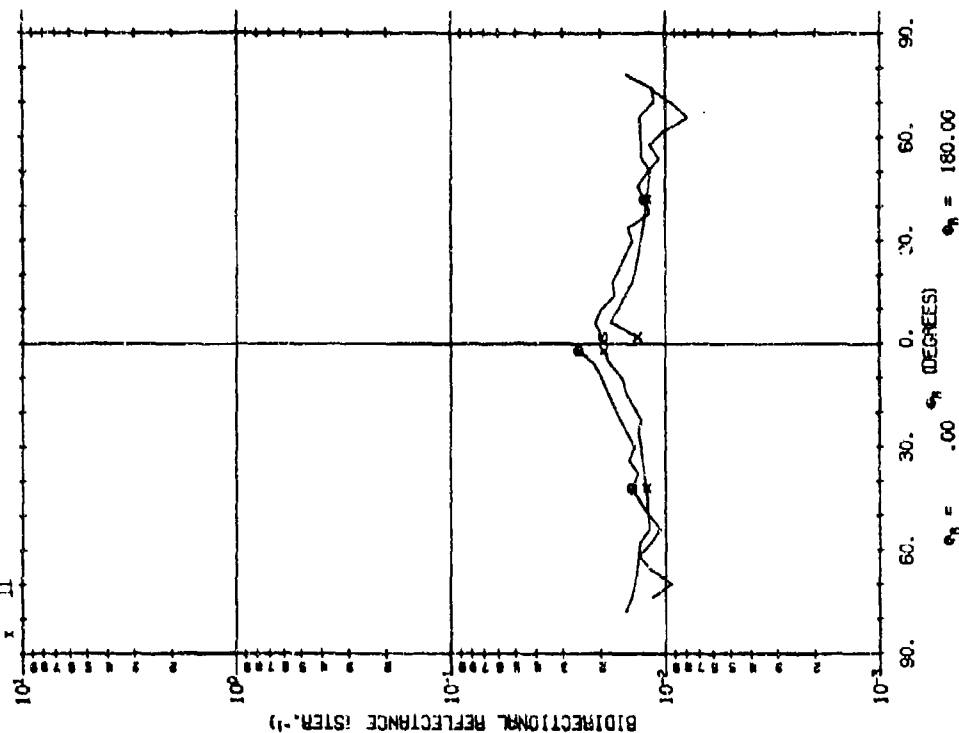
0 11  $\theta_i = 60.0$   
 + 11  $\theta_r = 180.0$   
 x 11  $\lambda = 0.46$   
 11 Y = UZ



R01673 101

Gray Treated Canvas, 8 Percent Reflectance

0 11  $\theta_i = 0.0$   
 + 11  $\theta_r = 0.3$   
 x 11  $\lambda = 0.63$



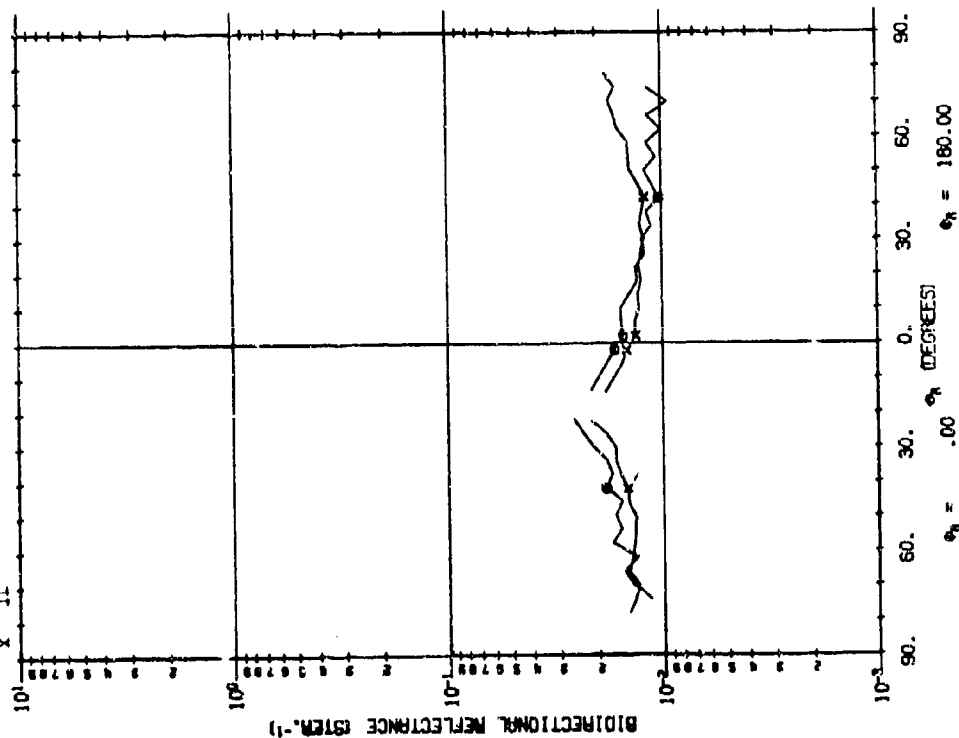
CLOTH AND CANVAS

R01673 101

Gray Treated Canvas, 8 Percent Reflectance

$\theta_i = 20.0$   
 $\theta_r = 0.0$   
 $\lambda = 0.63$

0 ||  
 + ||  
 A ||  
 X ||

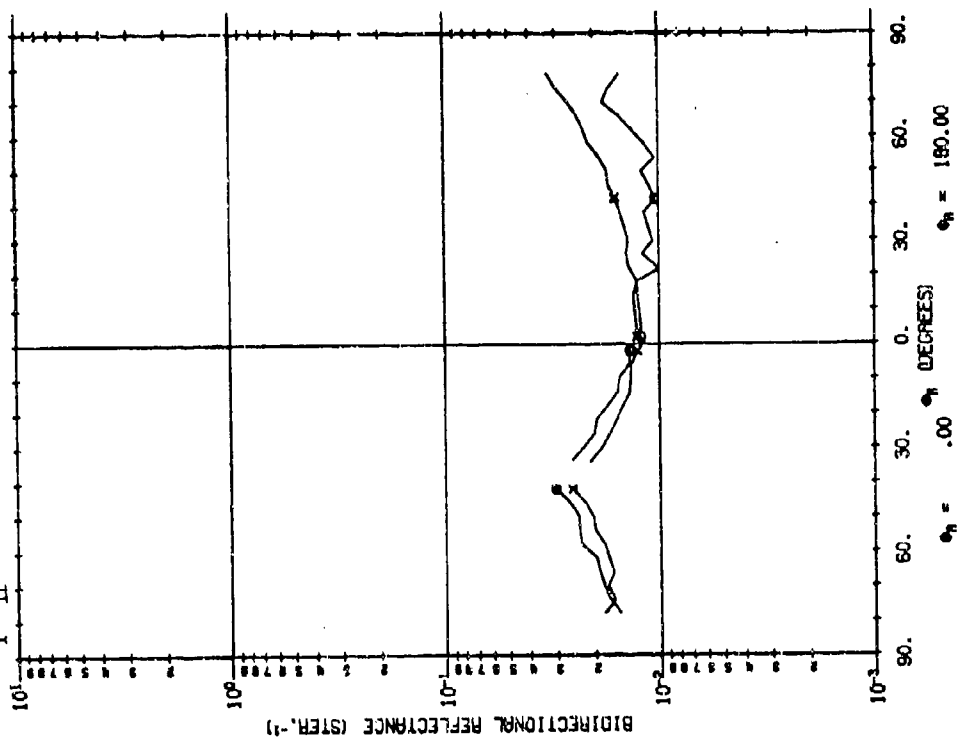


R01673 101

Gray Treated Canvas, 8 Percent Reflectance

$\theta_i = 40.0$   
 $\theta_r = 0.0$   
 $\lambda = 0.63$

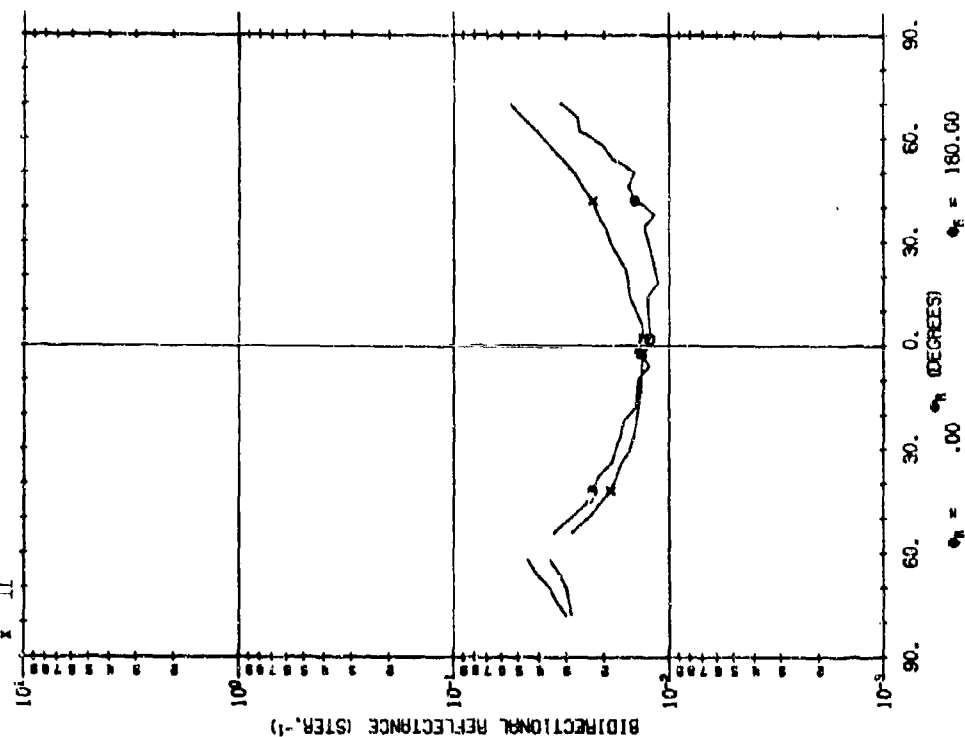
0 ||  
 + ||  
 A ||  
 X ||



A01673 101

Gray Treated Canvas, 2 Percent Reflectance

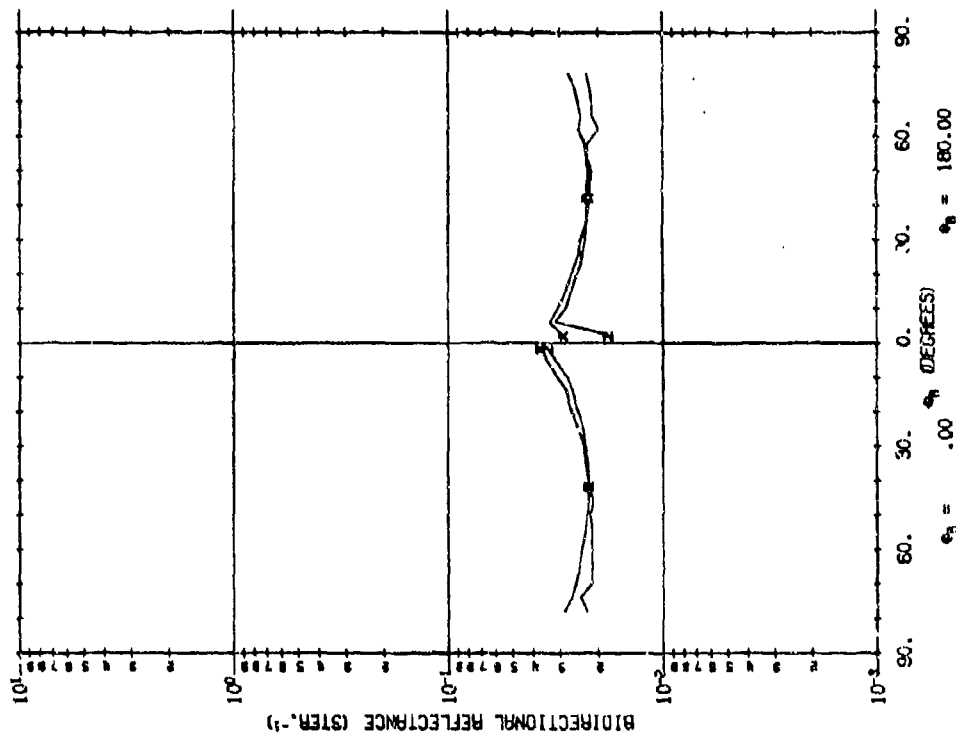
$\theta_1 = 60.0$   
 $\phi_1 = 0.0$   
 $\lambda = 0.63$



A01673 102

Gray Treated Canvas, 8 Percent Reflectance

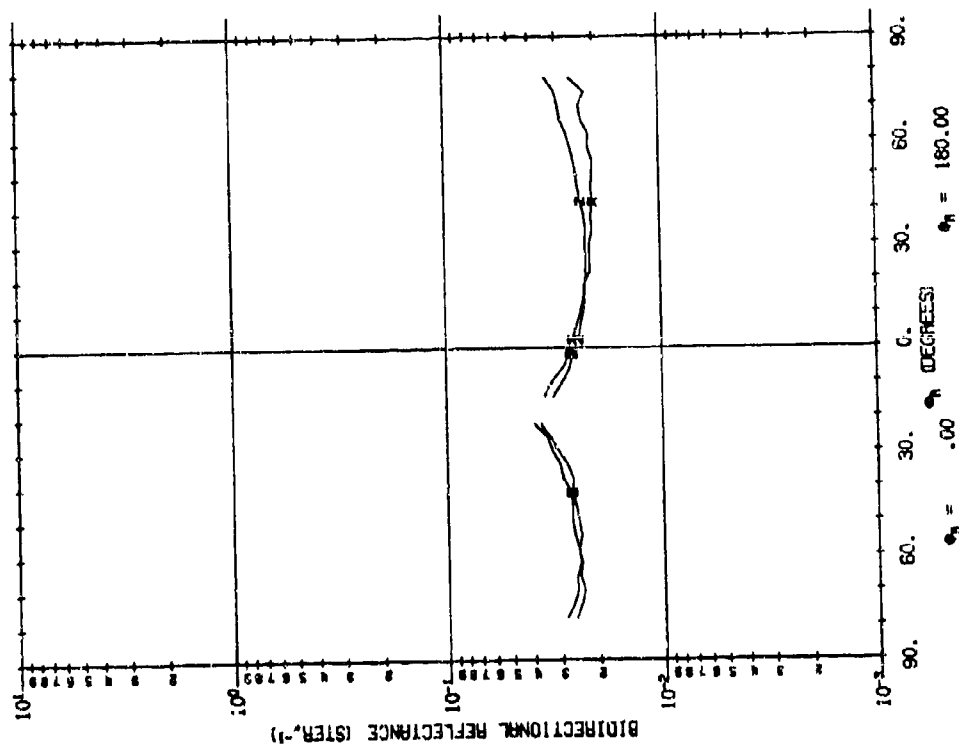
$\theta_1 = 0.0$   
 $\phi_1 = 0.0$   
 $\lambda = 0.63$



CLOTH AND CANVAS

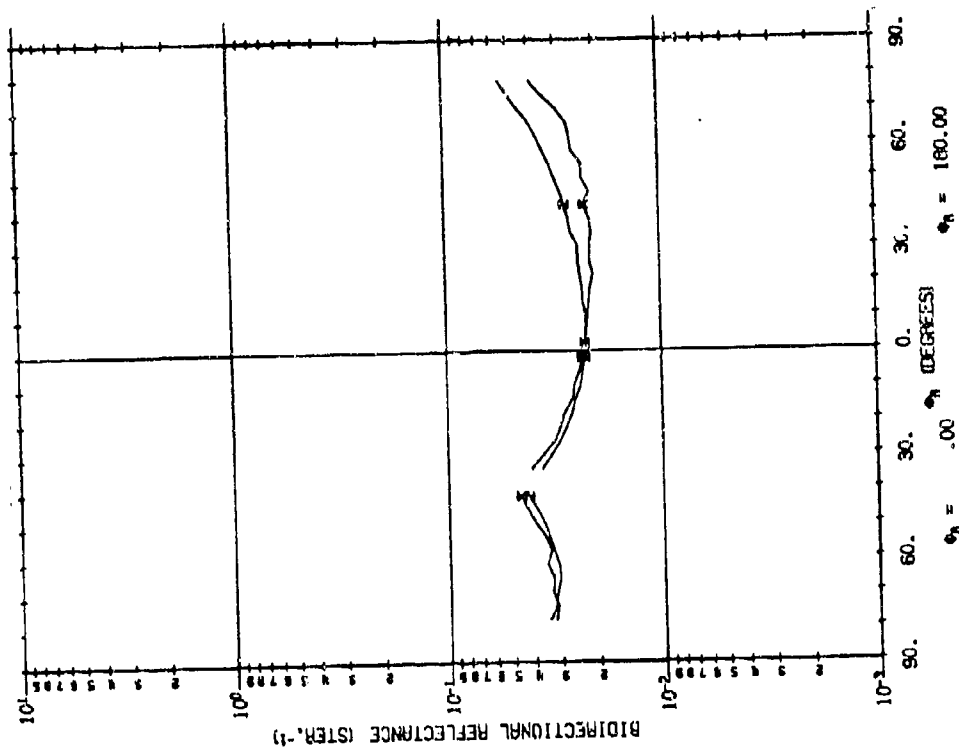
R01573 102  
 $\epsilon_1 = 20.0$   
 $\phi_1 = 0.0$   
 $\lambda = 0.63$

Gray Treated Curves, 8 Percent Reflectance



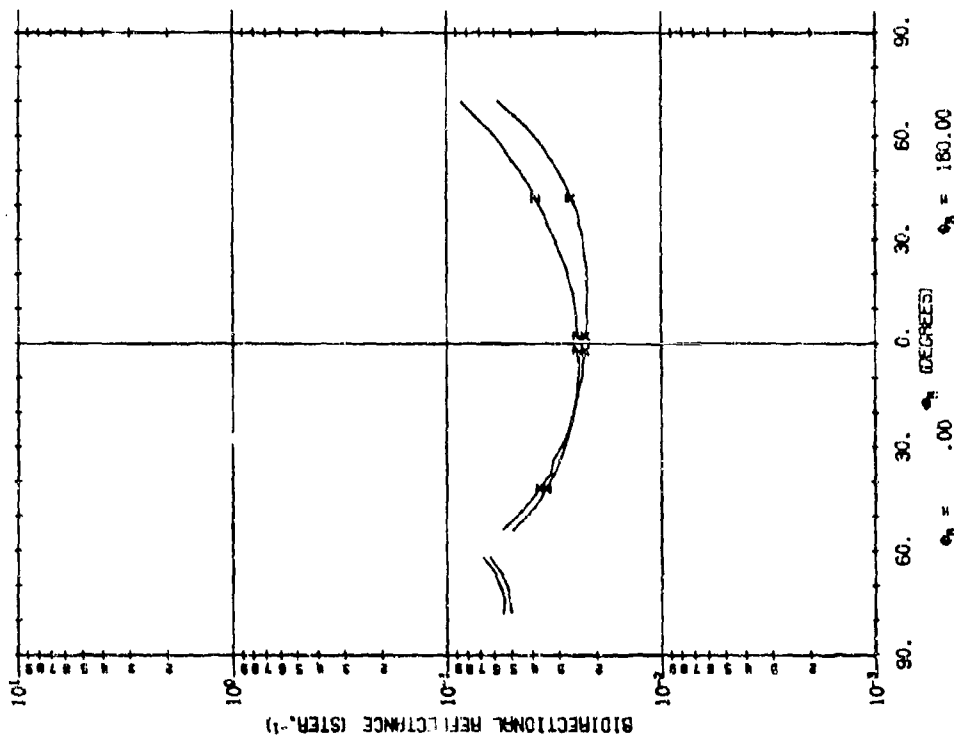
R01673 102  
 $\epsilon_1 = 40.0$   
 $\phi_1 = 6.0$   
 $\lambda = 0.63$

Gray Treated Curves, 8 Percent Reflectance



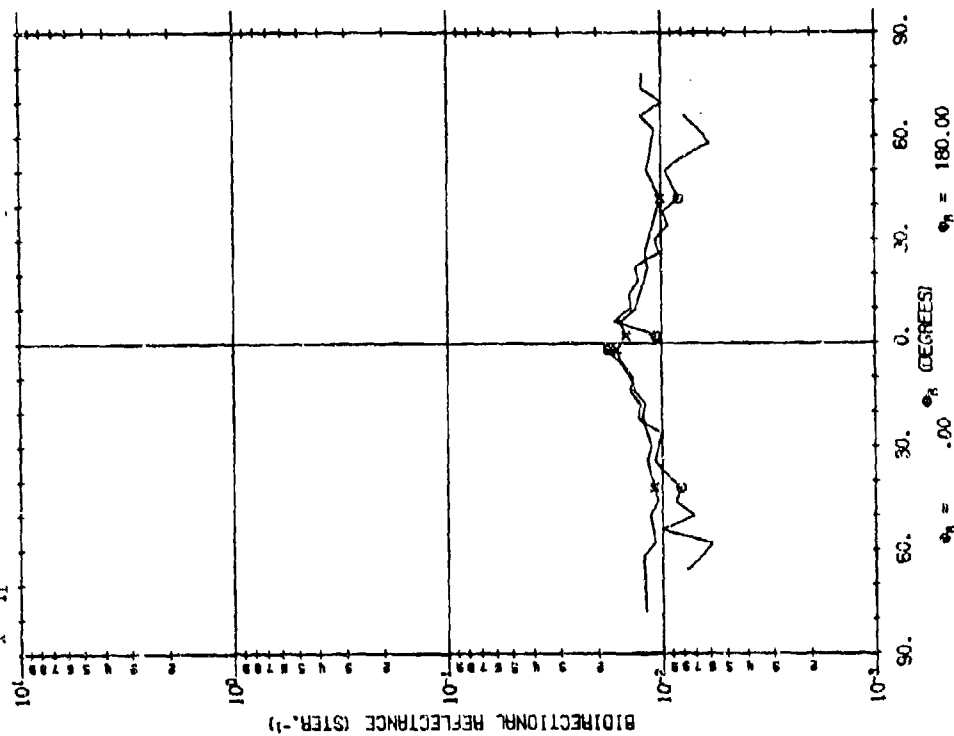
AO1673 102  
 1 1  
 2 2  
 $\theta_1 = 60.0$   
 $\theta_2 = 0.0$   
 $\lambda = 0.63$

Gray Treated Canvas, 8 Percent Reflectance

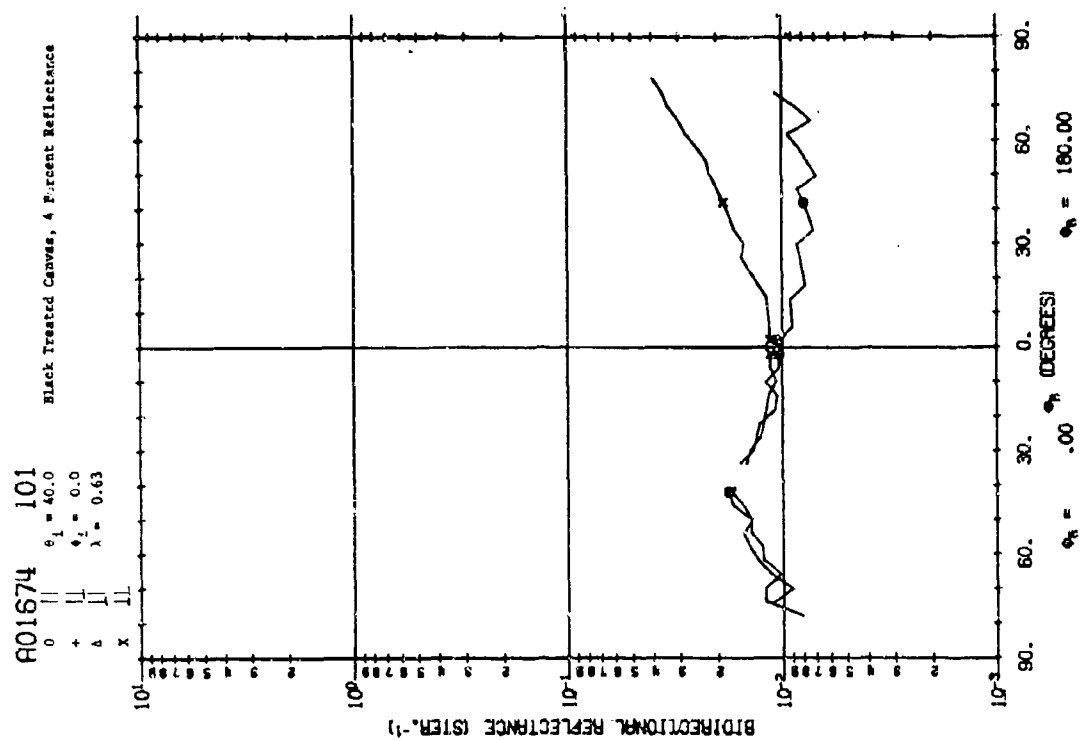
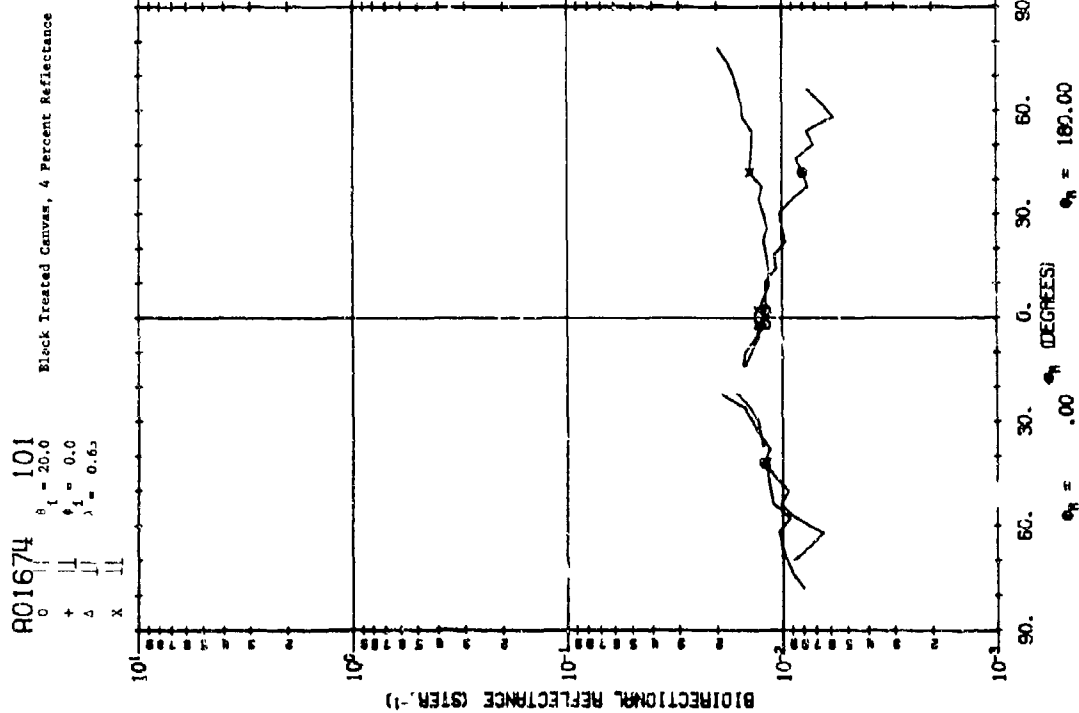


AO1674 101  
 0 1  
 + 1  
 2 1  
 X 1  
 $\theta_1 = 0.0$   
 $\theta_2 = 0.0$   
 $\lambda = 0.63$

Black Treated Canvas, 8 Percent Reflectance



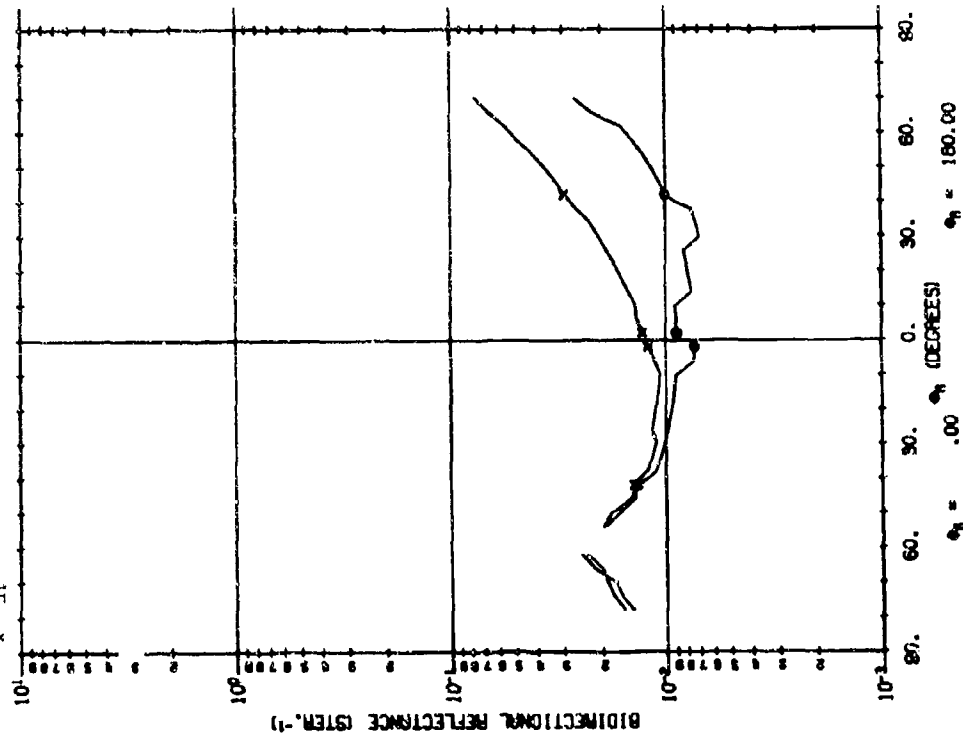
CLOTH AND CANVAS



R01674 101

Black Treated Canvas, 4 Percent Reflectance

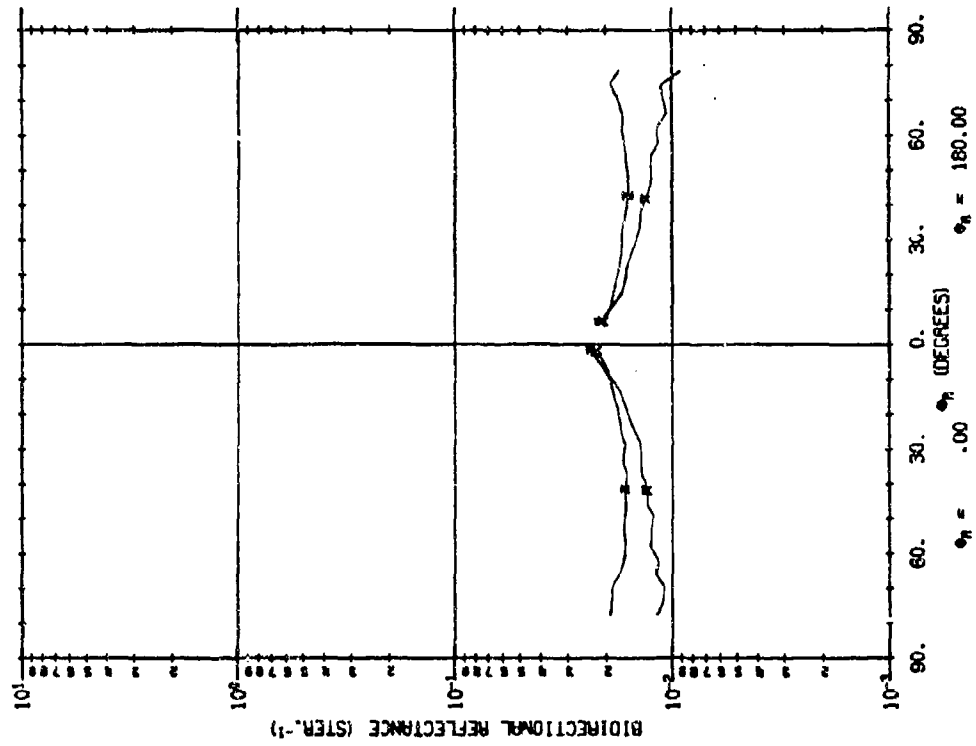
$\theta_i = 60.0$   
 $\phi_i = 0.0$   
 $\lambda = 0.63$



R01674 102

Black Treated Canvas, 4 Percent Reflectance

$\theta_i = 0.0$   
 $\phi_i = 0.0$   
 $\lambda = 0.63$

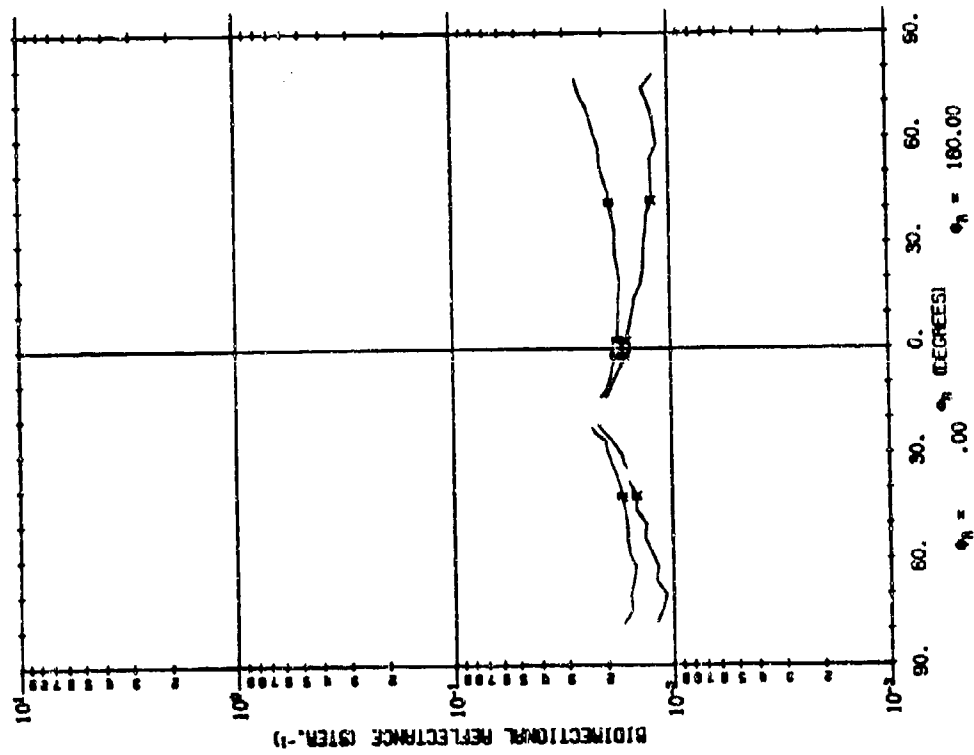


CLOTH AND CANVAS

A01674 102

Black Treated Canvas, 4 Percent Reflectance

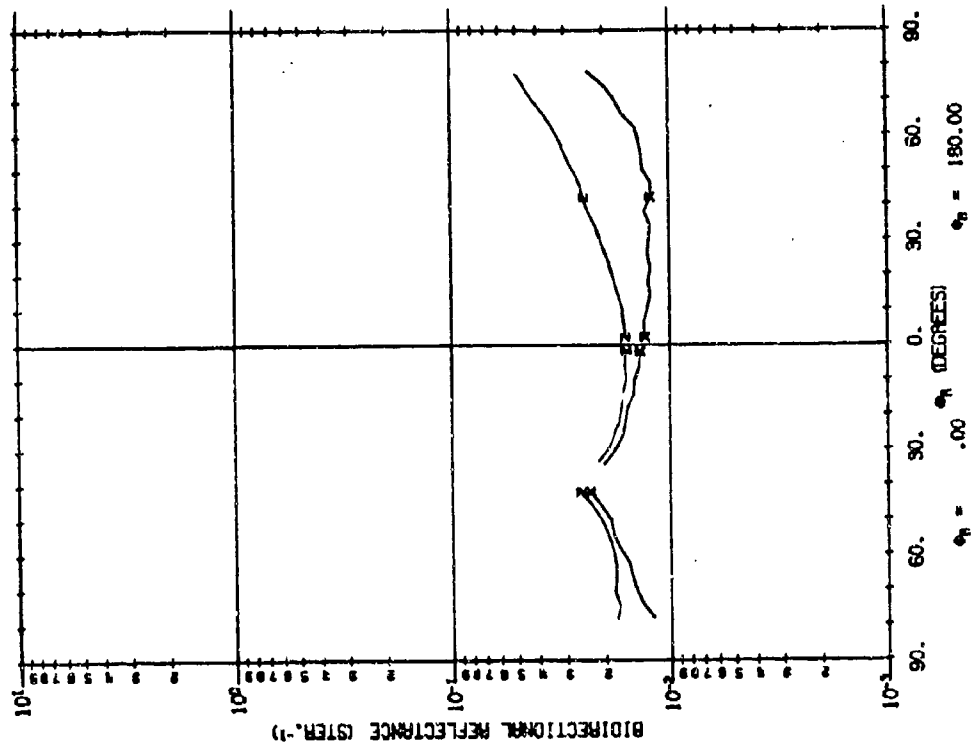
$\lambda$   $\tau$   $\phi_1 = 20.0$   
 $\lambda$   $\tau$   $\phi_1 = 0.0$   
 $\lambda = 0.63$



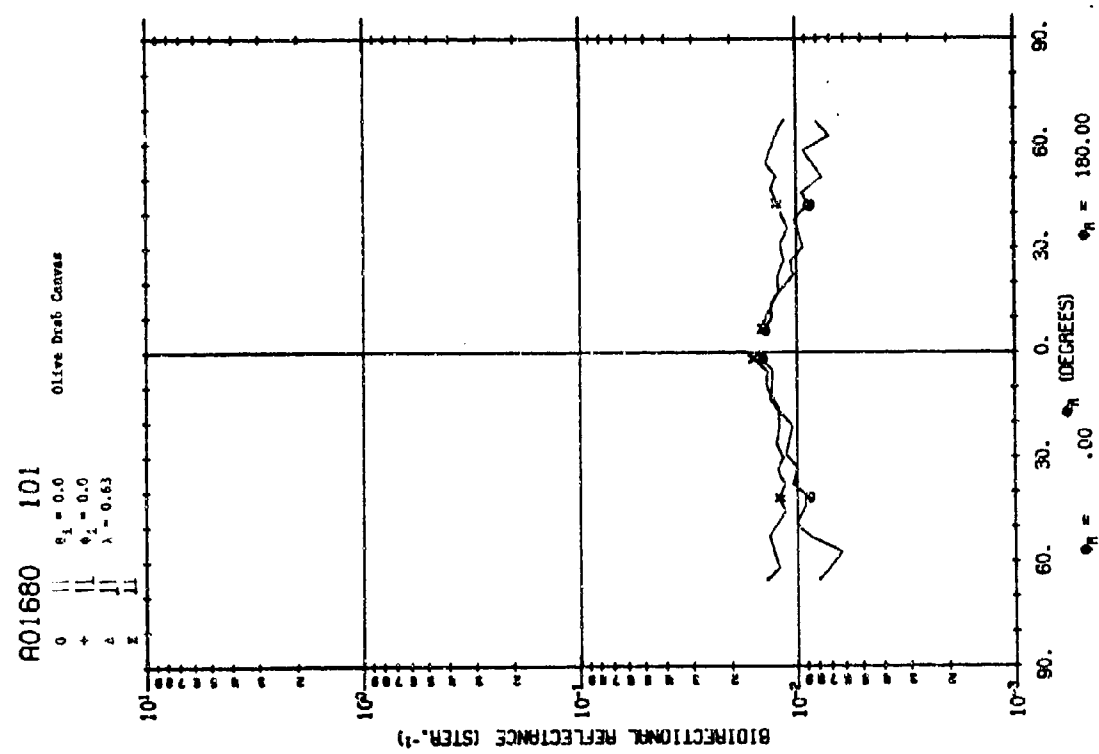
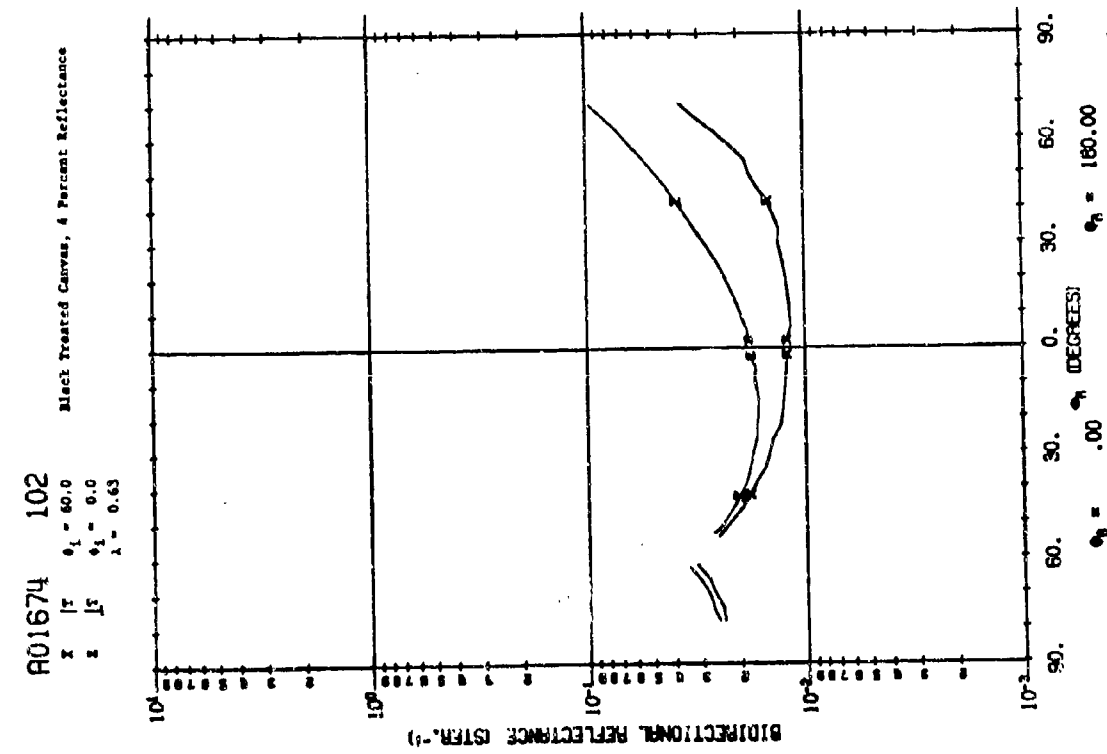
A01674 102

Black Treated Canvas, 4 Percent Reflectance

$\lambda$   $\tau$   $\phi_1 = 40.0$   
 $\lambda$   $\tau$   $\phi_1 = 0.0$   
 $\lambda = 0.63$





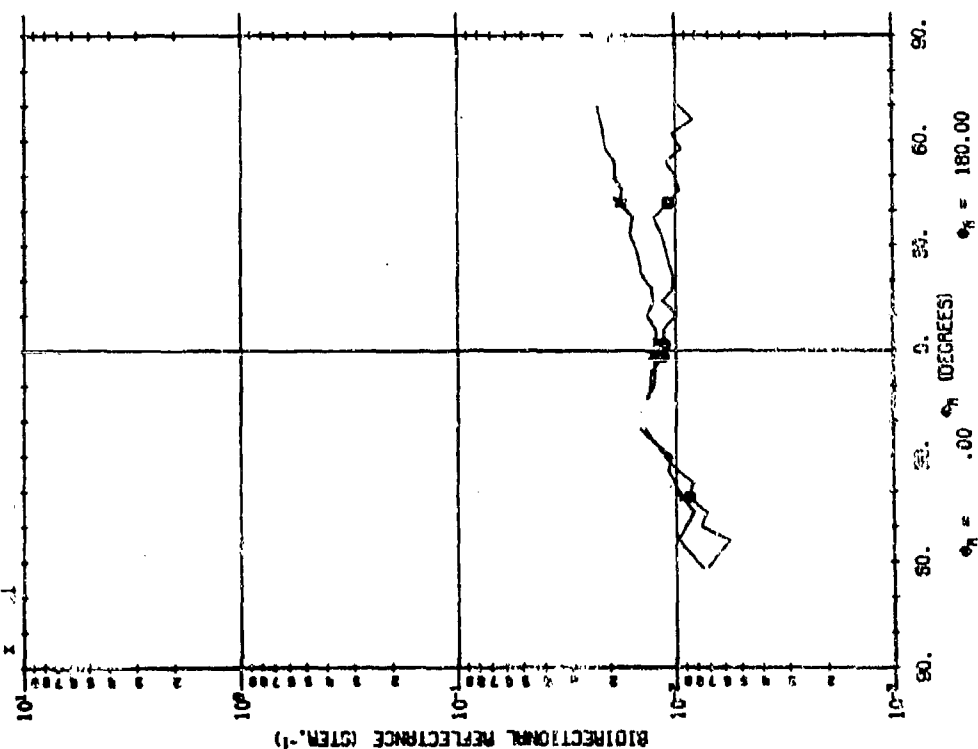


# CLOTH AND CANVAS

R01680 101

Olive Drab Canvas

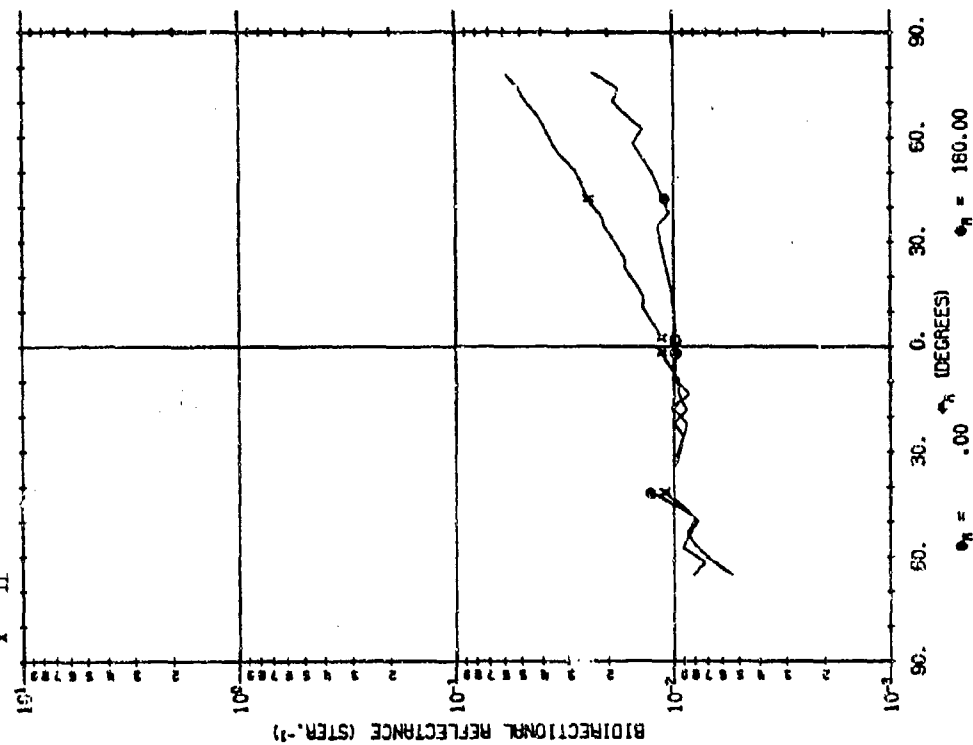
$\theta_1 = 20.0$   
 $\phi_1 = 0.0$   
 $\lambda = 0.63$



R01680 101

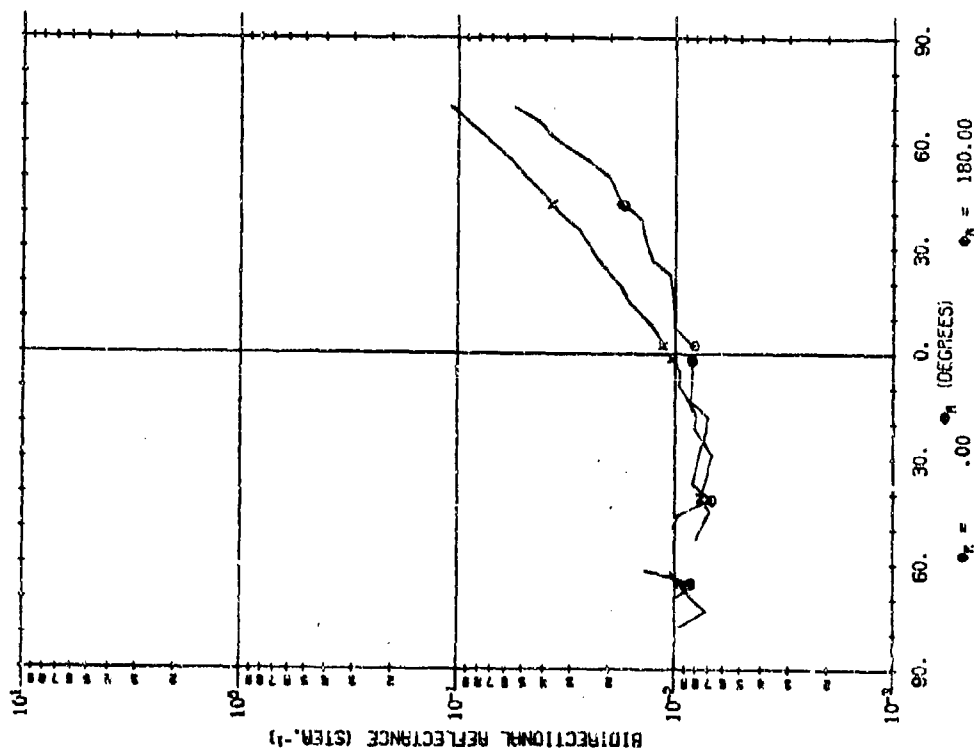
Olive Drab Canvas

$\theta_1 = 40.0$   
 $\phi_1 = 0.0$   
 $\lambda = 0.63$



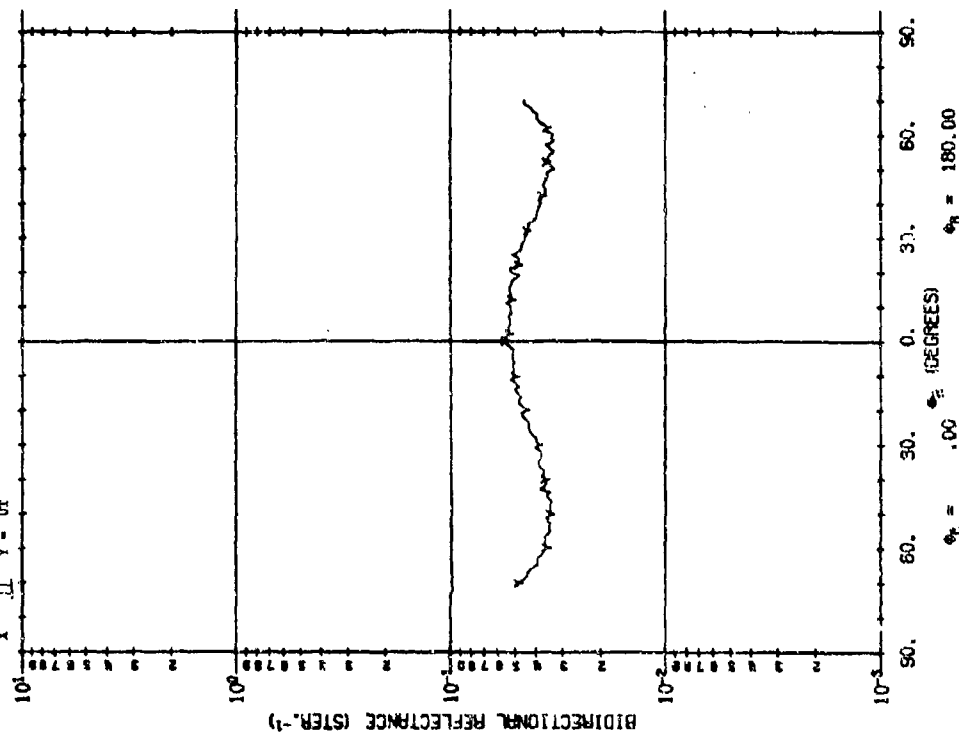
R01680 101  
 0 ||  $\theta_1 = 60.0$   
 + ||  $\theta_2 = 0.0$   
 Δ ||  $\lambda = 0.63$   
 x ||

OLIVE DRAB CANVAS



R01680 301  
 0 ||  $\theta_1 = 2.0$   
 + ||  $\theta_2 = 0.0$   
 Δ ||  $\lambda = 10.6$   
 x ||  $\gamma = 0.0$

OLIVE DRAB CANVAS

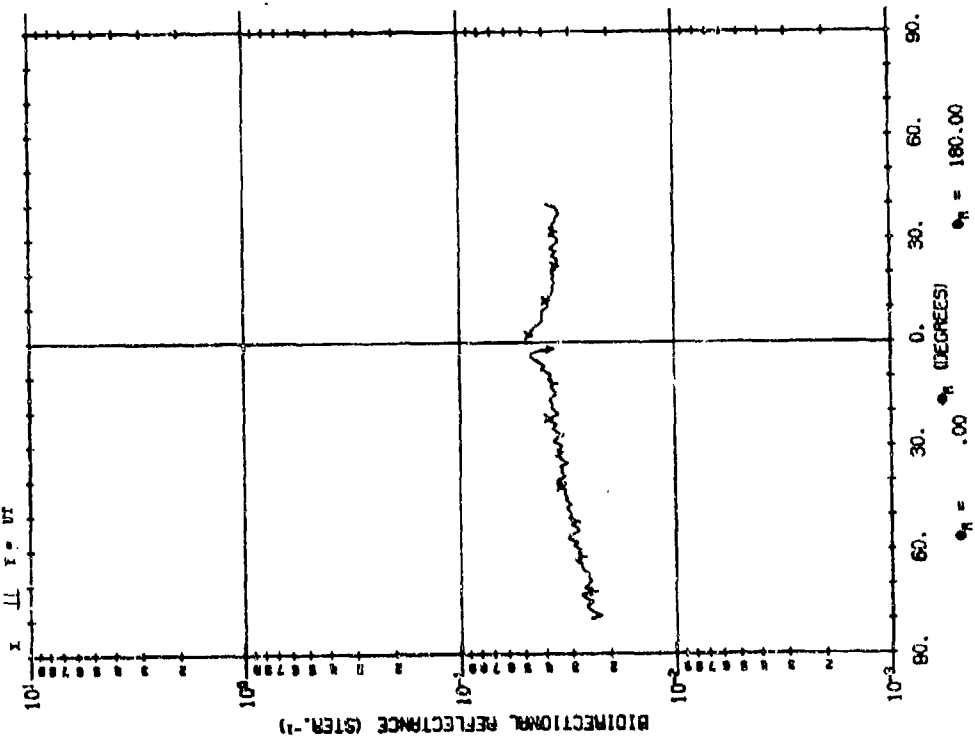


CLOTH AND CANVAS

A01680 301

OLIVE DRAB CANVAS

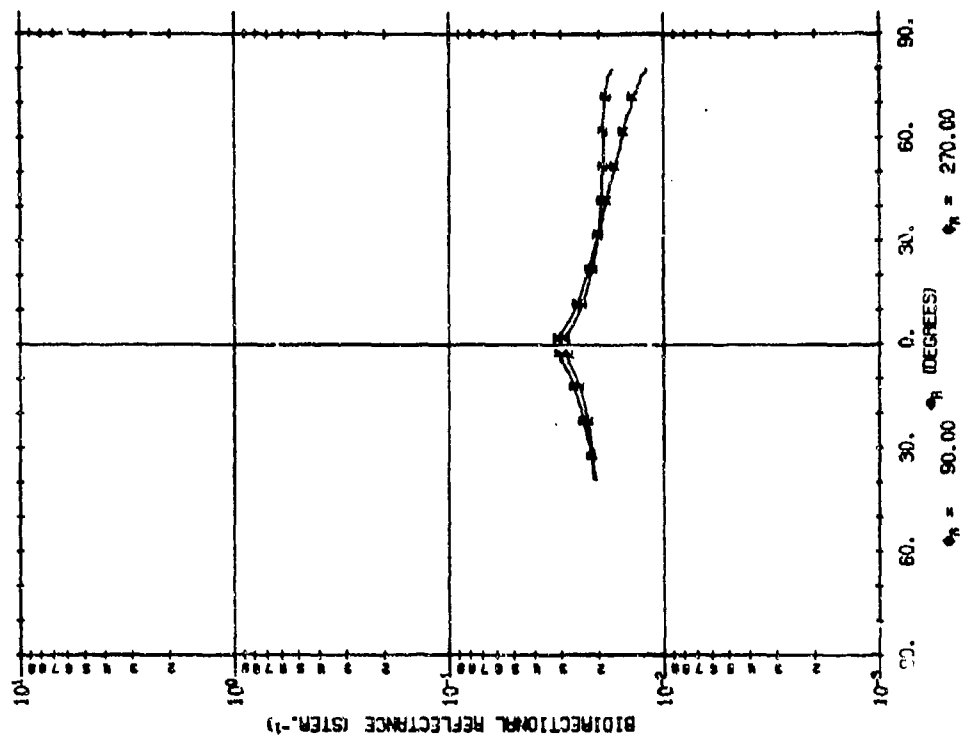
0 11  $\theta_1 = 6.0$   
 + 11  $\theta_1 = 180.0$   
 A 11  $\lambda = 10.6$   
 X 11  $\gamma = 0^\circ$



A01802 101

GRAY CANVAS, 8 PERCENT REFLECTANCE

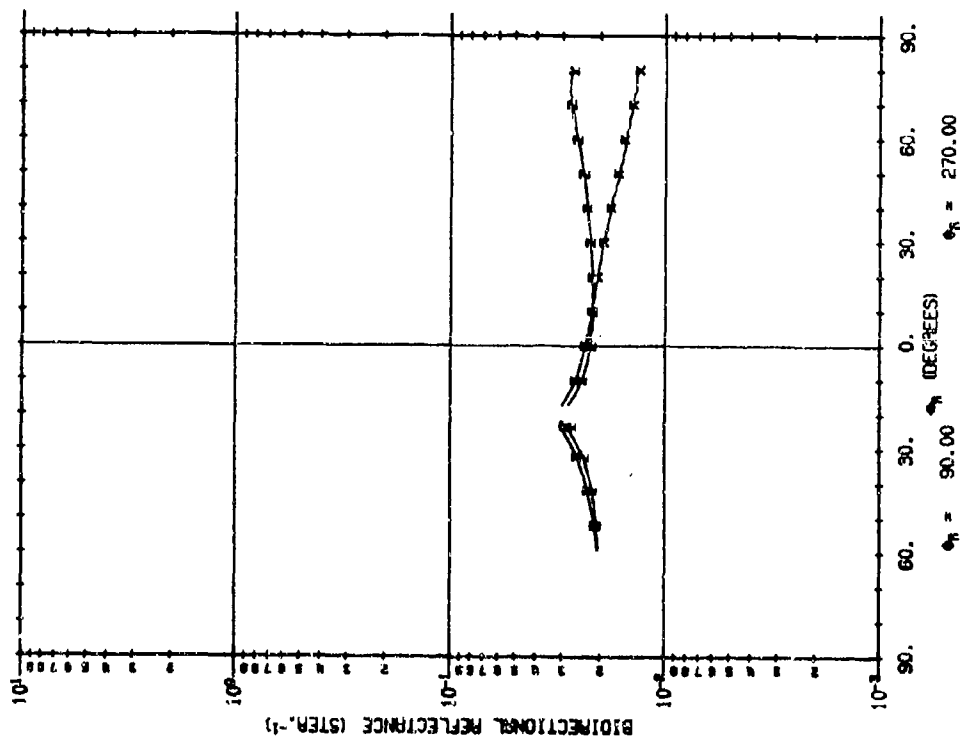
X 11  $\theta_1 = 6.0$   
 Z 11  $\theta_1 = 90.0$   
 A 11  $\lambda = 0.63$



R01802 101

GRAY CANVAS, 8 PERCENT REFLECTANCE

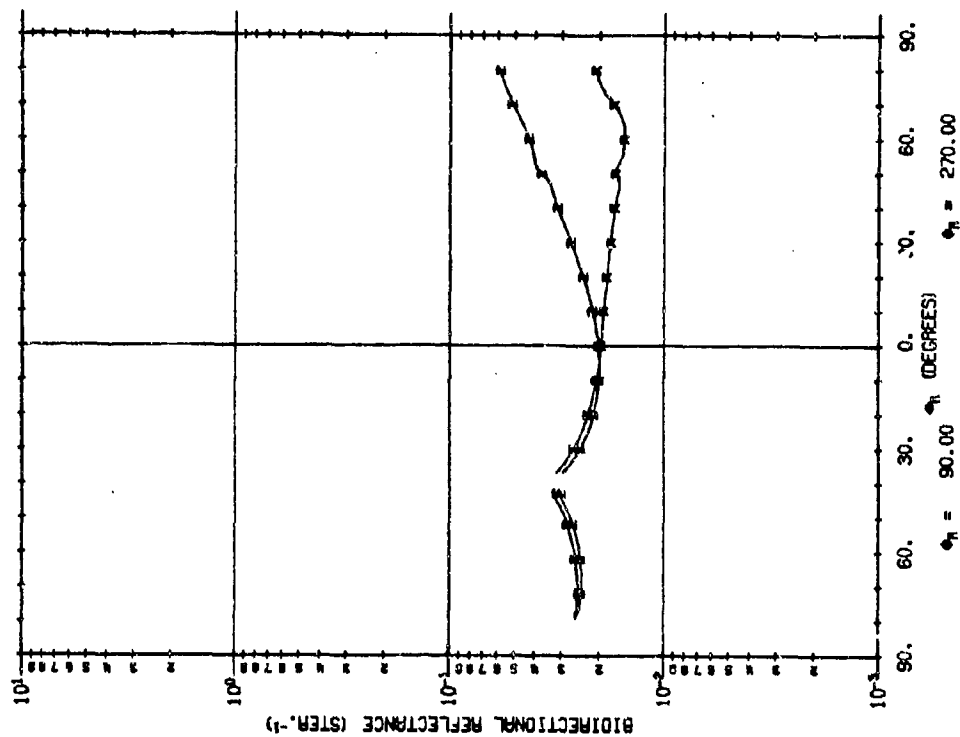
X  $\theta_i = 20.0$   
Z  $\phi_i = 90.0$   
 $\lambda = 0.63$



R01802 101

GRAY CANVAS, 8 PERCENT REFLECTANCE

X  $\theta_i = 40.0$   
Z  $\phi_i = 90.0$   
 $\lambda = 0.63$

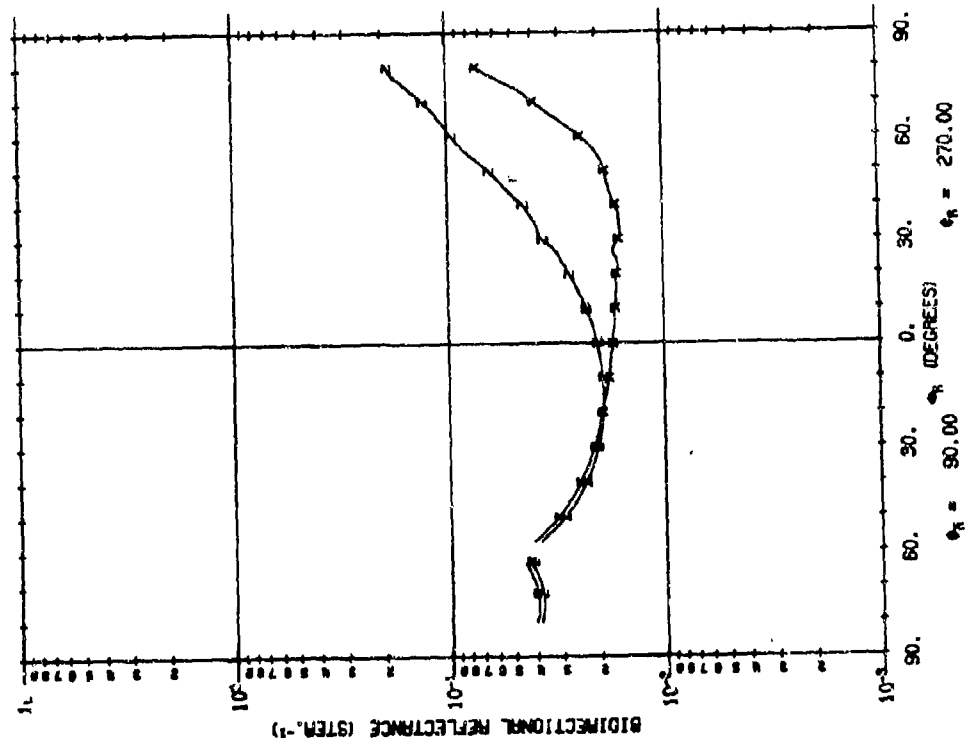


CLOTH AND CANVAS

R01802 101

GRAY CANVAS, 8 PERCENT REFLECTANCE

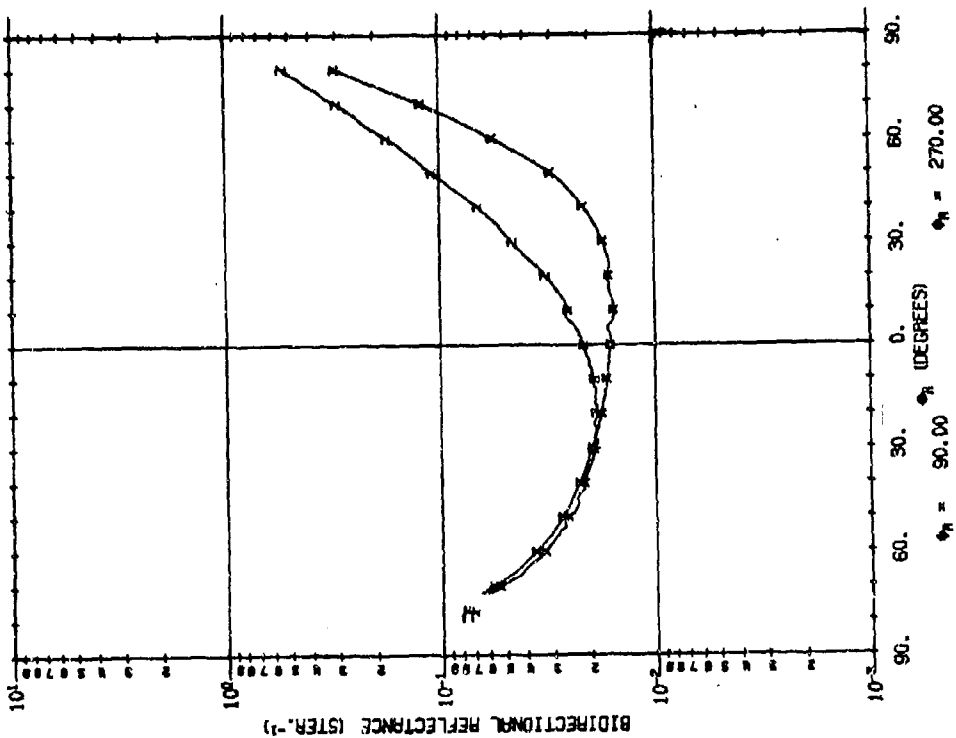
X  $\theta_i = 40.0$   
 Z  $\theta_i = 90.0$   
 $\lambda = 0.63$



R01802 101

GRAY CANVAS, 8 PERCENT REFLECTANCE

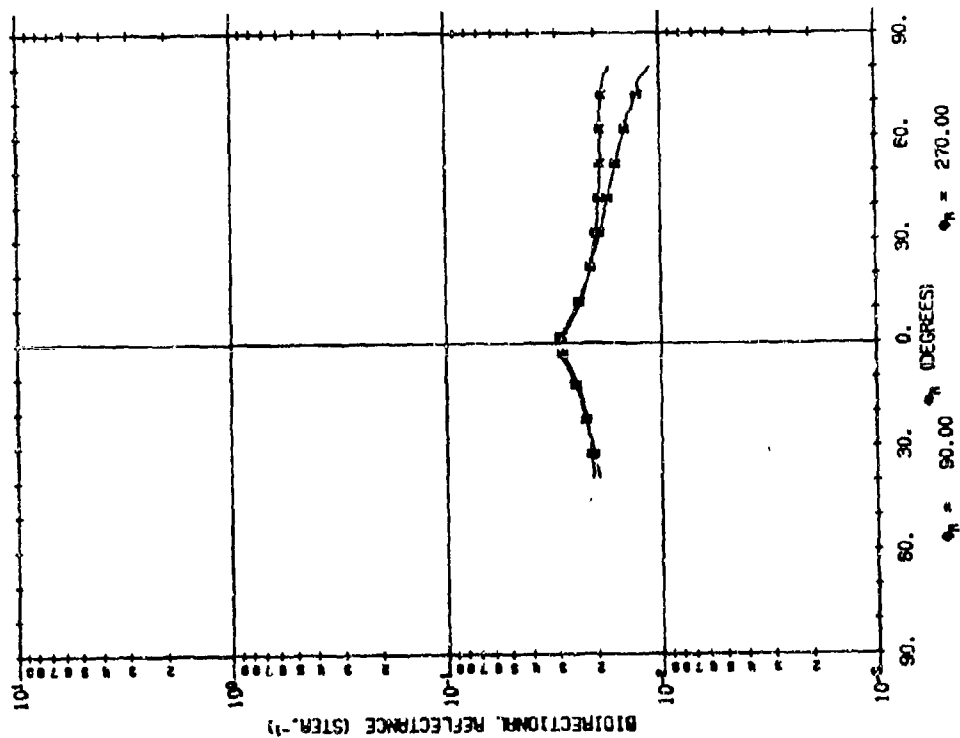
X  $\theta_i = 75.0$   
 Z  $\theta_i = 90.0$   
 $\lambda = 0.63$



R01802 101

GRAY CANVAS, 8 PERCENT REFLECTANCE

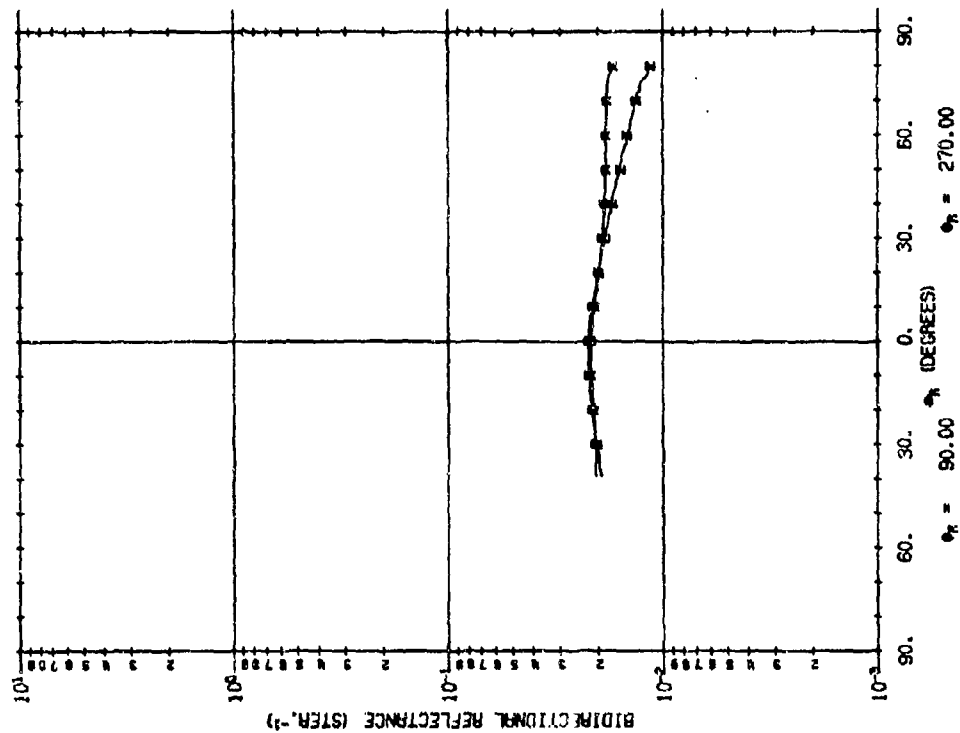
$\lambda = 0.63$   
 $\phi_1 = 0.0$   
 $\phi_2 = 0.0$



R01802 101

GRAY CANVAS, 8 PERCENT REFLECTANCE

$\lambda = 0.63$   
 $\phi_1 = 0.0$   
 $\phi_2 = 0.0$



CLOTH AND CANVAS

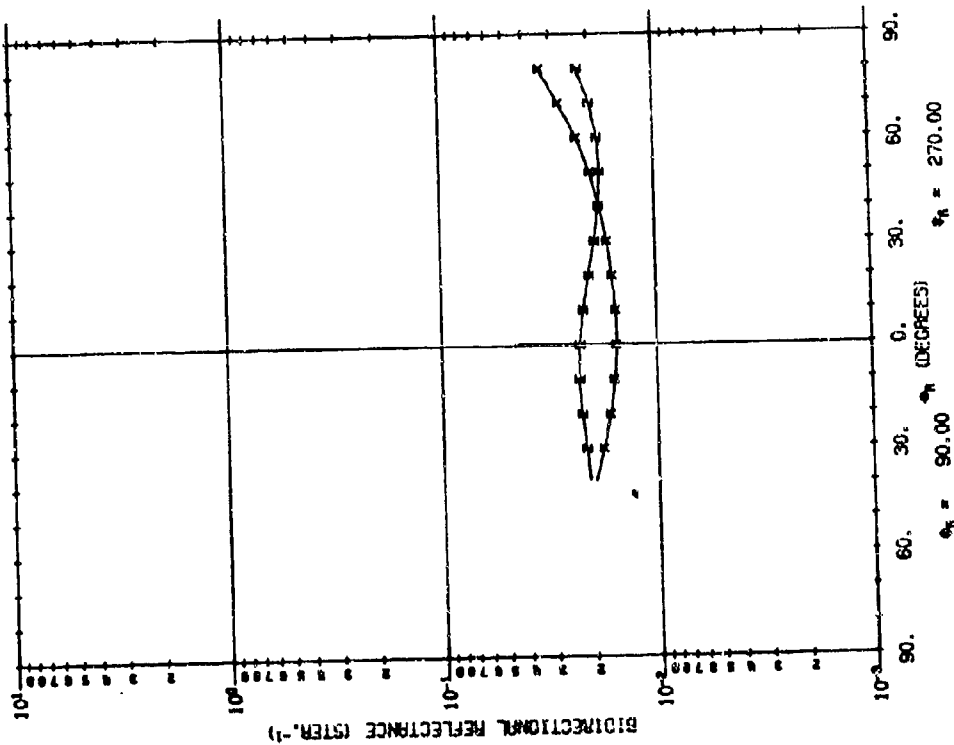




R01802 101

GRAY CANVAS, 8 PERCENT REFLECTANCE

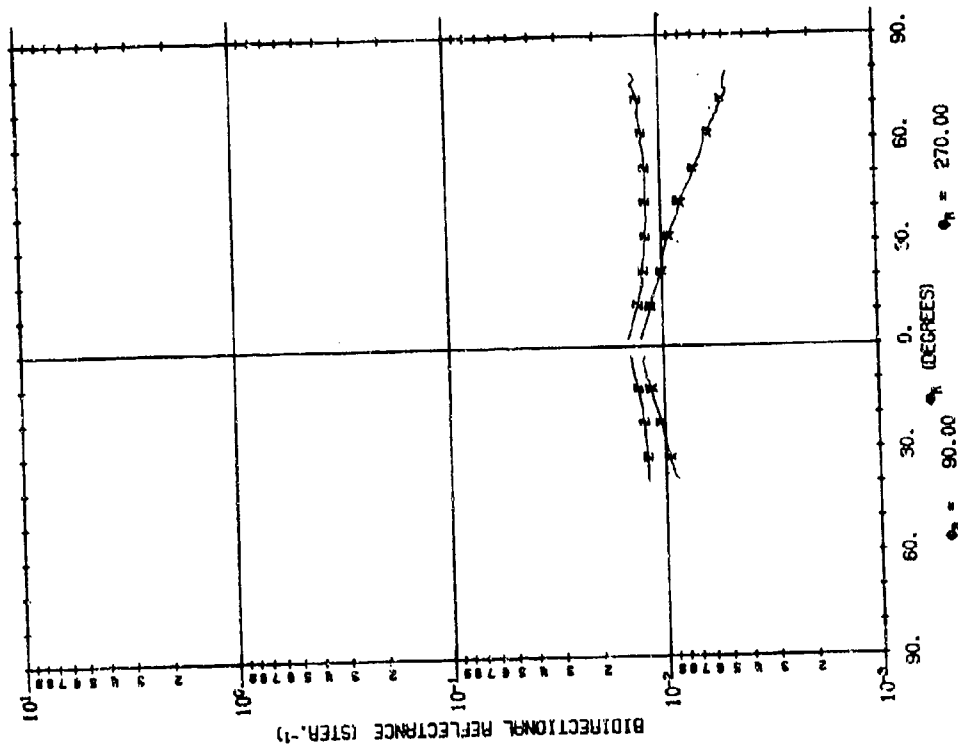
$\epsilon_1 = 75.0$   
 $\epsilon_2 = 0.0$   
 $\lambda = 0.63$



R01803 101

BLACK CANVAS, 4 PERCENT REFLECTANCE

$\epsilon_1 = 0.0$   
 $\epsilon_2 = 90.0$   
 $\lambda = 0.63$

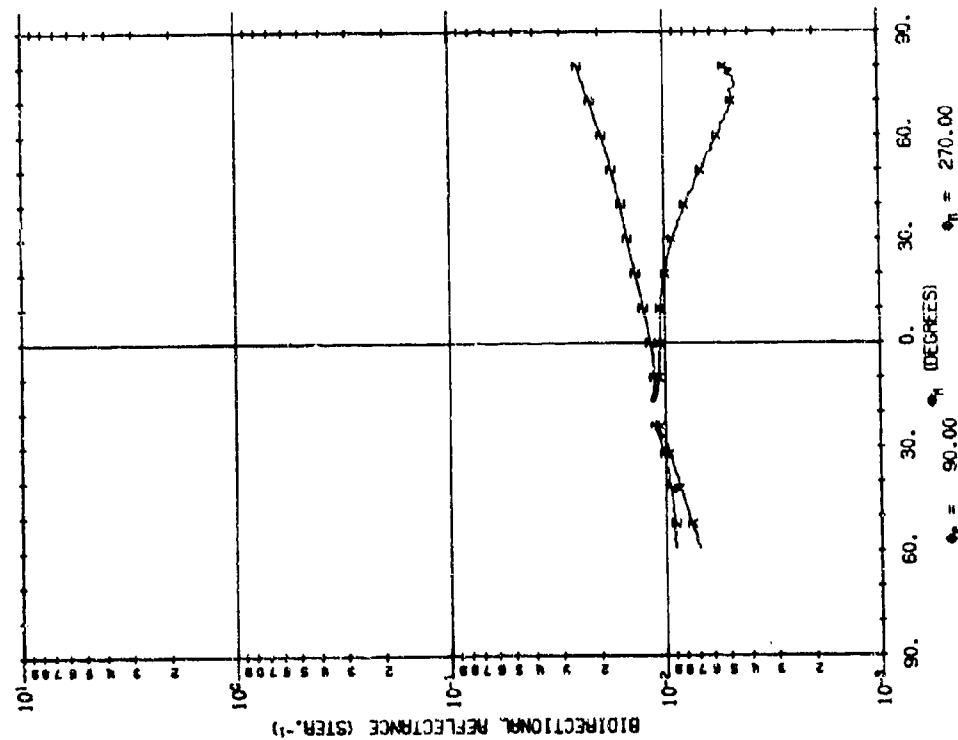


CLOTH AND CANVAS

R01803 101

BLACK CANVAS, 4 PERCENT REFLECTANCE

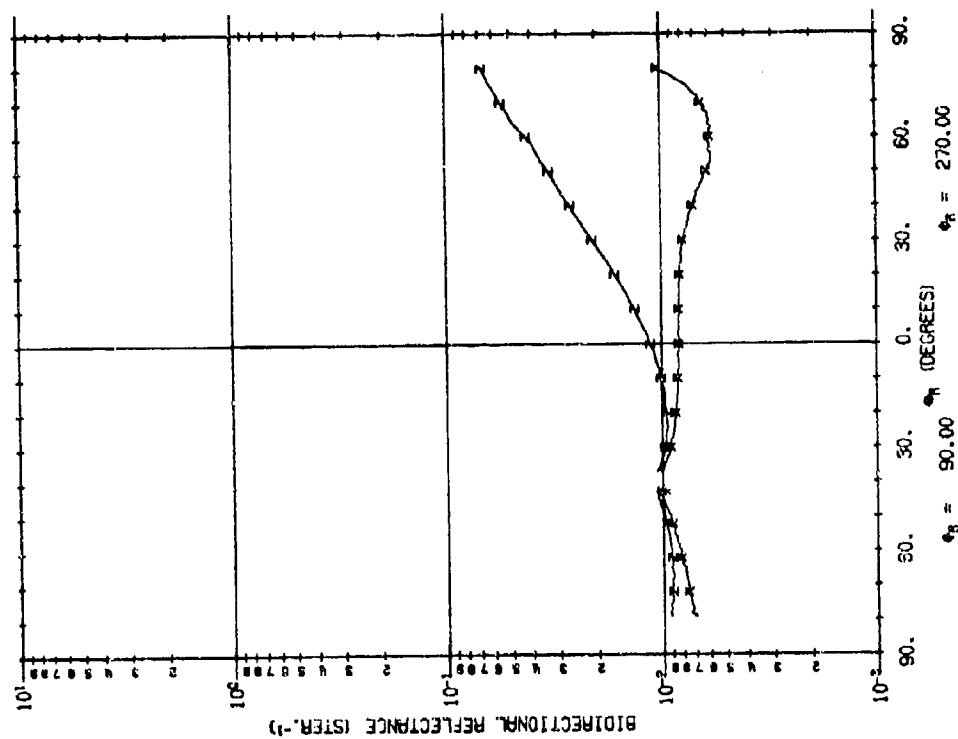
X  $\theta_1 = 90.0$   
Z  $\theta_2 = 90.0$   
 $\lambda = 0.63$



R01803 101

BLACK CANVAS, 4 PERCENT REFLECTANCE

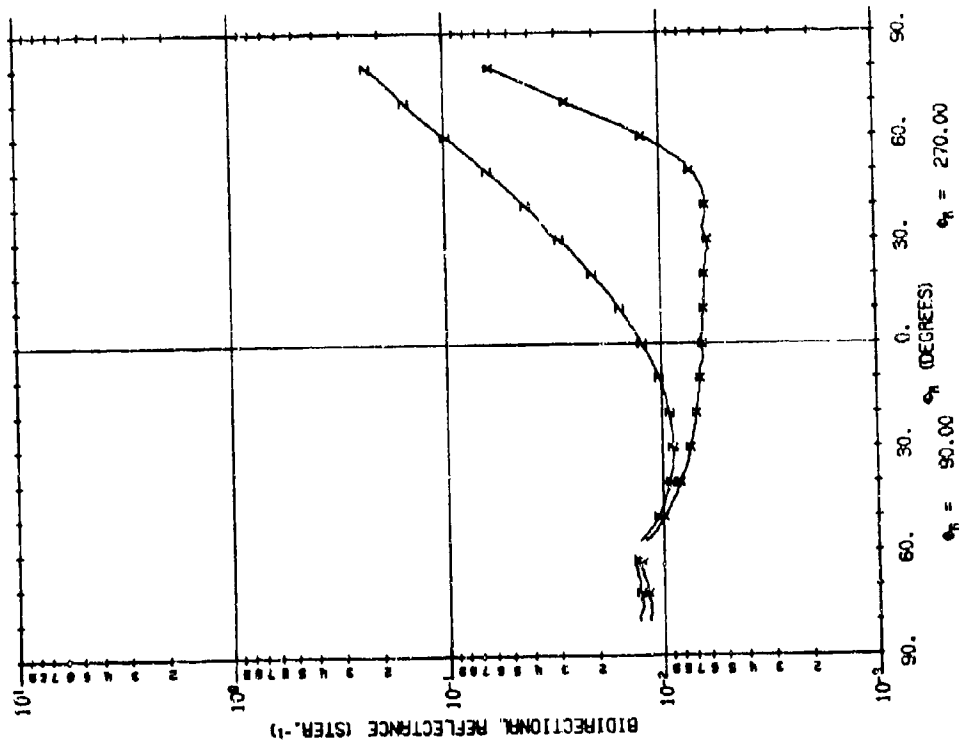
X  $\theta_1 = 40.0$   
Z  $\theta_2 = 90.0$   
 $\lambda = 0.63$



R01803 101

BLACK CANVAS, 4 PERCENT REFLECTANCE

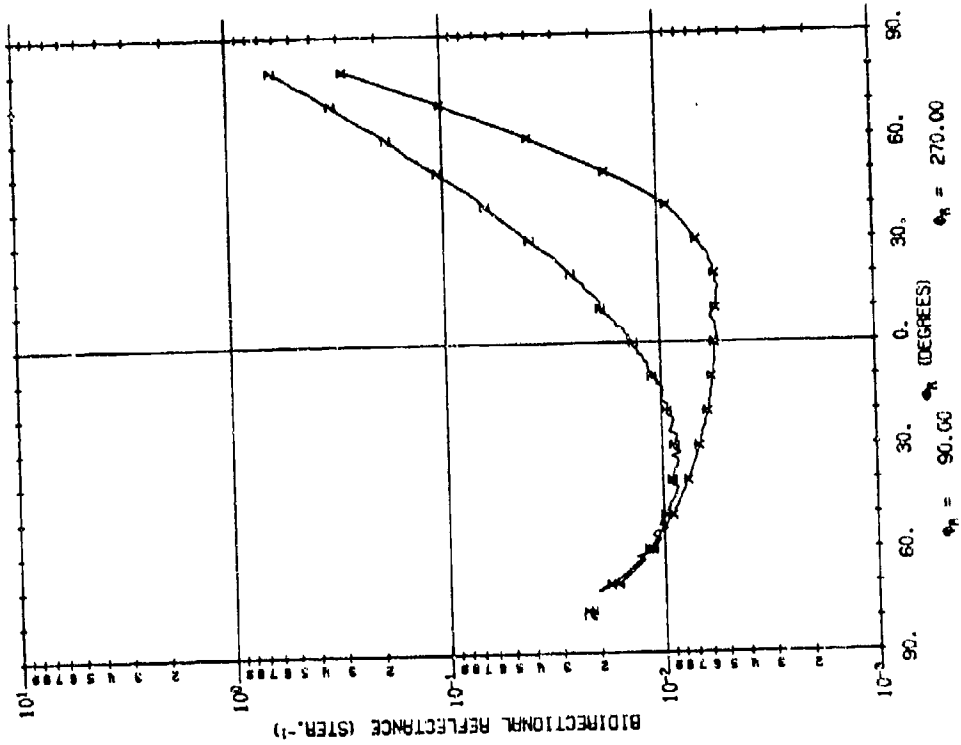
X  $\theta_i = 60.0$   
 Z  $\theta_i = 90.0$   
 $\lambda = 0.63$



R01803 101

BLACK CANVAS, 4 PERCENT REFLECTANCE

X  $\theta_i = 75.0$   
 Z  $\theta_i = 90.0$   
 $\lambda = 0.63$

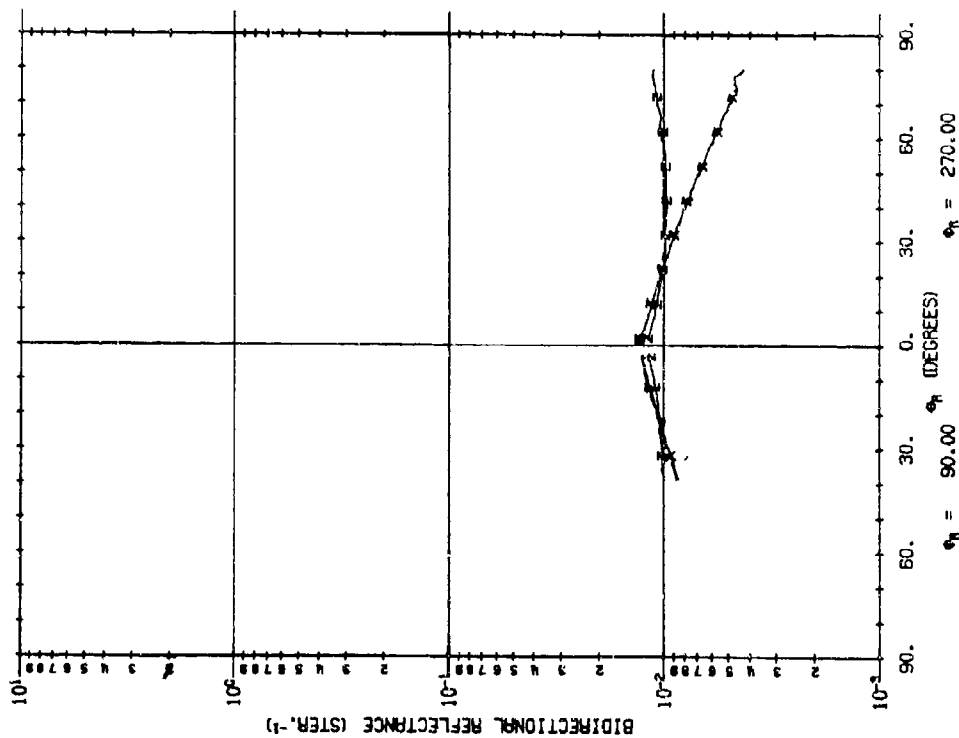


CLOTH AND CANVAS

A01803 101

BLACK CANVAS, 4 PERCENT REFLECTANCE

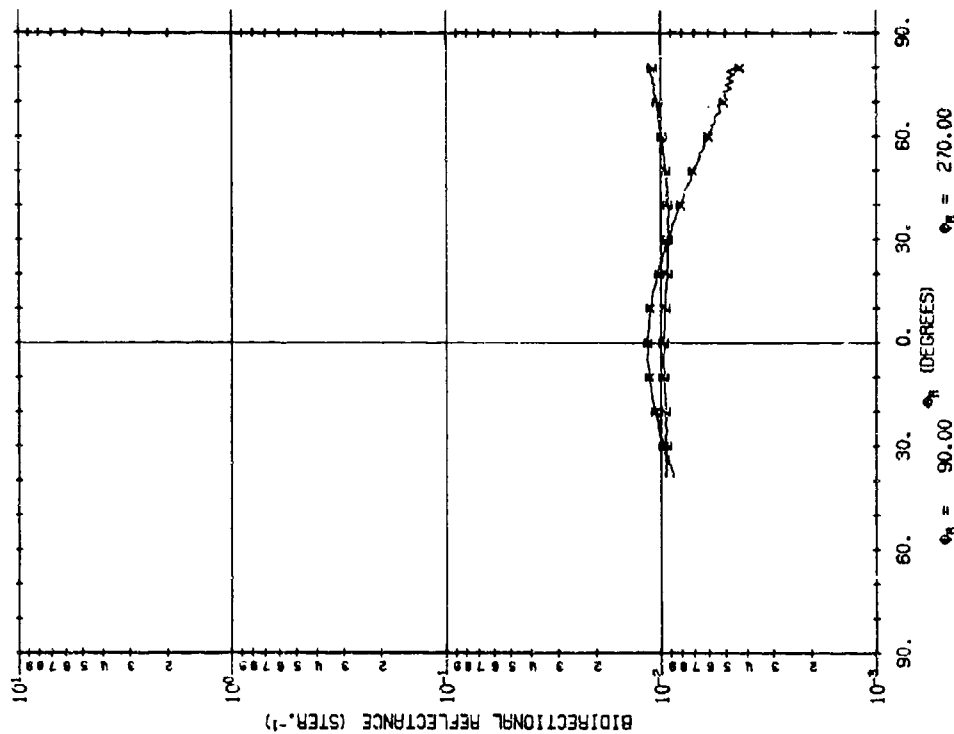
X  $\rho_i = 0.0$   
Z  $\rho_i = 0.0$   
 $\lambda = 0.63$



A01803 101

BLACK CANVAS, 4 PERCENT REFLECTANCE

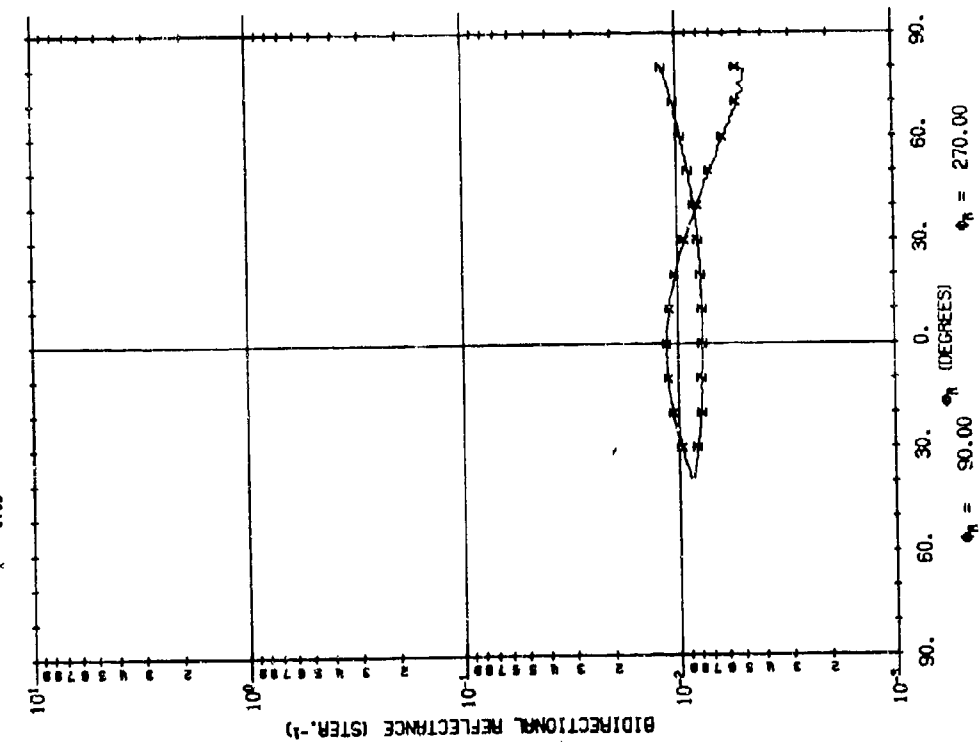
X  $\rho_i = 20.0$   
Z  $\rho_i = 0.0$   
 $\lambda = 0.63$



A01803 101

BLACK CANVAS, 4 PERCENT REFLECTANCE

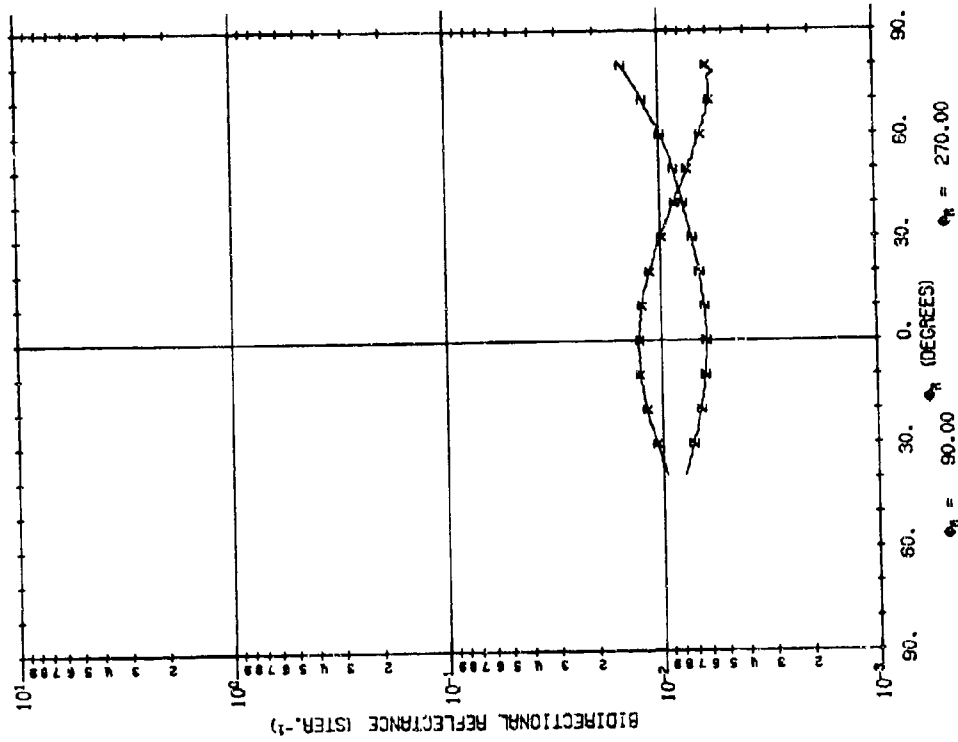
X  $\theta_1 = 40.0$   
Z  $\theta_2 = 0.0$   
 $\lambda = 0.63$



A01803 101

BLACK CANVAS, 4 PERCENT REFLECTANCE

X  $\theta_1 = 60.0$   
Z  $\theta_2 = 0.0$   
 $\lambda = 0.63$

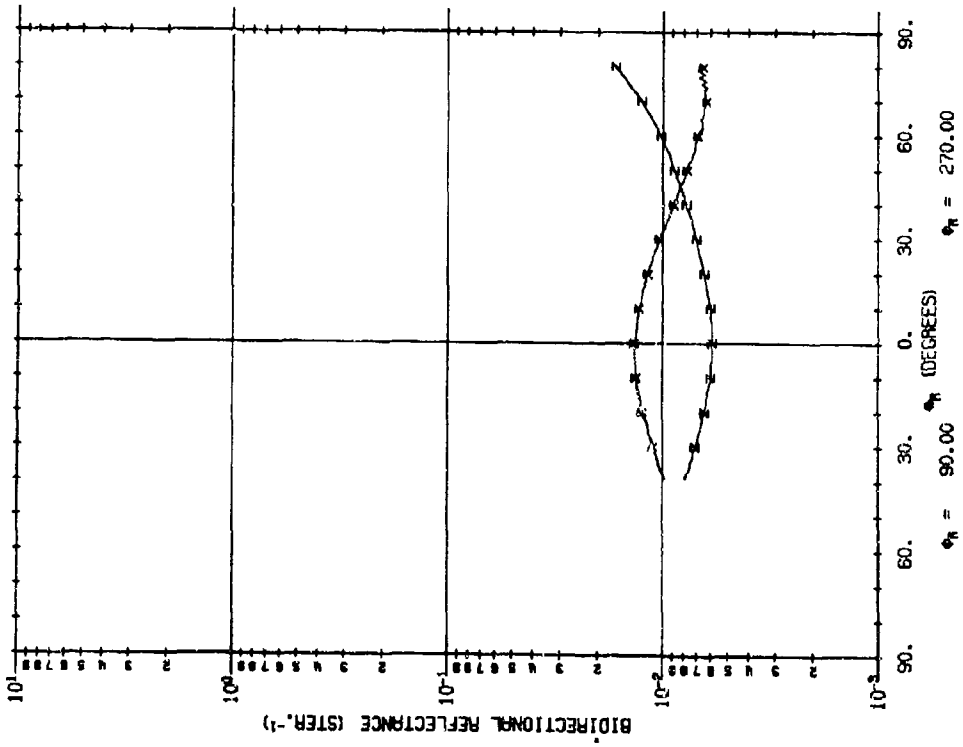


CLOTH AND CANVAS

A01803 101

BLACK CANVAS, 4 PERCENT REFLECTANCE

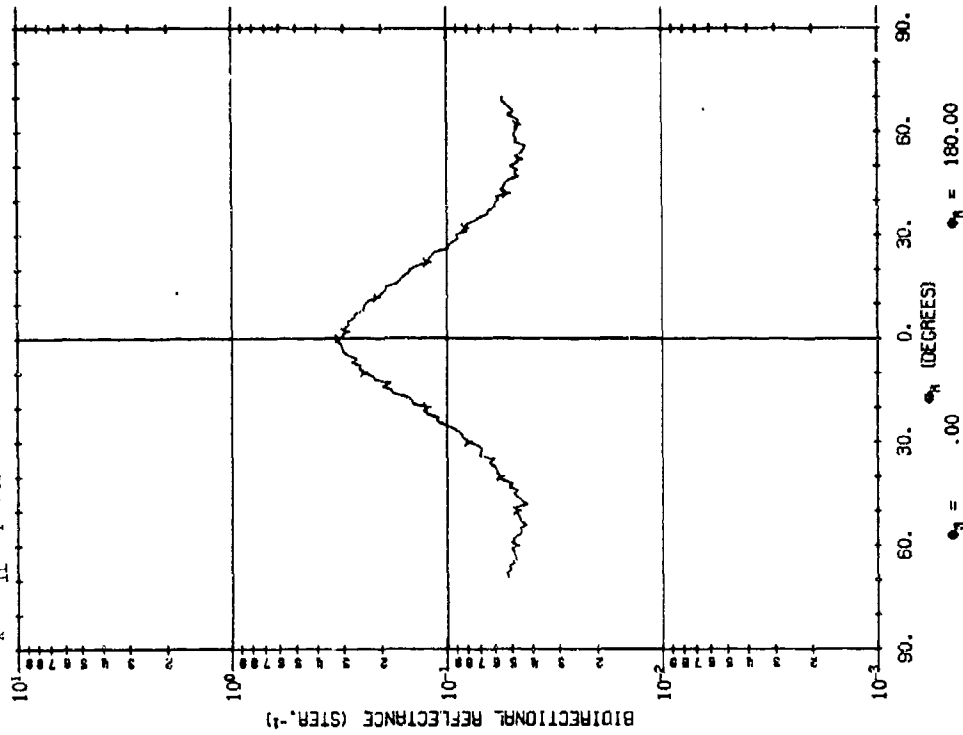
X  $\theta_i = 65.0$   
Z  $\phi_i = 0.0$   
 $\lambda = 0.63$

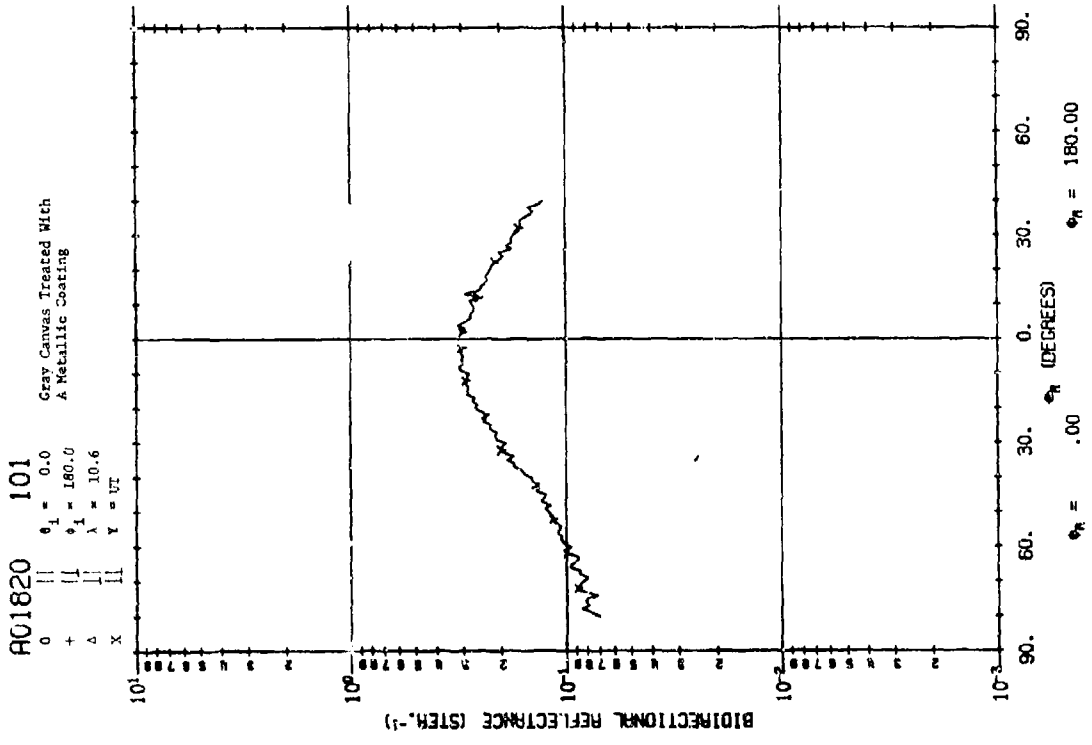
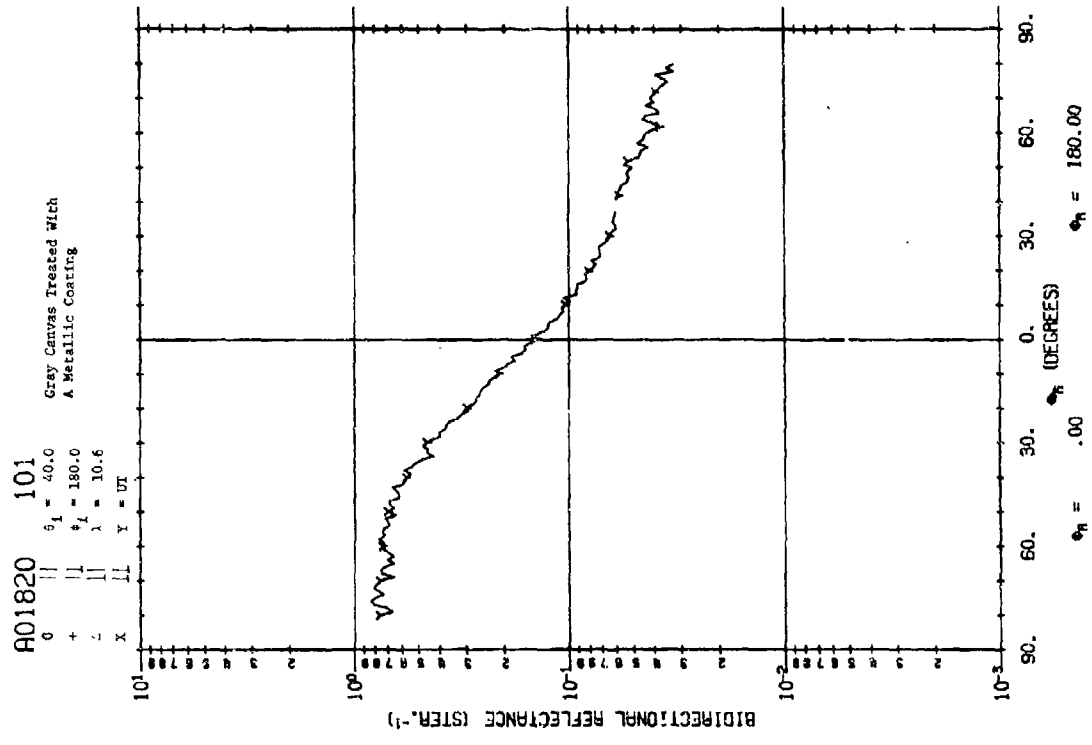


A01820 101

Gray Canvas Treated With  
A Metallic Coating

0  $2\theta = 2.0$   
+  $\phi_i = \phi_r$   
Z  $\lambda = 10.6$   
X  $\gamma = 0^\circ$



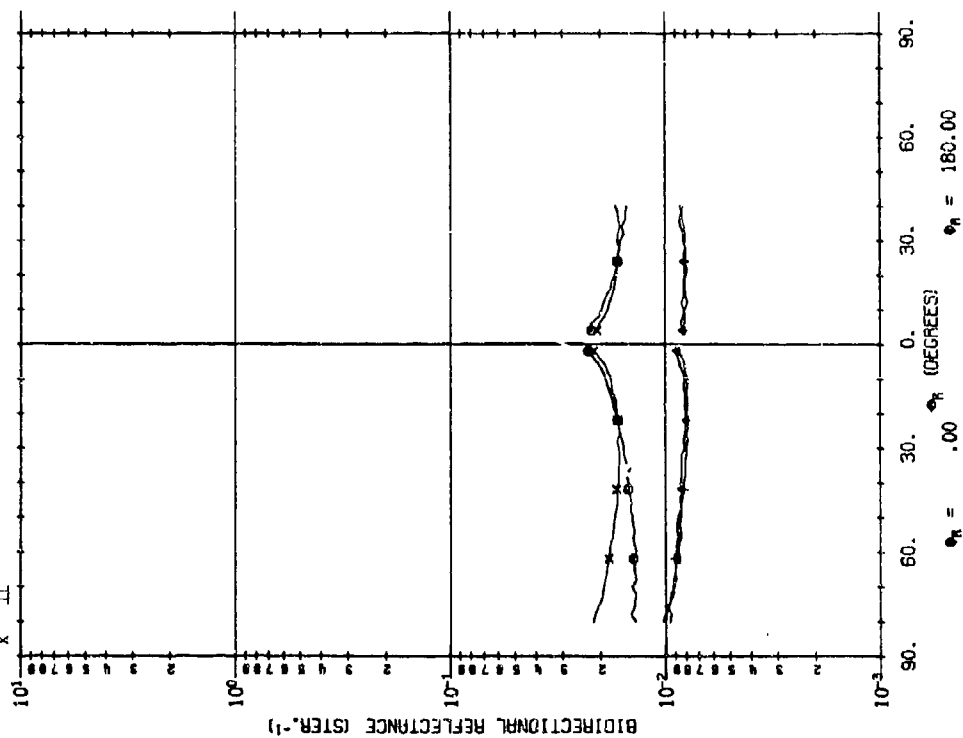


# CLOTH AND CANVAS

R01853 301

OLIVE DRAB CANVAS

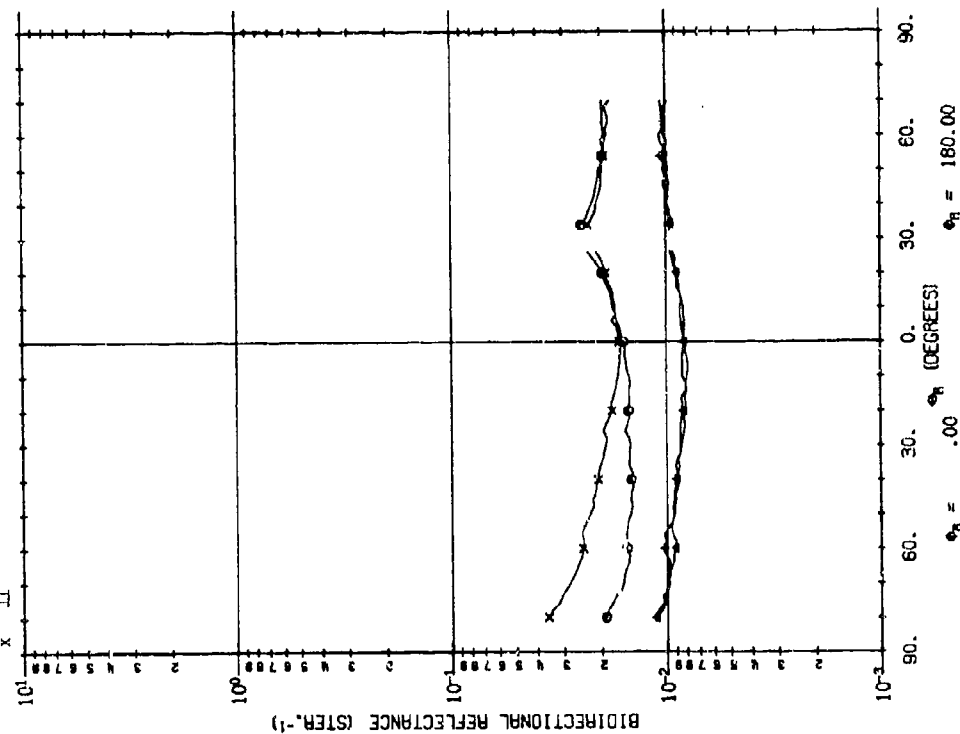
0  $\theta_i = 0.0$   
 +  $\theta_i = 180.0$   
 Δ  $\lambda = 1.06$   
 x  $\lambda = 1.06$



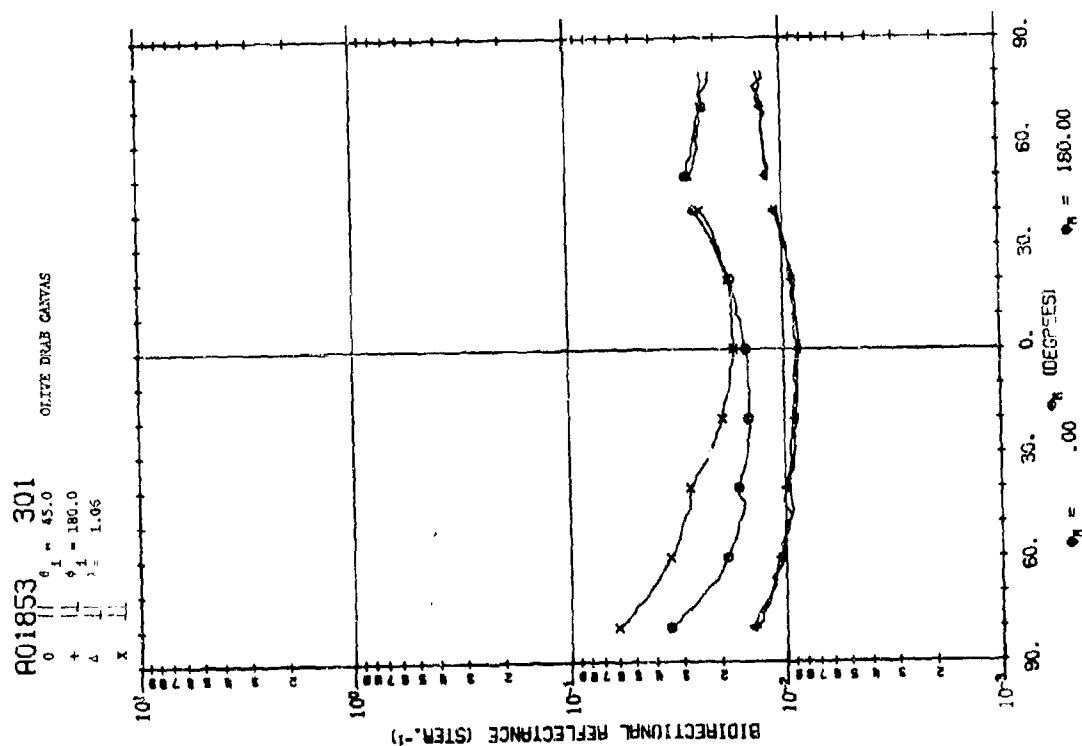
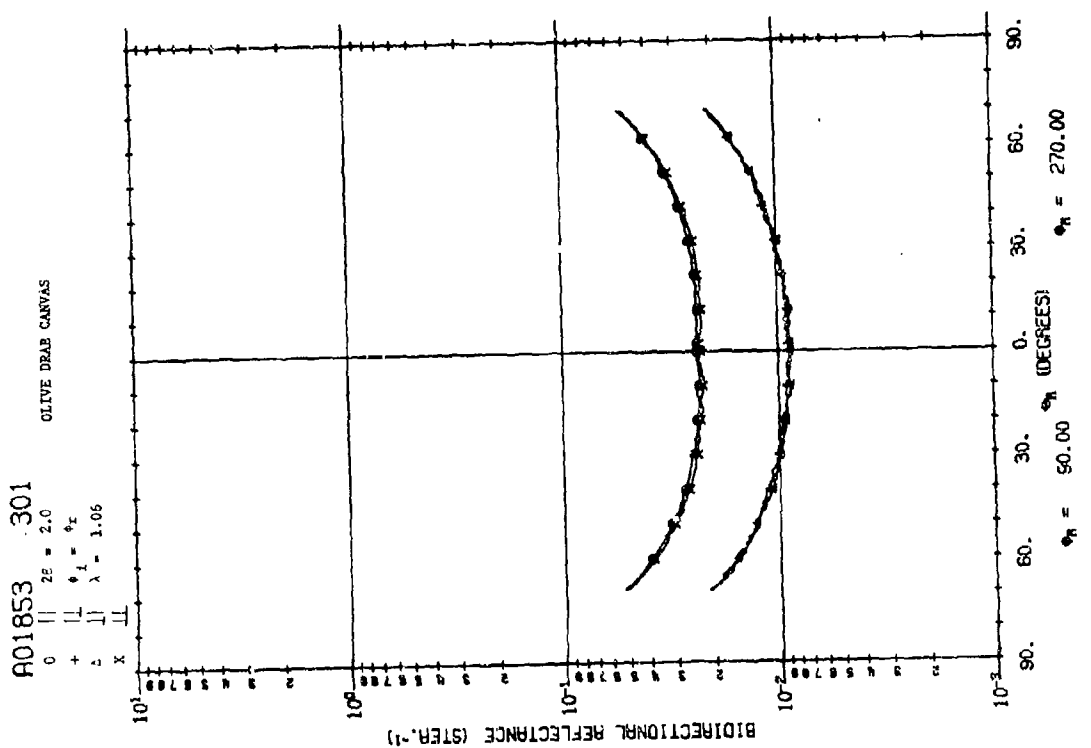
R01853 301

OLIVE DRAB CANVAS

0  $\theta_i = 30.0$   
 +  $\theta_i = 180.0$   
 Δ  $\lambda = 1.06$   
 x  $\lambda = 1.06$





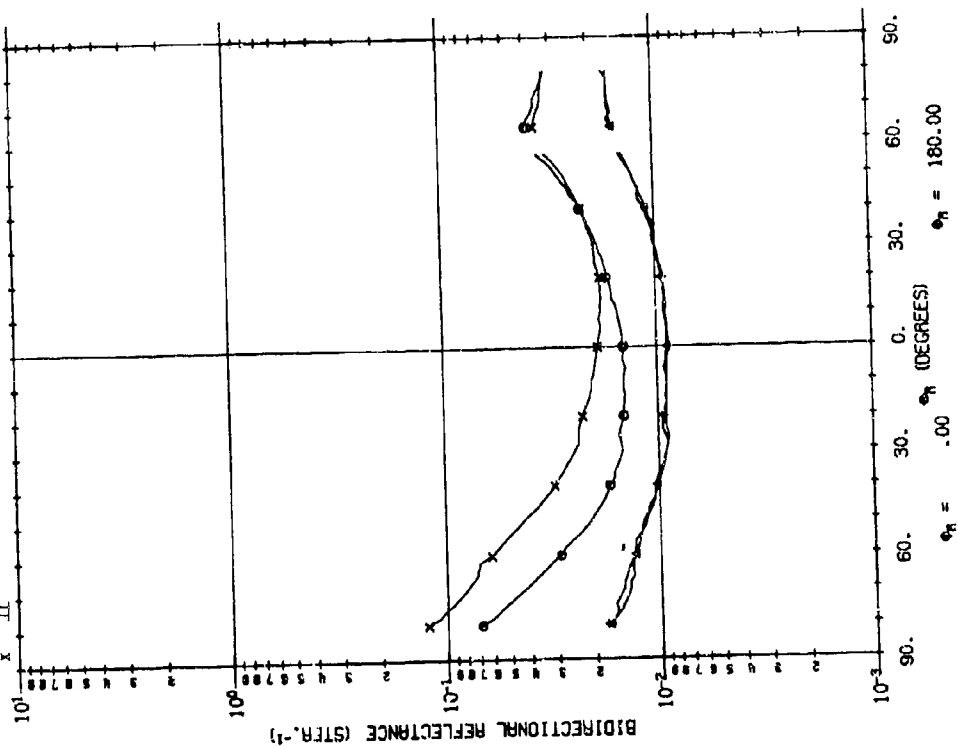


CLOTH AND CANVAS

R01853 301

OLIVE DRAB CANVAS

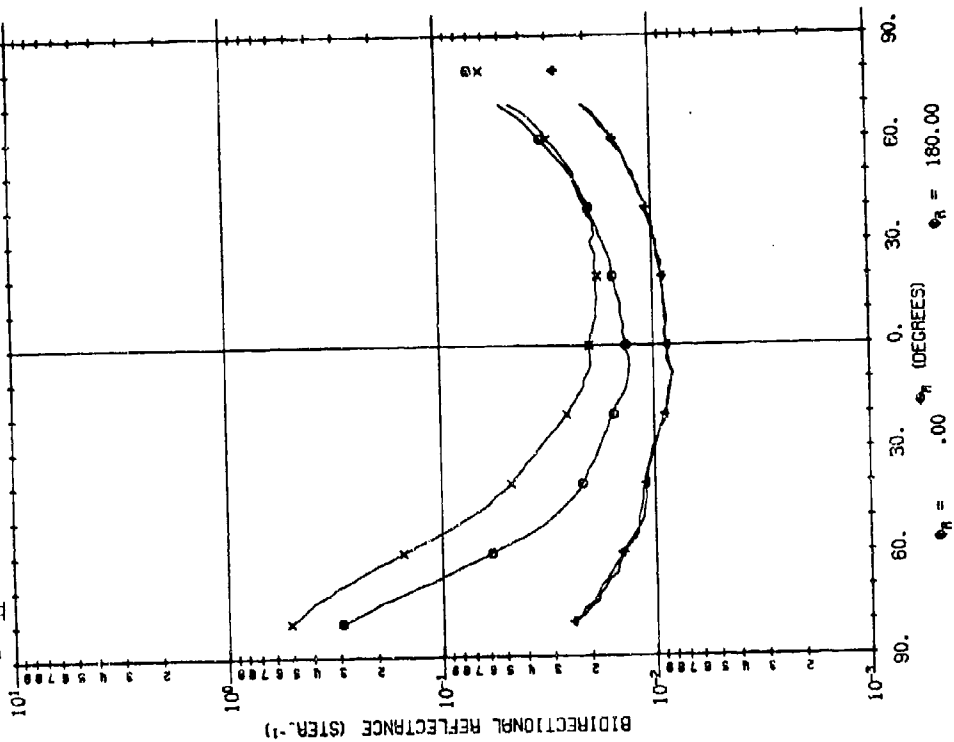
0 ||  $\theta_1 = 60.0$   
 + ||  $\theta_2 = 180.0$   
 A ||  $\lambda = 1.06$



R01853 301

OLIVE DRAB CANVAS

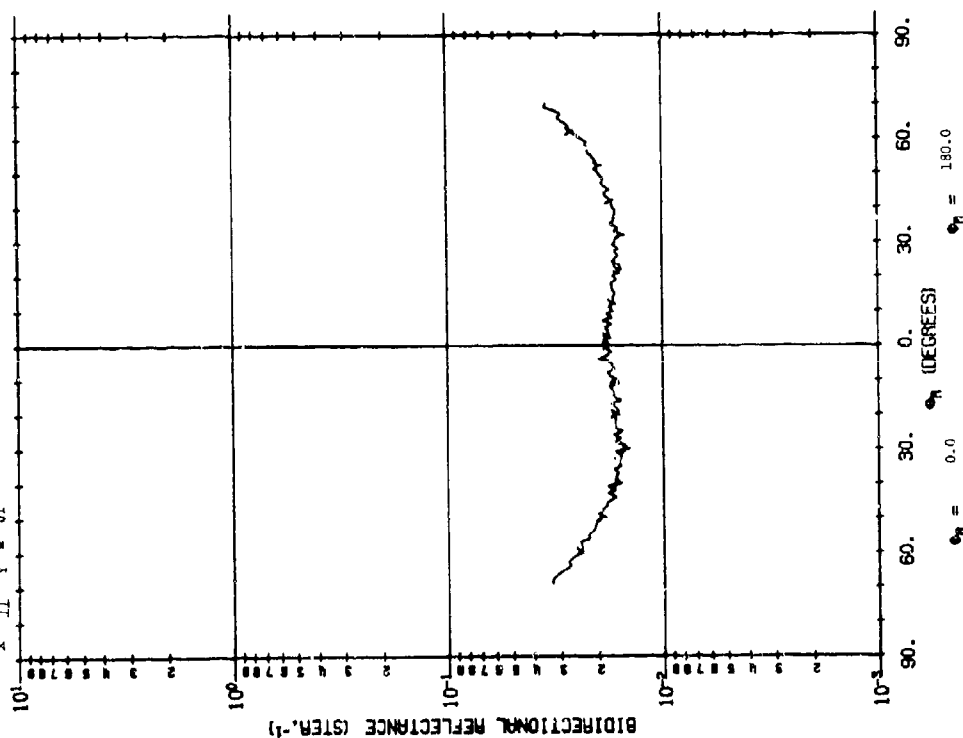
0 ||  $\theta_1 = 75.0$   
 + ||  $\theta_2 = 180.0$   
 A ||  $\lambda = 1.06$



A01890 101

Olive Drab Canvas

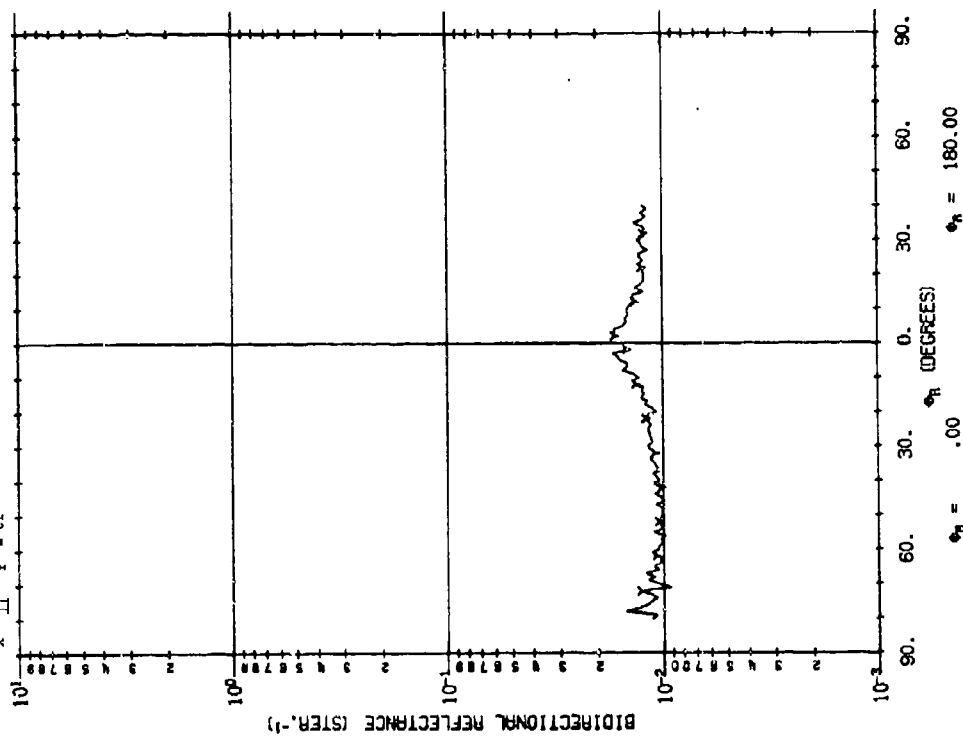
0 ||  $2\theta = 2.0$   
 + ||  $\theta_1 = \theta_r$   
 Δ ||  $\lambda = 10.6$   
 X || Y = VT



A01890 101

Olive Drab Canvas

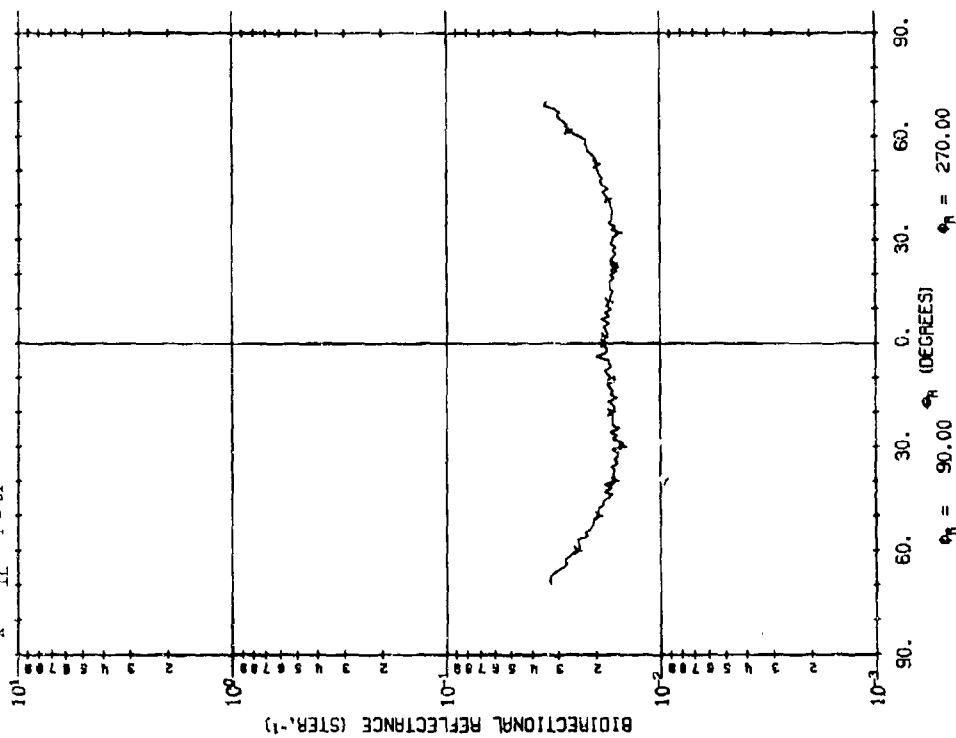
0 ||  $\theta_1 = 0.0$   
 + ||  $\theta_r = 180.0$   
 Δ ||  $\lambda = 10.6$   
 X || Y = VT



CLOTH AND CANVAS

R01890 101  
OLIVE DRAB CANVAS

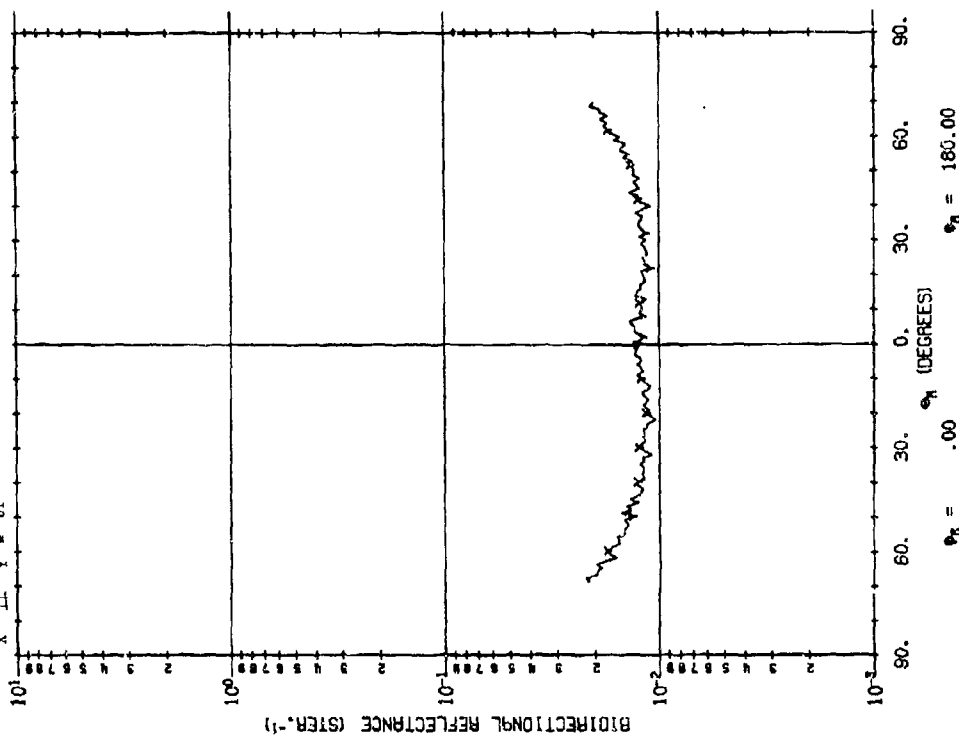
0 ||  $2\epsilon = 2.0$   
+ ||  $\phi_1 = \phi_2$   
 $\Delta$  ||  $\lambda = 10.5$   
X ||  $Y = UT$



$\phi_h = 90.00$   $\phi_h = 270.00$

R01891 101  
Vinyl Coated Olive Drab Canvas

0 ||  $2\epsilon = 2.0$   
+ ||  $\phi_1 = \phi_2$   
 $\Delta$  ||  $\lambda = 10.6$   
X ||  $Y = UT$

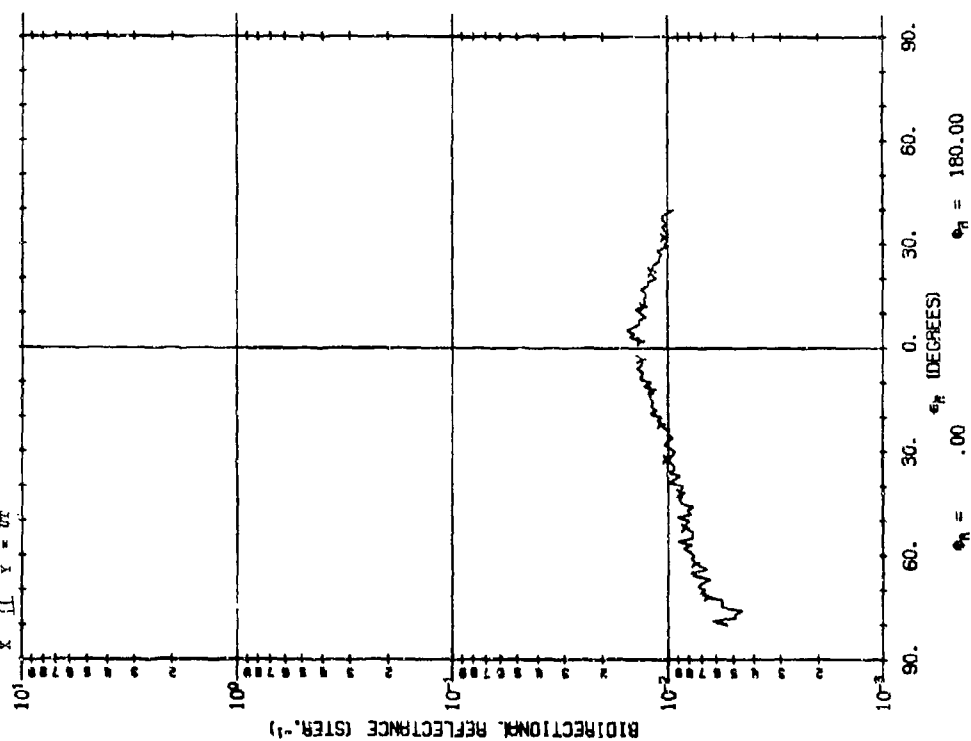


$\phi_h = .00$   $\phi_h = 180.00$

AC1891 101

Vinyl Coated Olive Drab Canvas

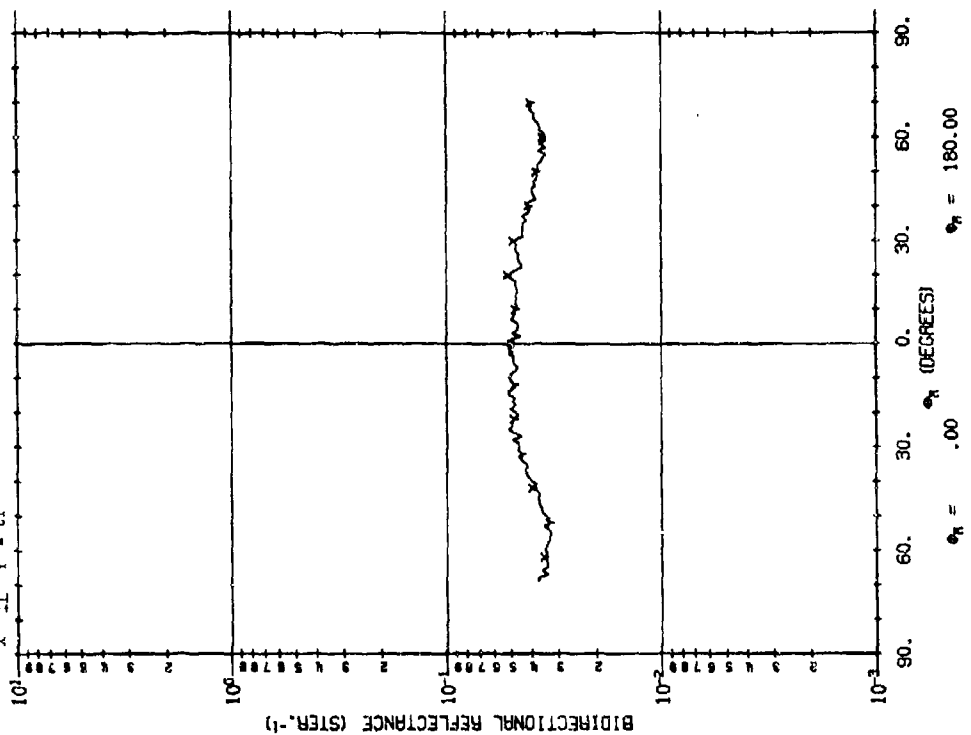
0 //  $\epsilon_1 = 0.0$   
 + //  $\epsilon_2 = 180.0$   
 $\lambda = 10.6$   
 X // Y = UT



AC1893 101

Olive Drab Canvas

0 //  $\epsilon_1 = 2.0$   
 + //  $\epsilon_2 = \epsilon_1$   
 $\lambda = 10.6$   
 X // Y = UT

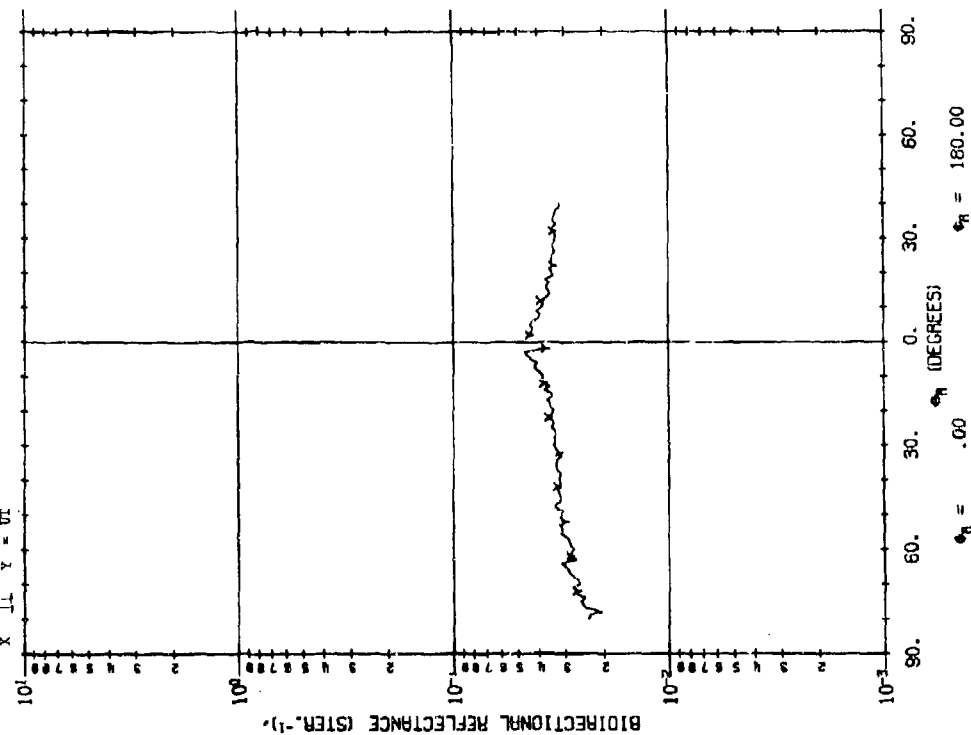


## CLOTH AND CANVAS

R01893 101

Olive Drab Paint on Aluminum

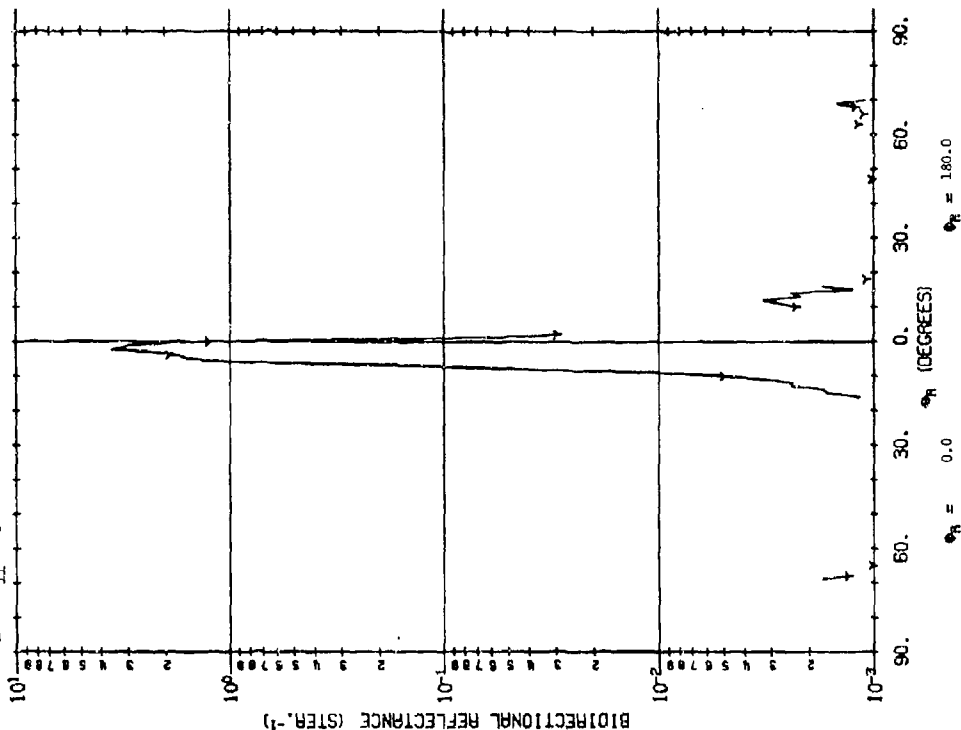
0  $\theta_i = 0.0$   
 +  $\theta_t = 180.0$   
 $\Delta$   $\lambda = 10.6$   
 X  $Y = UT$



R01900 101

Vinyl Coated Olive Drab Canvas

0  $25 = 2.0$   
 +  $\theta_i = 0.0$   
 $\Delta$   $\lambda = 10.6$   
 X  $Y = UT$

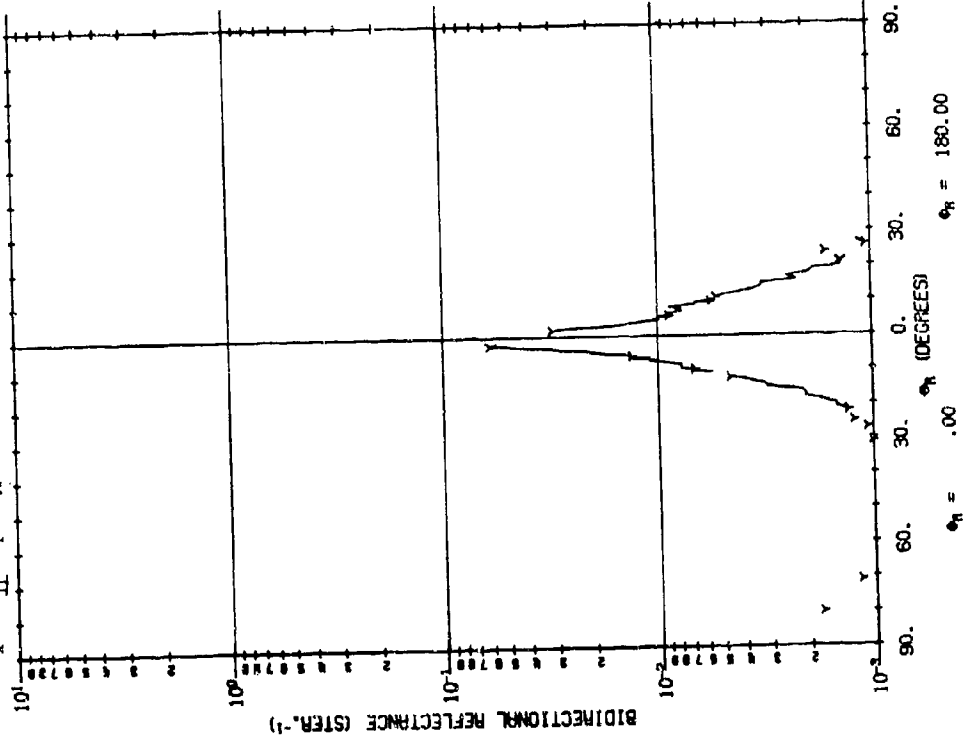


R01900 101

Viny. Coated Olive Drab Canvas

$\theta_i = 0.0$   
 $\theta_f = 180.0$   
 $\lambda = 10.6$   
 $\gamma = 97$

0  
 +  
 Δ  
 X

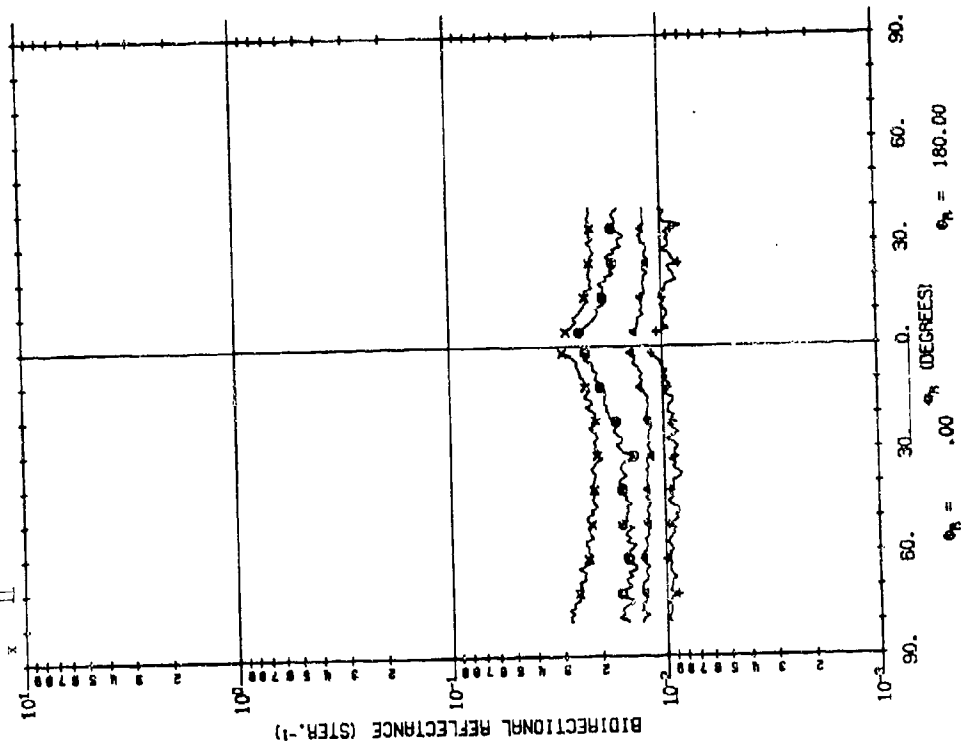


R01918 101

Black Canvas

$\theta_i = 0.0$   
 $\theta_f = 180.0$   
 $\lambda = 1.06$

0  
 +  
 Δ  
 X



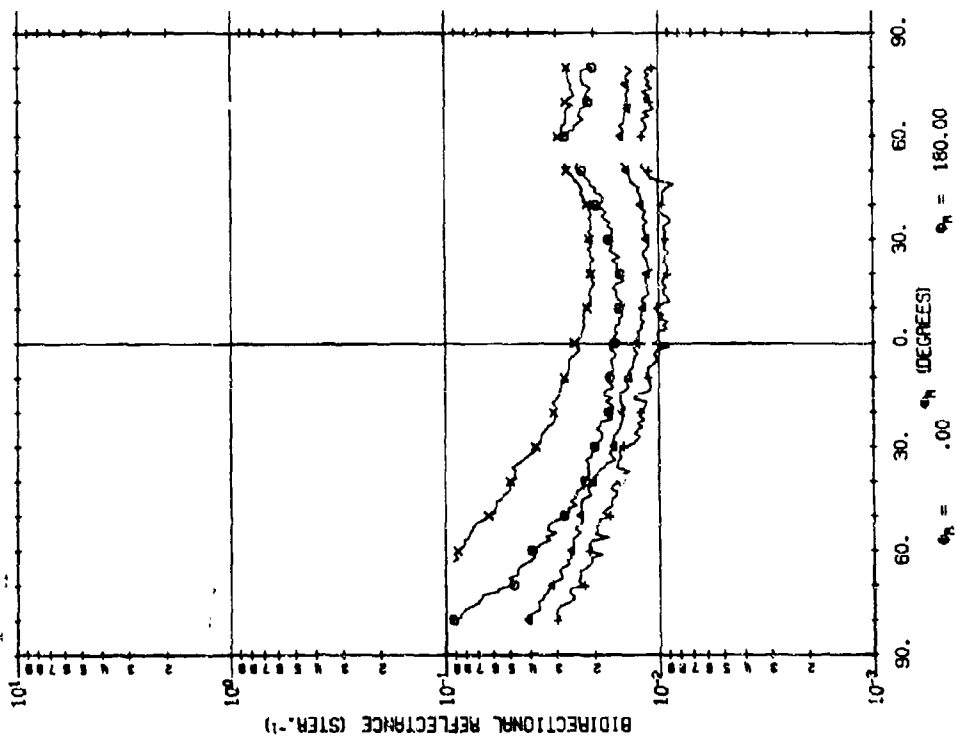
CLOTH AND CANVAS

R01918 101

Black Canvas

$\theta_i = 56.0$   
 $\phi_i = 180.0$   
 $\lambda = 1.06$

0  
 +  
 x

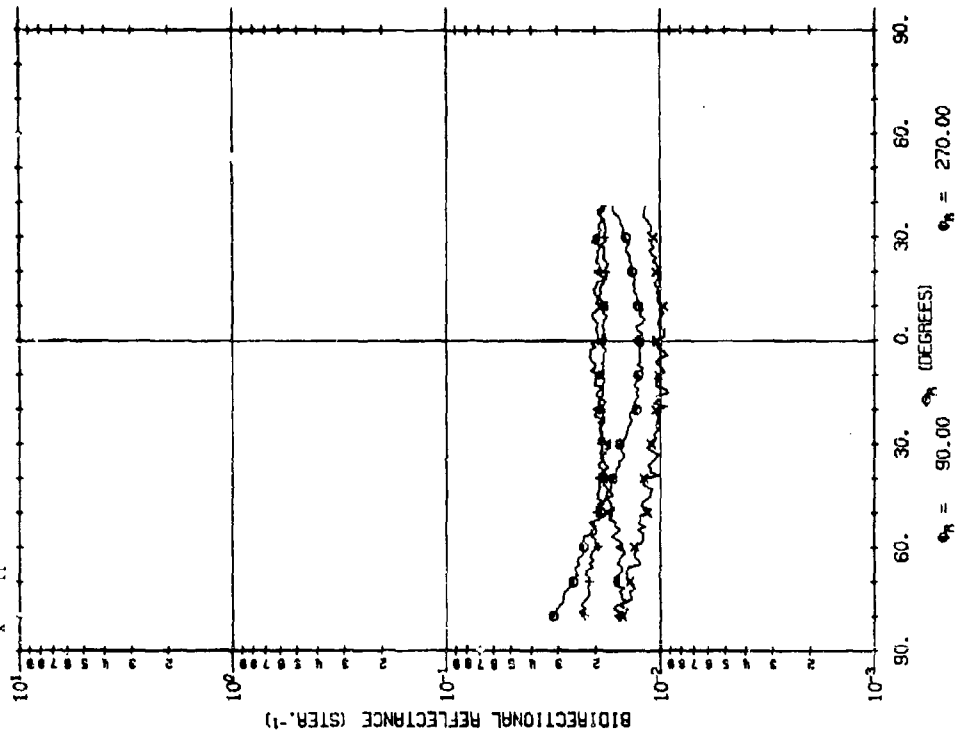


R01918 101

Black Canvas

$\theta_i = 56.0$   
 $\phi_i = 180.0$   
 $\lambda = 1.06$

0  
 +  
 x

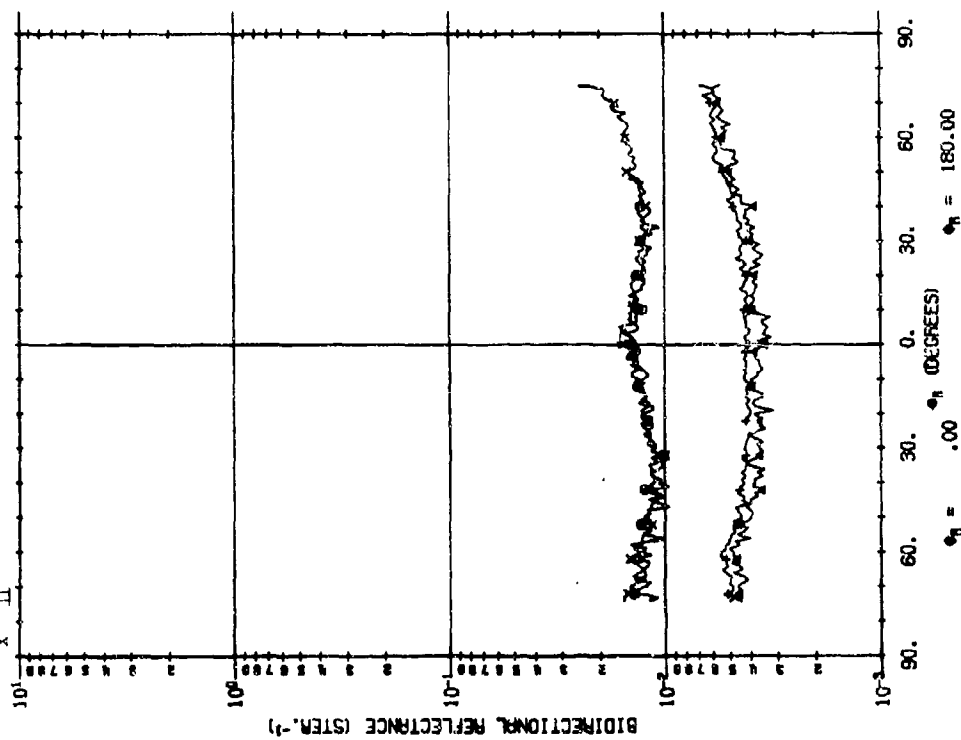




A01919 201

BLACK CANVAS

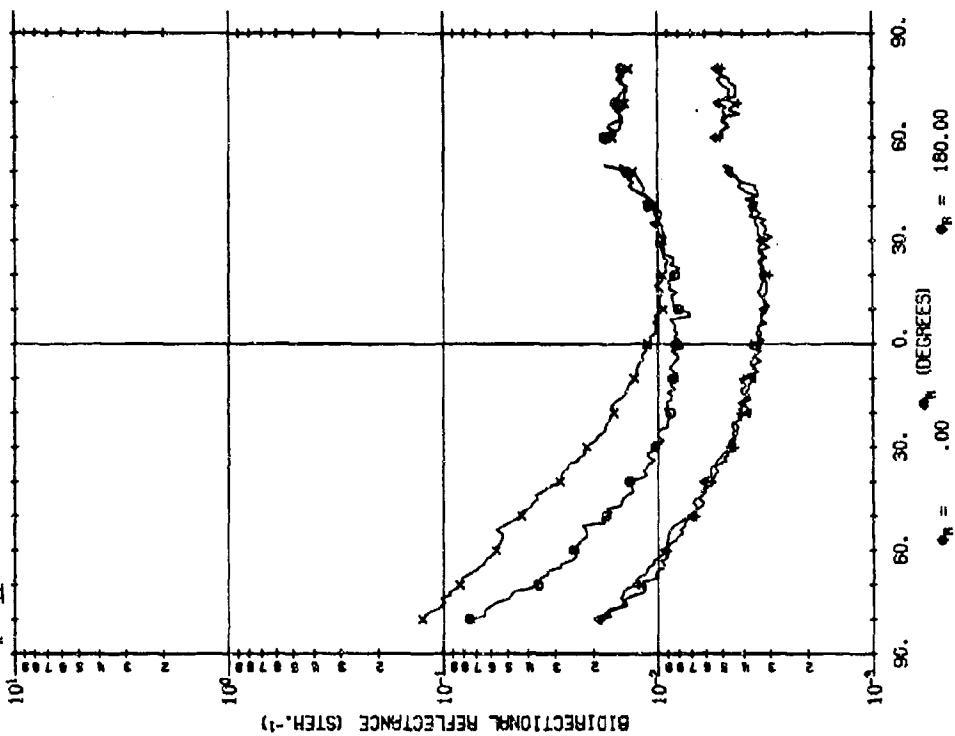
0 || 28 = 2.0  
+ ||  $\phi_1 = \phi_r$   
Δ ||  $\lambda = 1.06$   
x ||



A01919 201

BLACK CANVAS

0 ||  $\phi_1 = 56.0$   
+ ||  $\phi_1 = 180.0$   
Δ ||  $\lambda = 1.06$   
x ||

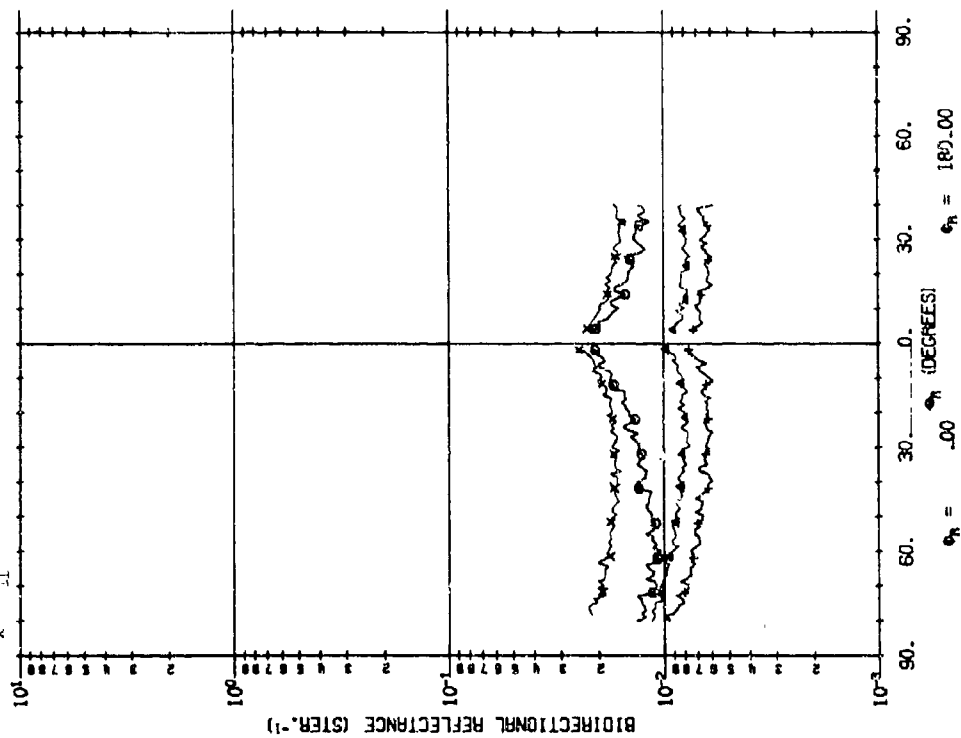


CLOTH AND CANVAS

R02002 101  
 0 11 11  
 + 11 11  
 Δ 11 11  
 X 11 11

$\theta_1 = 0.0$   
 $\phi_1 = 180.0$   
 $\lambda = 1.06$

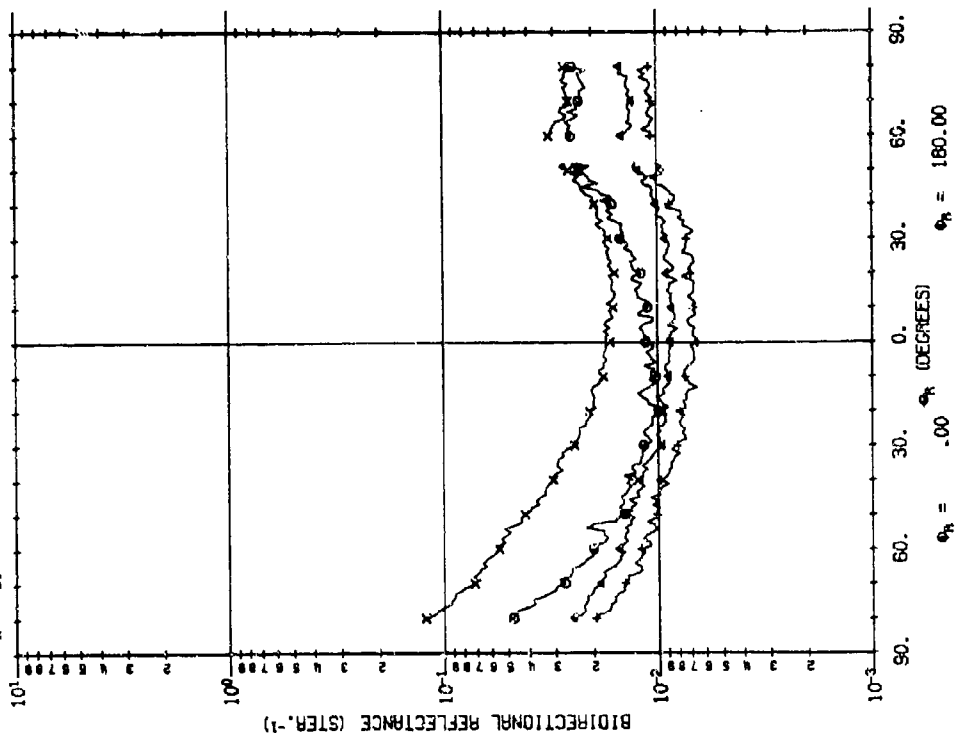
Olive Drab Canvases



R02002 101  
 0 11 11  
 + 11 11  
 Δ 11 11  
 X 11 11

$\theta_1 = 56.0$   
 $\phi_1 = 180.0$   
 $\lambda = 1.06$

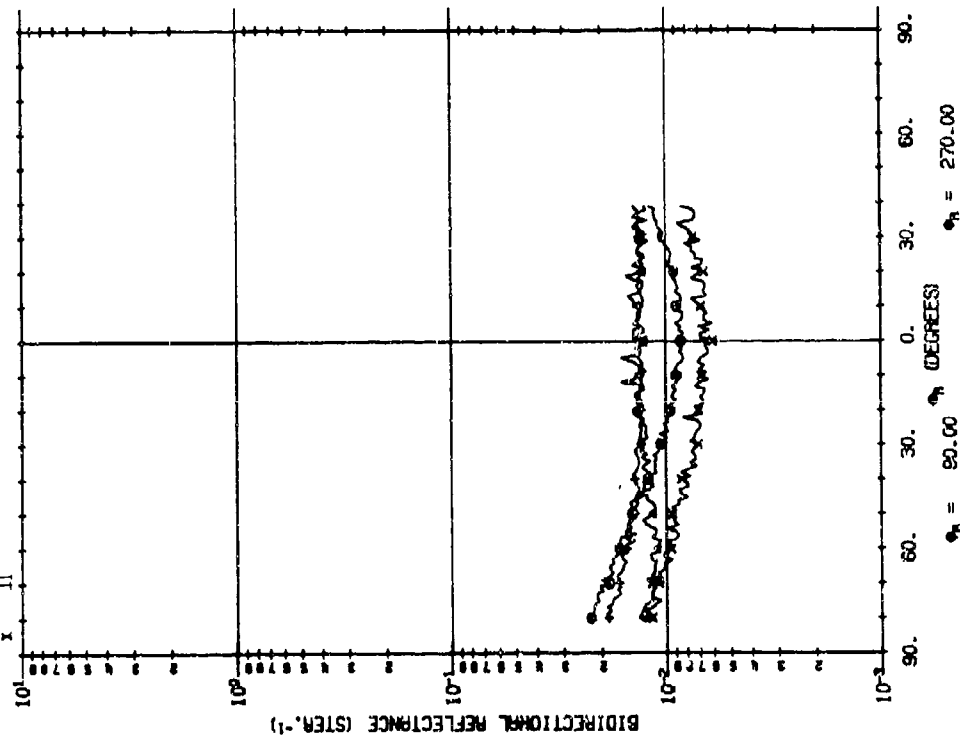
Olive Drab Canvases



A02002 101

Olive Drab Canvas

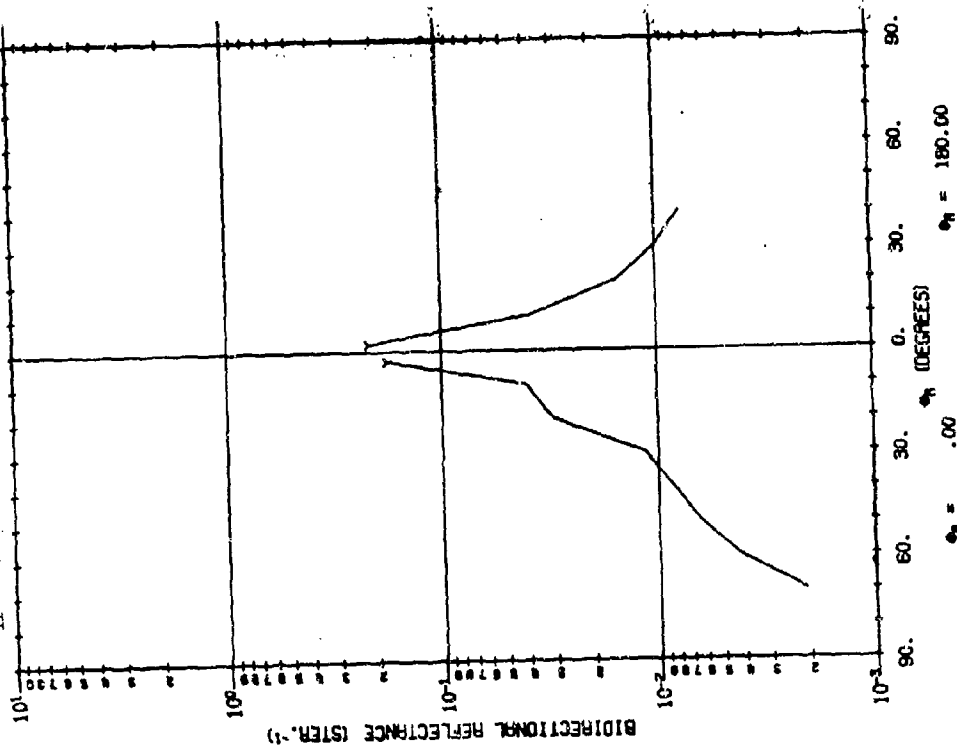
$\theta_i = 56.0$   
 $\phi_i = 180.0$   
 $\lambda = 1.06$



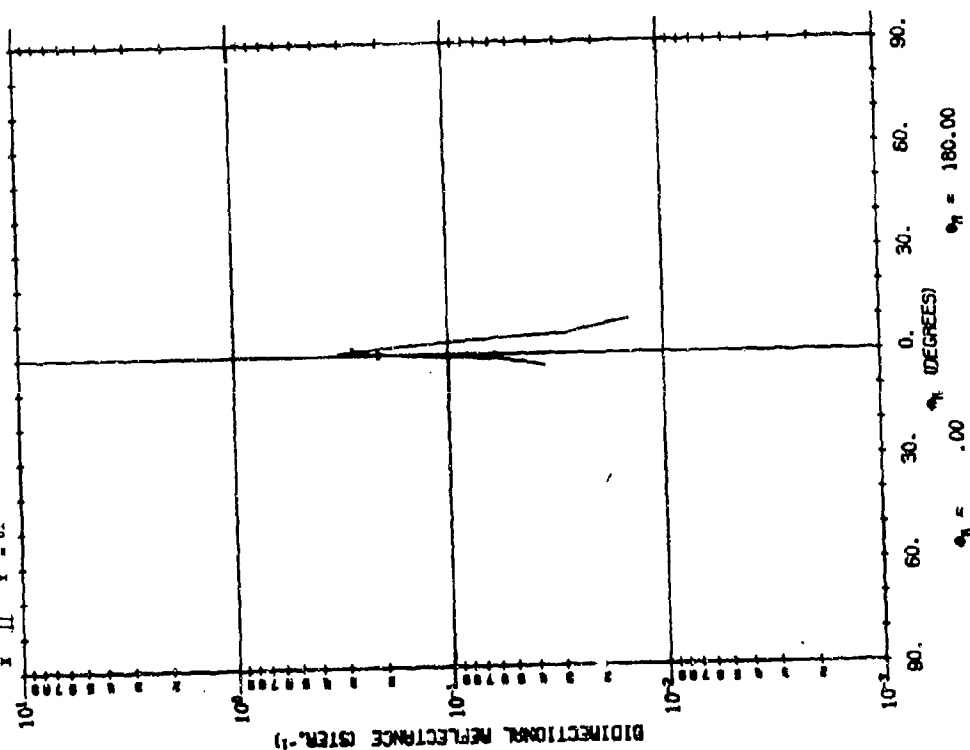
CLOTH AND CANVAS

WOOD

A00096 004 Redwood Block  
 $\theta_1 = 0.0$   
 $\phi_1 = 180.0$   
 $\lambda = 10.6$   
 $\chi = 0.0$



A00096 004 Redwood Block  
 $\theta_1 = 1.10$   
 $\phi_1 = 0.0$   
 $\lambda = 10.6$   
 $\chi = 0.0$

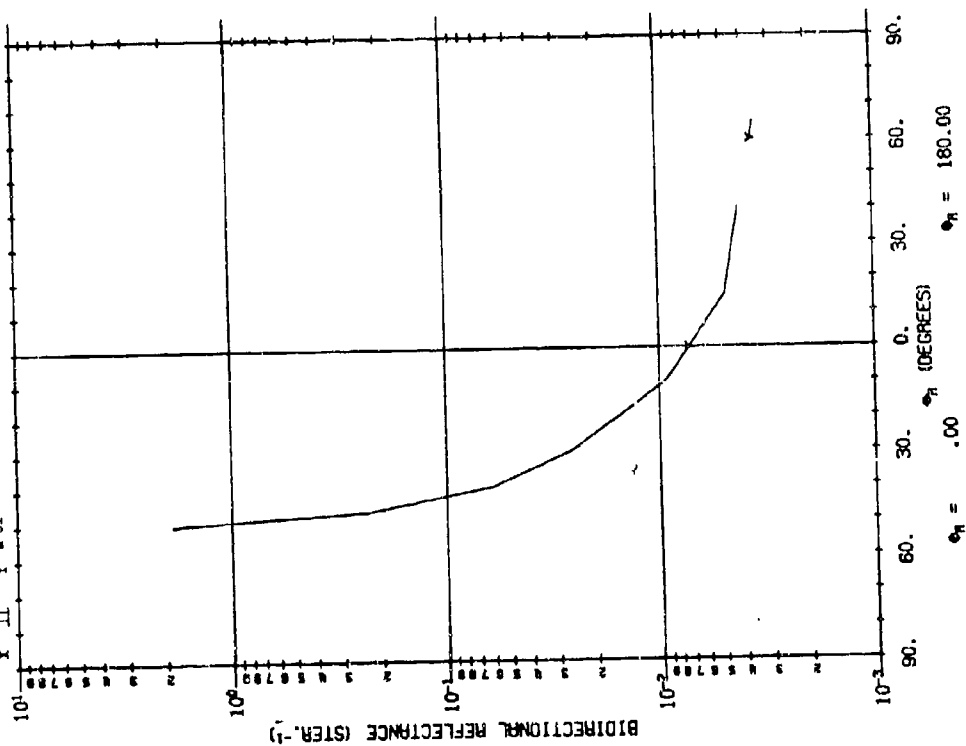


WOOD

A00096 004

Redwood Block

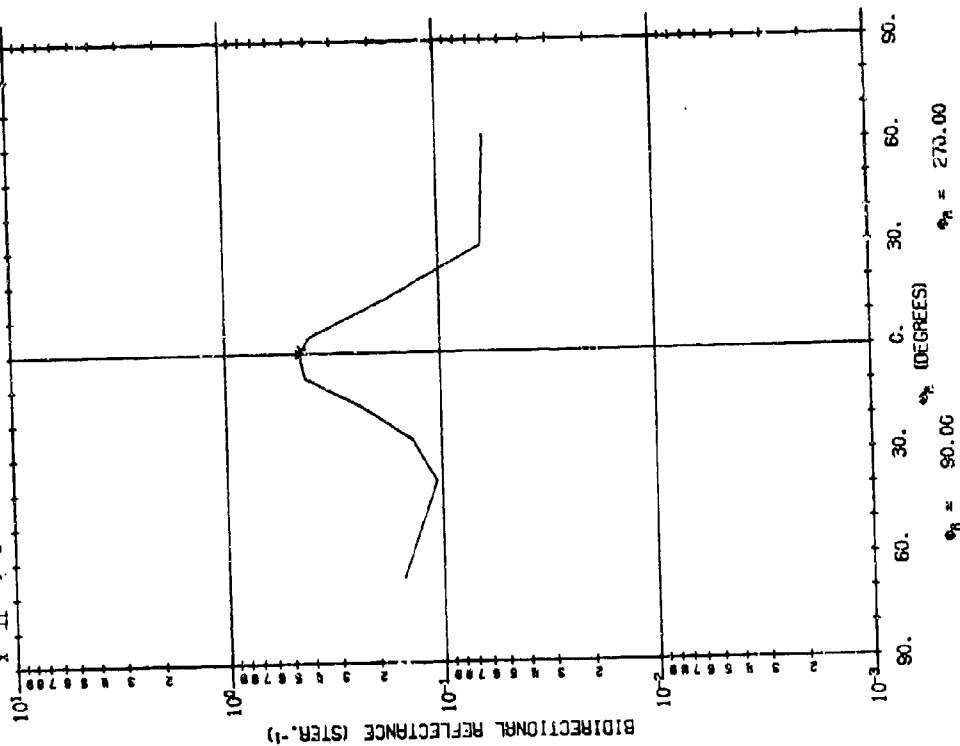
0 ||  $\phi_1 = 50.0$   
 + ||  $\phi_2 = 180.0$   
 Δ ||  $\lambda = 10.6$   
 X || Y = UT



A00096 004

Redwood Block

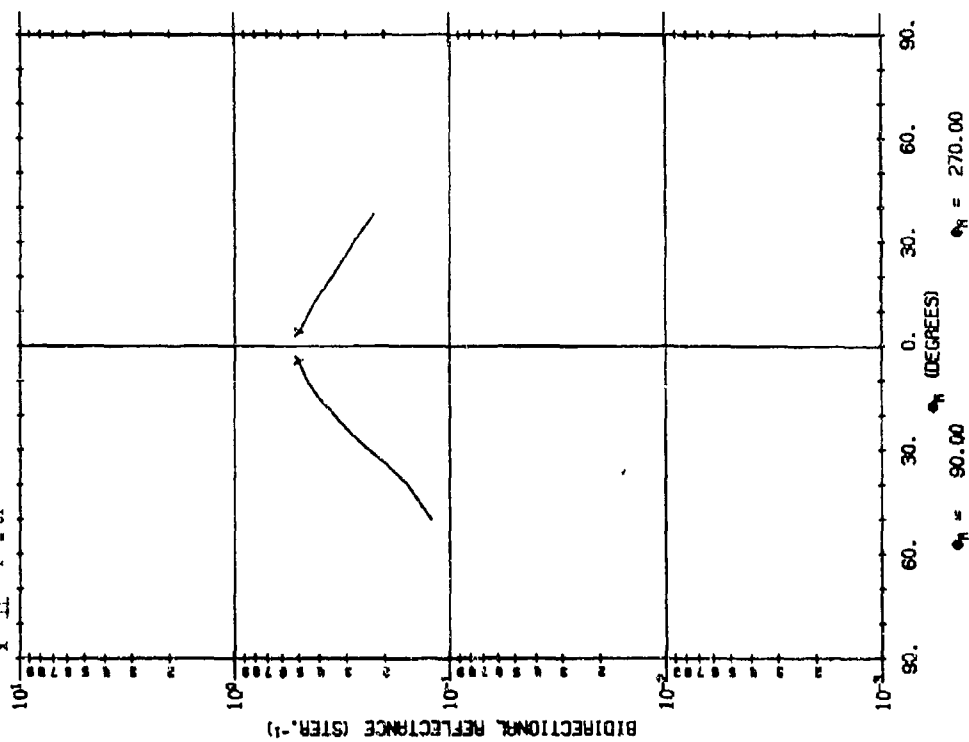
0 ||  $2\theta = 1.10$   
 + ||  $\phi_2 = \phi_1$   
 Δ ||  $\lambda = 10.6$   
 X || Y = UT



R00096 004

Redwood Block

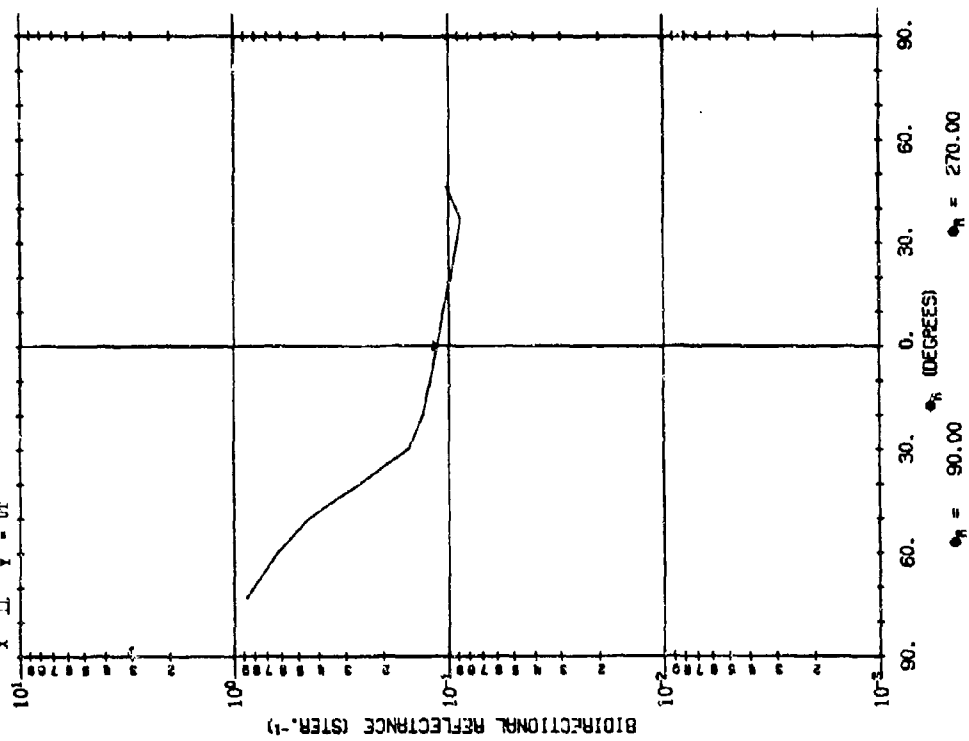
0 ||  $\phi_i = 0.0$   
 + ||  $\phi_i = 270.0$   
 Δ ||  $\lambda = 10.6$   
 X ||  $\gamma = 0.1$



R00095 004

Redwood Block

0 ||  $\phi_i = 50.0$   
 + ||  $\phi_i = 270.0$   
 Δ ||  $\lambda = 10.6$   
 X ||  $\gamma = 0.1$

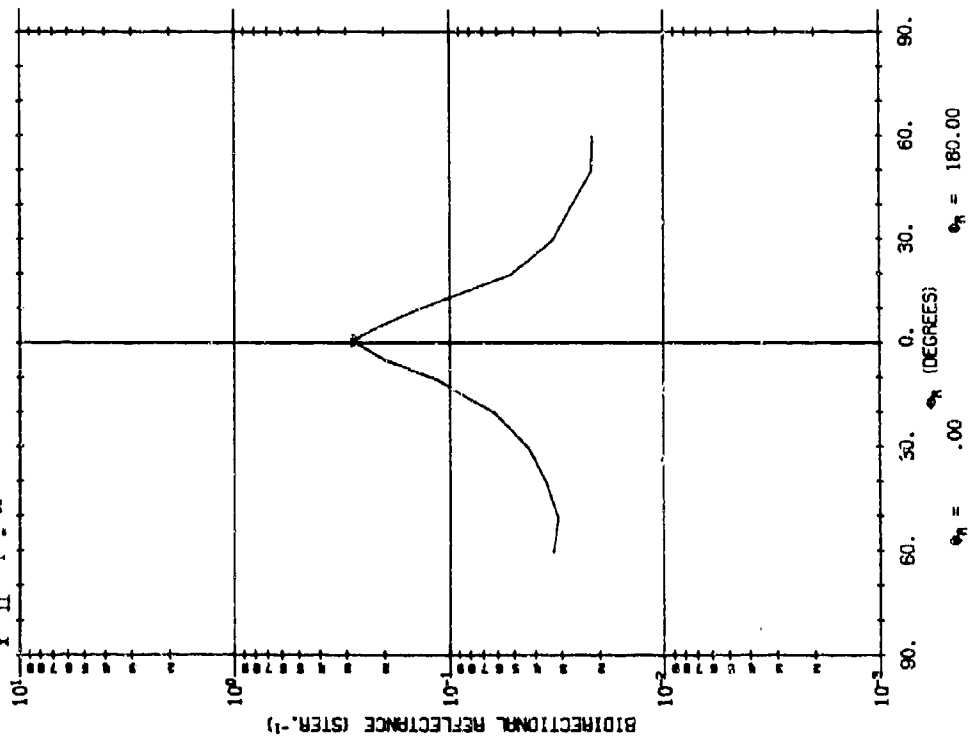


WOOD

R00106 002

White Oak Block

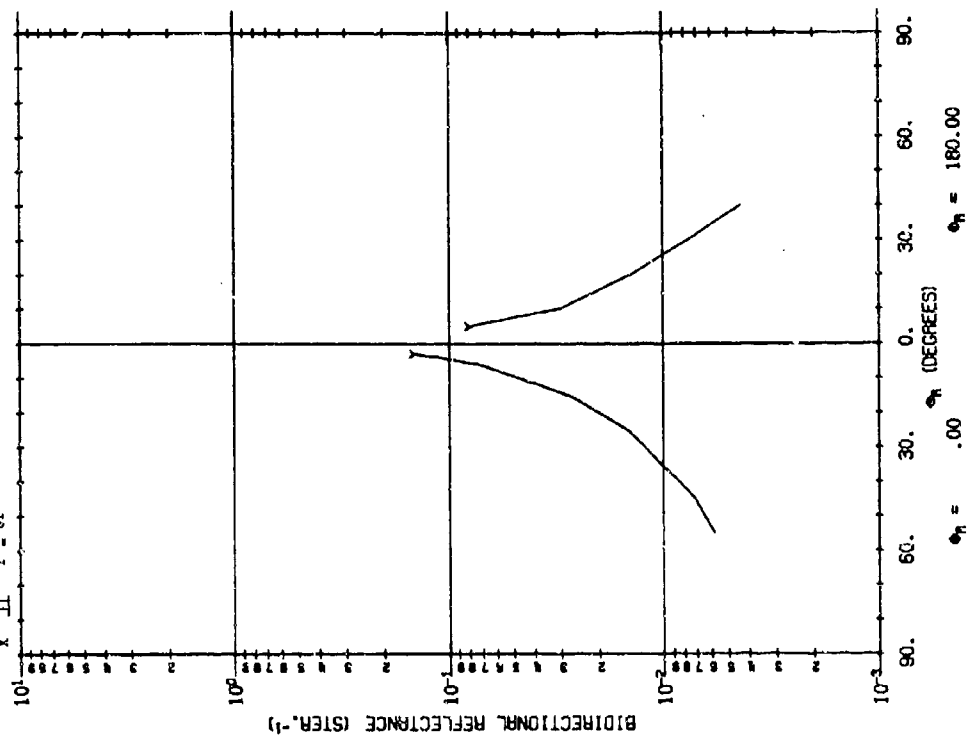
0 ||  $2\theta = 1.10$   
 + ||  $\phi_1 = \phi_r$   
 Δ ||  $\lambda = 10.6$   
 X ||  $Y = \text{UT}$



R00106 002

White Oak Block

0 ||  $\phi_1 = 0.0$   
 + ||  $\phi_1 = 180.0$   
 Δ ||  $\lambda = 10.6$   
 X ||  $Y = \text{UT}$

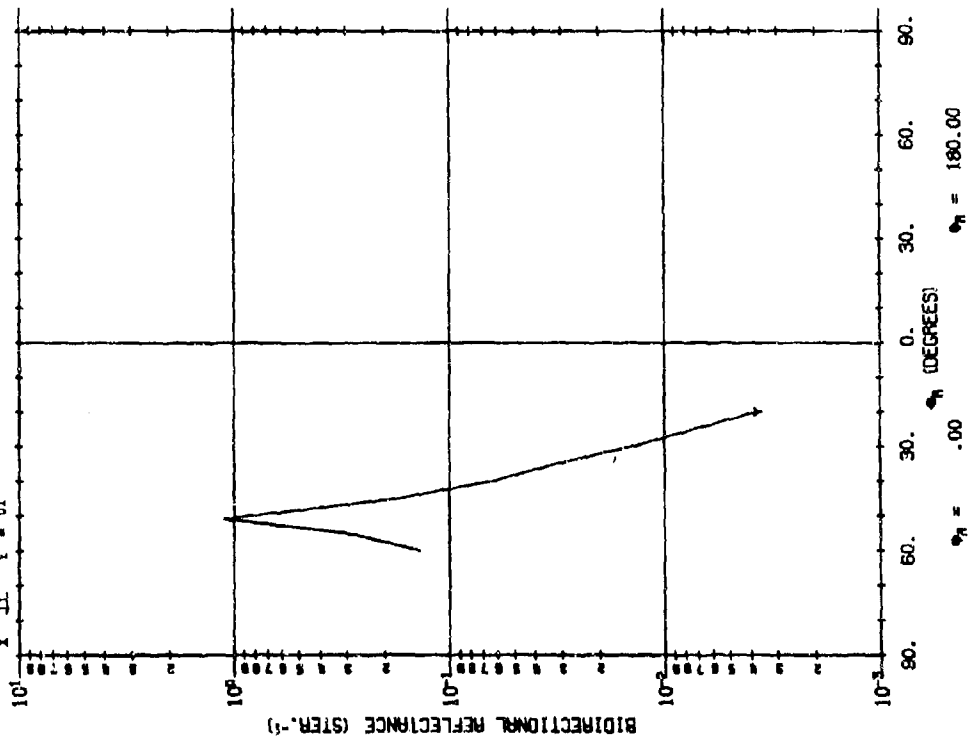




A00106 002

White Oak Block

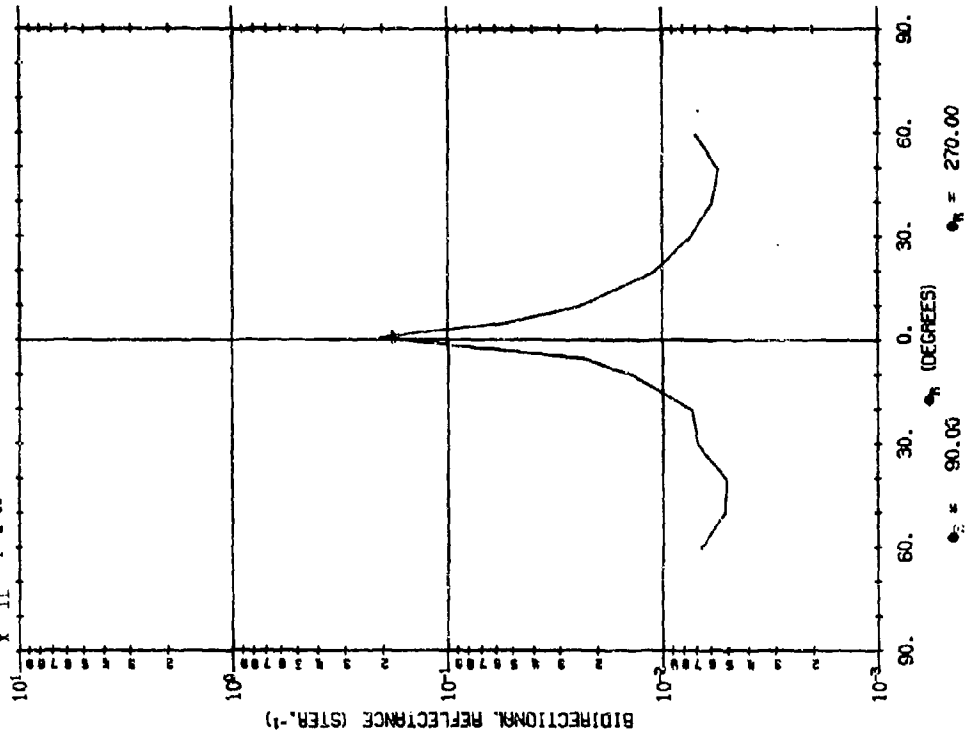
0 ||  $\theta_1 = 50.0$   
 + ||  $\phi_1 = 180.0$   
 Δ ||  $\lambda = 10.6$   
 X || Y = UT



A00106 002

White Oak Block

0 ||  $\theta_1 = 1.10$   
 + ||  $\phi_1 = 0$   
 Δ ||  $\lambda = 10.6$   
 X || Y = UT

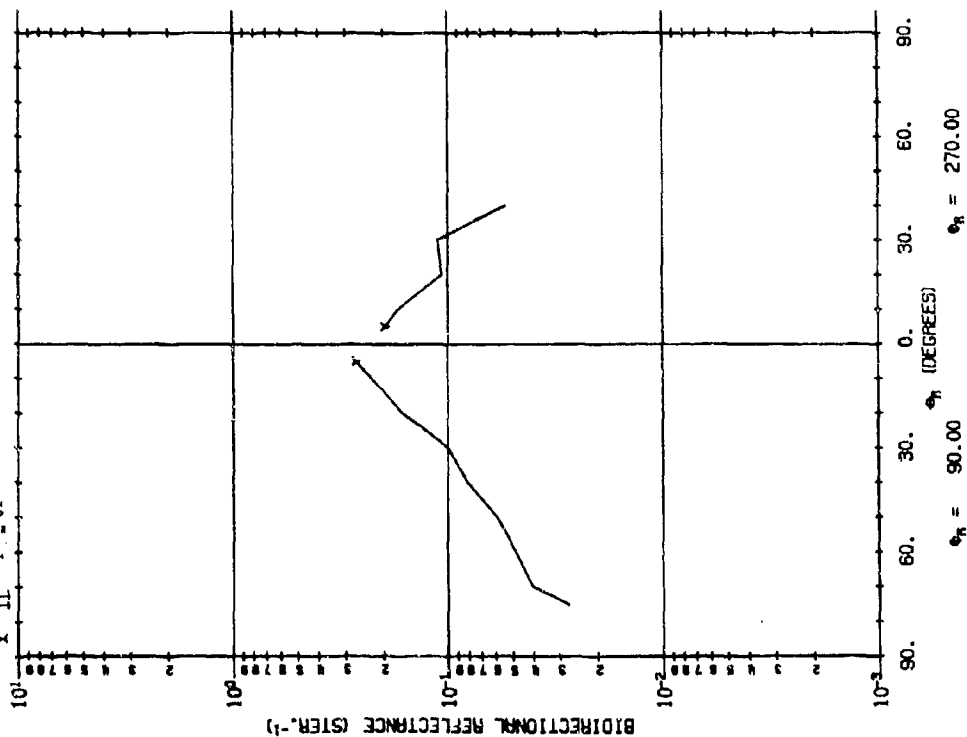


WOOD

A00106 002

White Oak Block

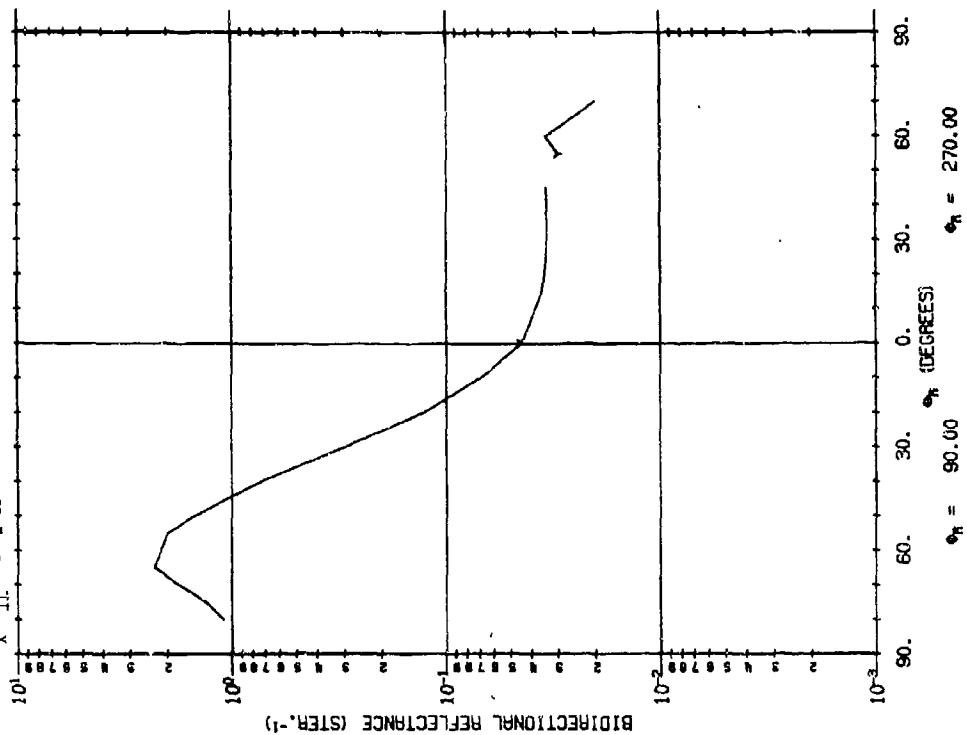
0 ||  $\theta_1 = 0.0$   
 + ||  $\phi_1 = 270.0$   
 Δ ||  $\lambda = 10.6$   
 x ||  $\gamma = UT$



A00106 002

White Oak Block

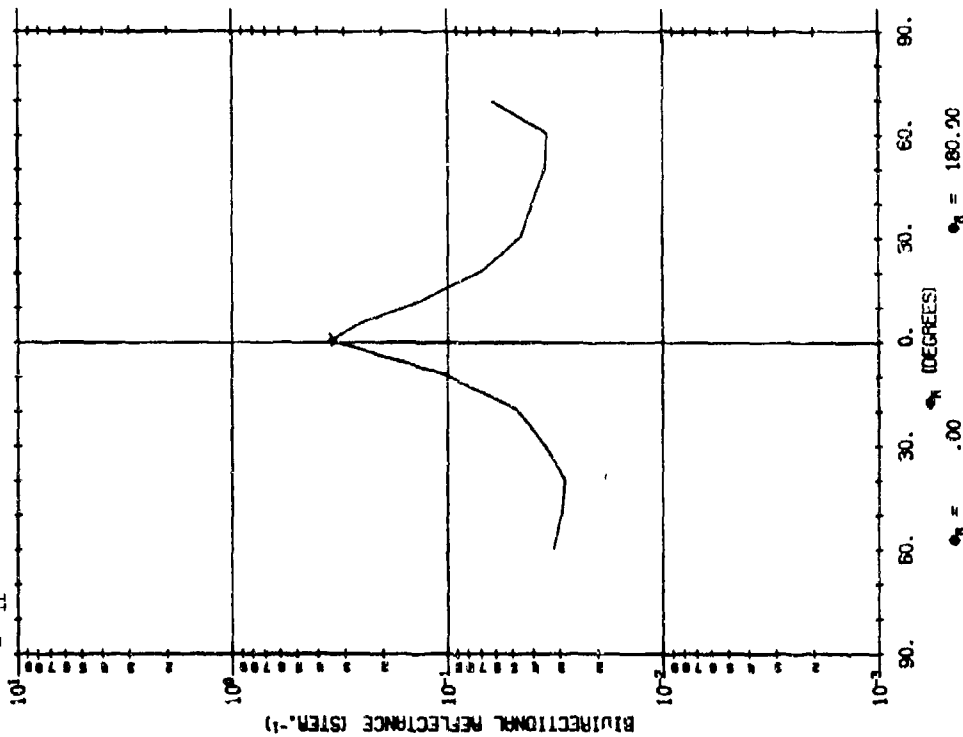
0 ||  $\theta_1 = 50.0$   
 + ||  $\phi_1 = 270.0$   
 Δ ||  $\lambda = 10.6$   
 x ||  $\gamma = UT$



R00118 002

Red Oak Block

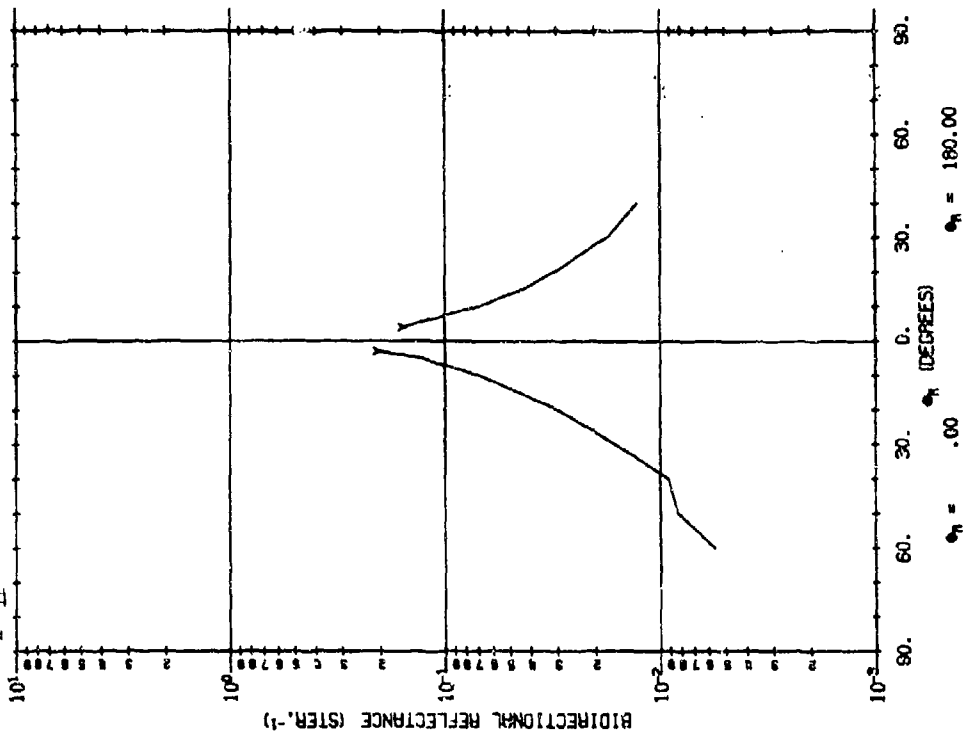
0 // 2B = 1.10  
 + //  $\phi_i = \phi_r$   
 A //  $\lambda = 10.6$   
 X //  $\gamma = 0^\circ$



R00118 002

Red Oak Block

0 //  $\phi_i = 0.0$   
 + //  $\phi_i = 180.0$   
 A //  $\lambda = 10.6$   
 X //  $\gamma = 0^\circ$

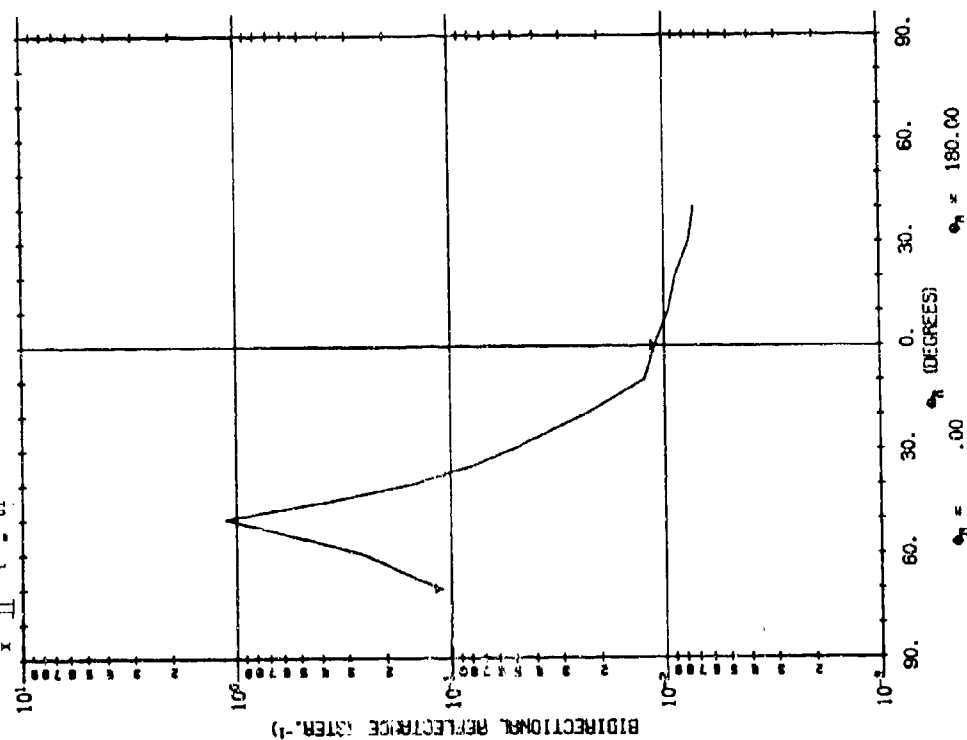


WOOD

R00118 002

Ref Oak Block

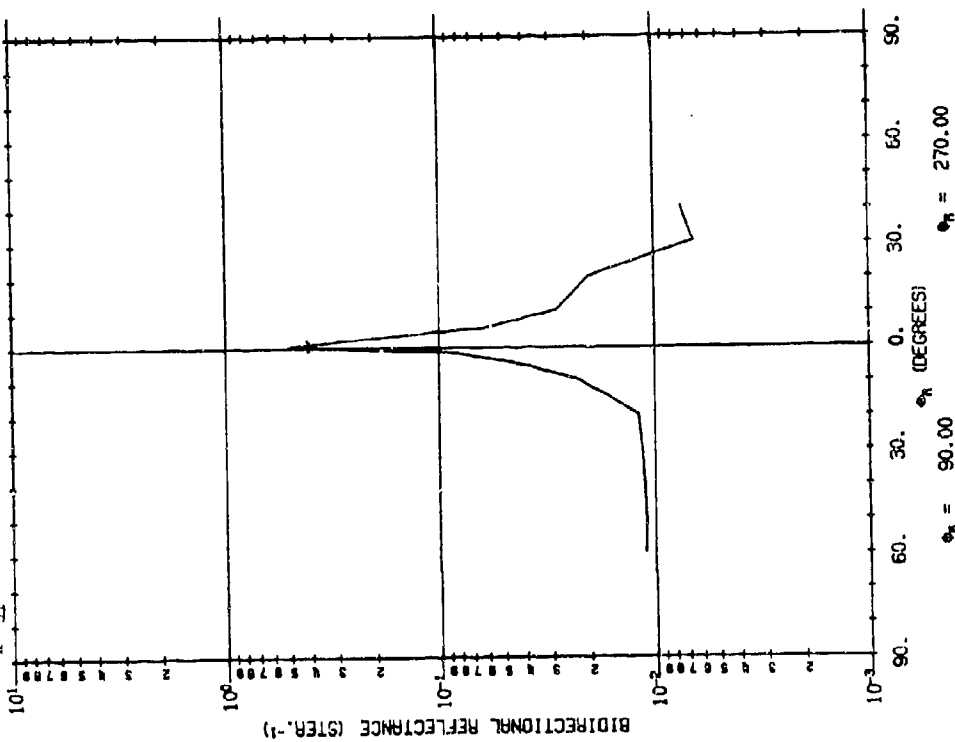
0 ||  $\theta_1 = 50.0$   
 + ||  $\phi_1 = 180.0$   
 Δ ||  $\lambda = 10.6$   
 X ||  $\gamma = 0^\circ$



R00118 002

Ref Oak Block

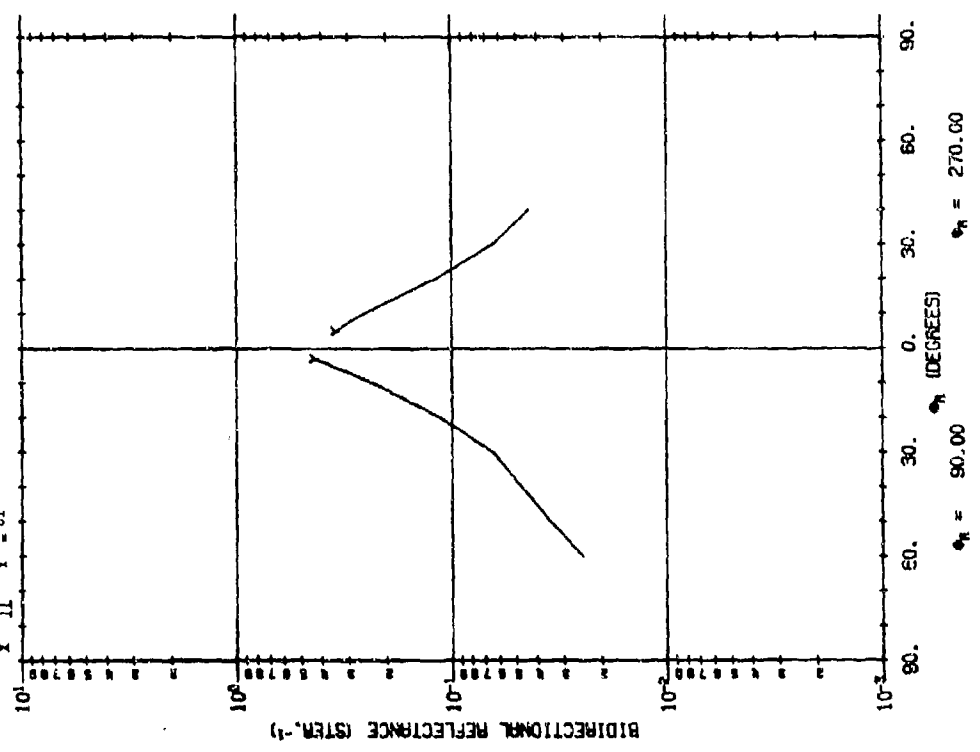
0 ||  $\theta_1 = 1.10$   
 + ||  $\phi_1 = 0^\circ$   
 Δ ||  $\lambda = 10.6$   
 X ||  $\gamma = 0^\circ$



A00118 002

Red Oak Block

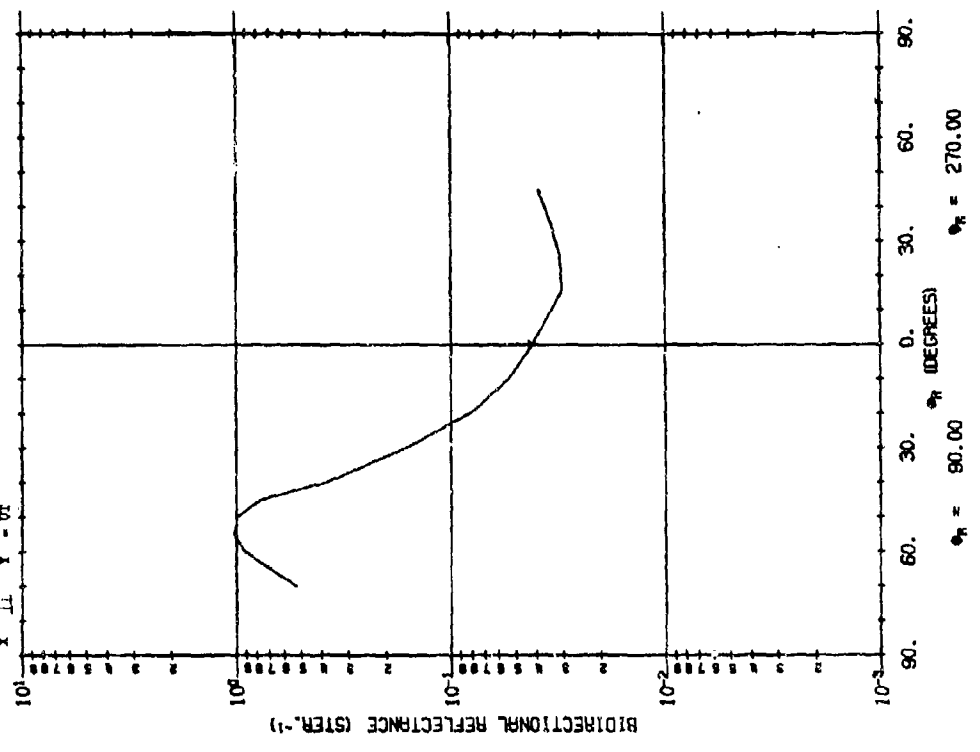
0 //  $\theta_1 = 0.0$   
 + //  $\phi_1 = 270.0$   
 Δ //  $\lambda = 10.6$   
 X //  $\chi = 0.0$



A00118 002

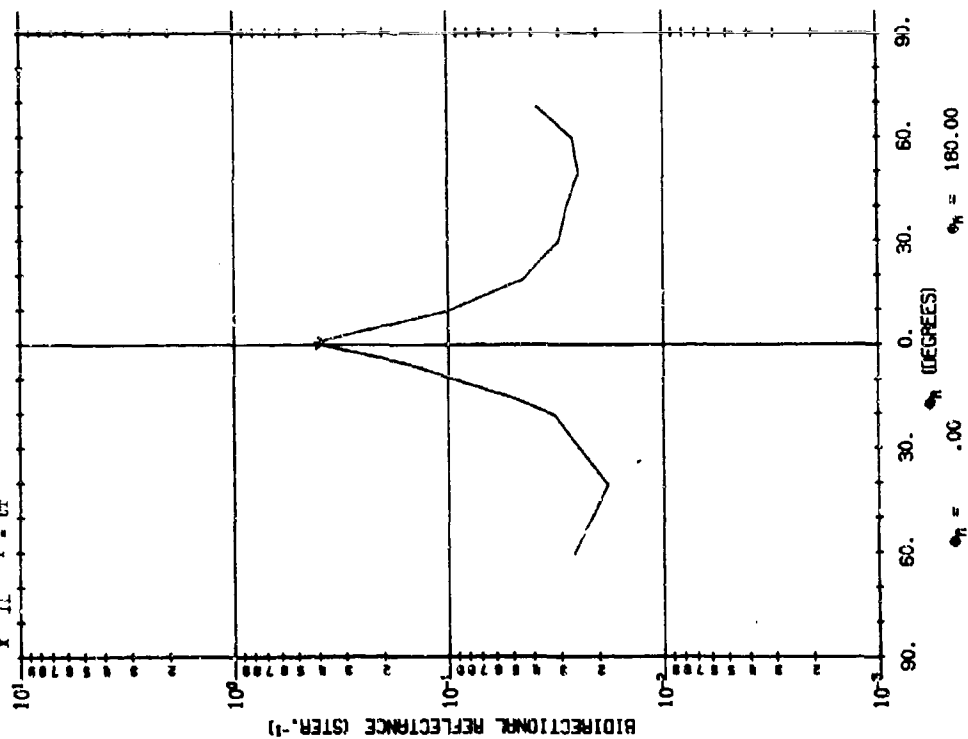
Red Oak Block

0 //  $\theta_1 = 50.0$   
 + //  $\phi_1 = 270.0$   
 Δ //  $\lambda = 10.6$   
 X //  $\chi = 0.0$



WOOD

California White Oak Block

$$0 \parallel 2R = 1.10$$
$$+ \quad \parallel \quad = \quad \phi_T$$
$$\Delta \int \lambda = 10.6$$
$$Y = \Gamma X$$


A00137 002

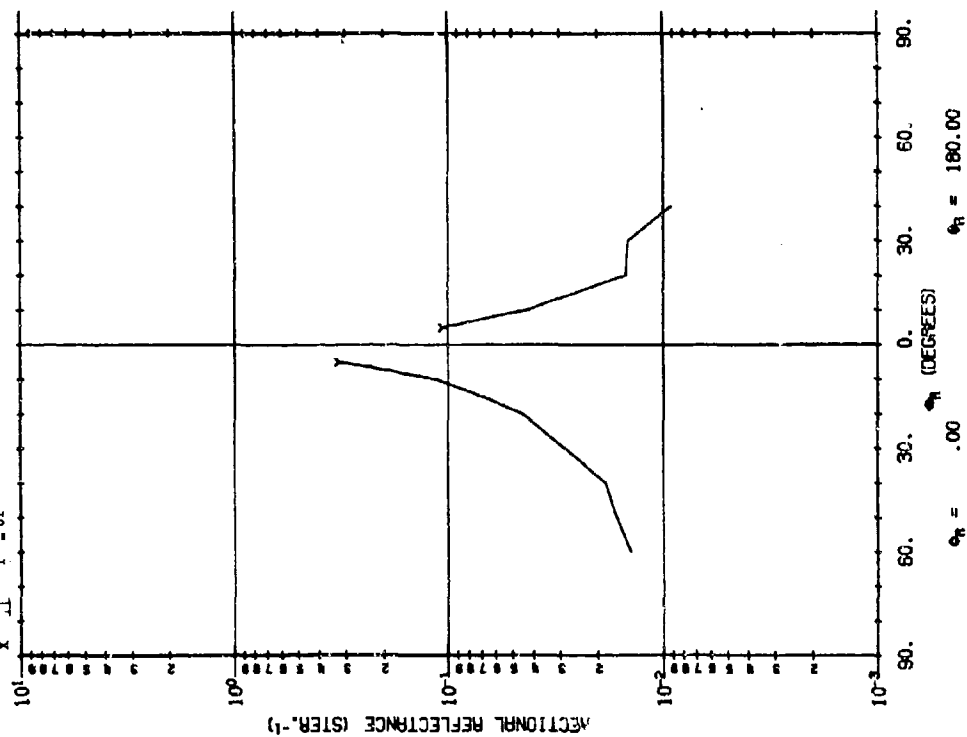
**California White Oak Block**

 $\theta_1 = 0.0$ 

$\phi_1 = 180.0$

 $\lambda^+ = 10.6$ 

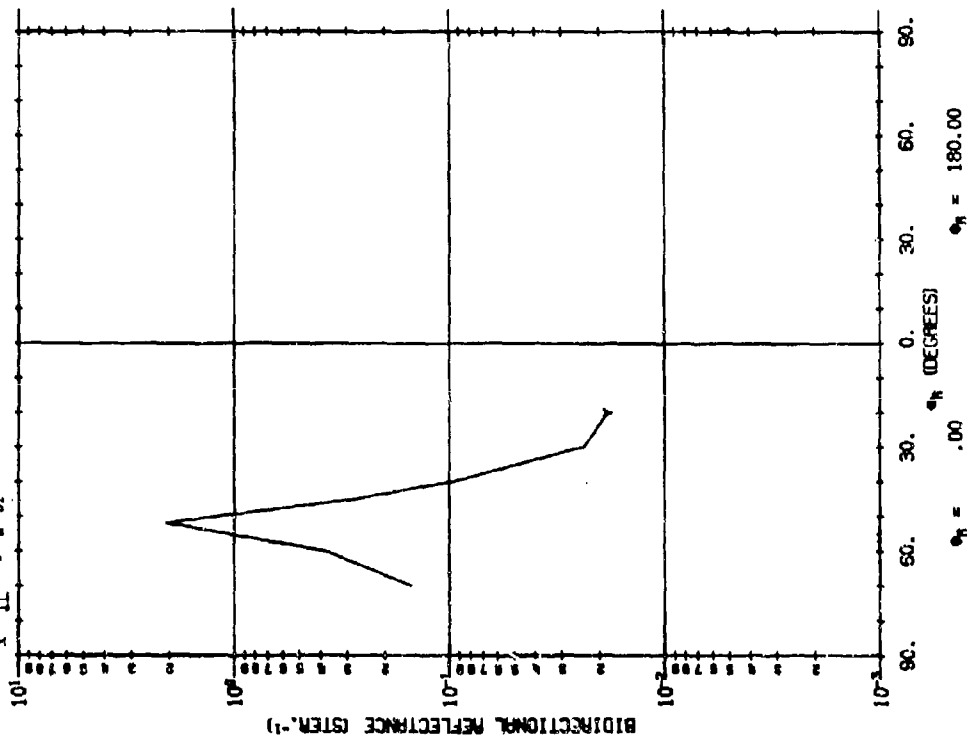
Y - 5T



R00137 002

California White Oak Block

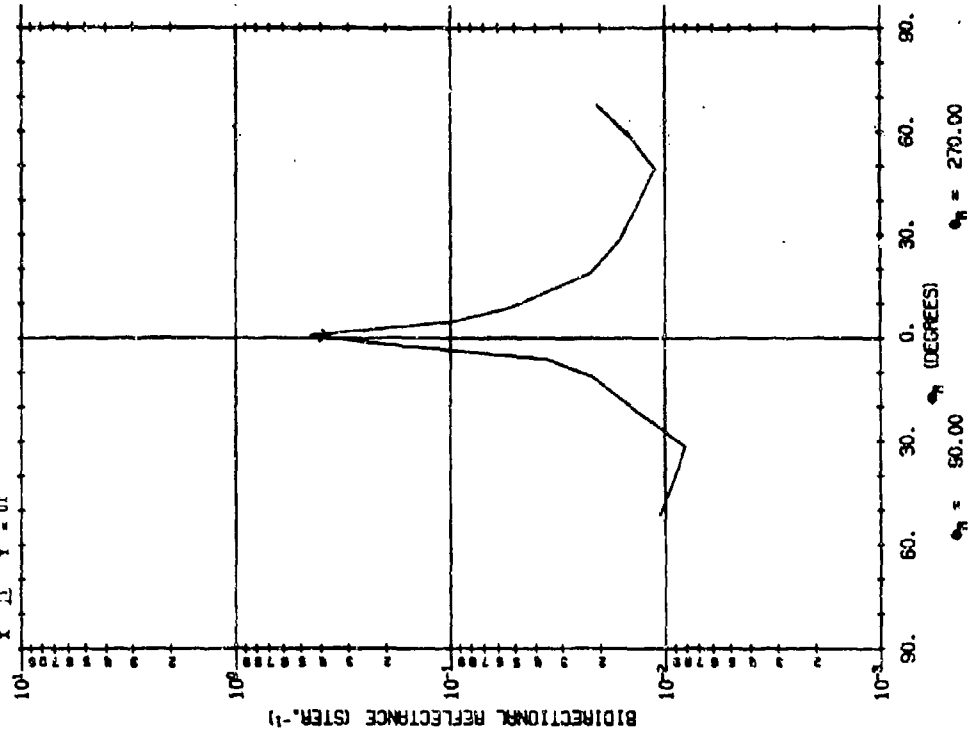
0 ||  $\phi_1 = 50.0$   
 + ||  $\phi_1 = 180.0$   
 Δ ||  $\lambda = 10.6$   
 X || Y = UT



R00137 002

California White Oak Block

0 ||  $\phi_1 = 1.10$   
 + ||  $\phi_1 = \phi_r$   
 Δ ||  $\lambda = 10.6$   
 X || Y = UT



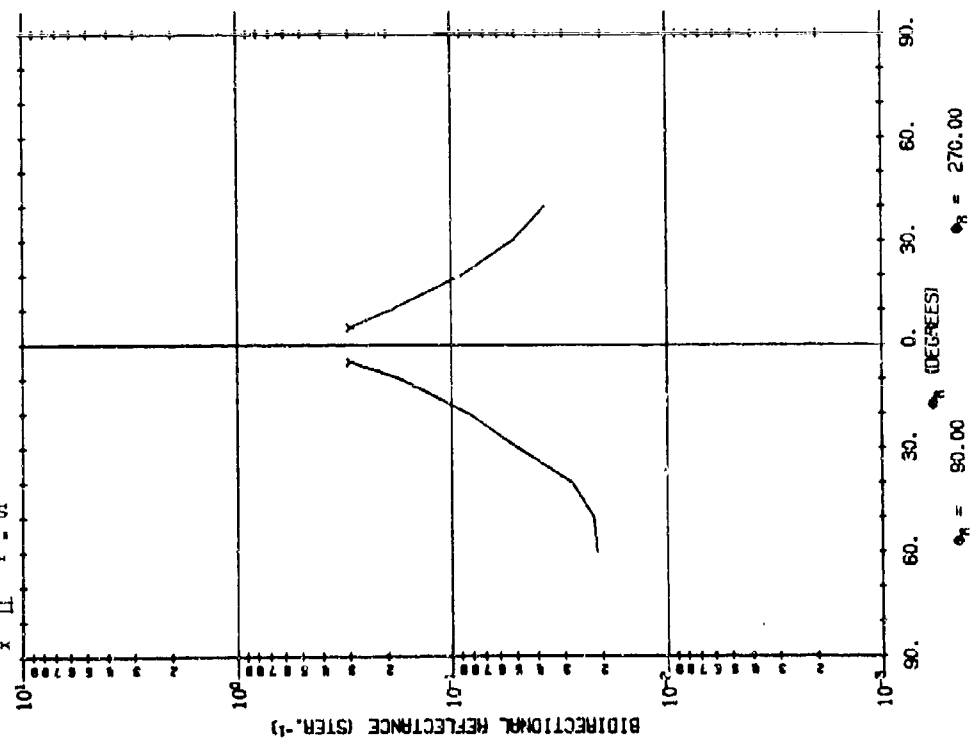
WOOD

1

A00137 002

California White Oak Block

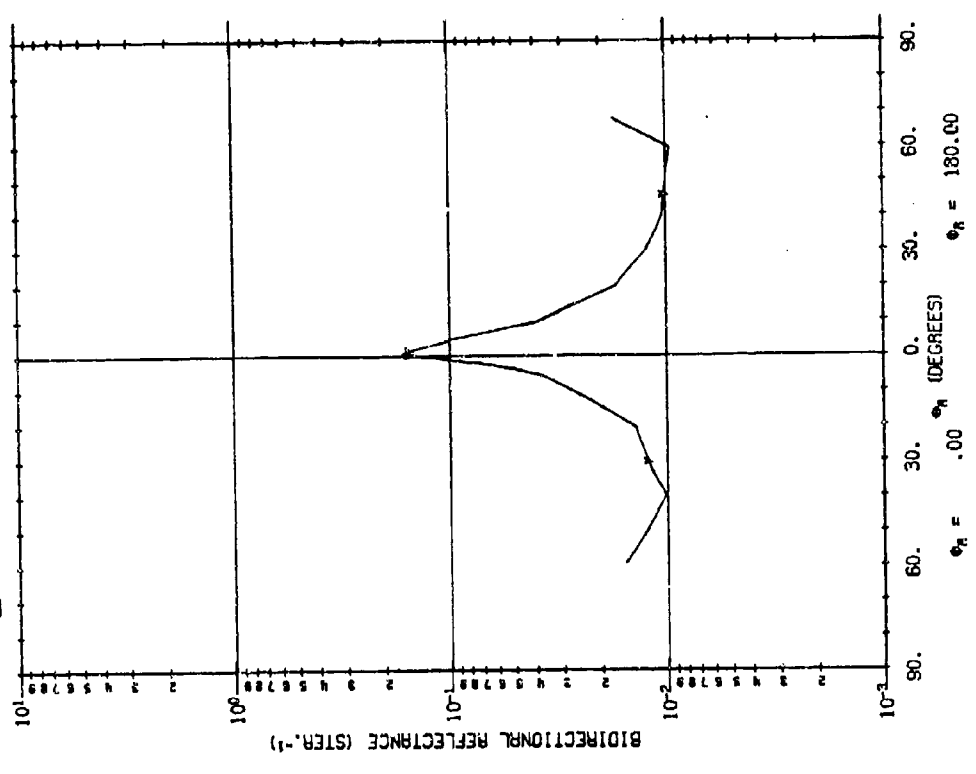
0 ||  $\theta_1 = 0.0$   
 + ||  $\phi_1 = 270.0$   
 Δ ||  $\lambda = 10.6$   
 X || Y = VT



A00153 002

White Pine Block

0 ||  $\theta_1 = 1.10$   
 + ||  $\phi_1 = \theta_c$   
 Δ ||  $\lambda = 10.6$   
 X || Y = VT

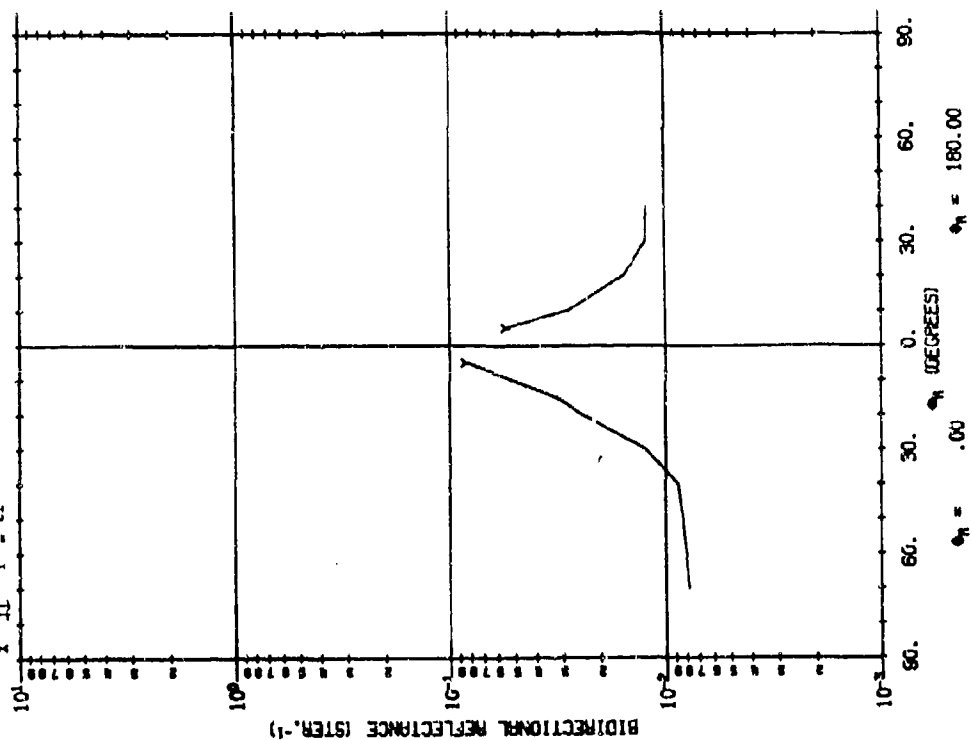




A00153 002

White Pine Block

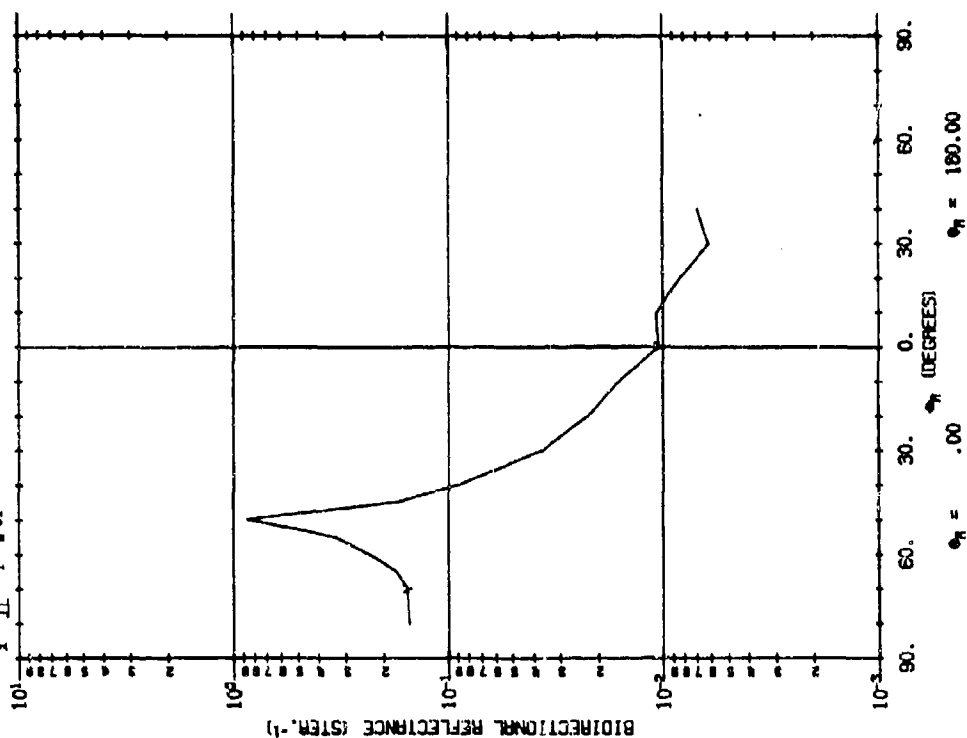
0 //  $\phi_1 = 0.0$   
 + //  $\phi_1 = 180.0$   
 Δ //  $\lambda = 10.6$   
 x //  $\gamma = 0^\circ$



A00153 002

White Pine Block

0 //  $\phi_1 = 50.0$   
 + //  $\phi_1 = 180.0$   
 Δ //  $\lambda = 10.6$   
 x //  $\gamma = 0^\circ$

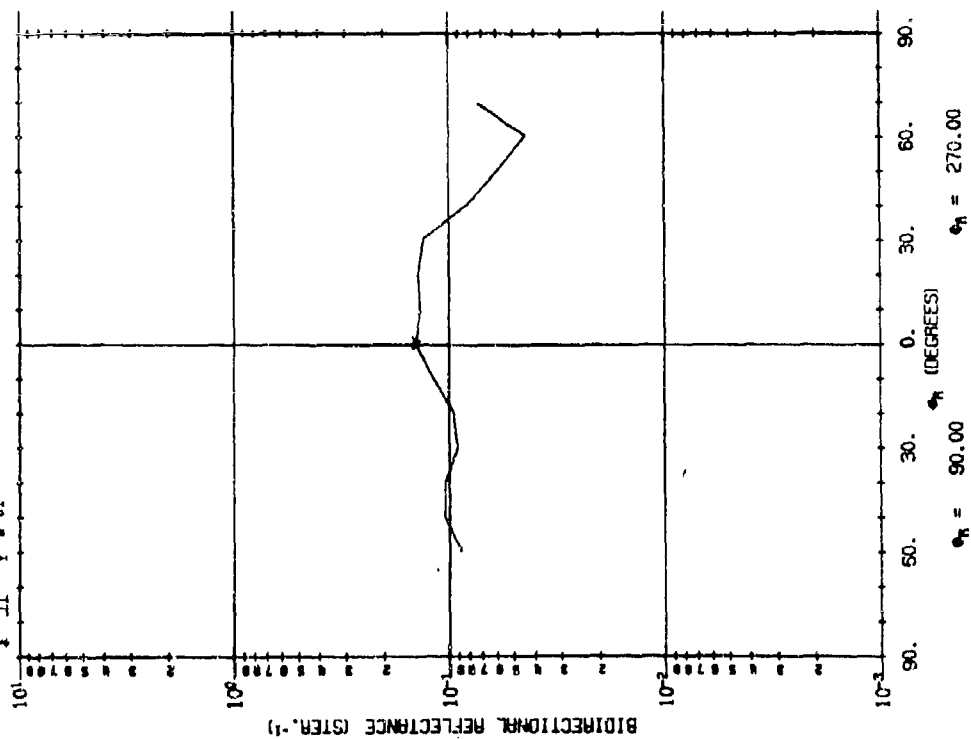


WOOD

R00153 002

White Pine Block

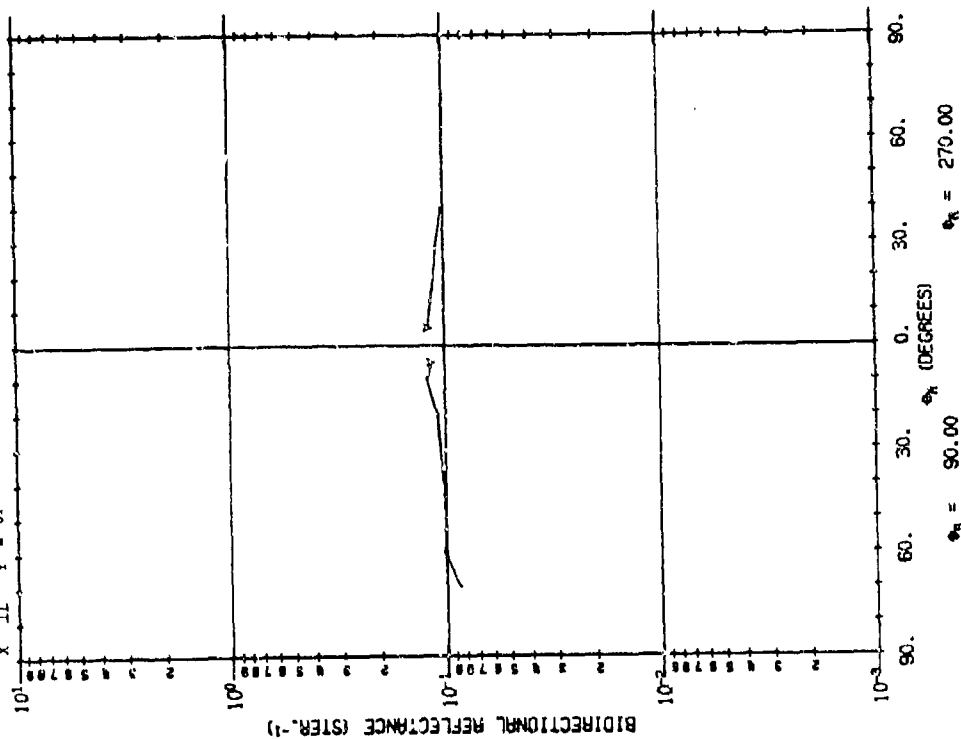
0 // 2a = 1.10  
+ //  $\epsilon_1 = \epsilon_r$   
Δ //  $\lambda = 10.6$   
X // Y = WT



R00153 002

White Pine Block

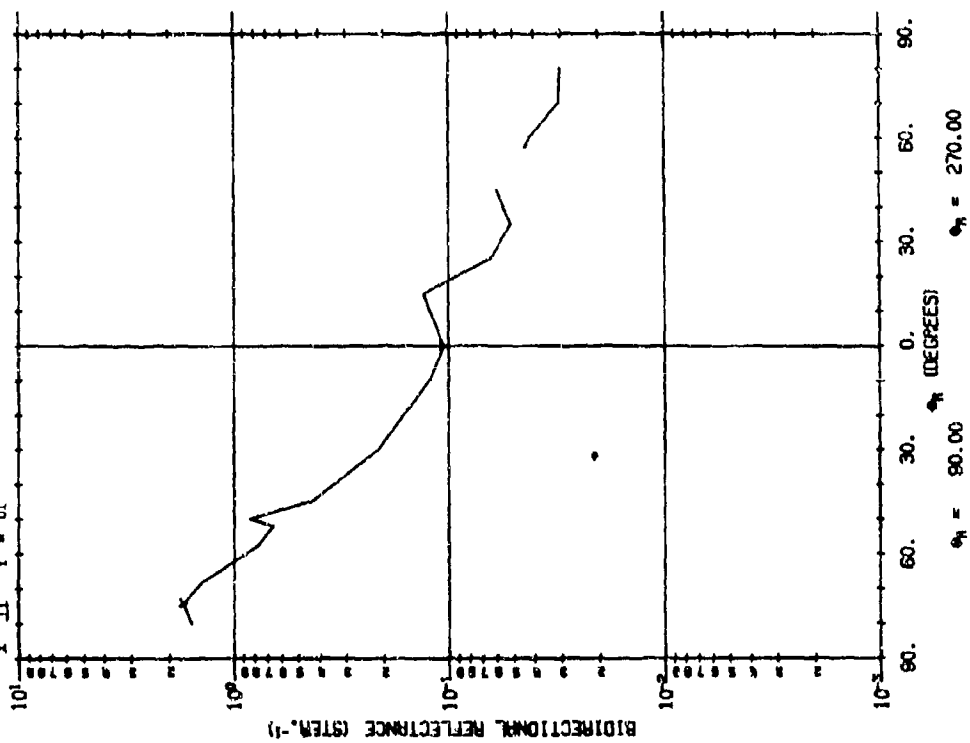
0 //  $\epsilon_1 = 0.0$   
+ //  $\epsilon_1 = 270.0$   
Δ //  $\lambda = 10.6$   
X // Y = WT



A00153 002

White Pine Block

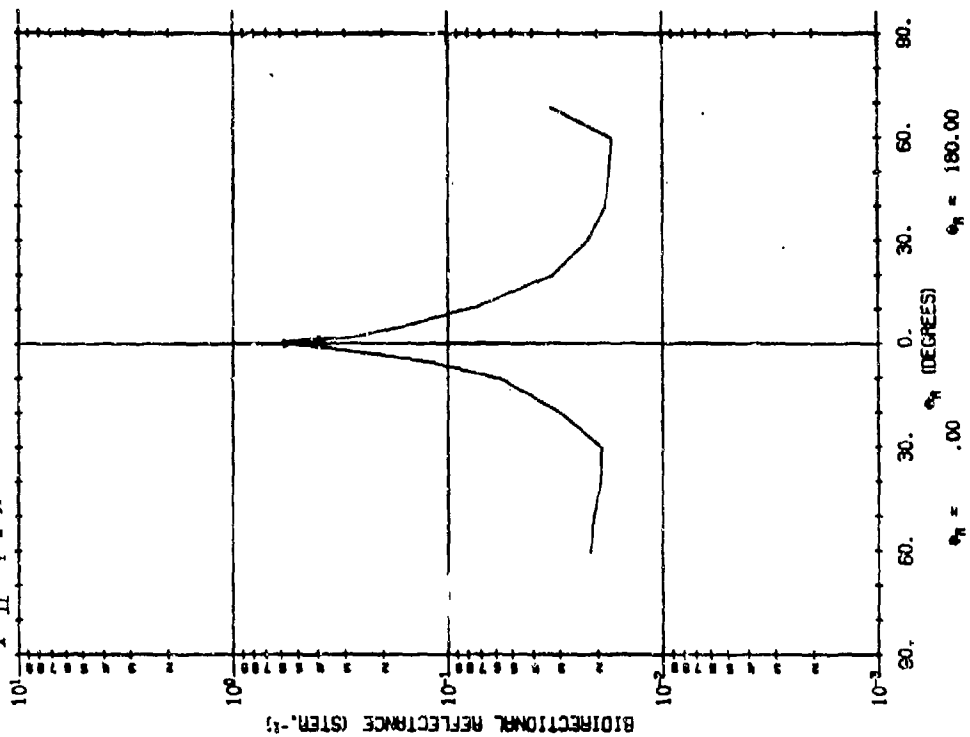
0 11  $\theta_i = 50.0$   
 + 11  $\theta_r = 270.0$   
 Δ 11  $\lambda = 10.6$   
 x 11 Y = UT



A00167 002

Oregon White Oak Block

0 11  $\theta_i = 1.10$   
 + 11  $\theta_r = 180.0$   
 Δ 11  $\lambda = 10.6$   
 x 11 Y = UT

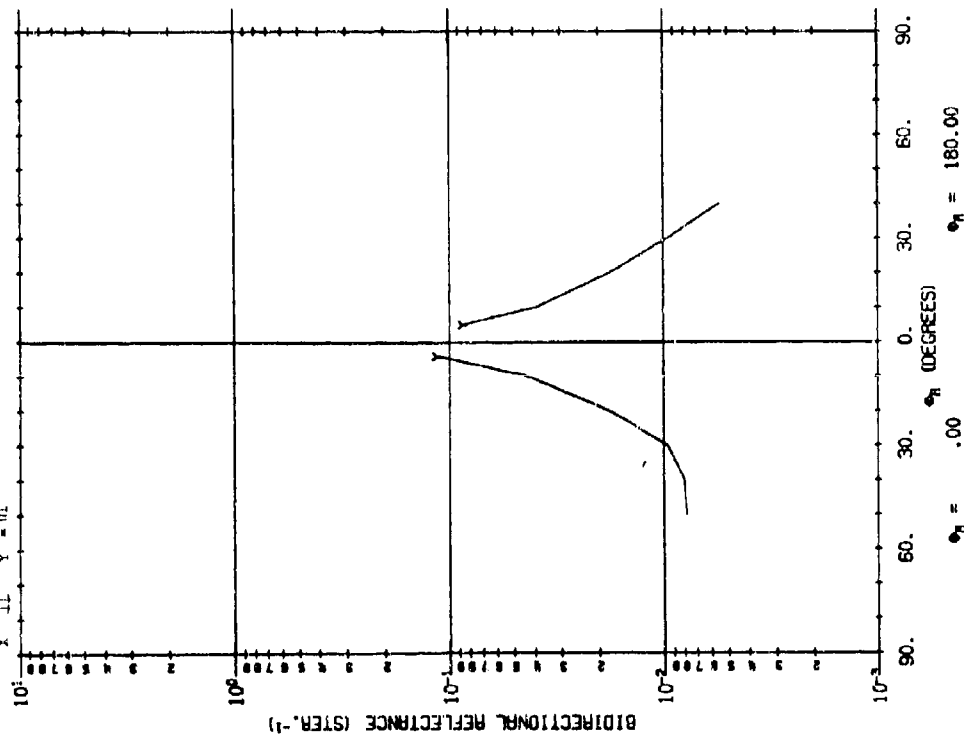


WOOD

R00167 002

Oregon White Oak Block

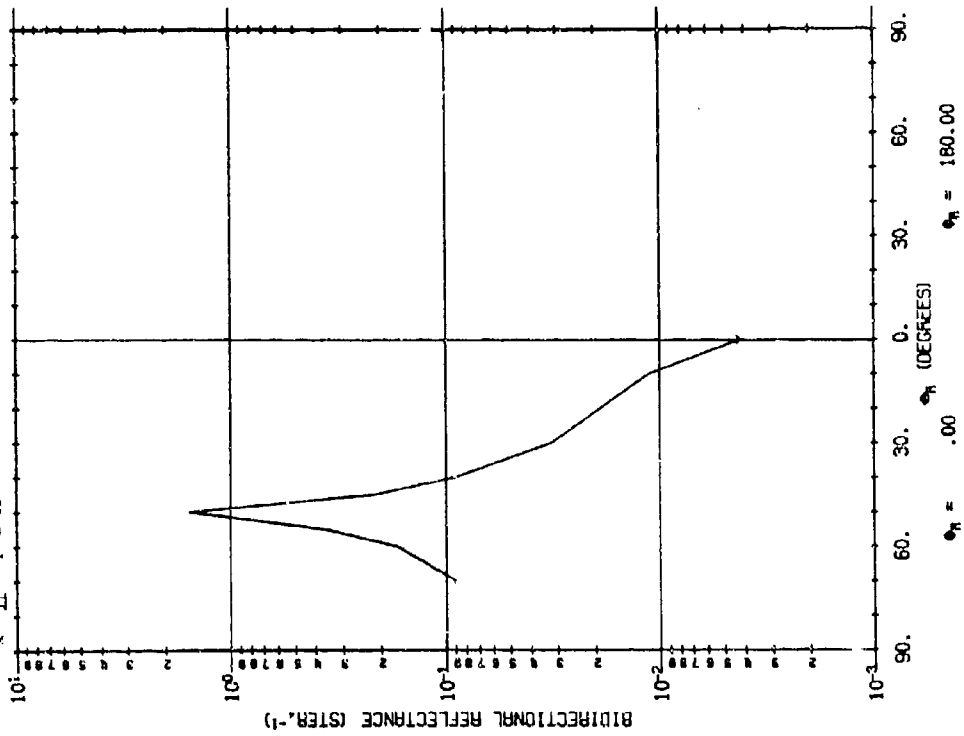
0 11  $\phi_1 = 0.0$   
 + 11  $\phi_1 = 180.0$   
 Δ 11  $\lambda = 10.6$   
 X 11  $\gamma = 1\pi$



R00167 002

Oregon White Oak Block

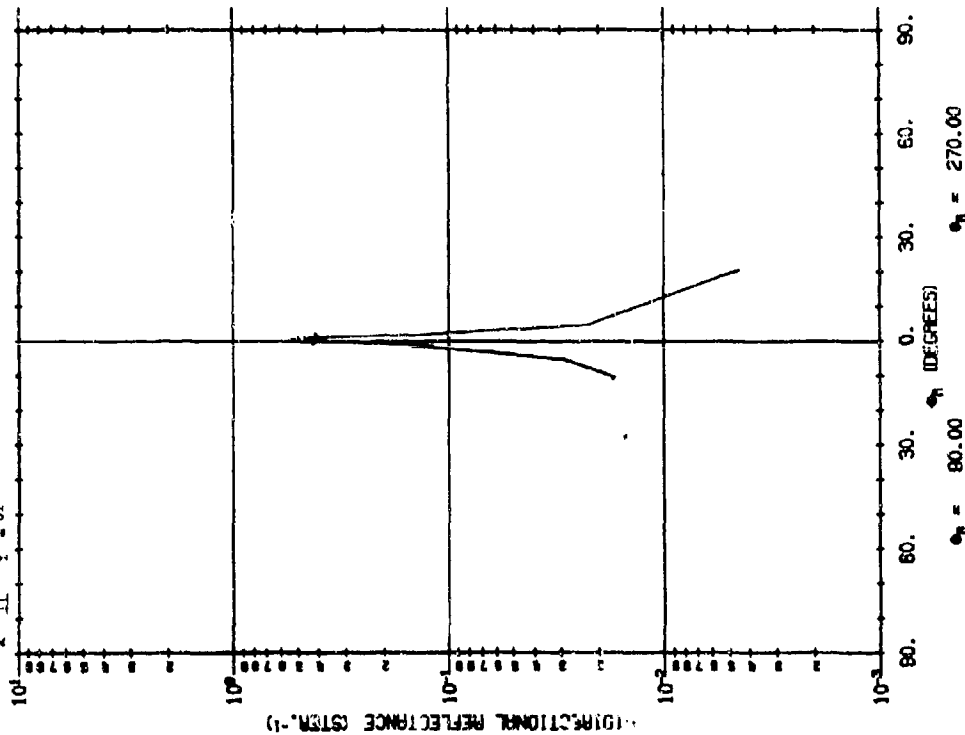
0 11  $\phi_1 = 50.00$   
 + 11  $\phi_1 = 130.0$   
 Δ 11  $\lambda = 10.6$   
 X 11  $\gamma = 1\pi$



A00167 002

Oregon White Oak Block

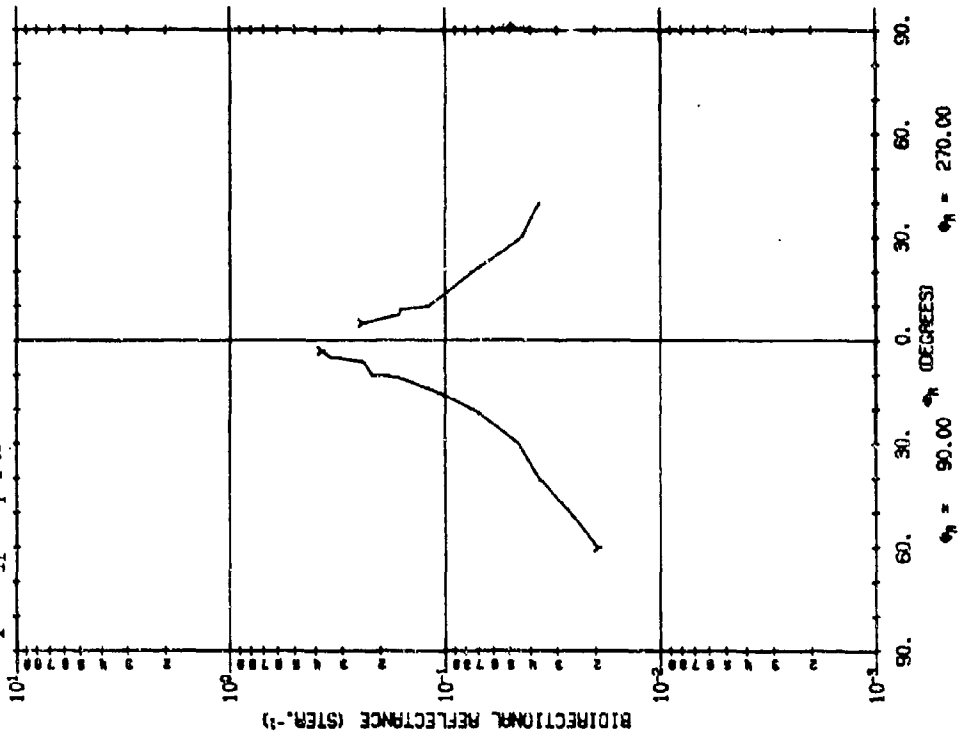
0 || 28 = 1.10  
+ ||  $\theta_1 = 4^\circ$   
Δ ||  $\lambda = 10.6$   
X ||  $\gamma = 0^\circ$



A00167 002

Oregon White Oak Block

0 ||  $\theta_1 = 0.0$   
+ ||  $\theta_1 = 270.0$   
Δ ||  $\lambda = 10.6$   
X ||  $\gamma = 0^\circ$

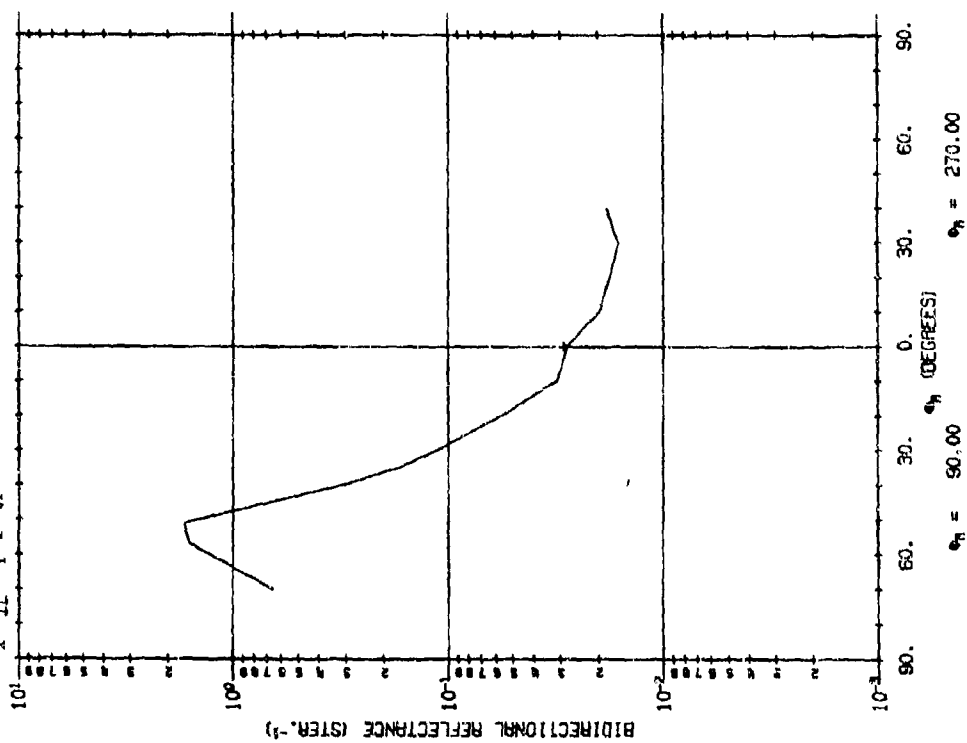


WOOD

R00167 002

Oregon White Oak Block

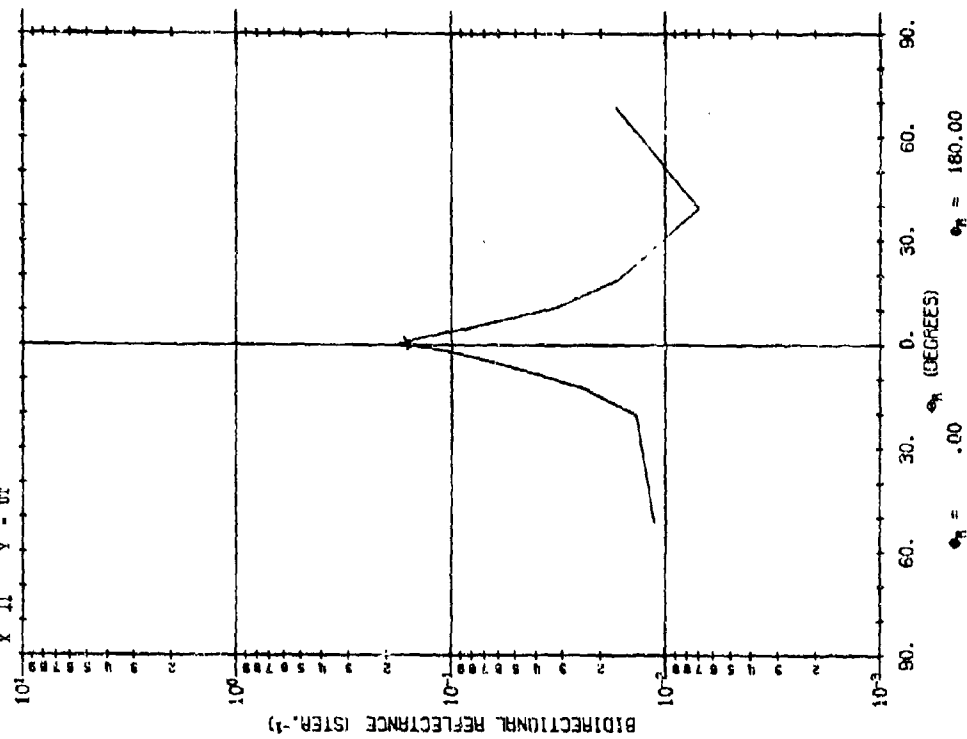
0 ||  $\epsilon_1 = 50.0$   
 + ||  $\epsilon_2 = 270.0$   
 x ||  $\lambda = 10.6$   
 Y = UT



R01585 001

Untreated Wood

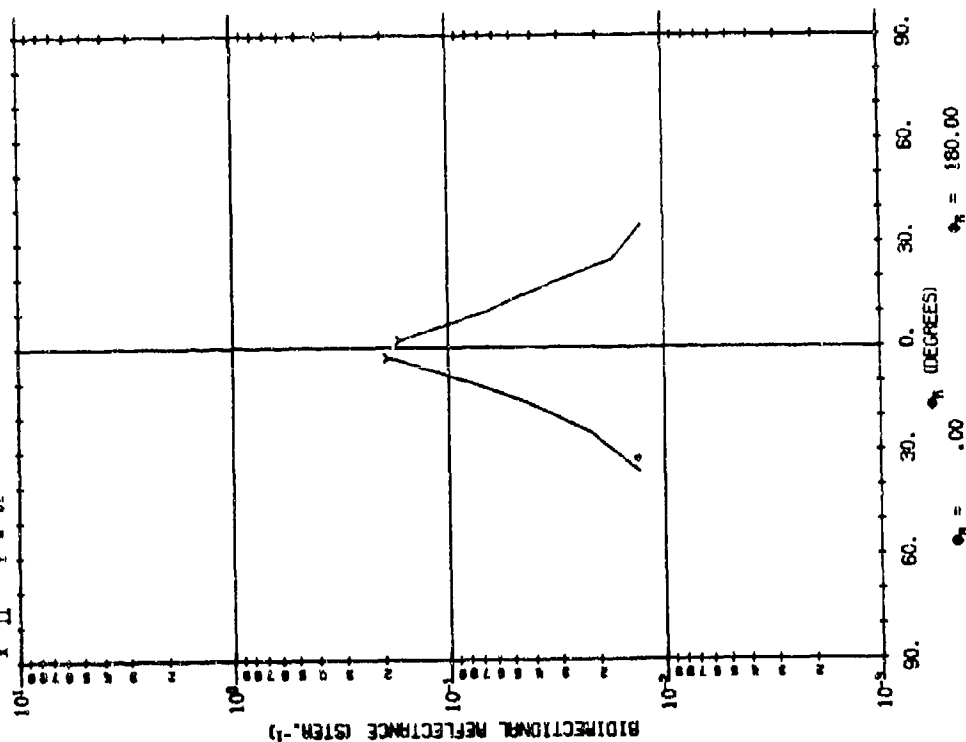
0 ||  $\epsilon_1 = 1.10$   
 + ||  $\epsilon_2 = 2$   
 x ||  $\lambda = 10.6$   
 Y = UT



R01585 001

Untreated Wood

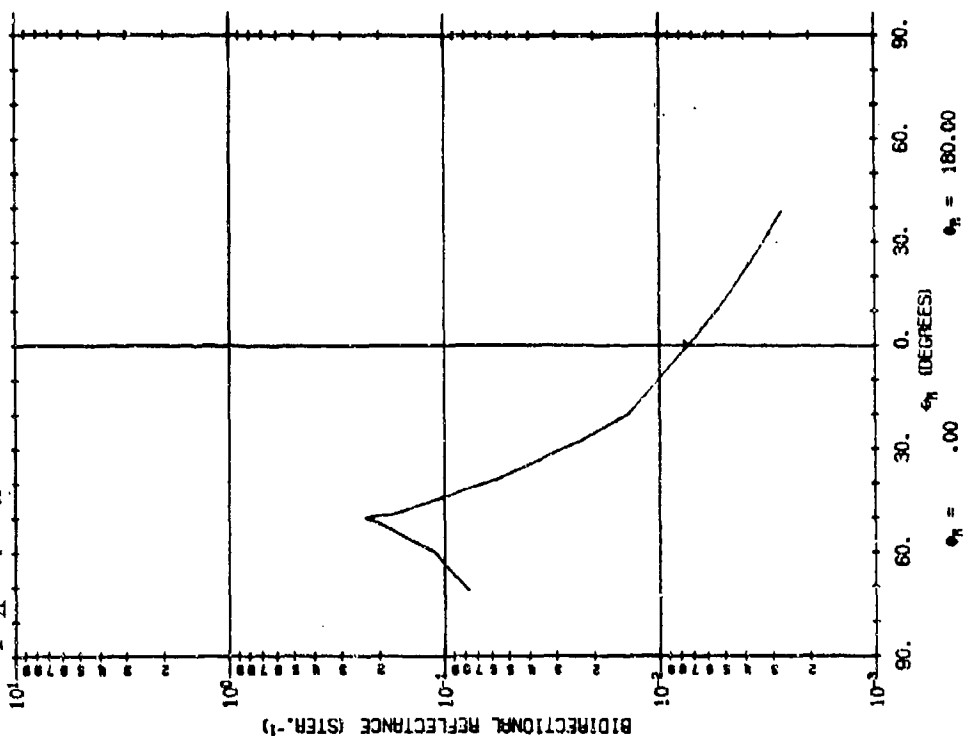
$\theta_1 = 0.0$   
 $\phi_1 = 180.0$   
 $\lambda = 10.6$   
 $Y = WT$



R01585 001

Untreated Wood

$\theta_1 = 50.0$   
 $\phi_1 = 180.0$   
 $\lambda = 10.6$   
 $Y = WT$

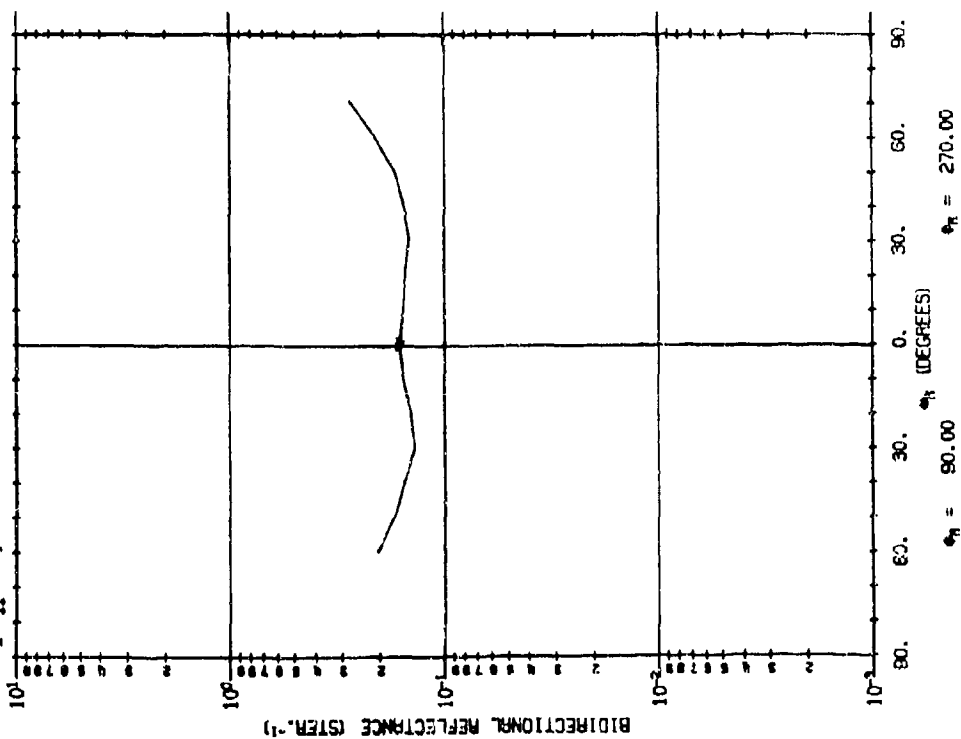


WOOD

R01585 001

Untreated Wood

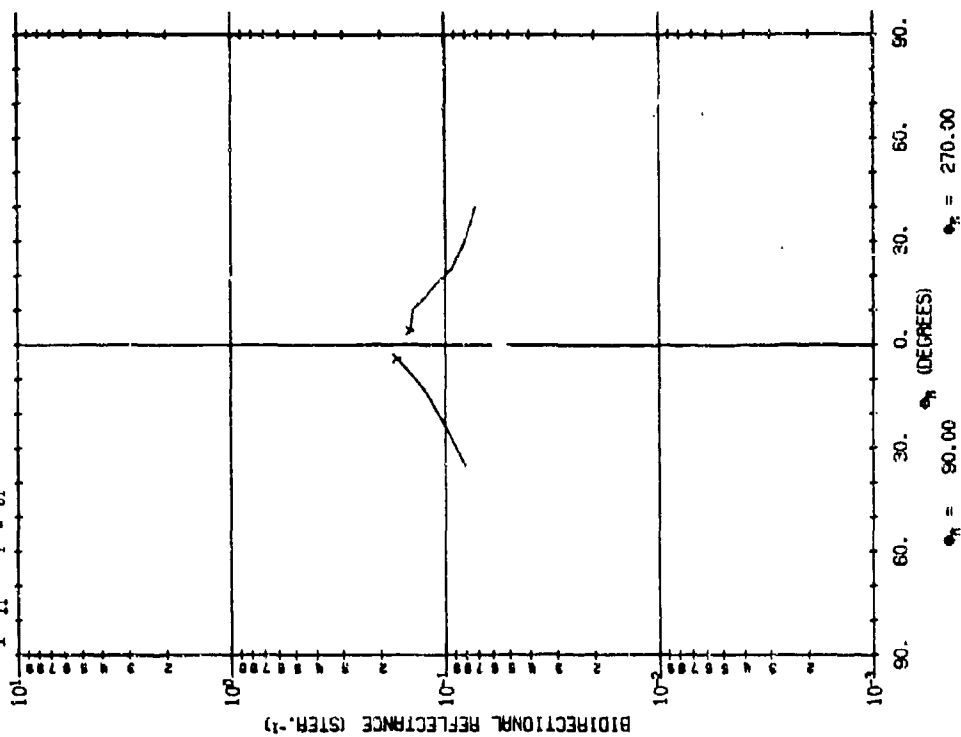
0 //  $2\theta = 1.10$   
 + //  $\phi_1 = \phi_r$   
 $\Delta$  //  $\lambda = 10.6$   
 X //  $\gamma = 0^\circ$



R01585 001

Untreated Wood

0 //  $\theta_1 = 0.0$   
 + //  $\phi_1 = 270.0$   
 $\Delta$  //  $\lambda = 10.6$   
 X //  $\gamma = 0^\circ$

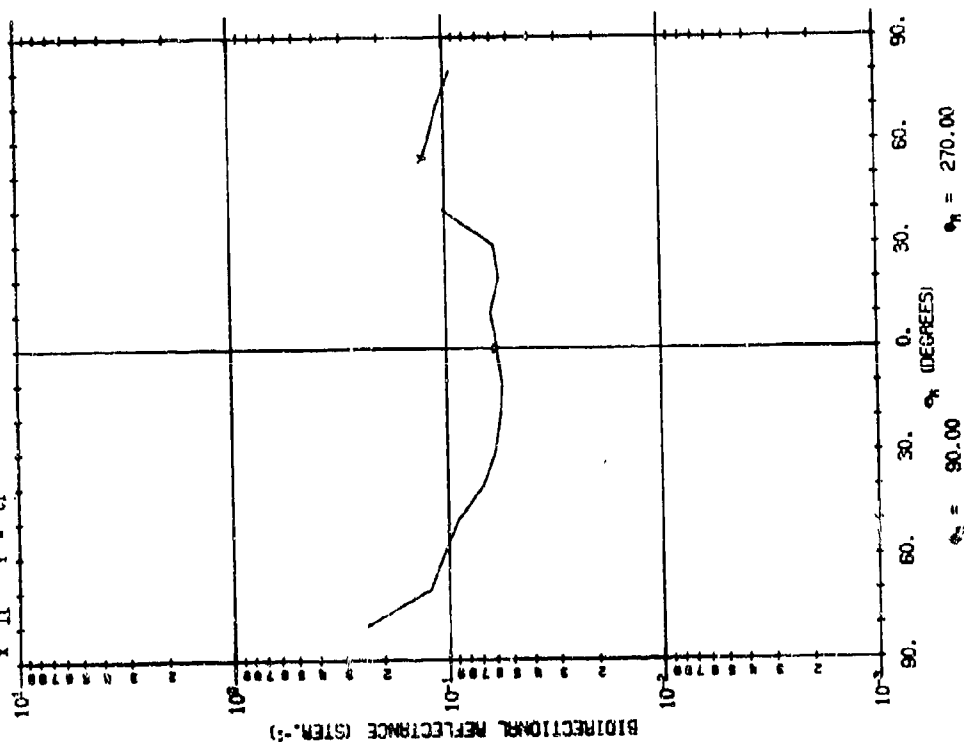




R01585 001

Untreated Wood

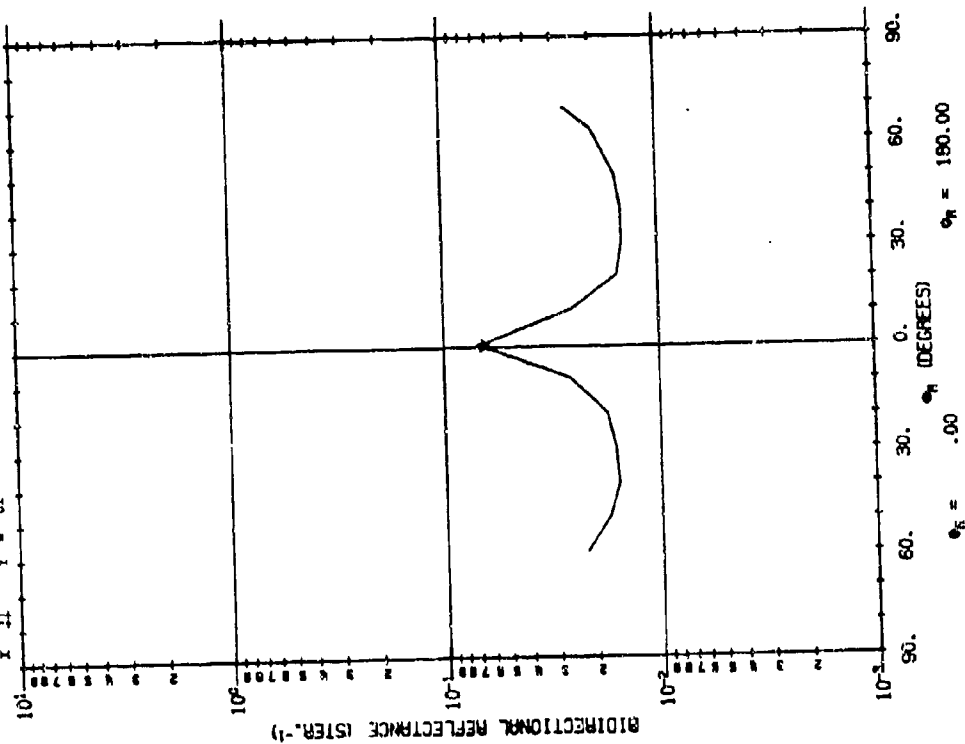
$\phi_i = 50.0$   
 $\phi_r = 270.0$   
 $\lambda = 10.6$   
 $\chi = \psi$



R01590 001

Unpainted Plywood

$\phi_i = 1.10$   
 $\phi_r = \psi$   
 $\lambda = 10.6$   
 $\chi = \psi$

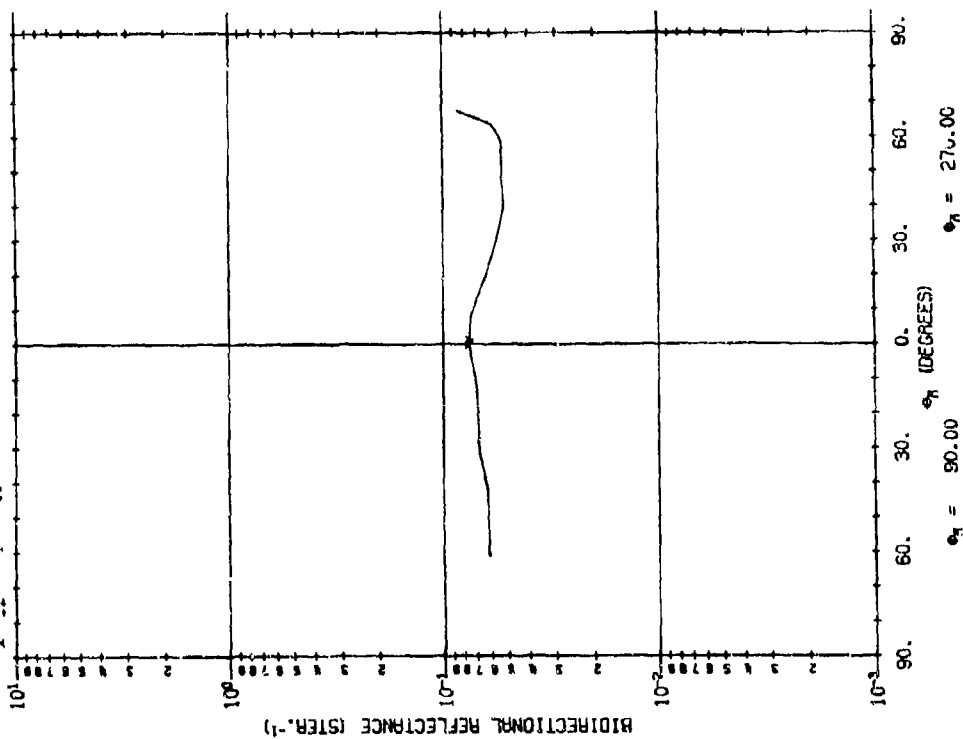


WOOD

AG1590 001

Unpainted Plywood

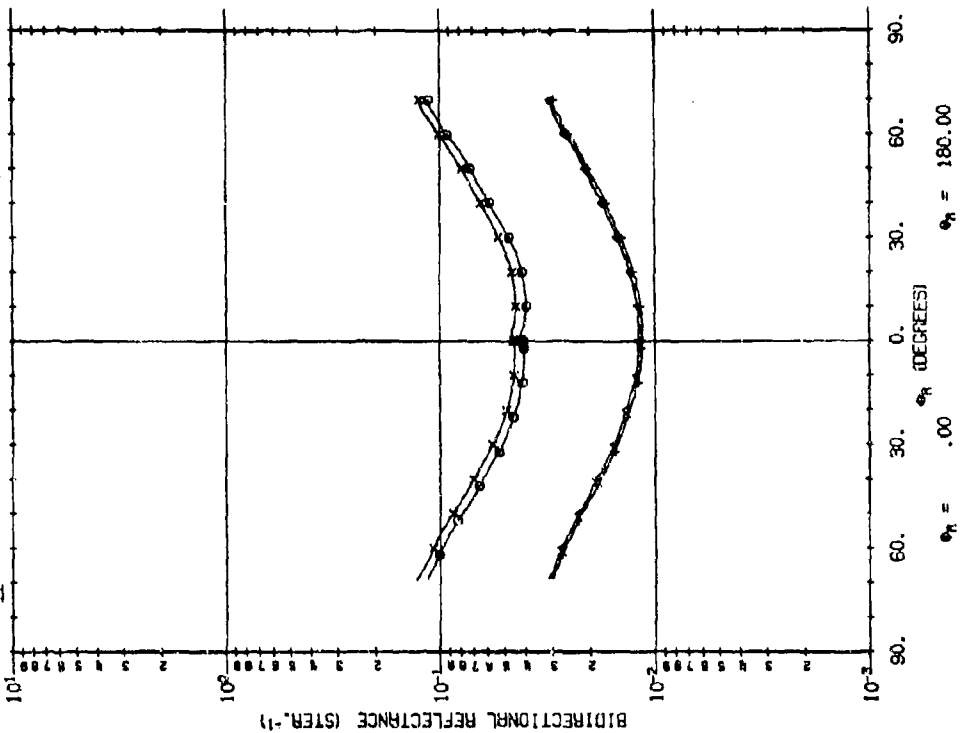
$2f = 1.10$   
 $\phi_1 = \phi_r$   
 $\lambda = 10.6$   
 $\lambda = 10.6$   
 $\lambda = 10.6$



AG1693 101

WOOD

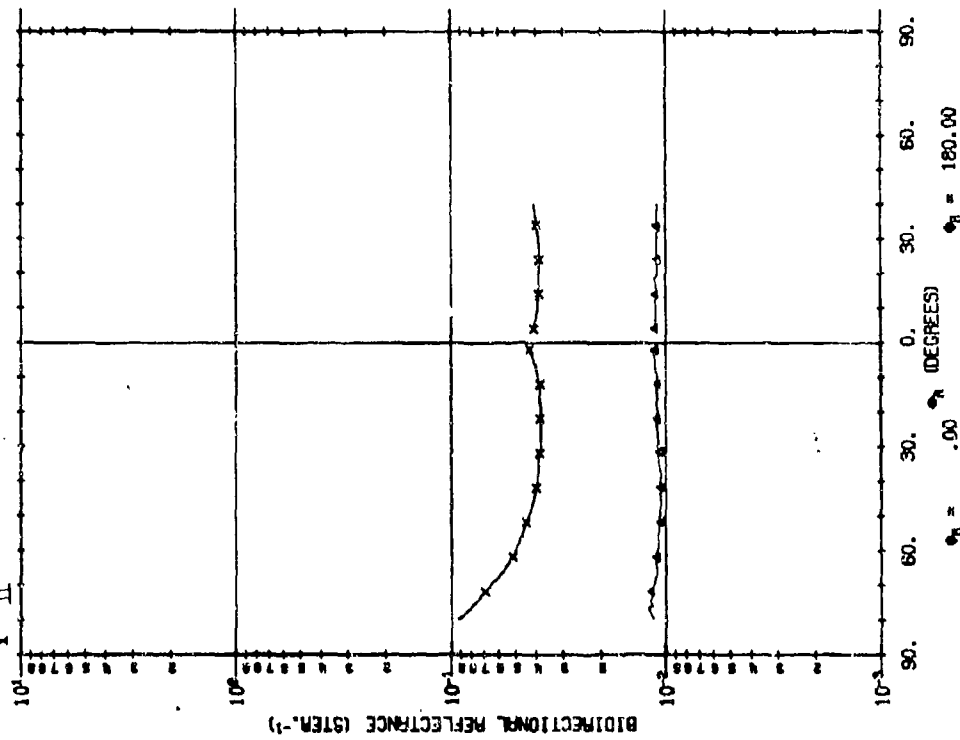
$2f = 2.0$   
 $\phi_1 = \phi_r$   
 $\lambda = 0.63$   
 $\lambda = 0.63$   
 $\lambda = 0.63$



A01699 101

WOOD

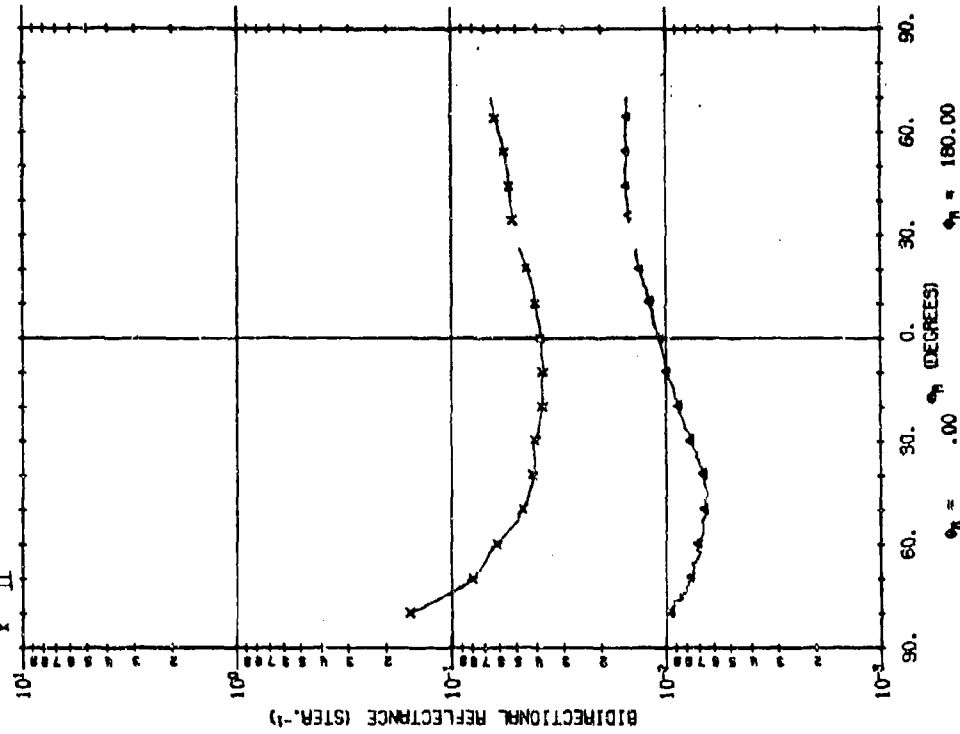
$\phi_1 = 0.0$   
 $\phi_2 = 180.0$   
 $\lambda = 0.63$



A01699 101

WOOD

$\phi_1 = 30.0$   
 $\phi_2 = 180.0$   
 $\lambda = 0.63$

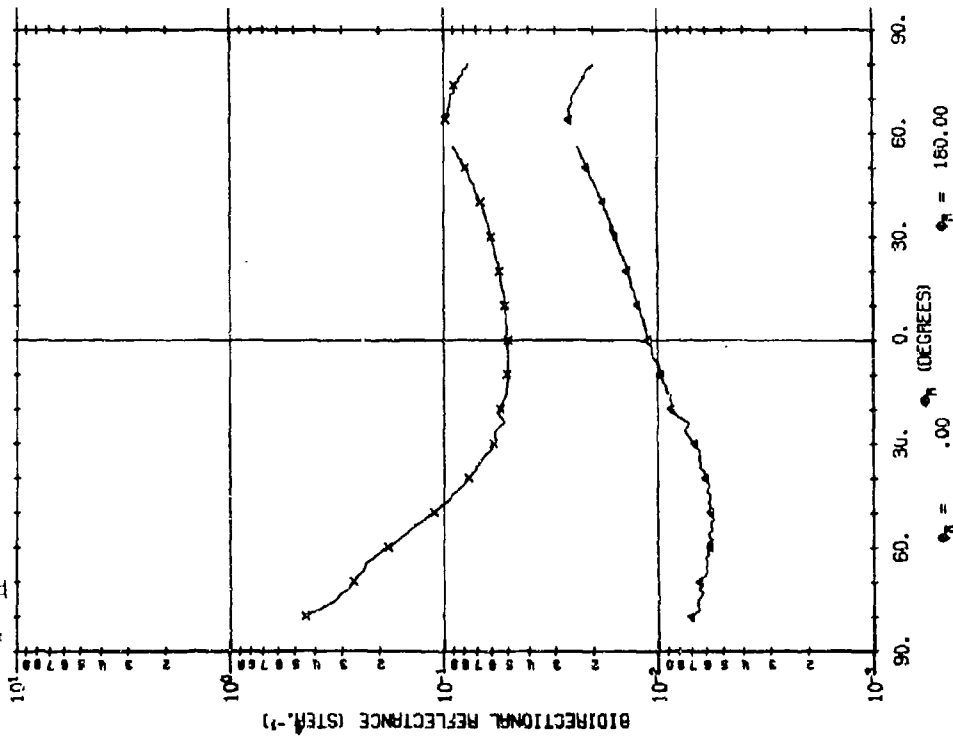


WOOD

A01699 101

WOOD

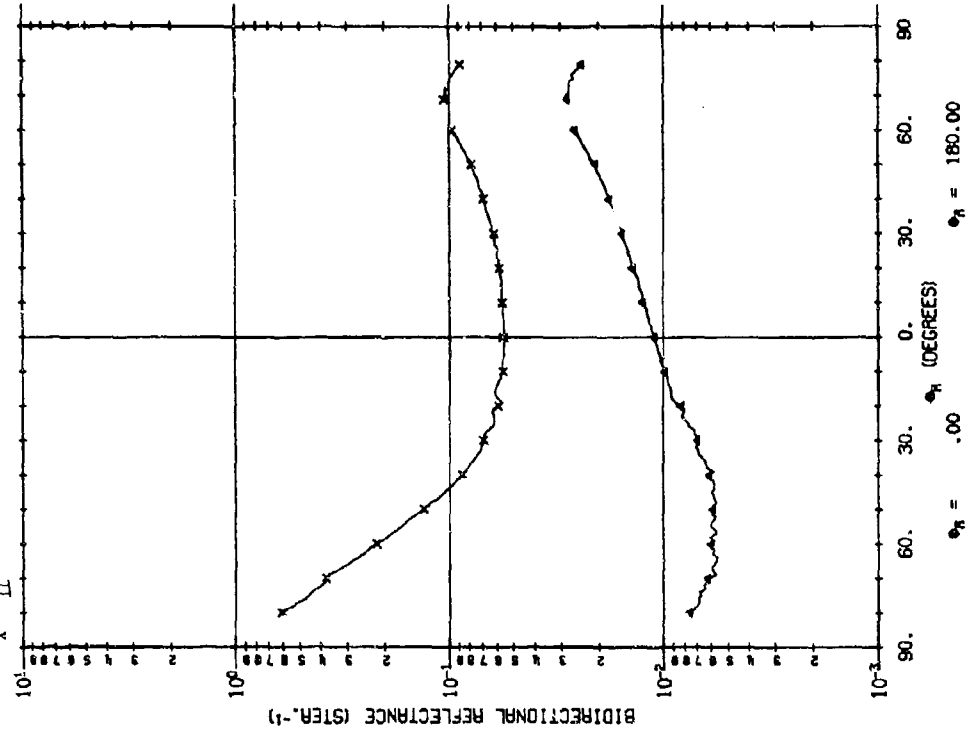
0 ||  $\theta_1 = 60.0$   
 + ||  $\theta_1 = 180.0$   
 Δ ||  $\lambda = 0.63$   
 x ||



A01699 101

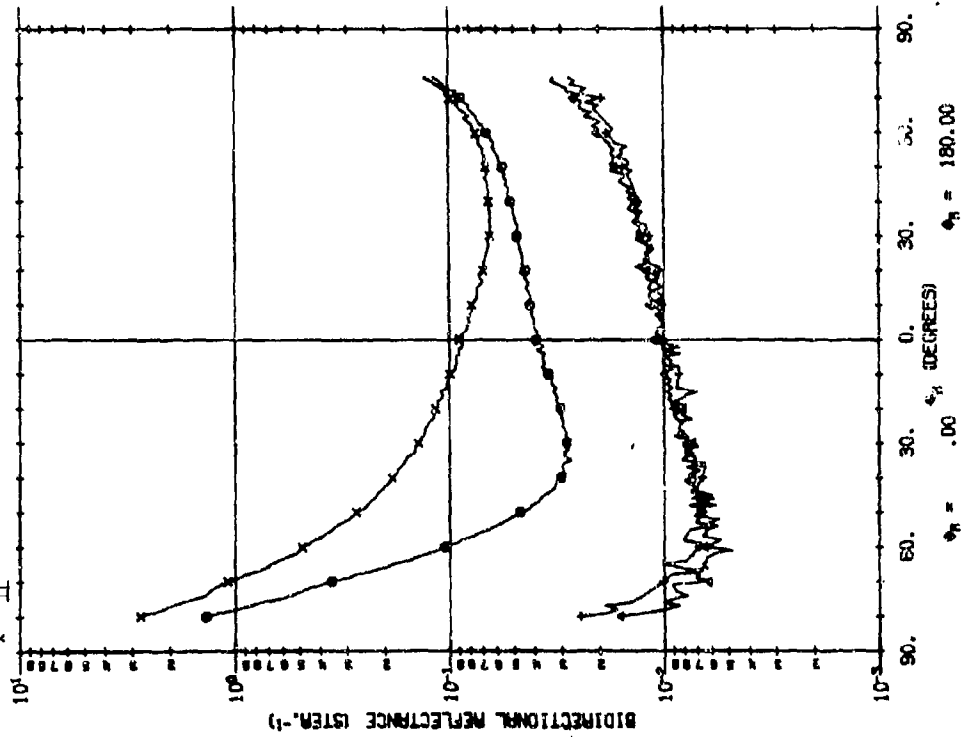
WOOD

0 ||  $\theta_1 = 65.0$   
 + ||  $\theta_1 = 180.0$   
 Δ ||  $\lambda = 0.63$   
 x ||



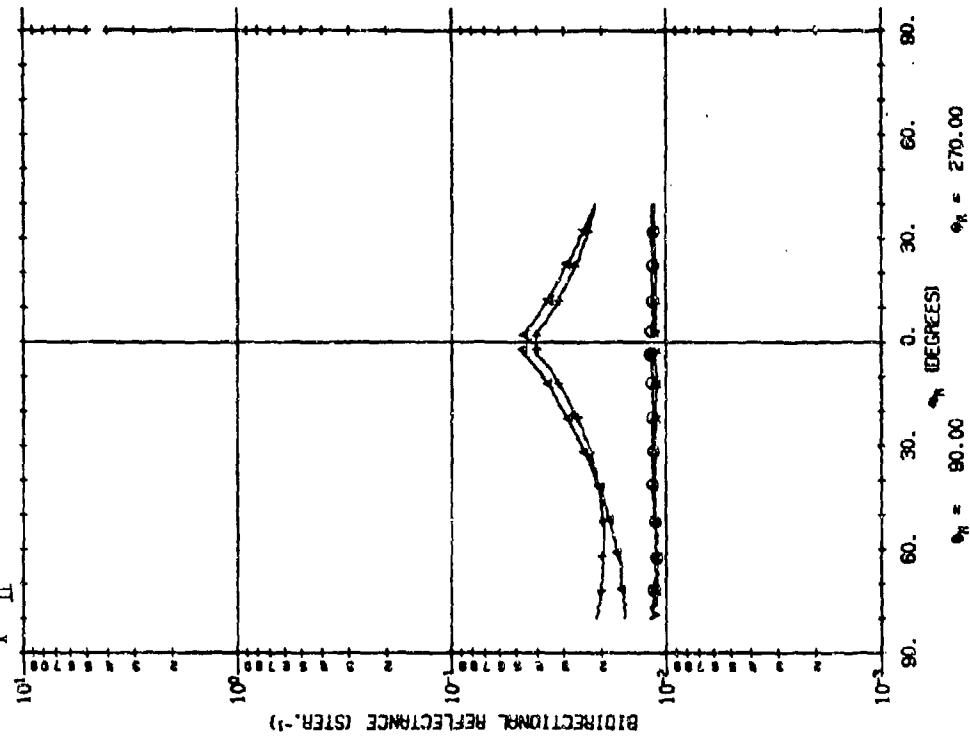
A01699 101  
 0 ||  $\theta_1 = 80.0$   
 + ||  $\theta_2 = 180.0$   
 Δ ||  $\lambda = 0.63$   
 x ||

WOOD



A01699 101  
 0 ||  $\theta_1 = 0.0$   
 + ||  $\theta_2 = 180.0$   
 Δ ||  $\lambda = 0.63$   
 x ||

WOOD

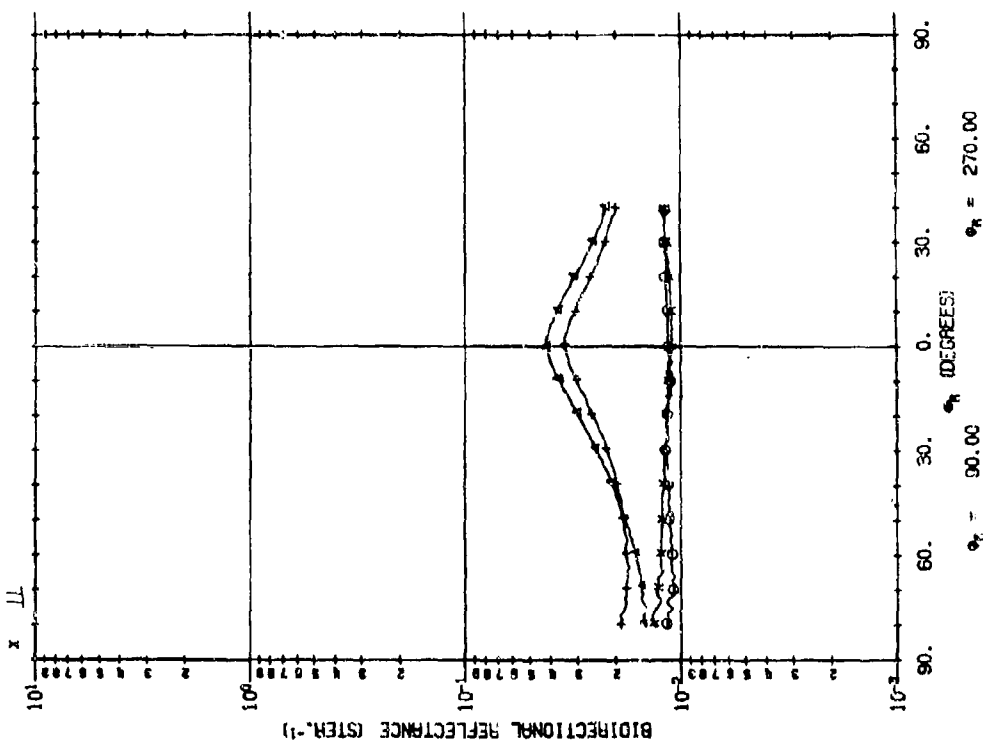


WOOD

R01699 101

WOOD

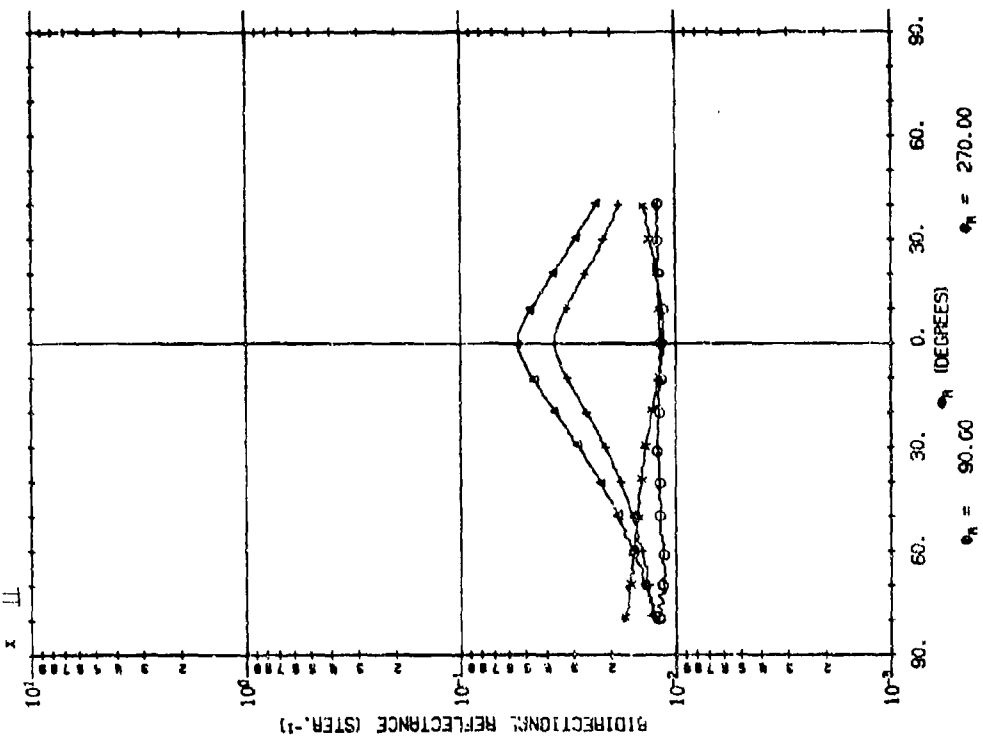
$\epsilon_1 = 39.0$   
 $\phi_1 = 180.0$   
 $\lambda = 0.63$



R01699 101

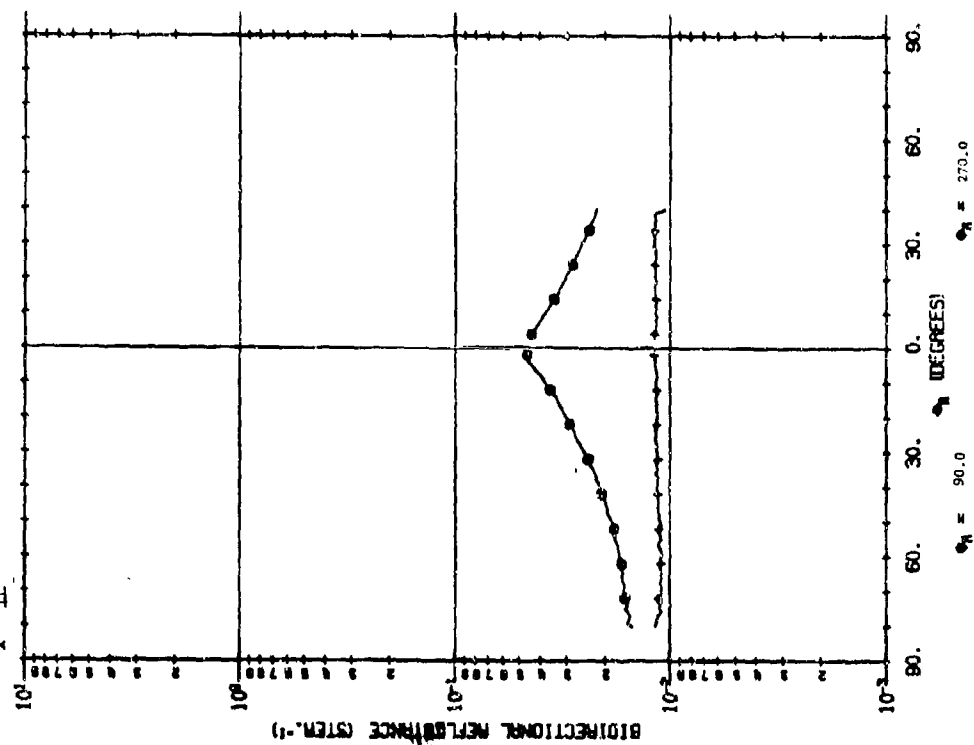
WOOD

$\epsilon_1 = 60.0$   
 $\phi_1 = 180.0$   
 $\lambda = 0.63$



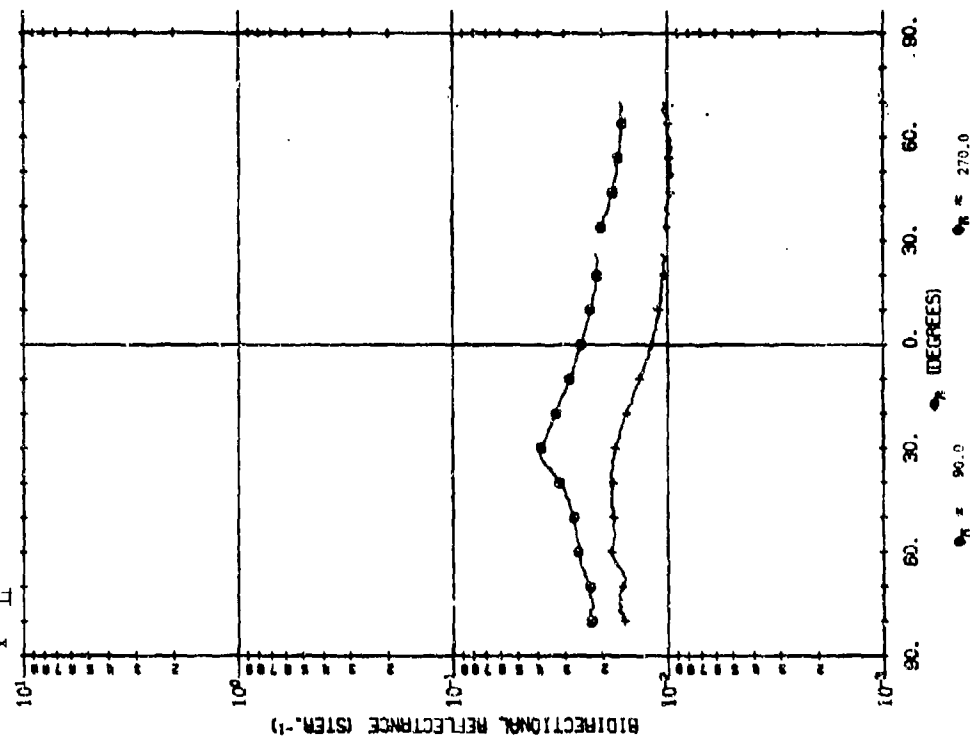
R01699 101  
 $\theta_1 = 0.0$   
 $\theta_2 = 270.0$   
 $\lambda = 0.63$

WOOD



R01699 101  
 $\theta_1 = 30.0$   
 $\theta_2 = 270.0$   
 $\lambda = 0.63$

WOOD

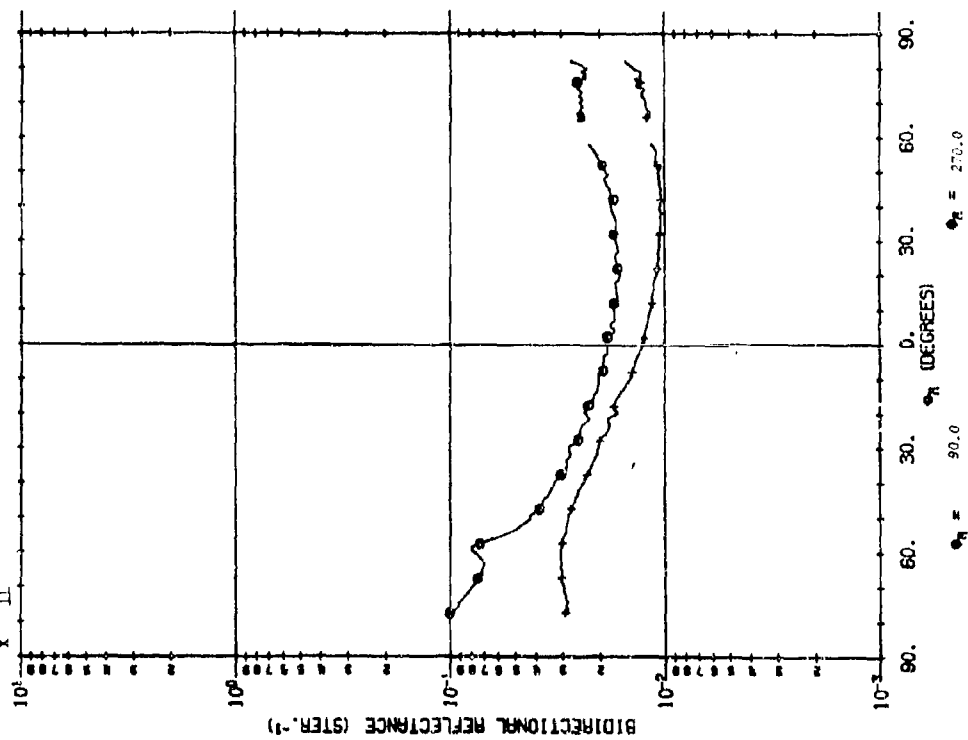


WOOD

AC1699 101

WOOD

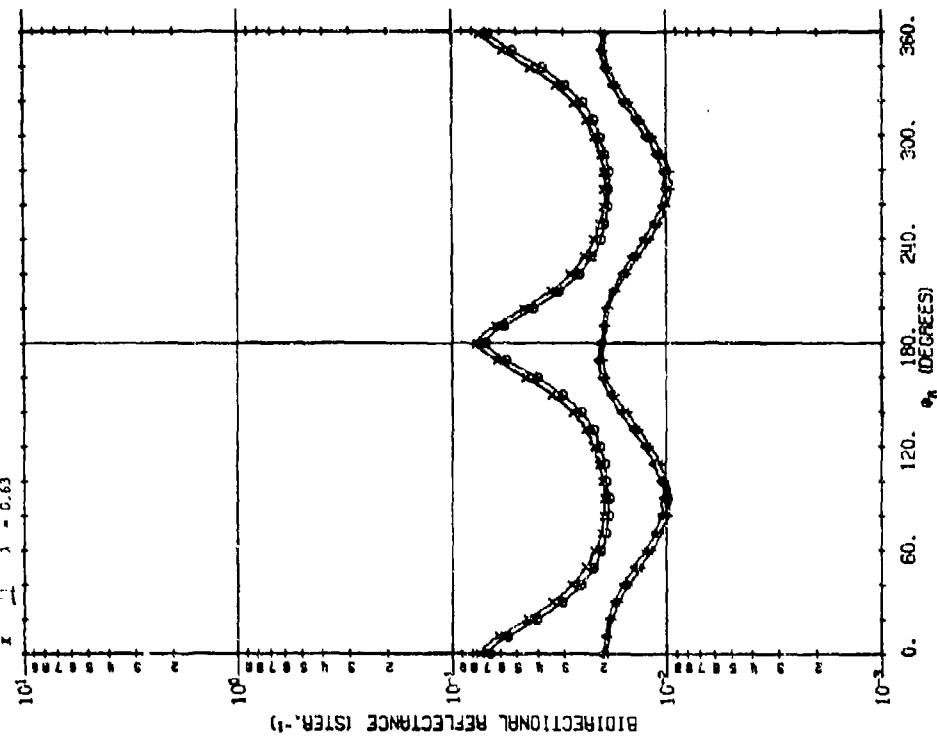
0  $\theta_i = 60.0$   
 +  $\theta_r = 270.0$   
 Δ  $\lambda = 0.63$   
 x  $\lambda = 0.63$



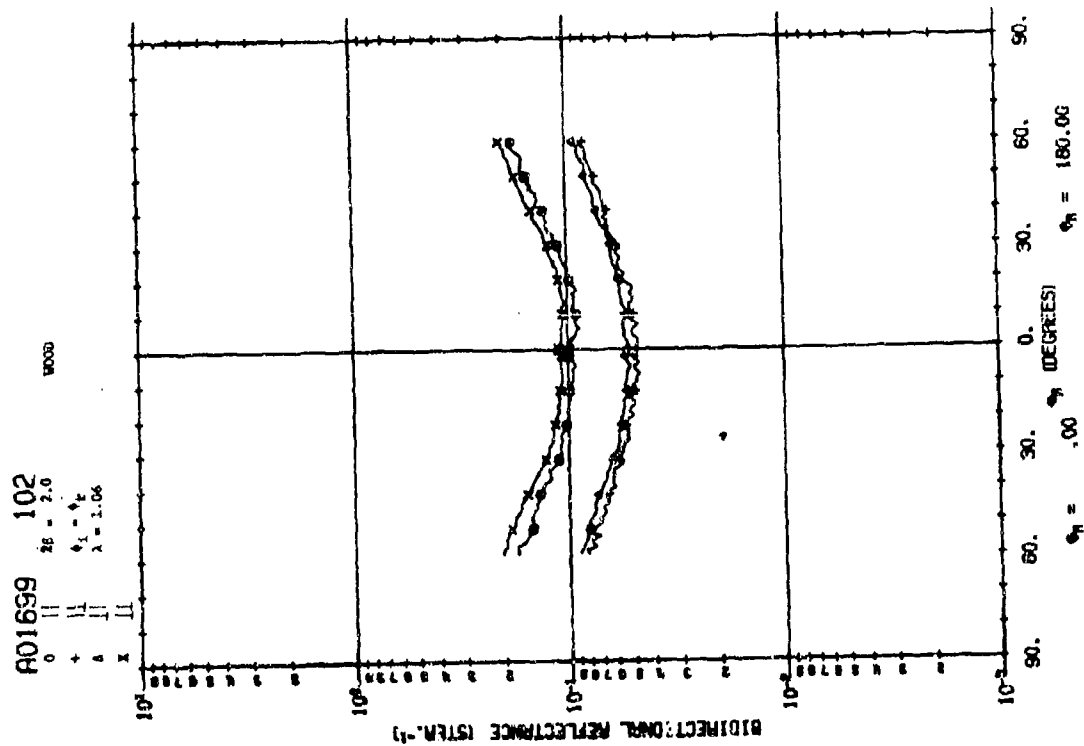
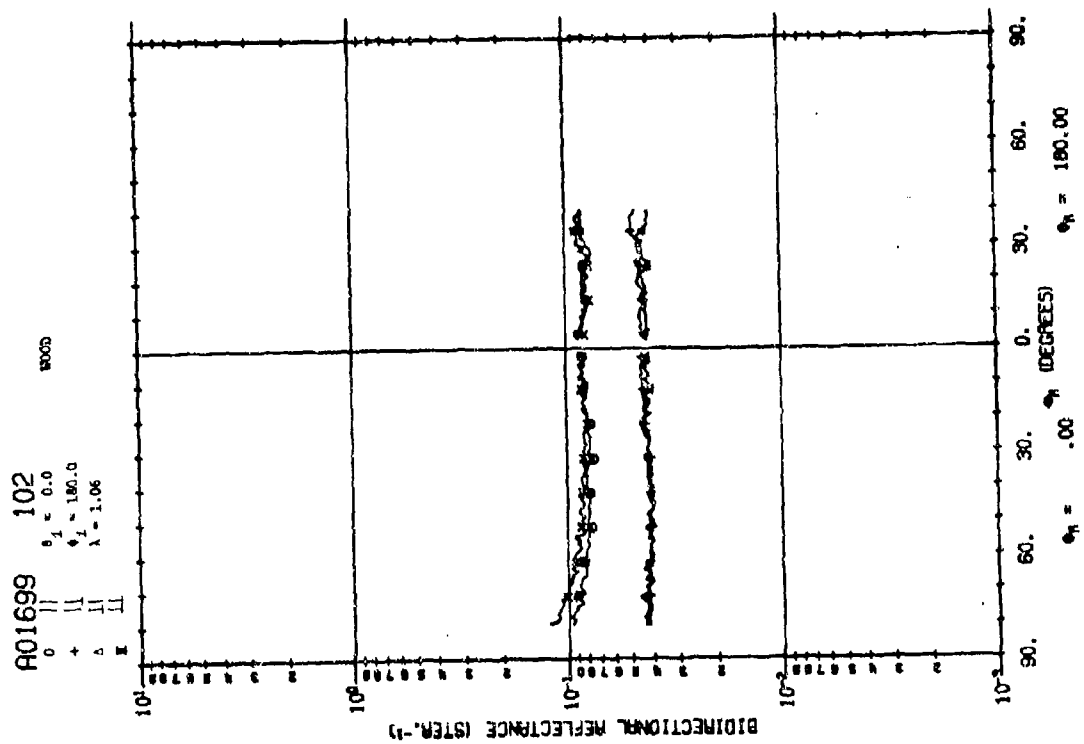
AC1699 101

WOOD

0  $\theta_i = 45.0$   
 +  $\theta_r = 47.0$ ,  $23 = 2.0$   
 Δ  $\theta_i = 60$   
 x  $\lambda = 0.63$





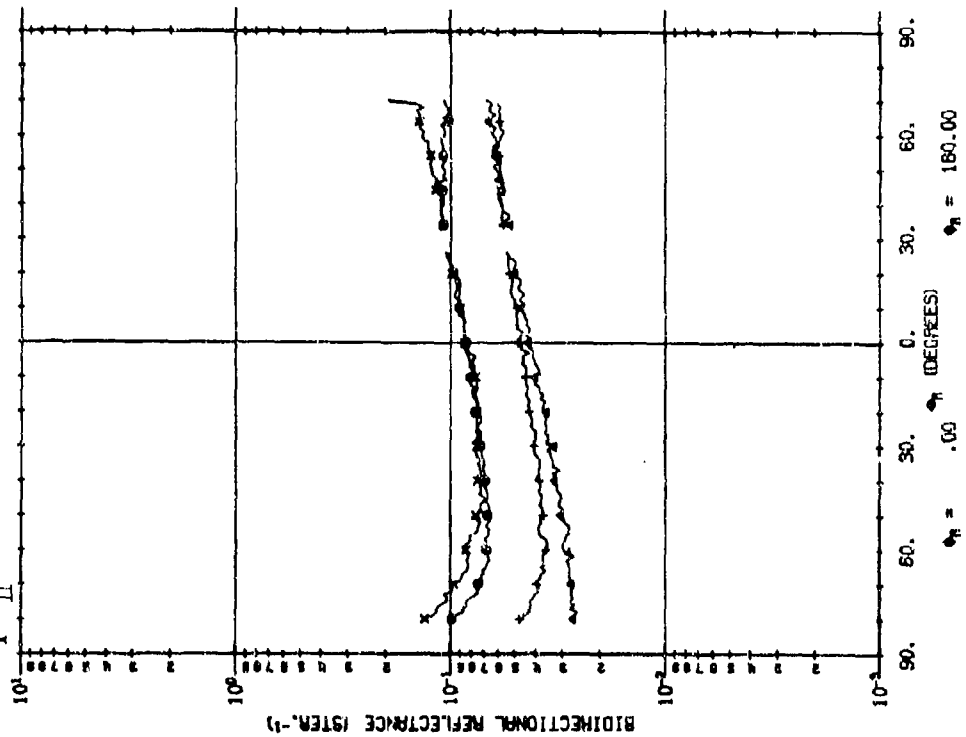


WOOD

R01699 102

WOOD

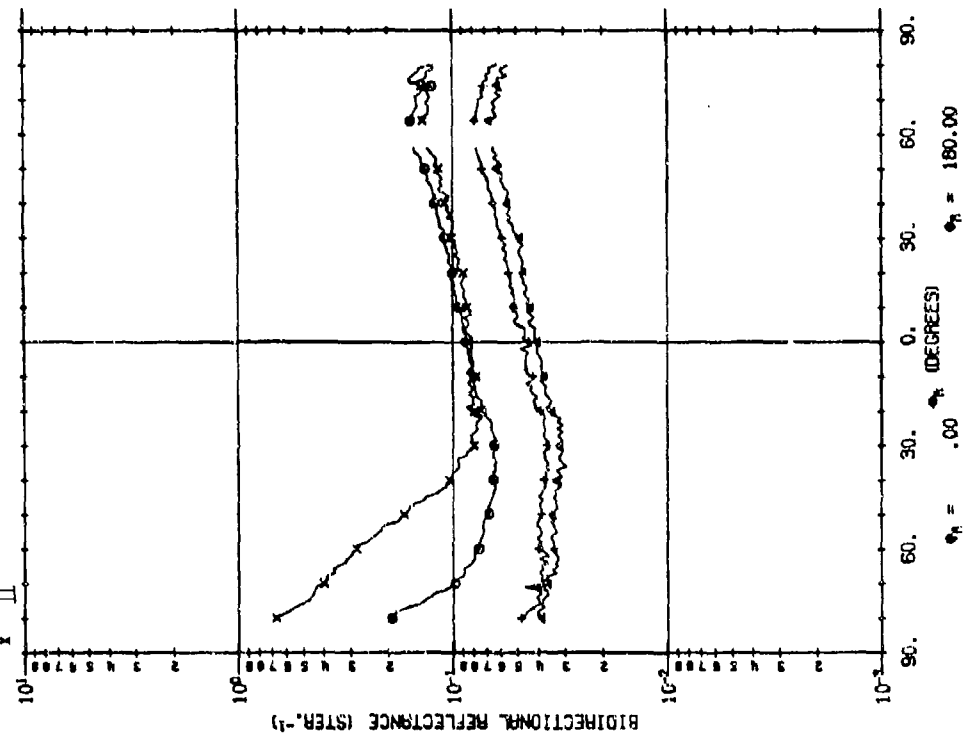
$\theta_1 = 30.0$   
 $\phi_1 = 180.0$   
 $\lambda = 1.06$



R01699 102

WOOD

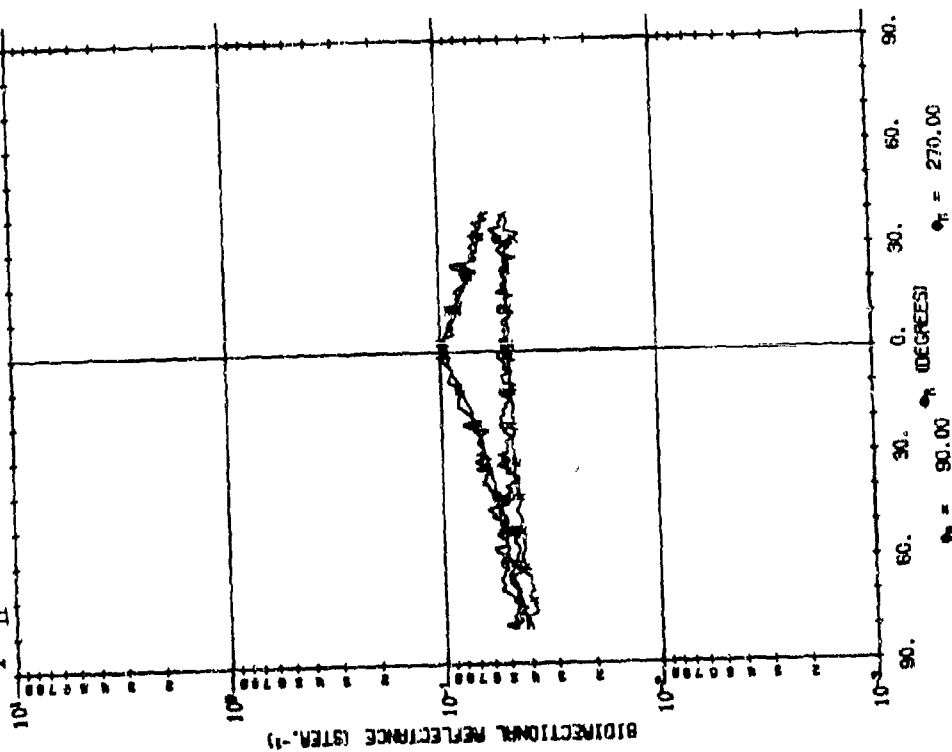
$\theta_1 = 60.0$   
 $\phi_1 = 180.0$   
 $\lambda = 1.06$



R01699 102

WOOD

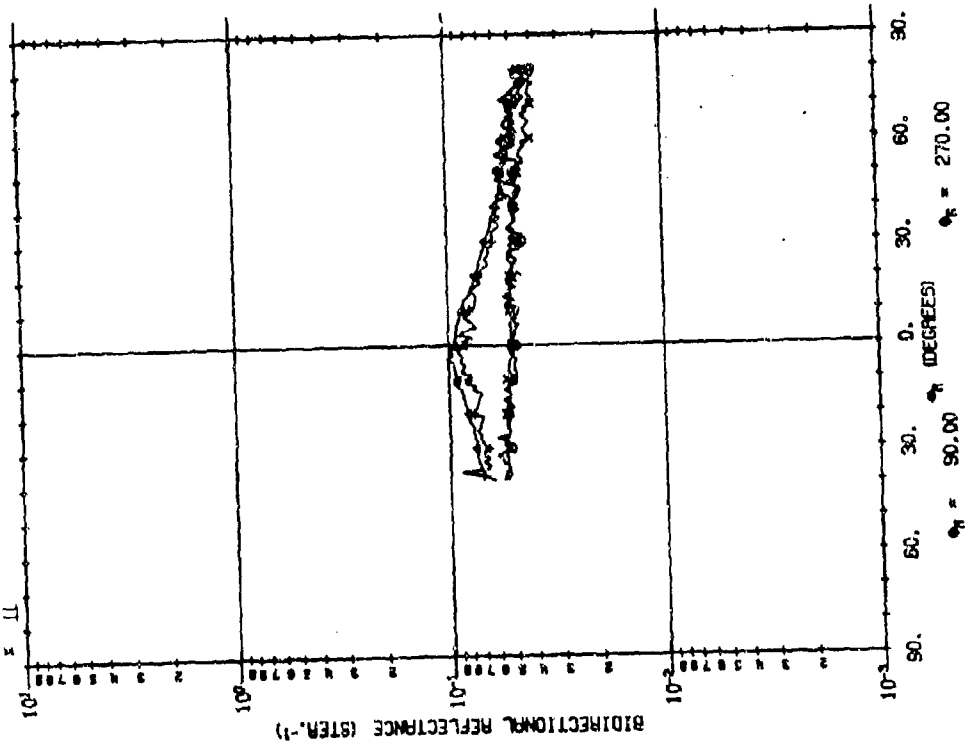
$\theta_i = 0.0$   
 $\phi_i = 120.0$   
 $\lambda = 1.06$



R01699 102

WOOD

$\theta_i = 30.0$   
 $\phi_i = 180.0$   
 $\lambda = 1.06$

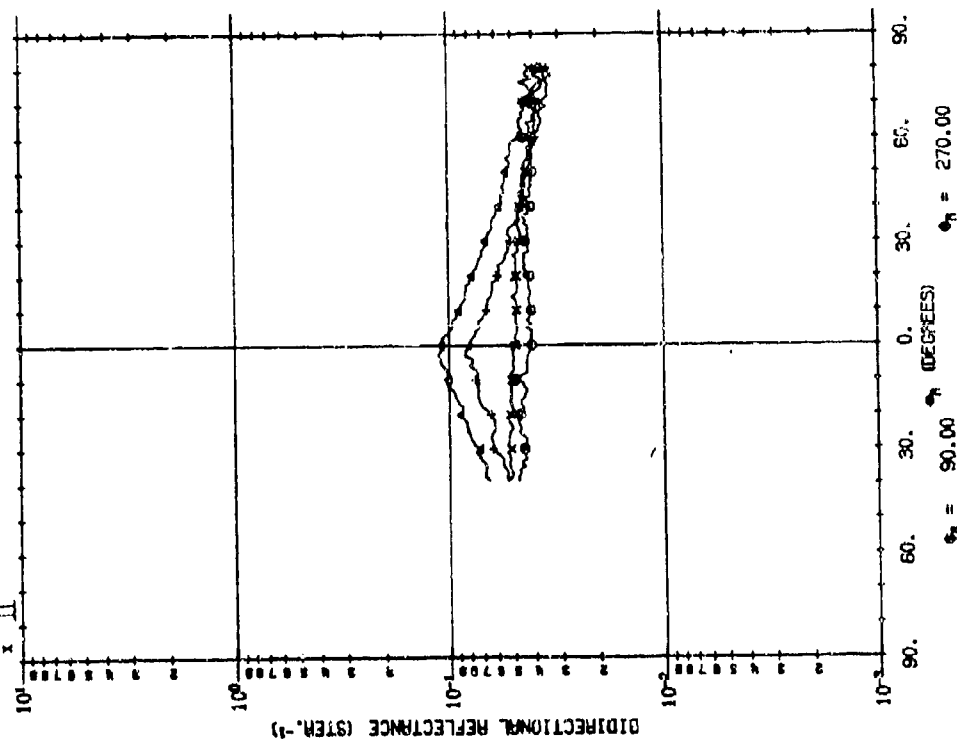


WOOD

A01699 102

WOOD

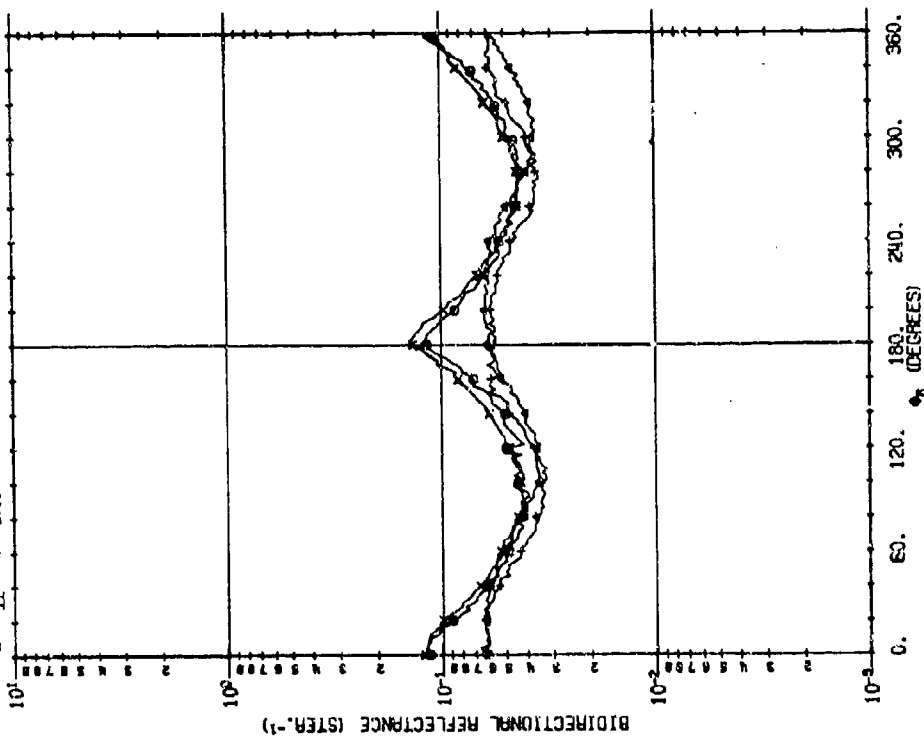
0 ||  $\theta_1 = 63.0$   
 + ||  $\theta_2 = 180.0$   
 x ||  $\lambda = 1.06$



A01699 102

WOOD

0 ||  $\theta_1 = 45.0$   
 + ||  $\theta_2 = 47.0$   
 x ||  $\theta_1 = \theta_2$   
 ||  $\lambda = 1.06$

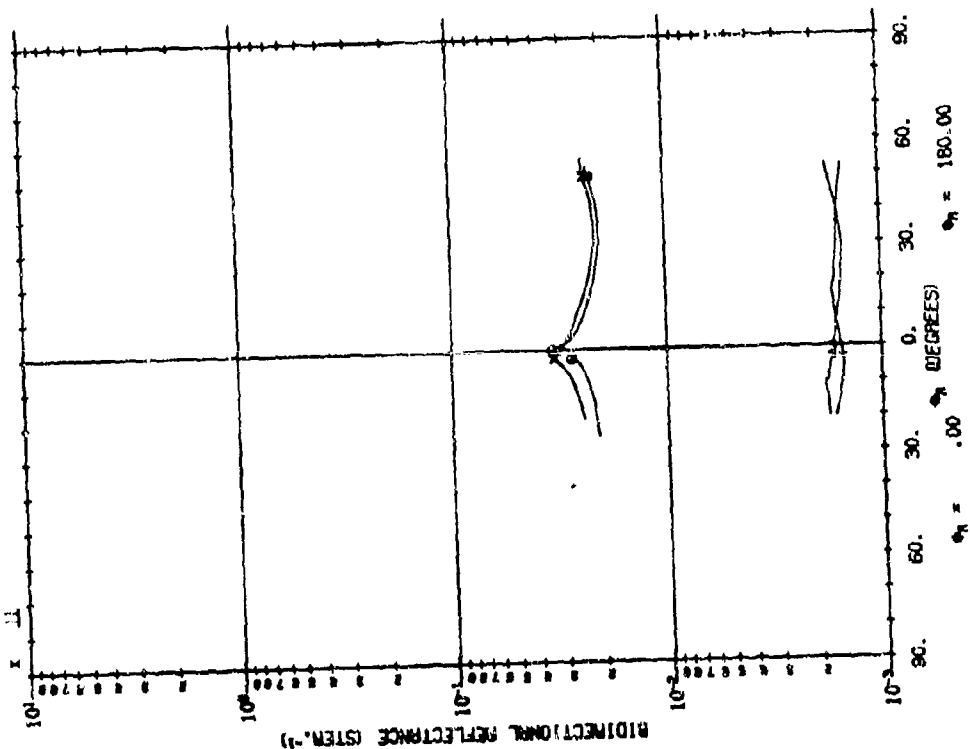


SOIL

R01959 101

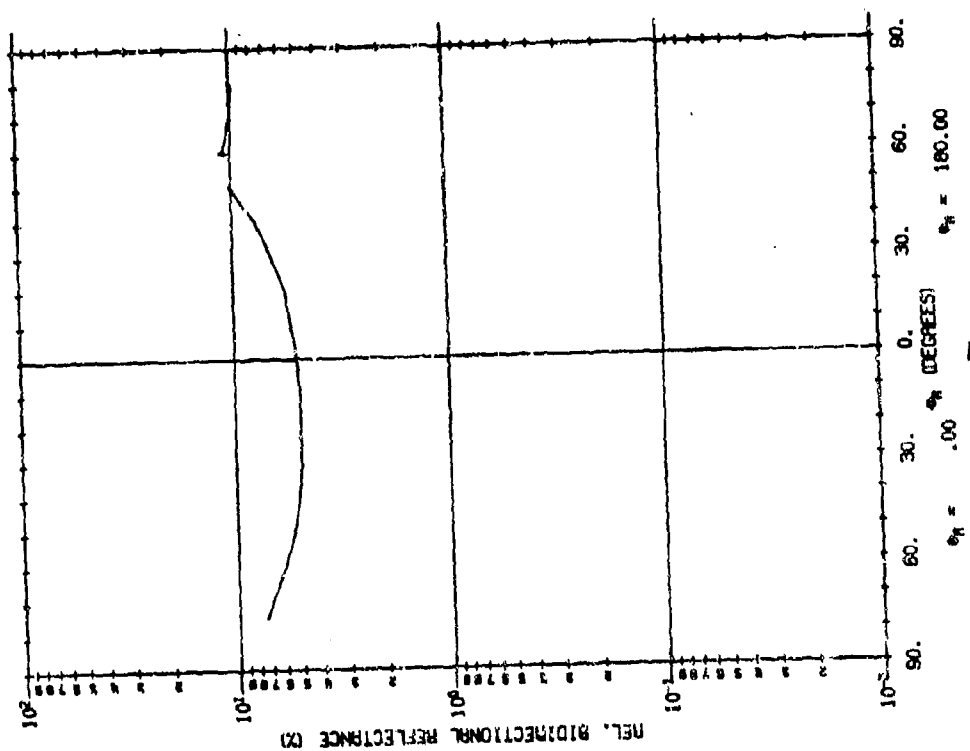
SAME WITH OTHER PARTICLES IN IT  
FROM CALIFORNIA

0 11 28 = 2.5  
+ 11  $\phi_1 = \phi_2$   
A 11  $\lambda = 10.6$



B09010 014

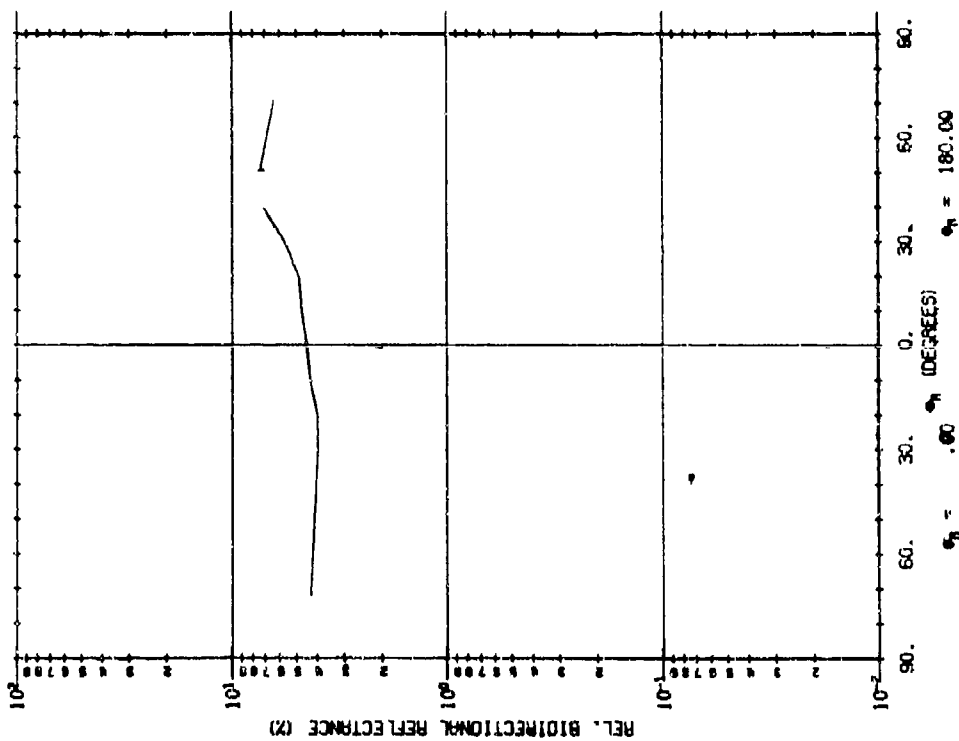
1 - 07 RED CLAY, DNE  
 $\lambda = .4920$   
 $\phi_1 = 51.0$   
 $\phi_2 = 180.0$



SOIL

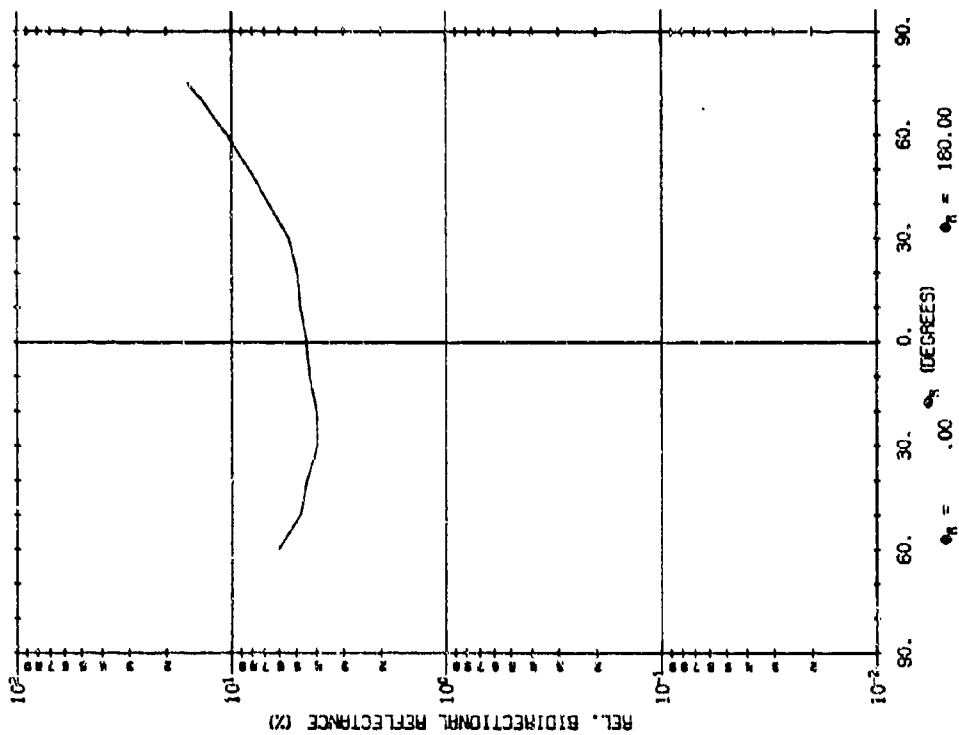
809010 019

UT  
 $\lambda = .5200$  RED CLAY, DRY  
 $\theta_1 = 45.0$   
 $\phi_1 = 180.0$



809010 017

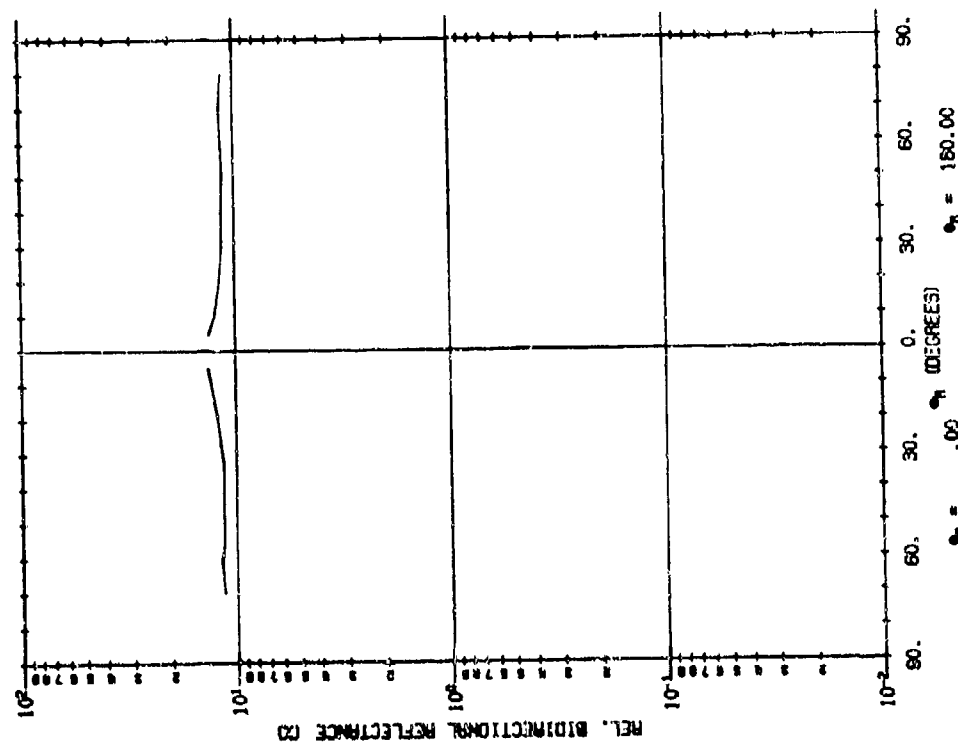
UT  
 $\lambda = .5200$  RED CLAY, DRY  
 $\theta_1 = 85.0$   
 $\phi_1 = 185.0$



609010 006

1 - UT  
 1 = .6430  
 $\phi_1 = 0.0$   
 $\phi_2 = 180.0$

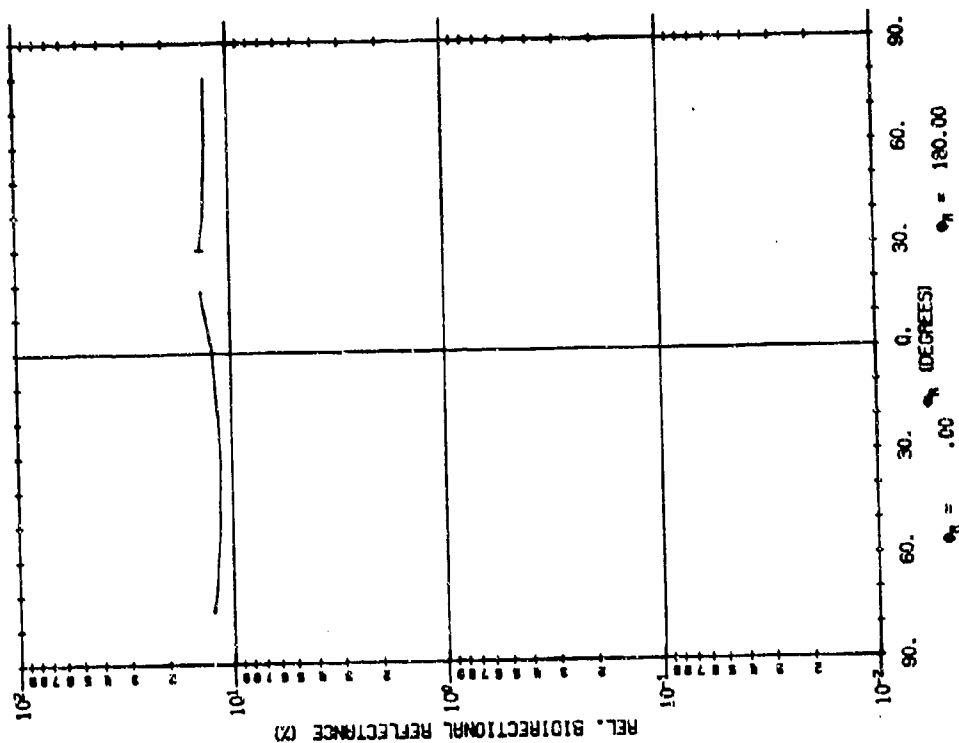
RED CLAY, DRY



609010 005

1 - UT  
 1 = .6430  
 $\phi_1 = 23.0$   
 $\phi_2 = 180.0$

RED CLAY, DRY



SOIL



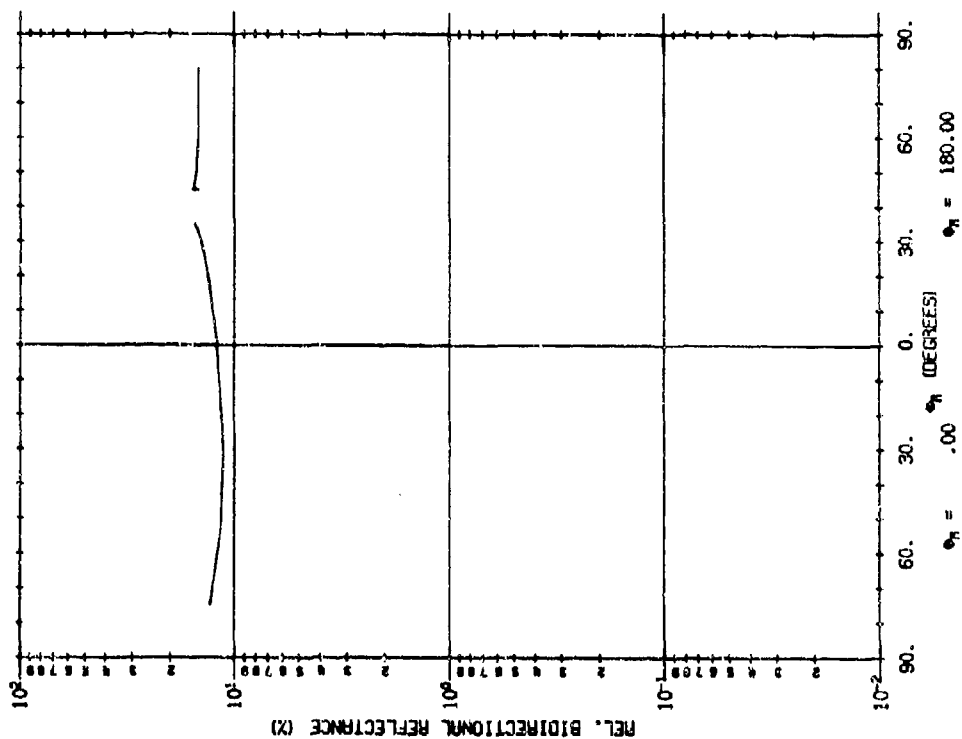
809010 004

RED CLAY, DRY

$\lambda = .6430$   
 $\phi_1 = 37.0$   
 $\phi_2 = 180.0$

RED CLAY, DRY

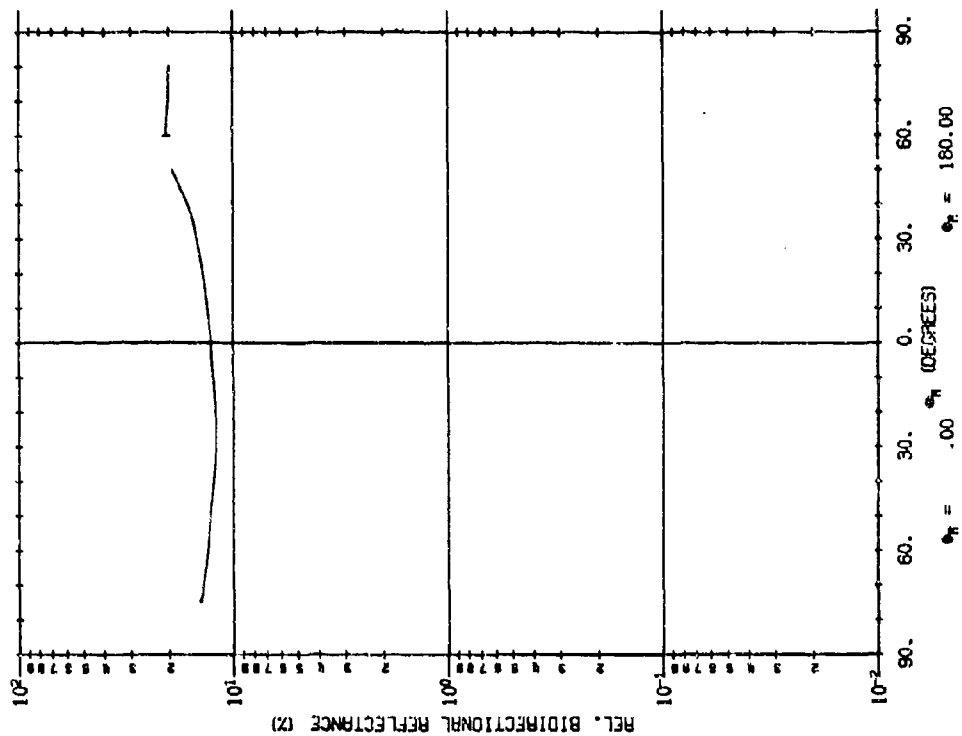
$\lambda = .6430$   
 $\phi_1 = 37.0$   
 $\phi_2 = 180.0$



809010 003

RED CLAY, DRY

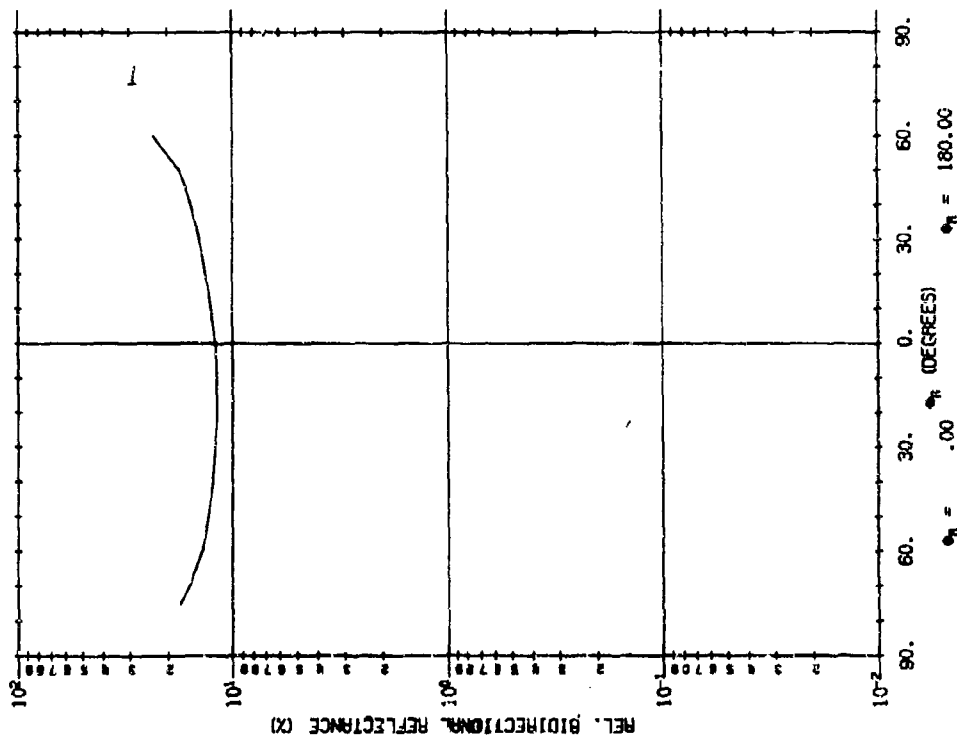
$\lambda = .6430$   
 $\phi_1 = 37.0$   
 $\phi_2 = 180.0$



B09010 002

λ = .6430  
 ρ<sub>1</sub> = 65.0  
 ϕ<sub>1</sub> = 180.0

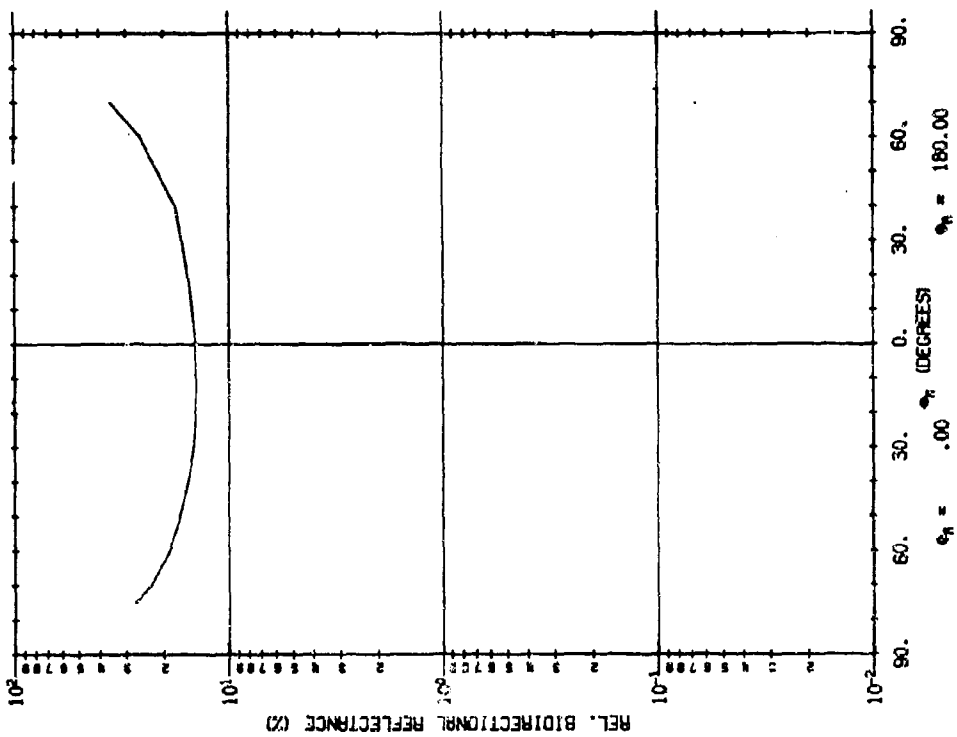
RED CLAY, DRY



B09010 001

λ = .6430  
 ρ<sub>1</sub> = 78.0  
 ϕ<sub>1</sub> = 180.0

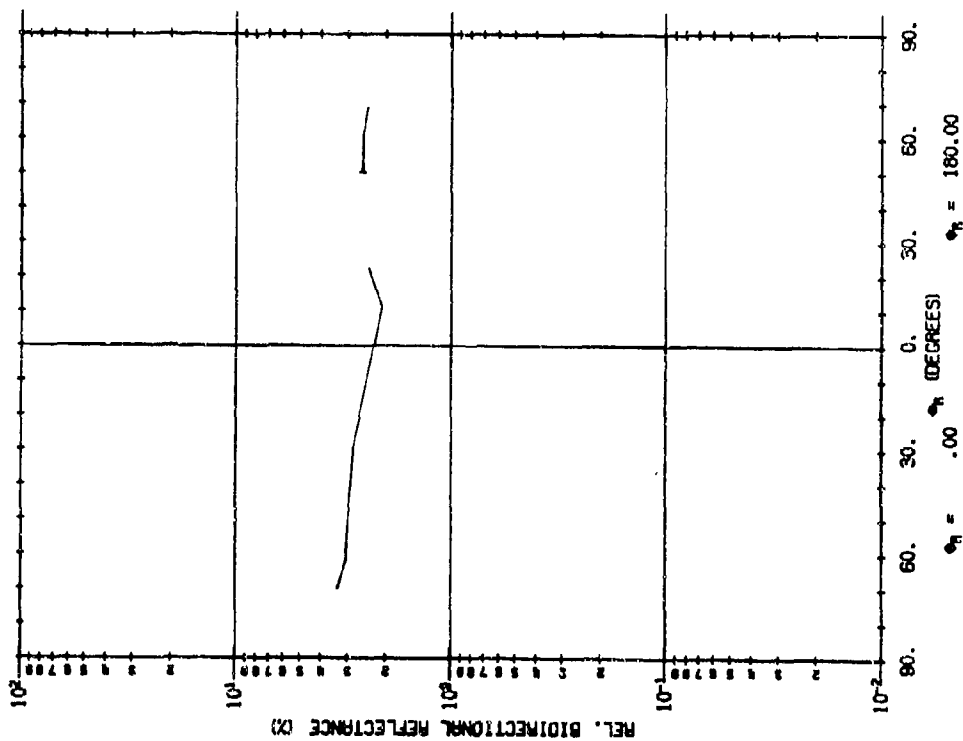
RED CLAY, DRY



SOIL

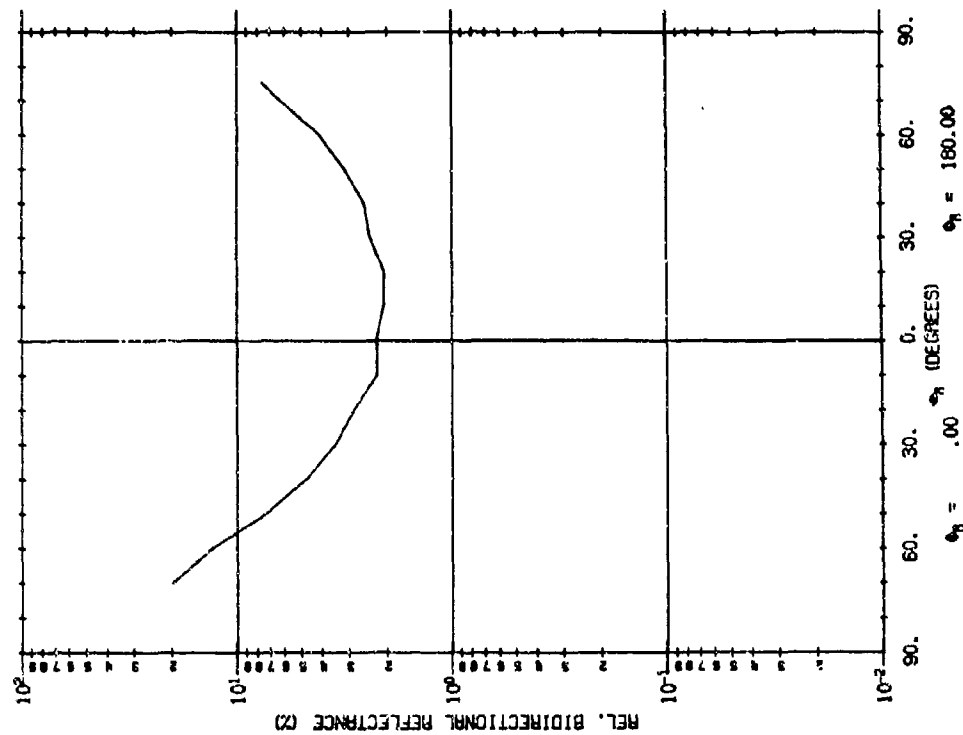
B09010 020

$\lambda = 0.5200$  RED CLAY, WET  
 $\phi_1 = 45.0$   
 $\phi_2 = 180.0$



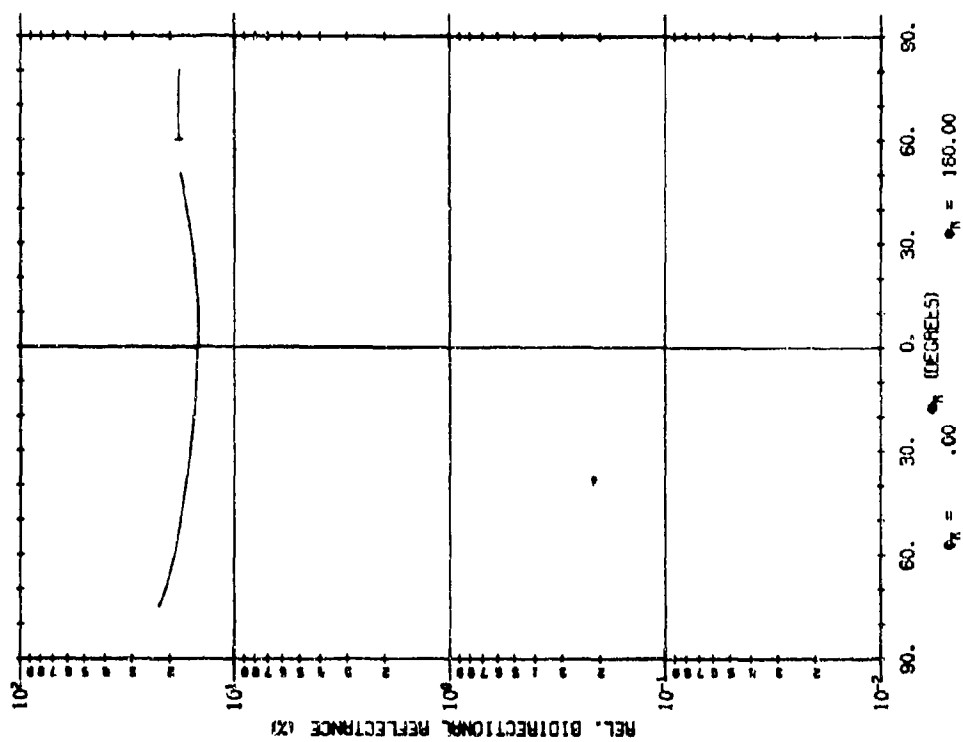
B09010 018

$\lambda = 0.5200$  RED CLAY, WET  
 $\phi_1 = 80.0$   
 $\phi_2 = 180.0$



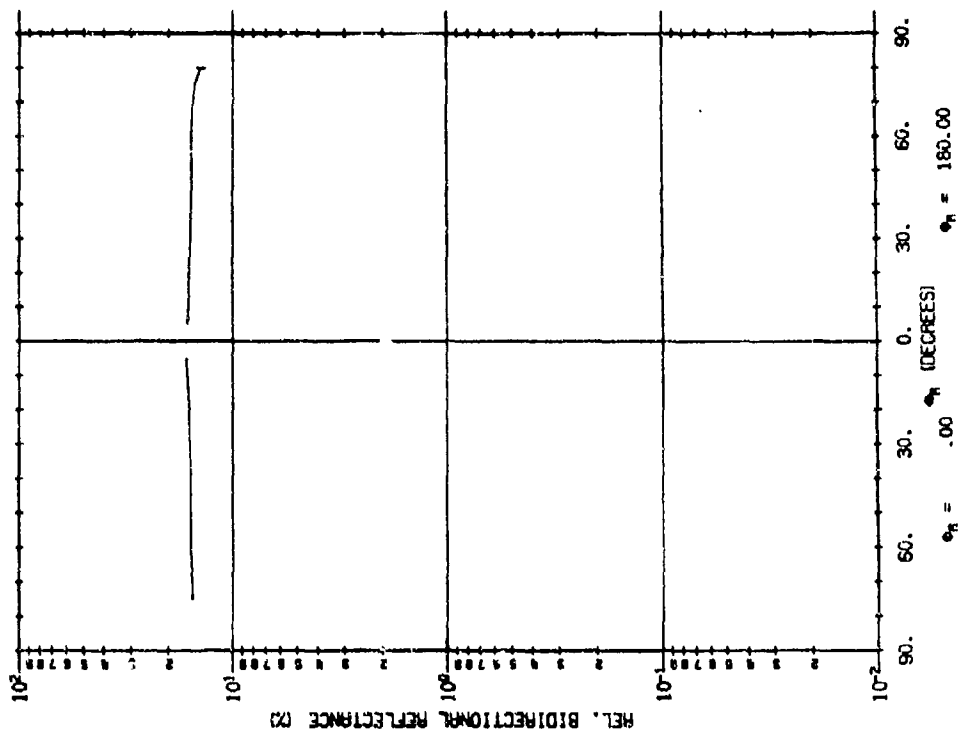
B09010 041

WHITE QUARTZ SAND  
 $\lambda = .4920$   
 $\phi_1 = 53.6$   
 $\phi_2 = 180.0$



B09010 030

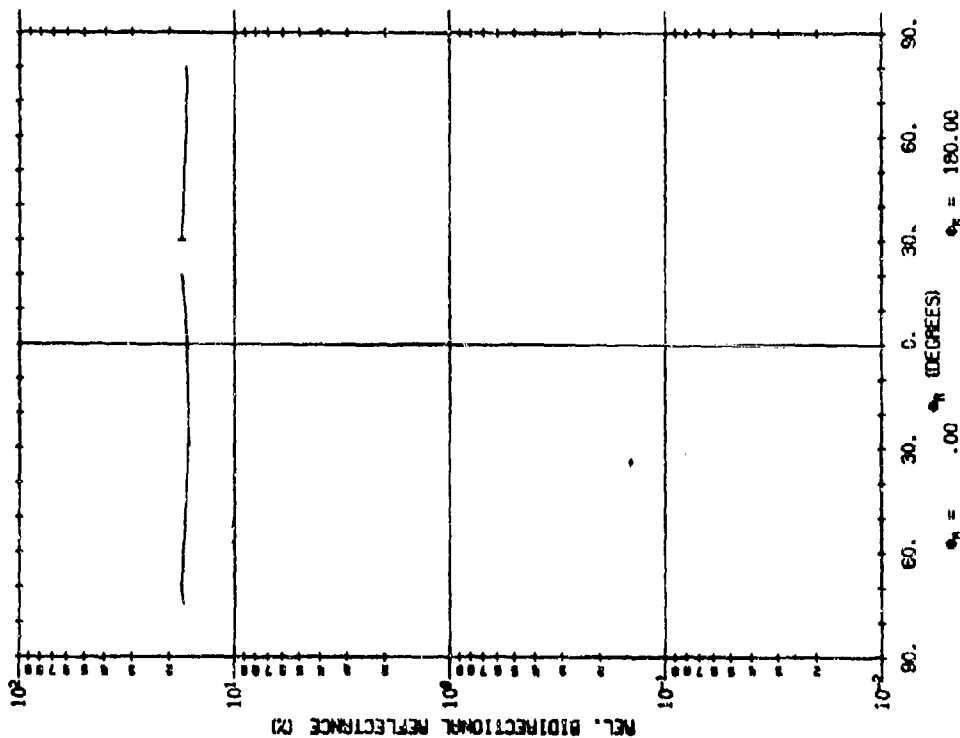
WHITE QUARTZ SAND  
 $\lambda = .6130$   
 $\phi_1 = 0.0$   
 $\phi_2 = 180.0$



SOIL

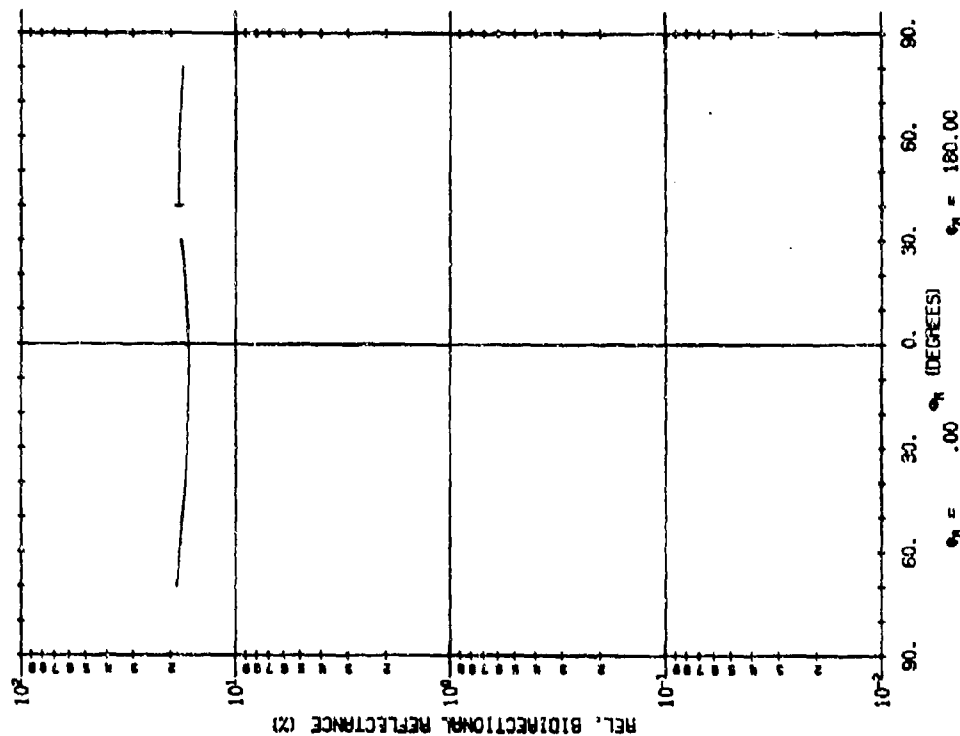
B09010 029

| - UT  $\lambda = 6430$  WHITE QUARTZ SAND  
 $\phi_1 = 23.0$   
 $\phi_2 = 180.0$



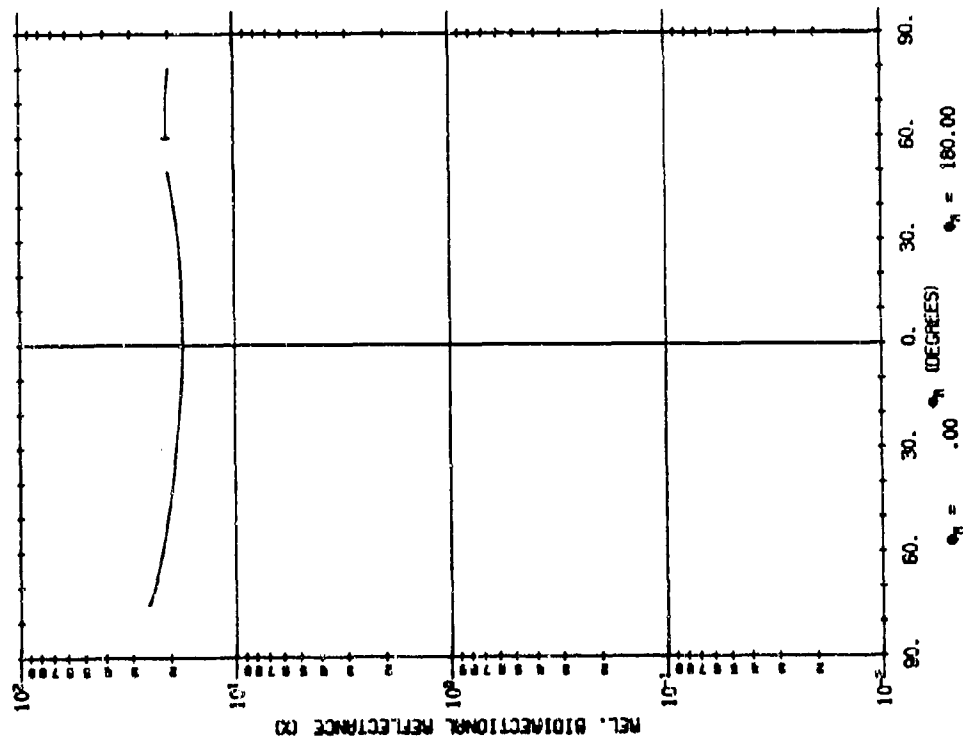
B09010 028

| - UT  $\lambda = 6430$  WHITE QUARTZ SAND  
 $\phi_1 = 27.0$   
 $\phi_2 = 180.0$



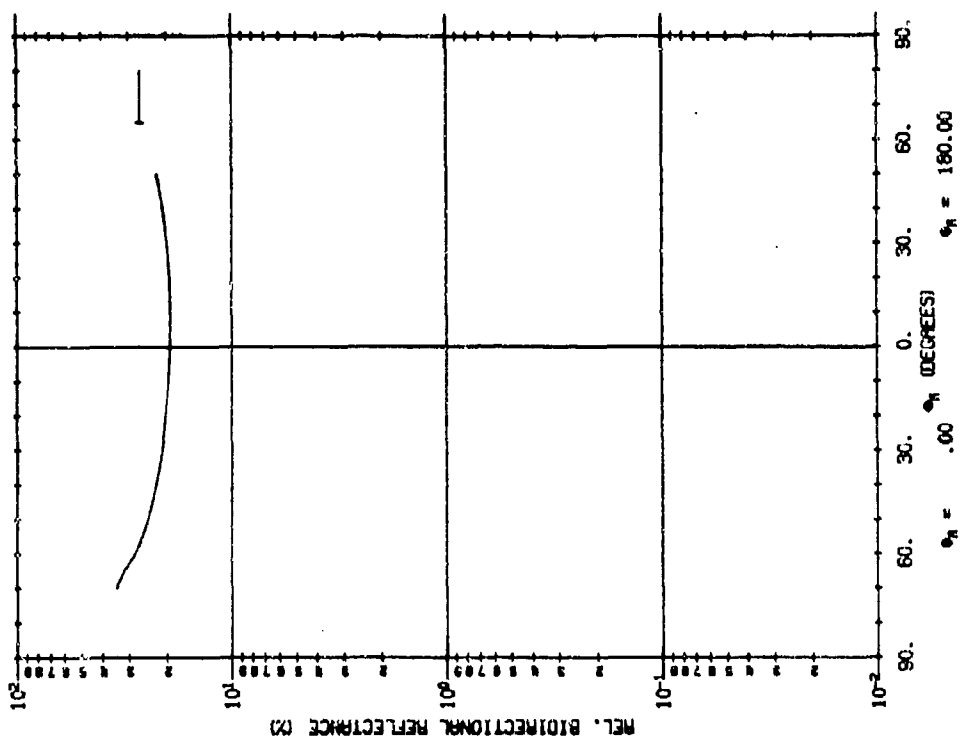
B09010 027

| - UT WHITE QUARTZ SAND  
 $\lambda = .6430$   
 $\phi_1 = 53.0$   
 $\phi_2 = 180.0$



B09010 026

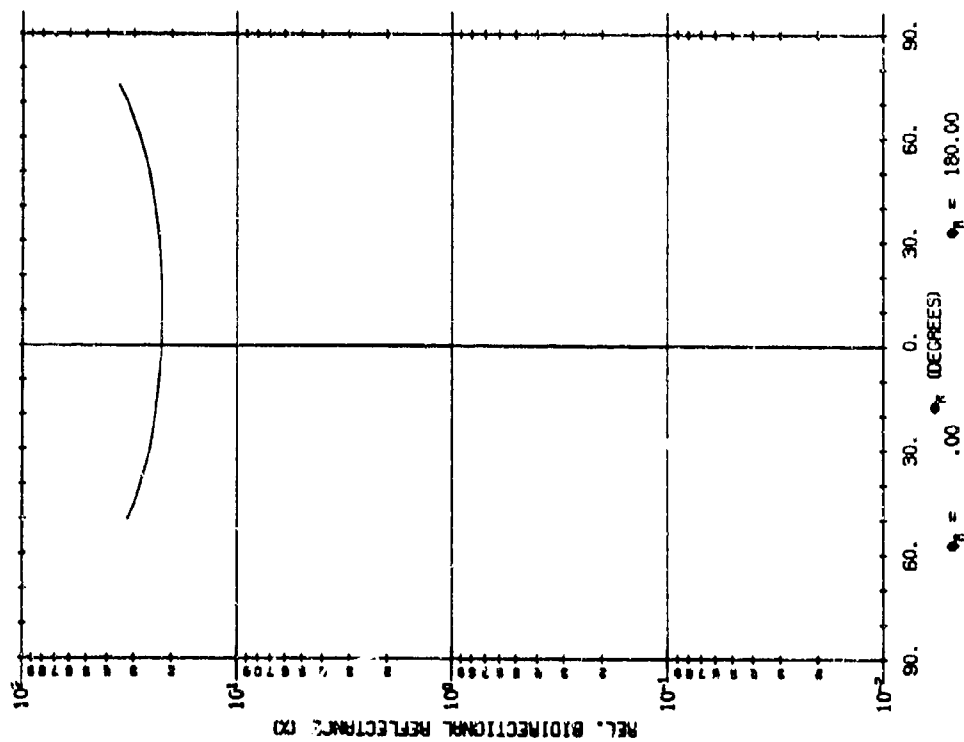
| - UT WHITE QUARTZ SAND  
 $\lambda = .6430$   
 $\phi_1 = 66.0$   
 $\phi_2 = 180.0$



SOIL

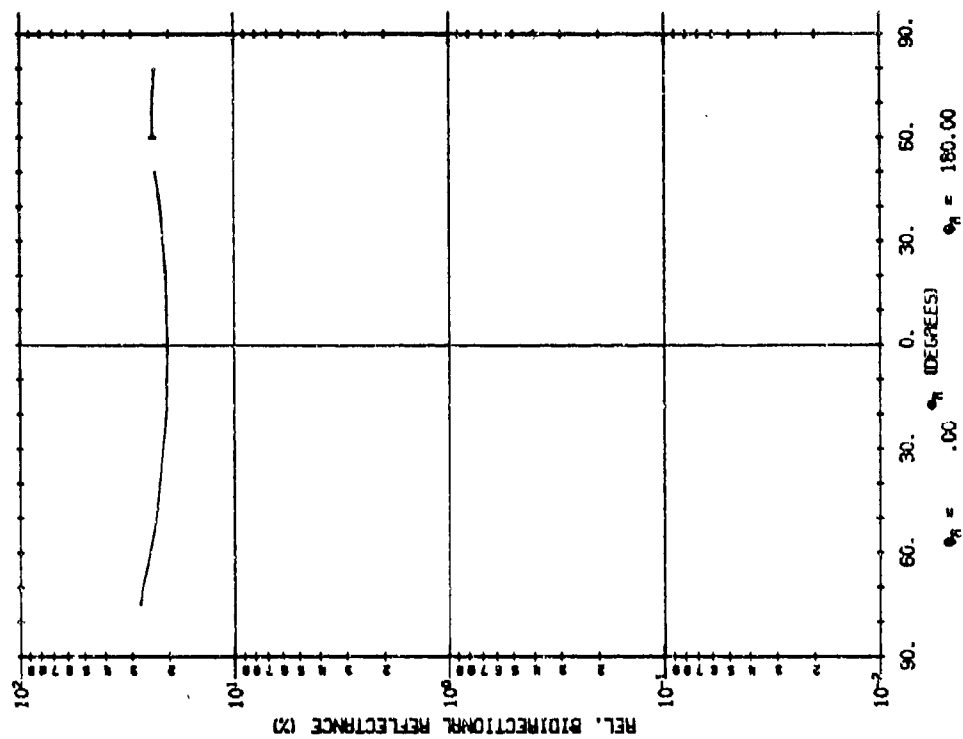
B09010 025

$\lambda = 0.7$  WHITE QUARTZ SAND  
 $\phi_1 = 78.0$   
 $\phi_2 = 180.0$



B09010 039

$\lambda = 0.7$  WHITE QUARTZ SAND  
 $\phi_1 = 53.0$   
 $\phi_2 = 180.0$



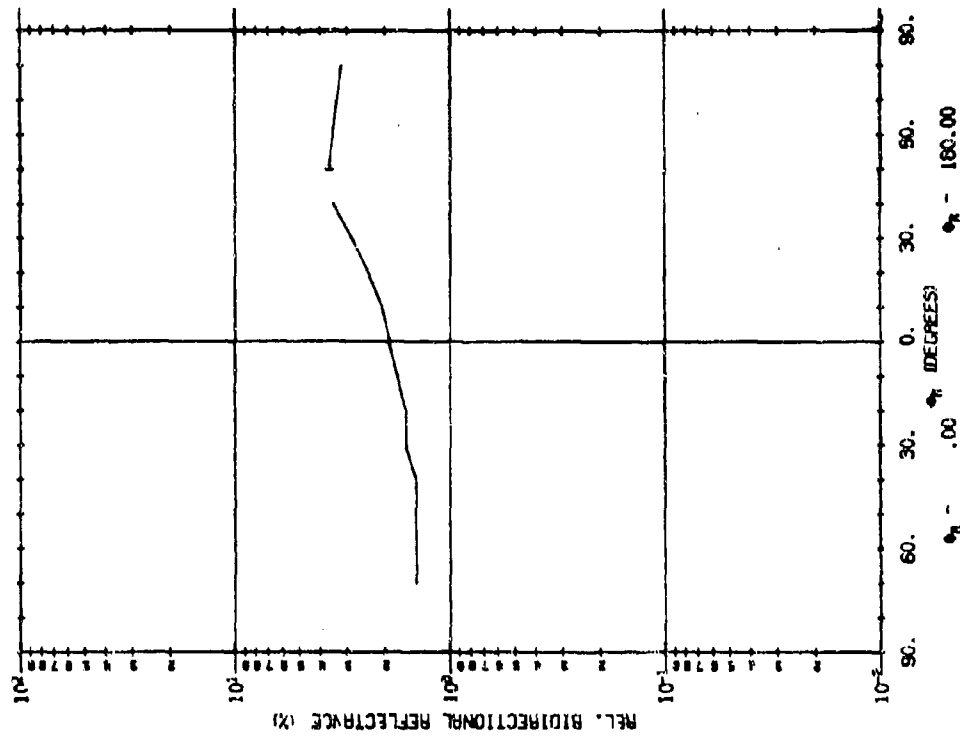
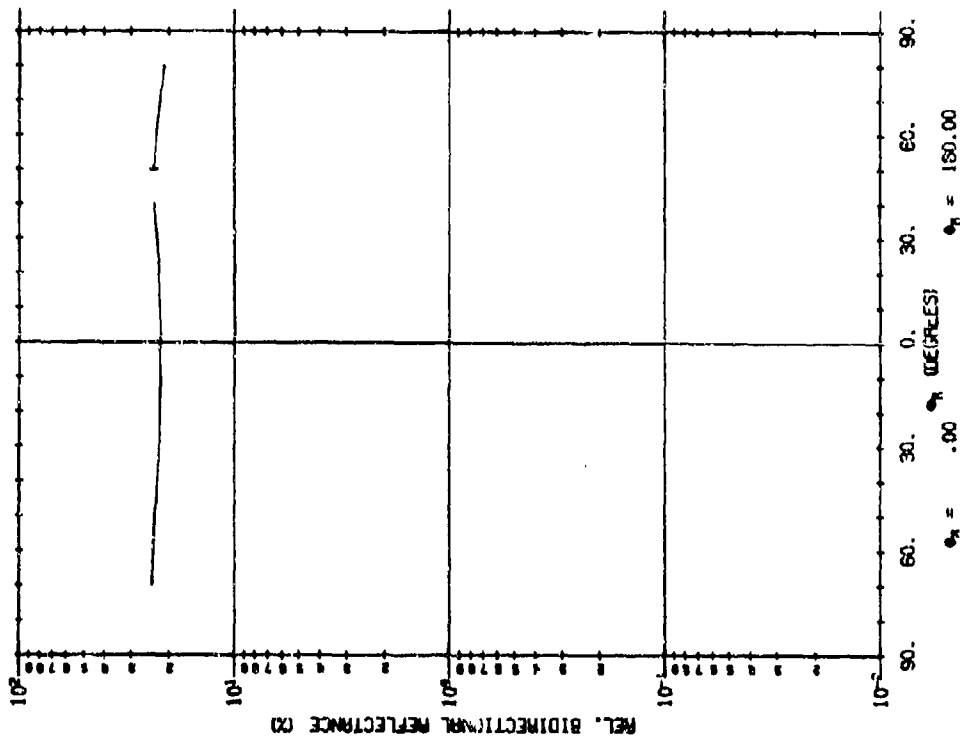
B09010 045

WHITE CFT-304 SAND  
 $\lambda = .5200$   
 $\phi_1 = 50.0$   
 $\phi_2 = 180.0$

I - UT

BLACK LOAN SOIL  
 $\lambda = .5200$   
 $\phi_1 = 50.0$   
 $\phi_2 = 180.0$

B09010 045



SOIL

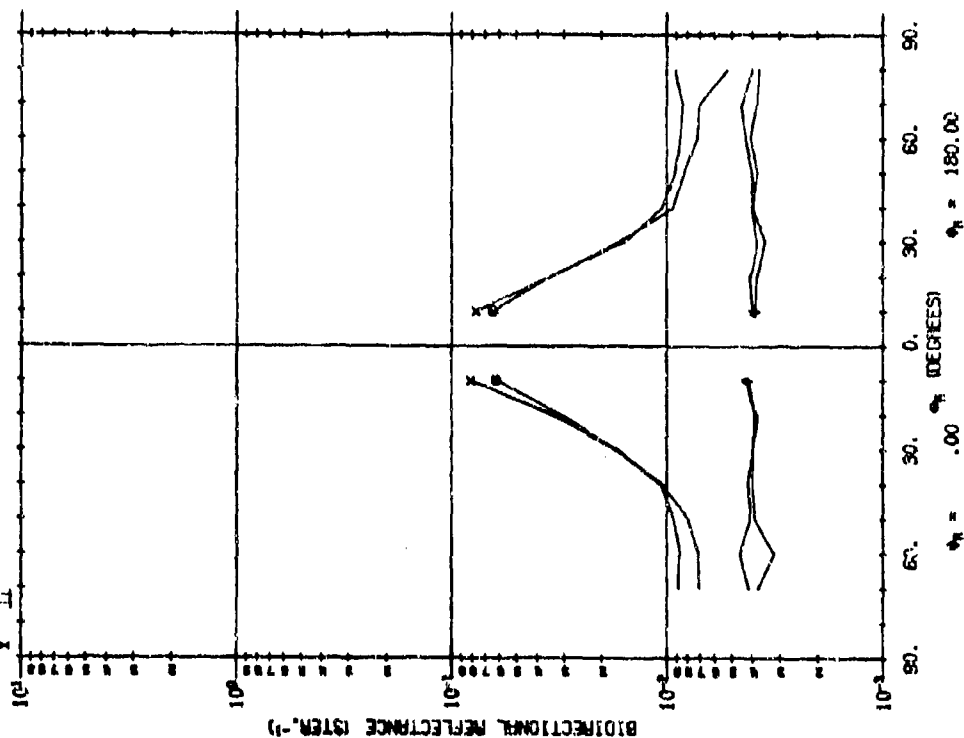


VEGETATION

R01324 001

MATURE MULBERRY LEAF, 2 HOURS OLD

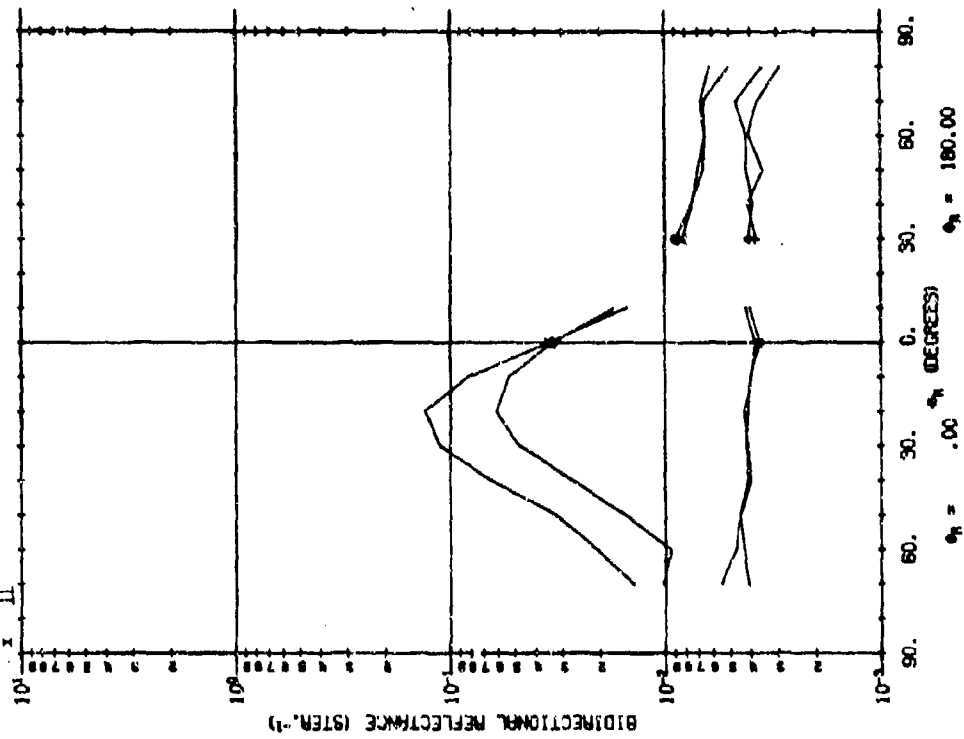
0 ||  $\phi_1 = 0.0$   
 + ||  $\phi_2 = 180.0$   
 A ||  $\lambda = 0.63$



R01324 001

MATURE MULBERRY LEAF, 2 HOURS OLD

0 ||  $\phi_1 = 20.0$   
 + ||  $\phi_2 = 180.0$   
 A ||  $\lambda = 0.63$

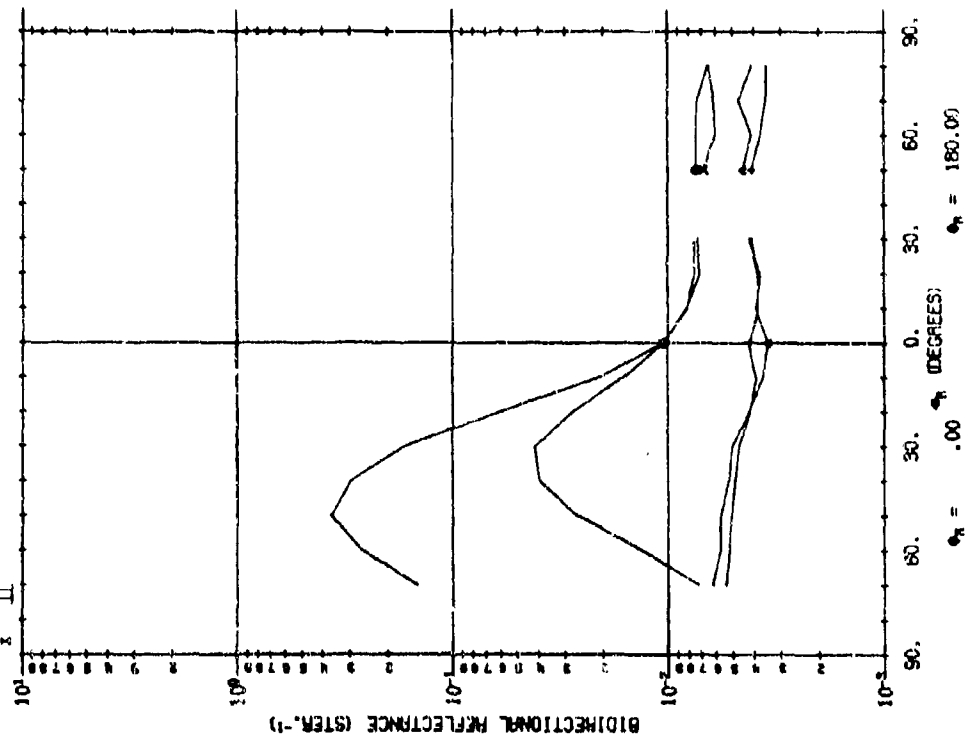


VEGETATION

R01324 001

MATURE MILBERRY LEAF, 2 MONTHS OLD

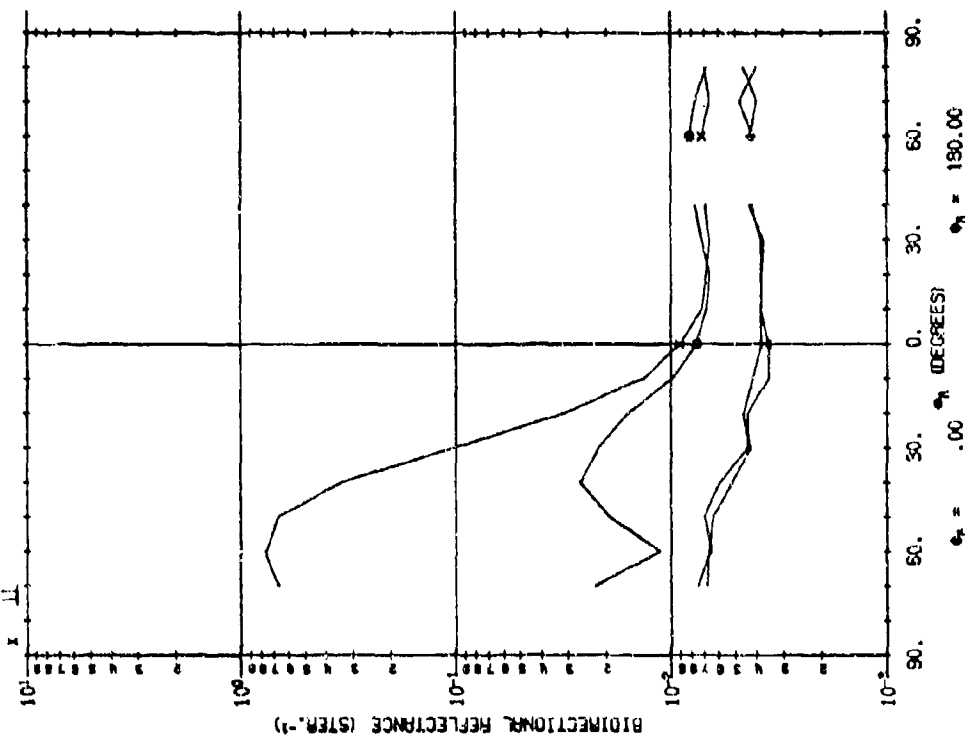
0 ||  $\theta_1 = 40.0$   
 + ||  $\theta_1 = 180.0$   
 A ||  $\lambda = 0.63$



R01324 001

MATURE MILBERRY LEAF, 2 MONTHS OLD

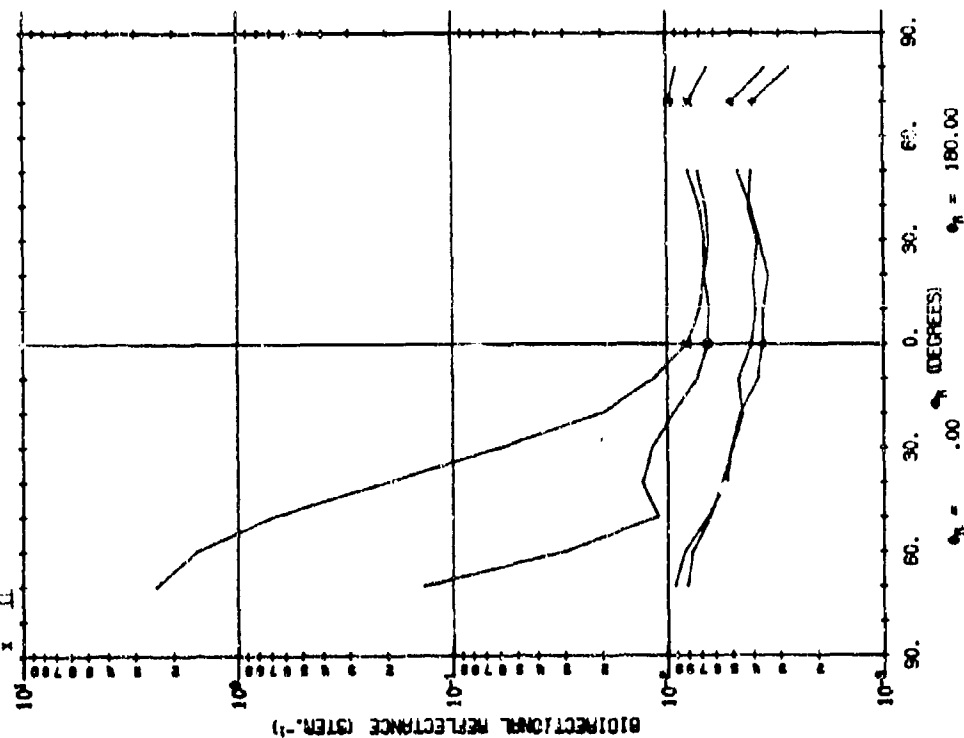
0 ||  $\theta_1 = 50.0$   
 + ||  $\theta_1 = 180.0$   
 A ||  $\lambda = 0.63$



R01324 001

MATURE WETLAND LEAF, 2 BOOTS OLD

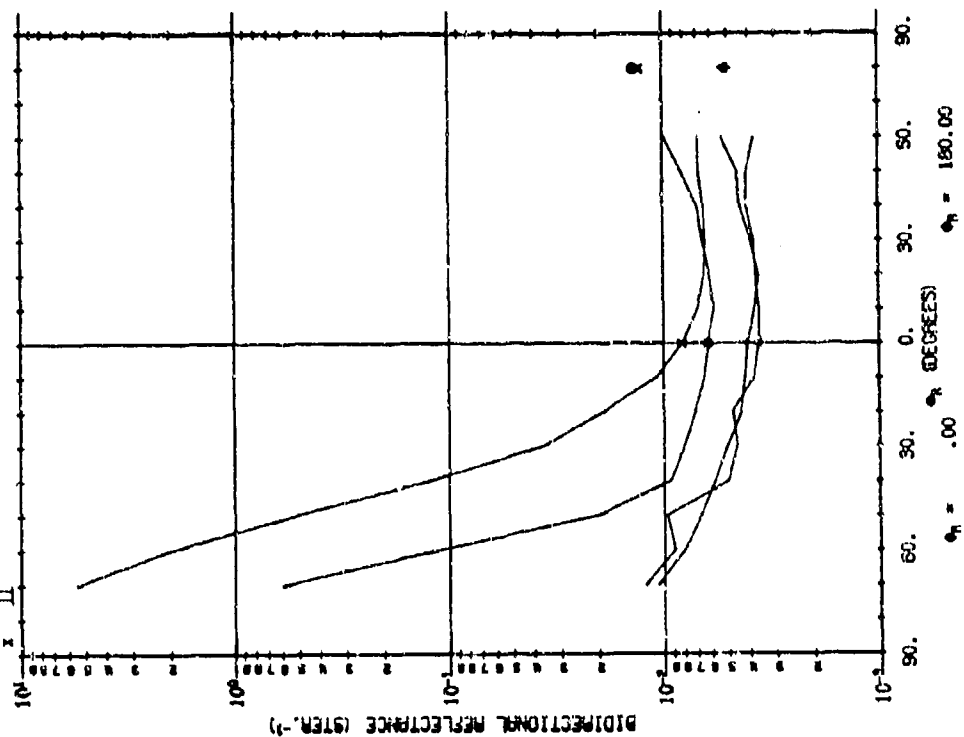
0  $\theta_1 = 60.0$   
 +  $\theta_1 = 100.0$   
 A  $\theta_1 = 0.63$



R01324 001

MATURE WETLAND LEAF, 2 BOOTS OLD

0  $\theta_1 = 70.0$   
 +  $\theta_1 = 100.0$   
 A  $\theta_1 = 0.63$

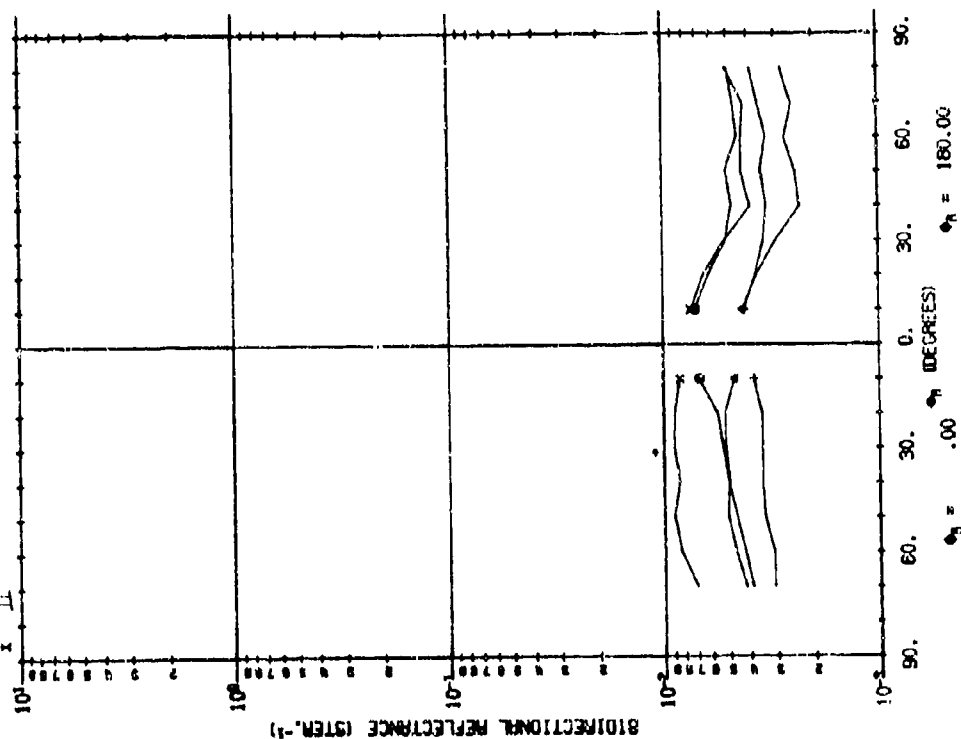


VEGETATION

R01327 001

YELLOW BLADE GRASS GROWING IN SANDY SOIL

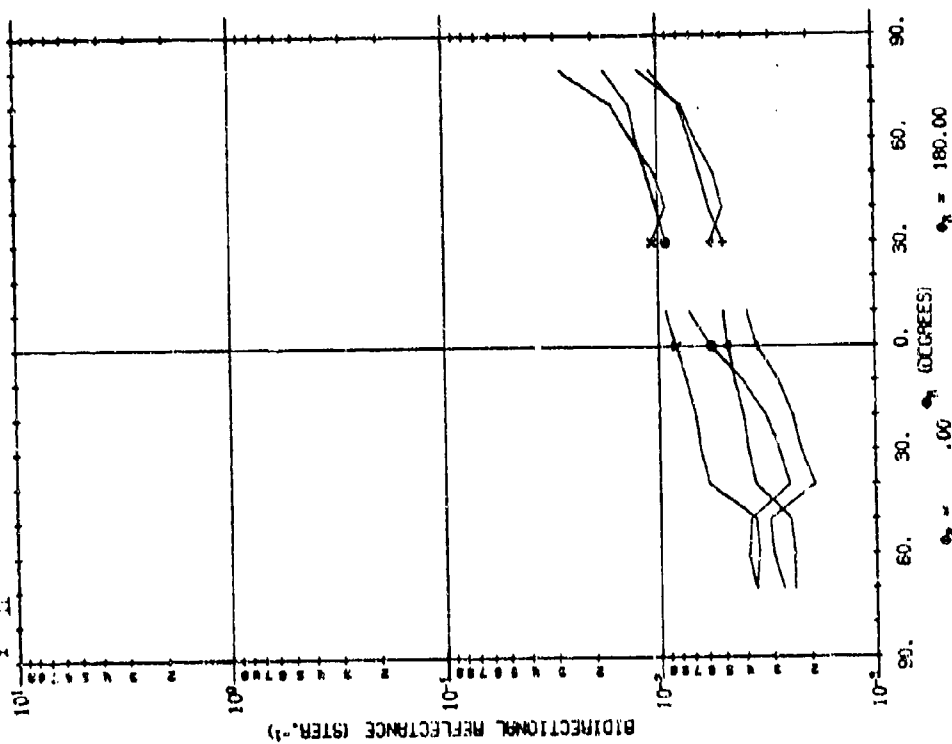
0 11 0.0  
+ 11 180.0  
x 11 0.63



R01327 001

YELLOW BLADE GRASS GROWING IN SANDY SOIL

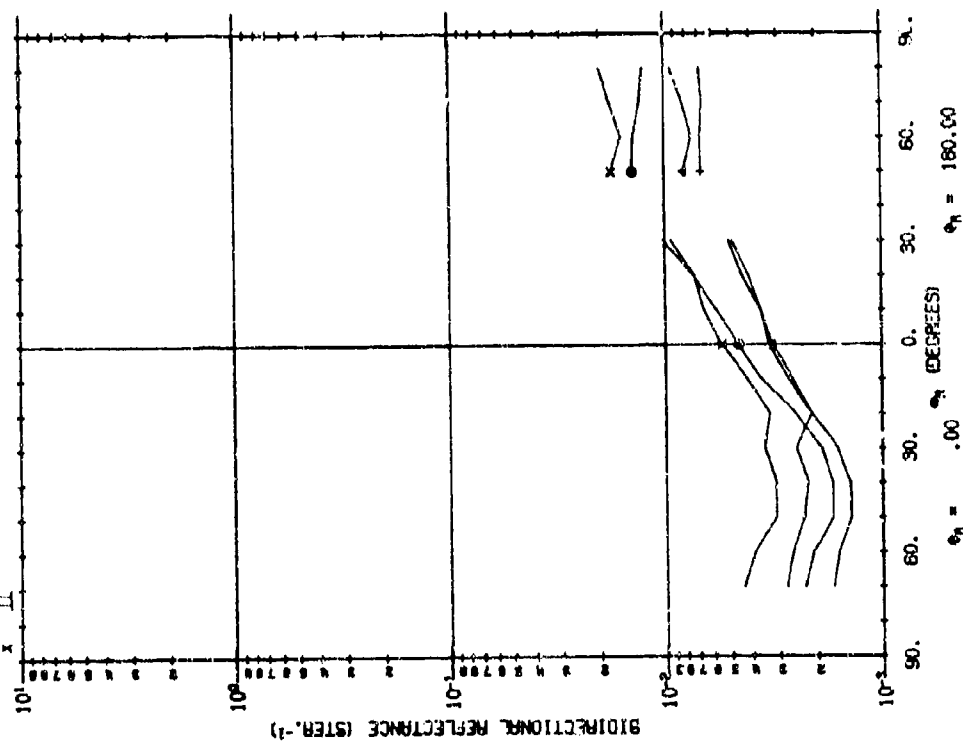
0 11 20.0  
+ 11 180.0  
x 11 2.63



A01327 001

MEXICAN BLUZE GRASS GROWING IN SANDY SOIL

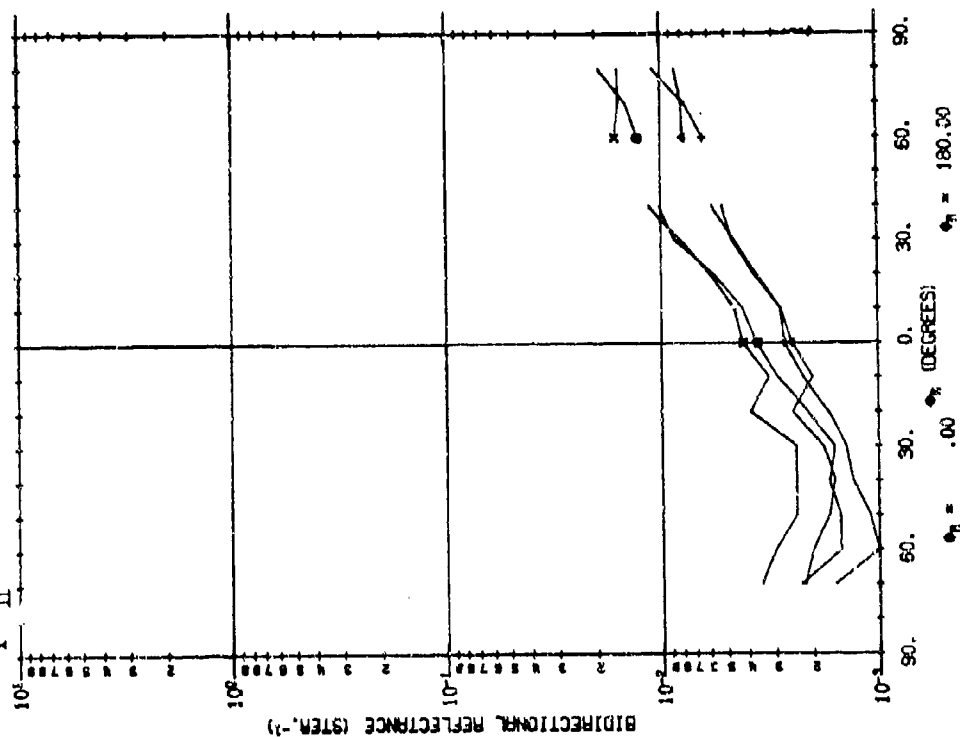
0 11  $\theta_1 = 40.0$   
 + 11  $\theta_1 = 180.0$   
 x 11  $\lambda = 0.63$



A01327 001

MEXICAN BLUZE GRASS GROWING IN SANDY SOIL

0 11  $\theta_1 = 50.0$   
 + 11  $\theta_1 = 180.0$   
 x 11  $\lambda = 0.63$

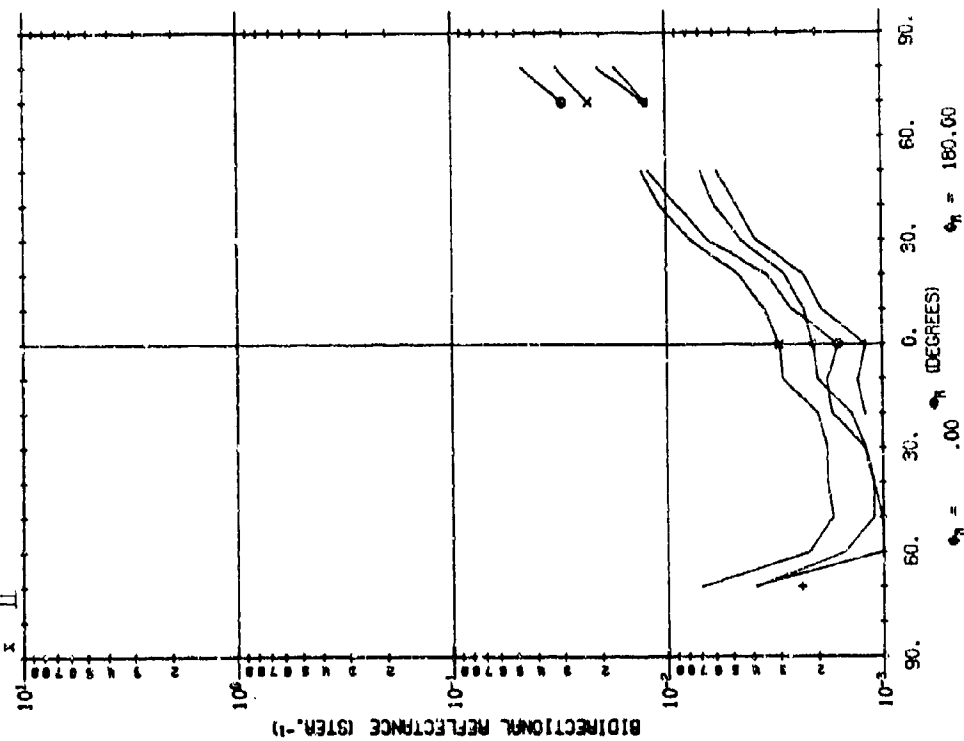


VEGETATION

R01327 001

MERION BLUE GRASS GROWING IN SANDY SOIL

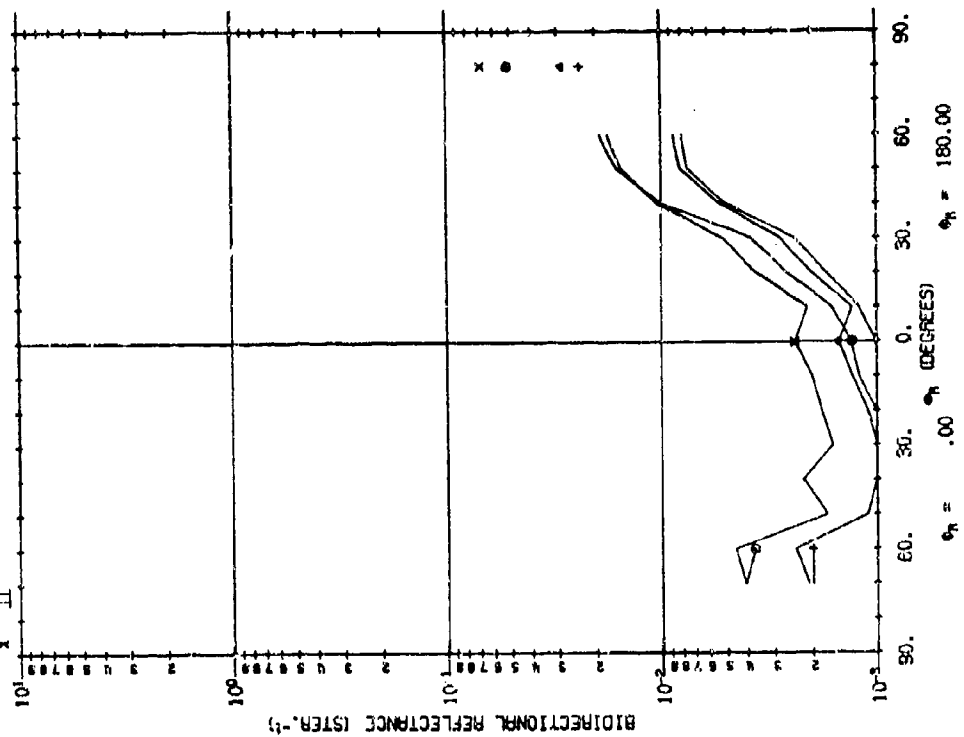
0 ||  $\phi_1 = 50.0$   
 + ||  $\phi_1 = 180.0$   
 x ||  $\lambda = 0.53$



R01327 001

MERION BLUE GRASS GROWING IN SANDY SOIL

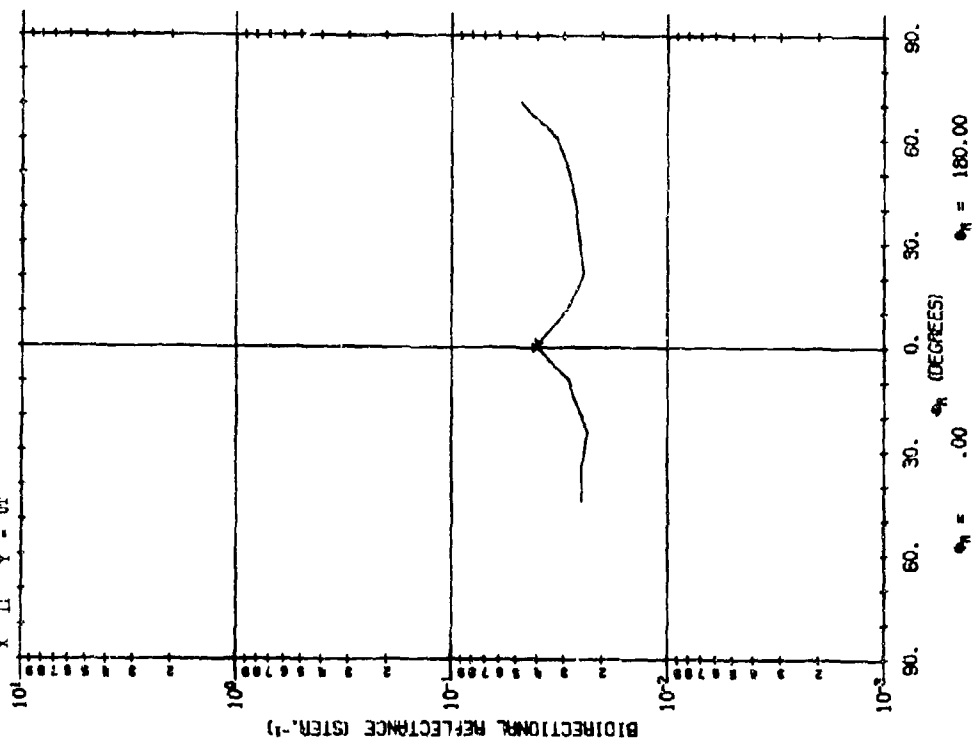
0 ||  $\phi_1 = 70.0$   
 + ||  $\phi_1 = 180.0$   
 x ||  $\lambda = 0.63$



R01516 003

Tree Bark

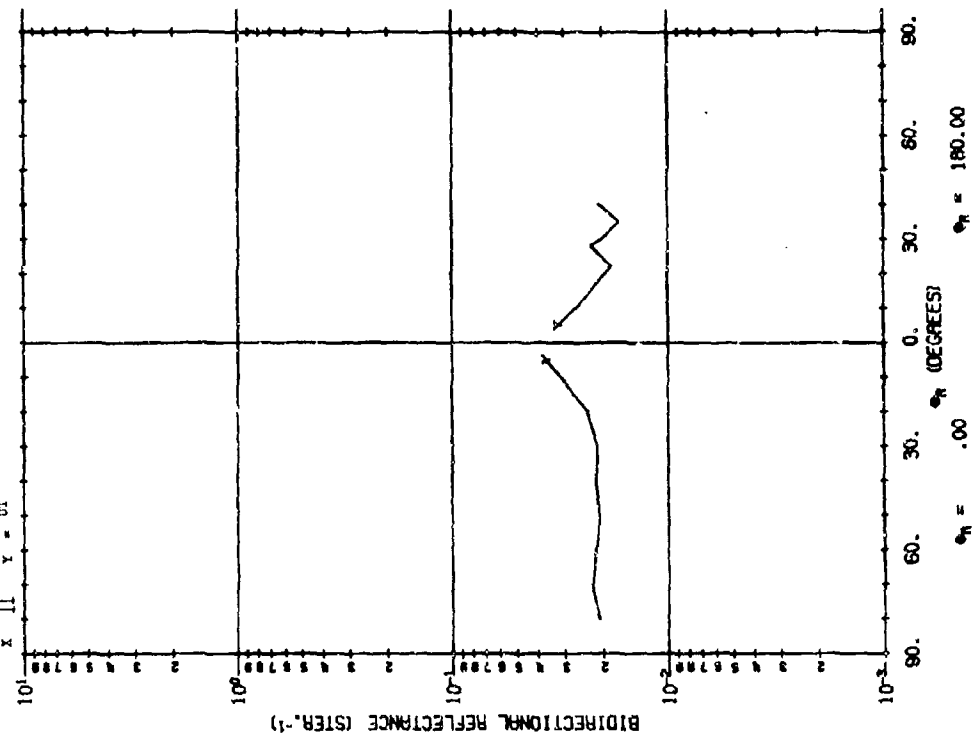
0 || 28 = 1.10  
+ ||  $\phi_i = \phi_r$   
Δ || λ = 10.6  
X || Y = UT



R01516 003

Tree Bark

0 ||  $\phi_i = 0.0$   
+ ||  $\phi_i = 180.0$   
Δ || λ = 10.6  
X || Y = UT



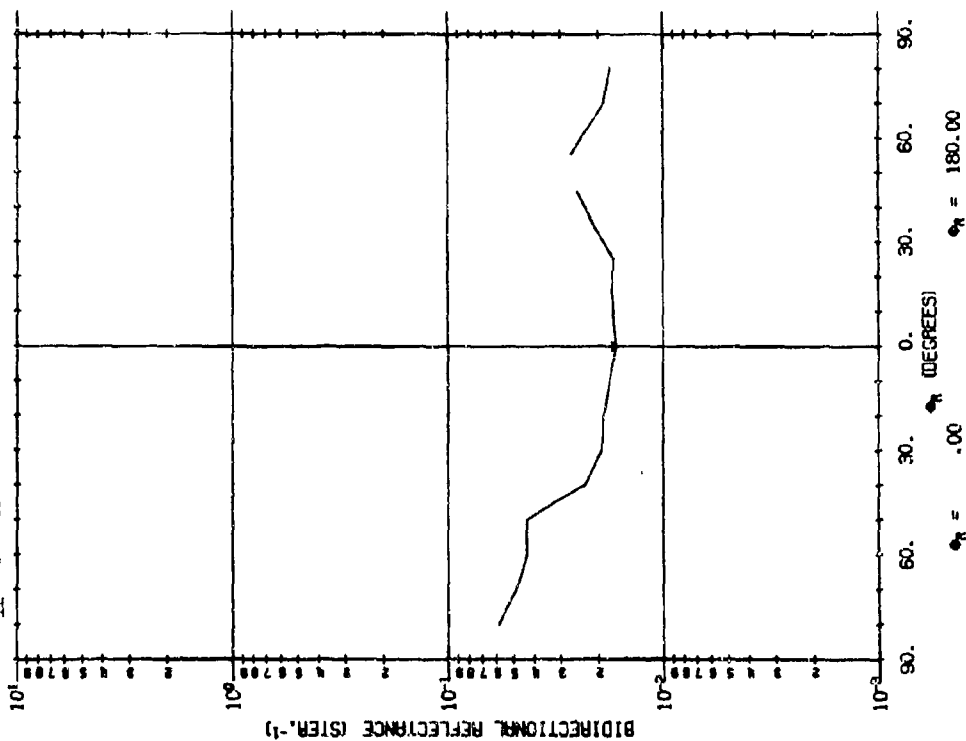
VEGETATION



A01516 003

Tree Bark

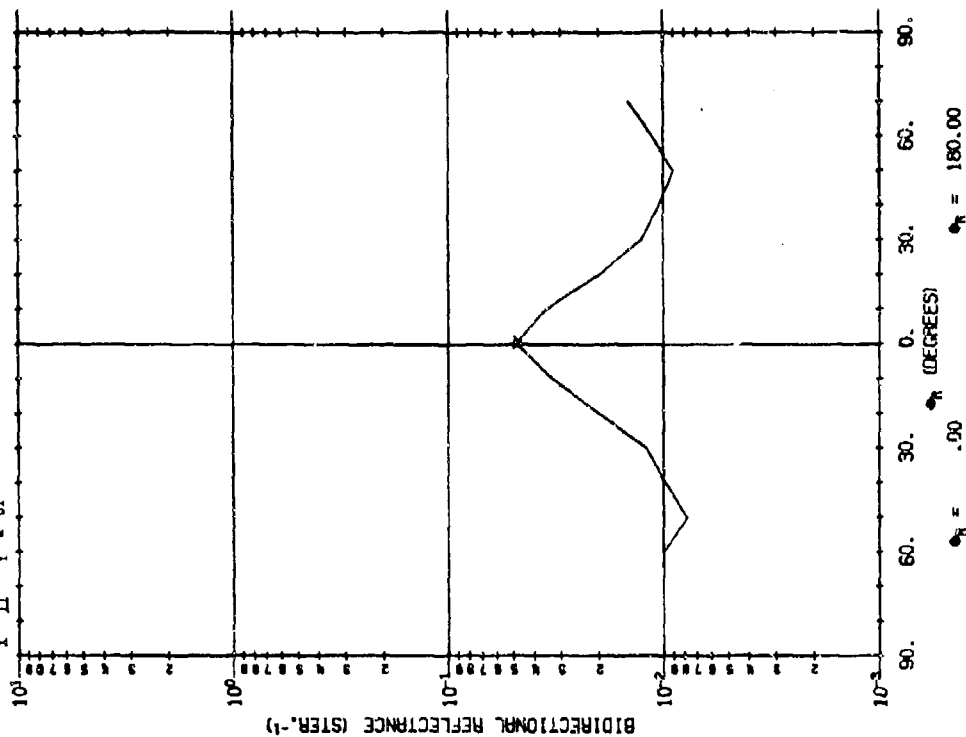
0 ||  $\theta_i = 50.0$   
 + ||  $\phi_i = 180.0$   
 Δ ||  $\lambda = 16.6$   
 X ||  $\gamma = UT$



A01517 002

Pine Tree Bark

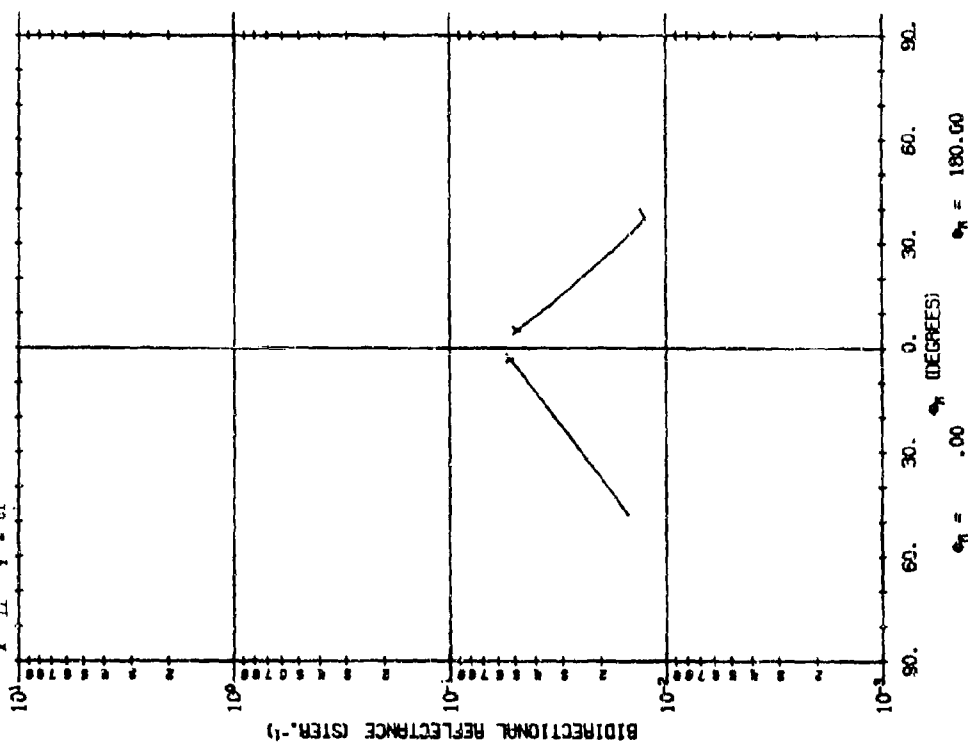
0 ||  $\theta_i = 1.10$   
 + ||  $\phi_i = 0$   
 Δ ||  $\lambda = 10.6$   
 X ||  $\gamma = UT$



A01517 002

Pine Tree Bark

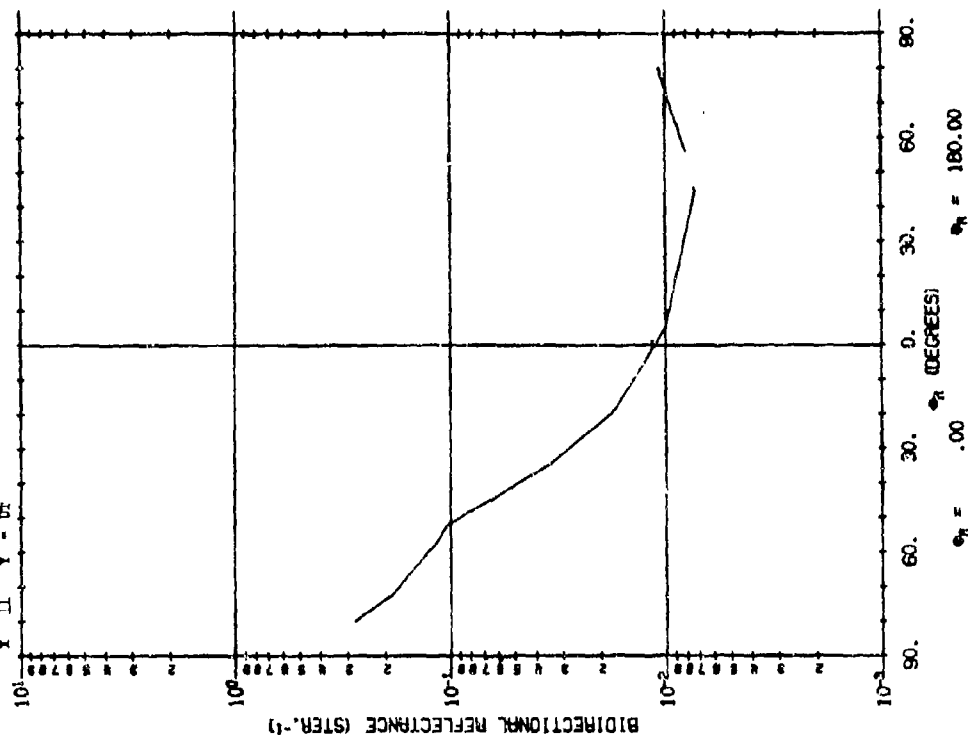
0 //  $\theta_1 = 0.0$   
 + //  $\phi_1 = 180.0$   
 A //  $\lambda = 10.6$   
 X //  $\gamma = 0^\circ$



A01517 002

Pine Tree Bark

0 //  $\theta_1 = 50.0$   
 + //  $\phi_1 = 180.0$   
 A //  $\lambda = 10.6$   
 X //  $\gamma = 0^\circ$



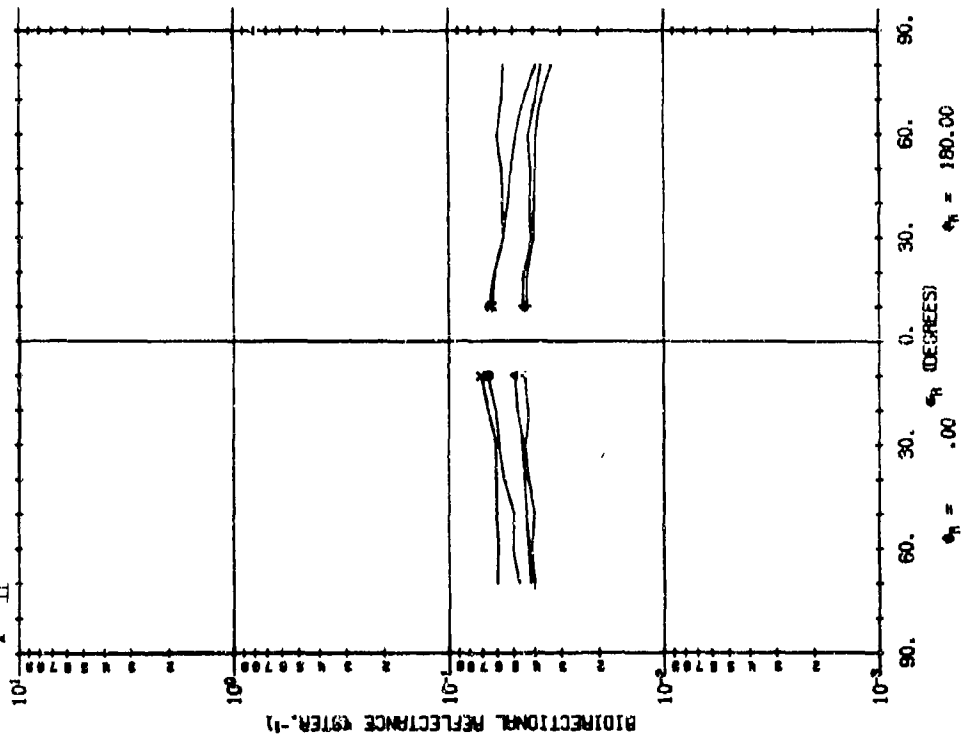
VEGETATION

# ASPHALT AND CONCRETE

A01329 001

CONCRETE

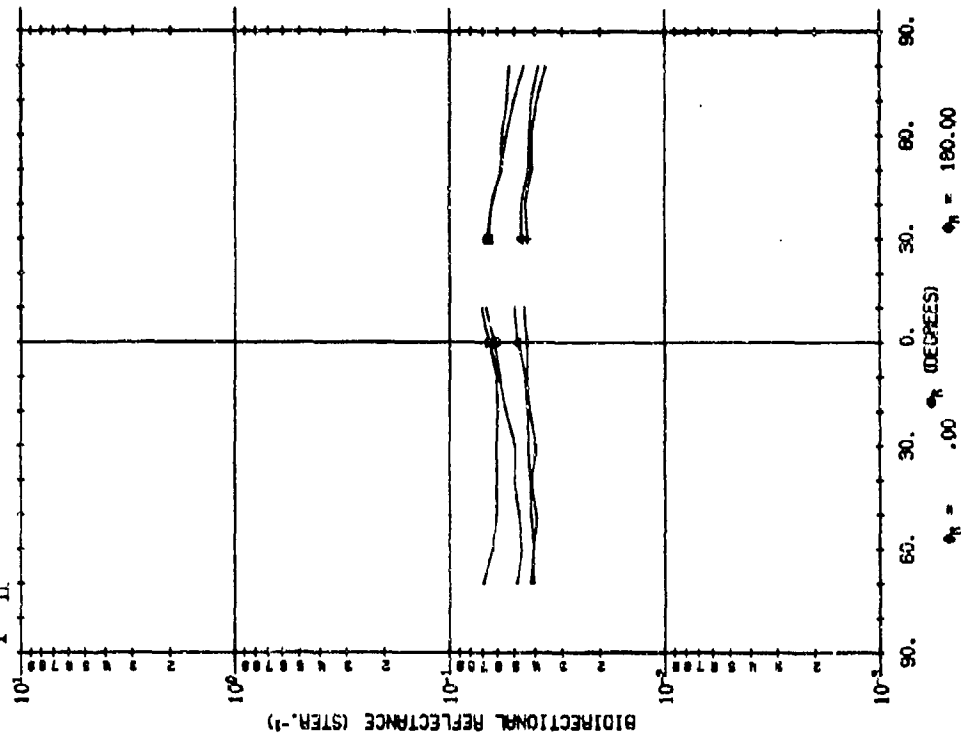
0 ||  $\theta_1 = 0.0$   
 + ||  $\theta_1 = 180.0$   
 x ||  $\lambda = 0.63$



A01329 001

CONCRETE

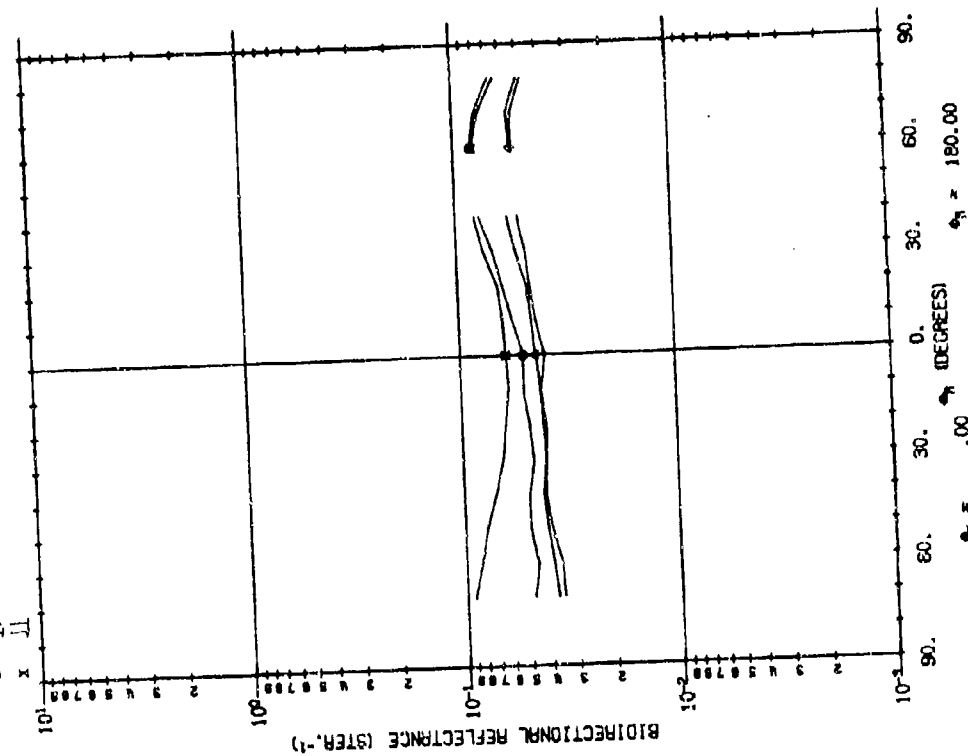
0 ||  $\theta_1 = 20.0$   
 + ||  $\theta_1 = 180.0$   
 x ||  $\lambda = 0.63$



# ASPHALT AND CONCRETE

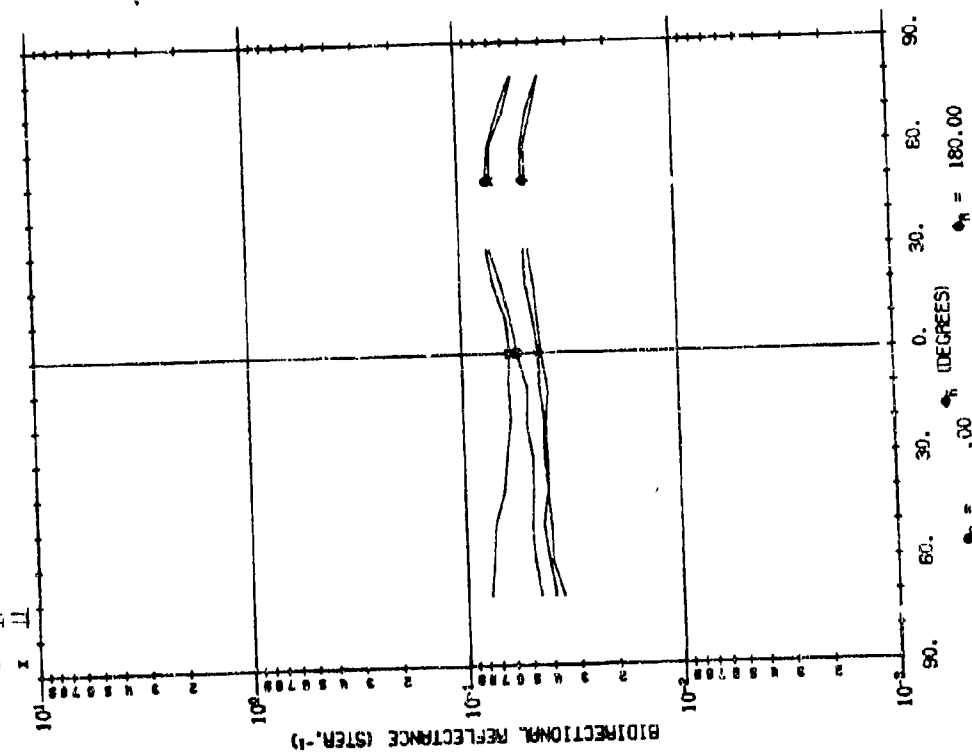
A01329 001 CONCRETE

$\epsilon_1 = 50.0$   
 $\epsilon_2 = 130.0$   
 $\lambda = 0.63$



A01329 001 CONCRETE

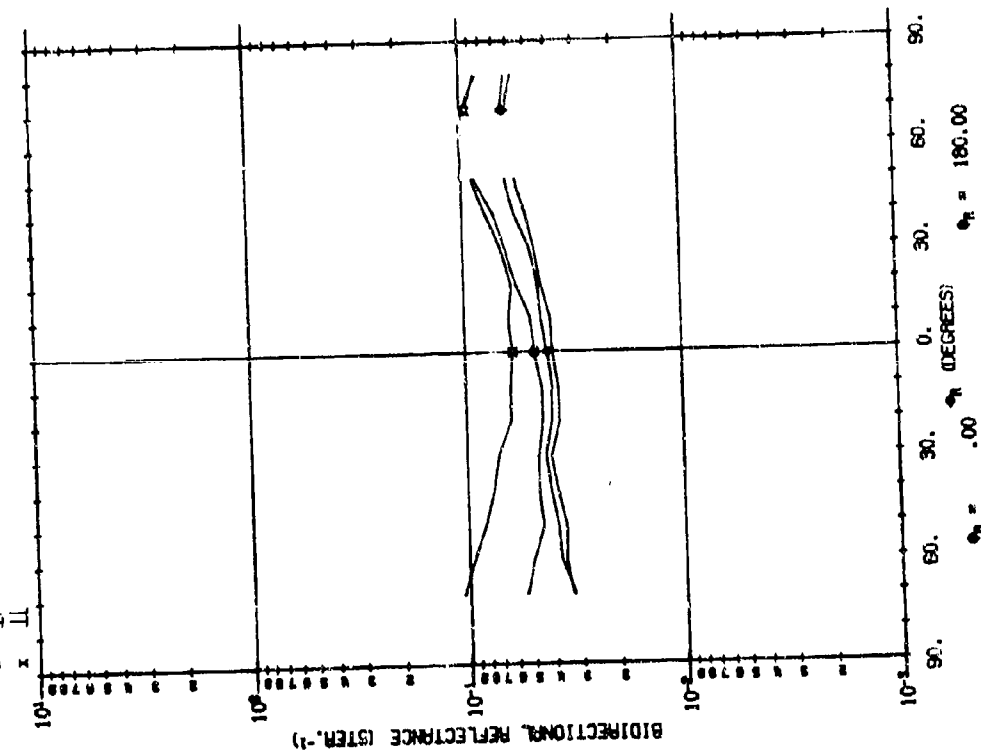
$\epsilon_1 = 40.0$   
 $\epsilon_2 = 180.0$   
 $\lambda = 0.63$



A01329 001

CONCRETE

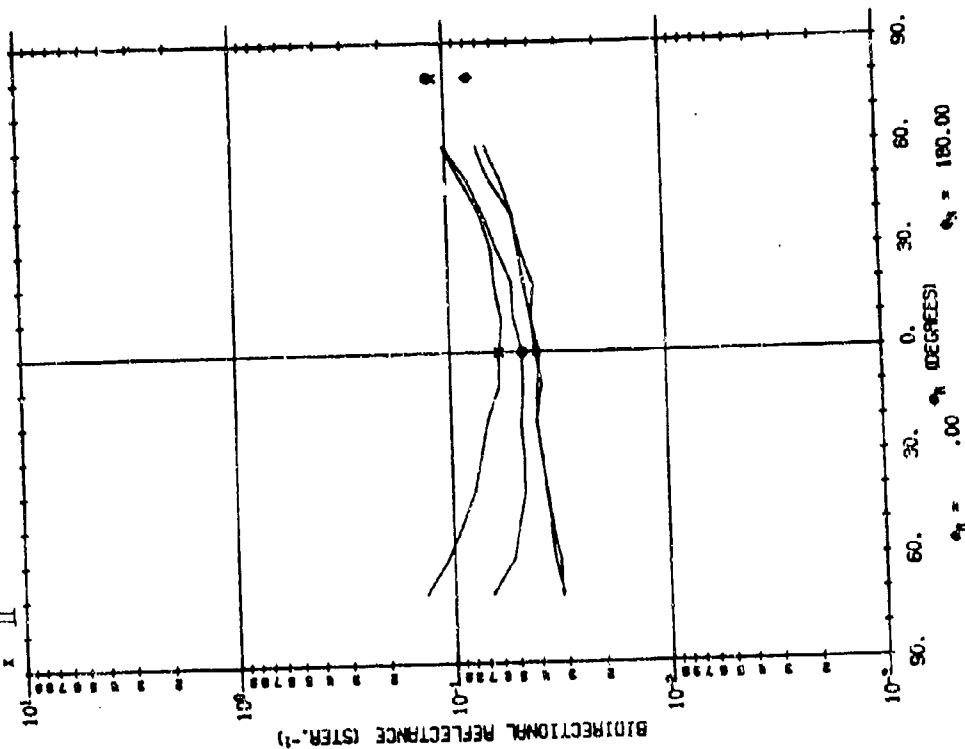
$\theta_1 = 60.0$   
 $\theta_2 = 180.0$   
 $\lambda = 0.63$



A01329 001

CONCRETE

$\theta_1 = 70.0$   
 $\theta_2 = 180.0$   
 $\lambda = 0.63$



ASPHALT AND CONCRETE

R01530 002

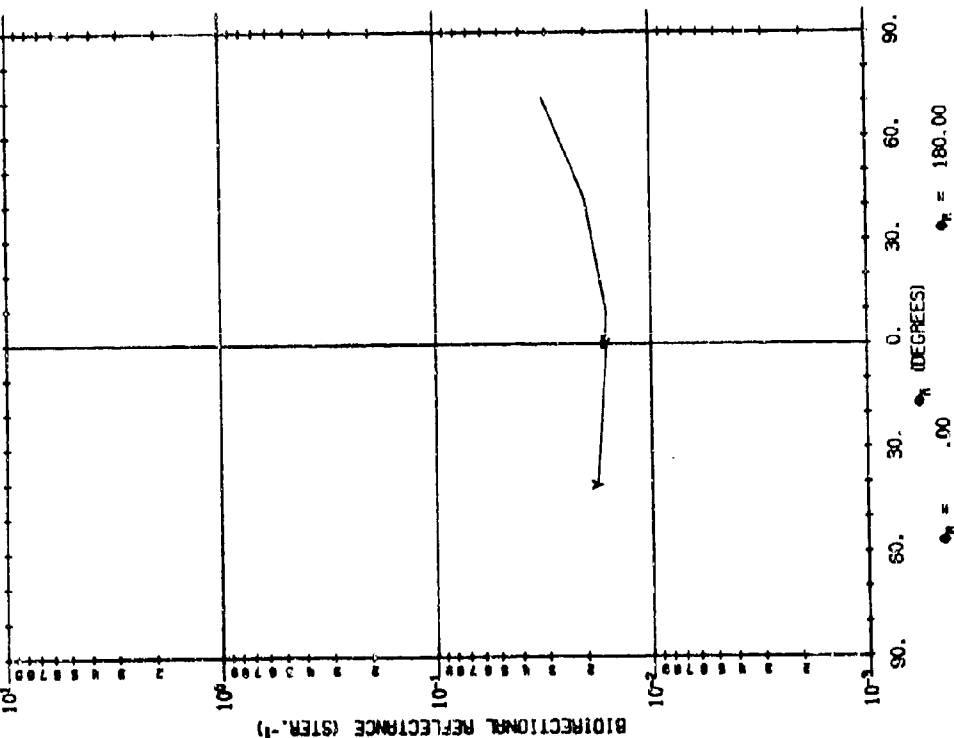
Fine Textured Concrete

0 || 28 = 1.10

+ || 1 = 1.00

Δ || 1 = 10.6

X || 1 = 0.0



R01530 002

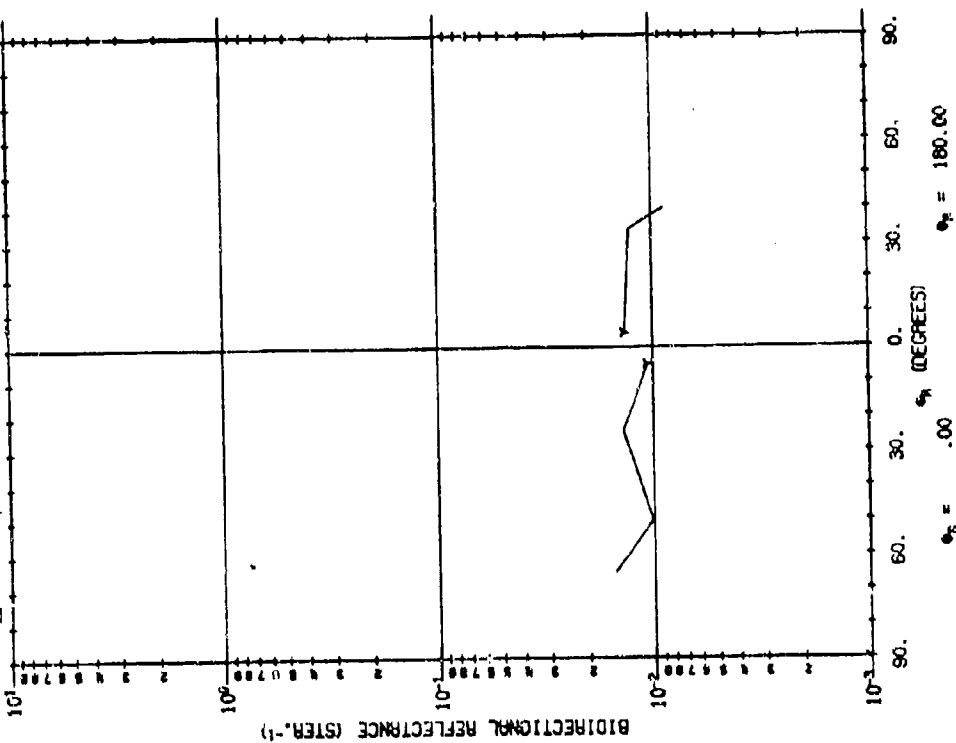
Fine Textured Concrete

0 || 31 = 0.0

+ || 1 = 180.0

Δ || 1 = 10.6

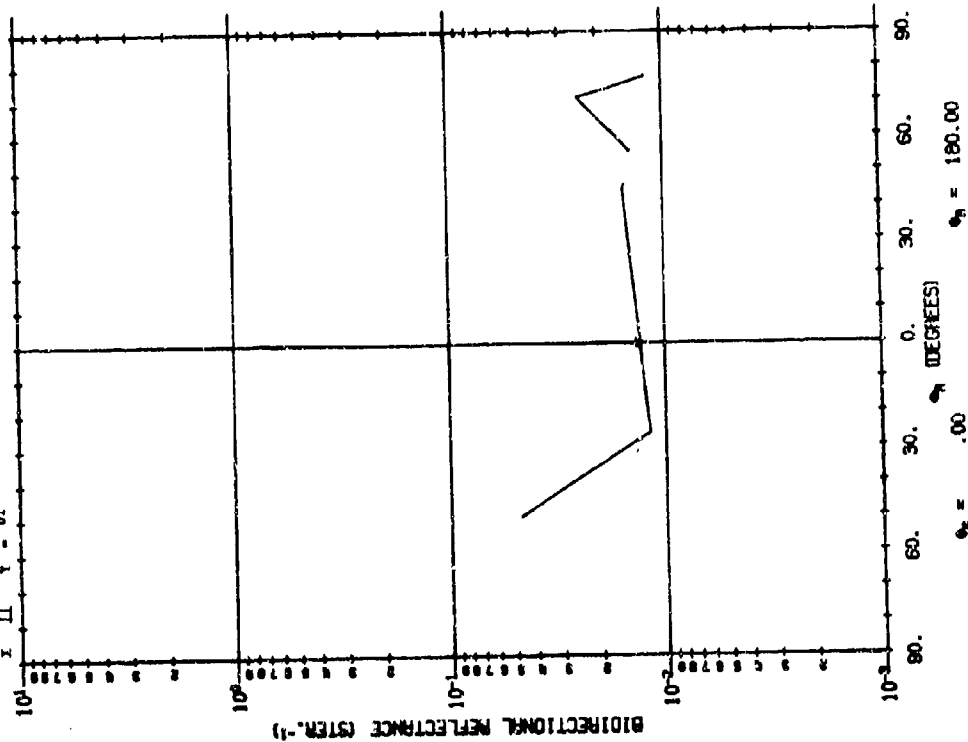
X || 1 = 0.0



R01530 002

Fine Textured Concrete

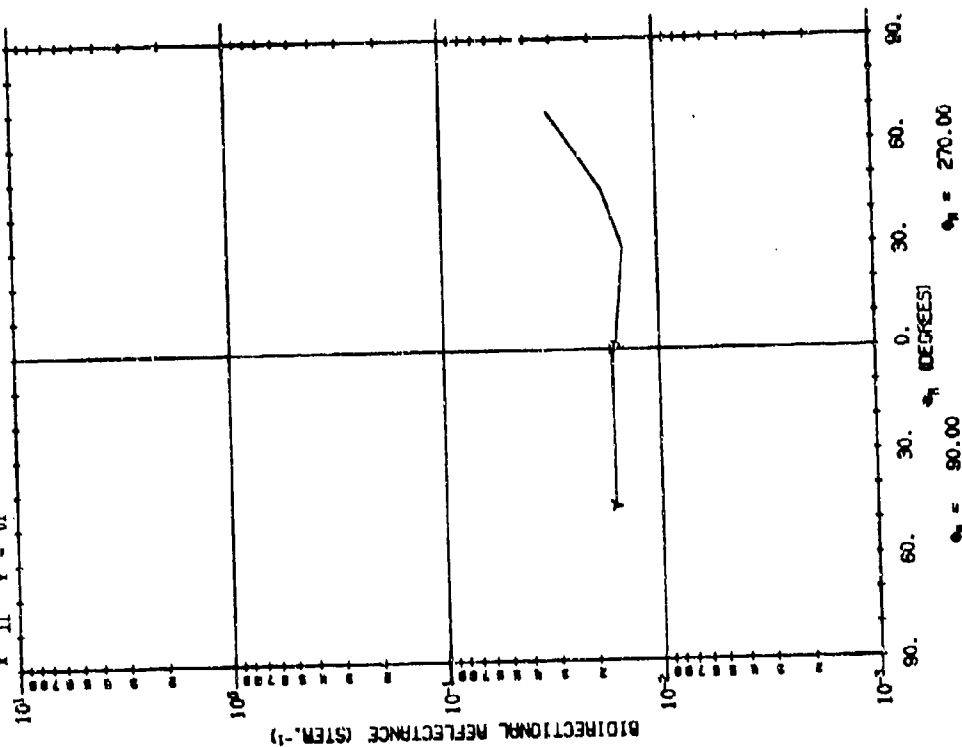
0 II  $\phi_1 = 50.0$   
 + II  $\phi_2 = 180.0$   
 A II  $\lambda = 10.6$   
 X II Y = 07



R01530 002

Fine Textured Concrete

0 II  $\phi_1 = 1.10$   
 + II  $\phi_2 = 0$   
 A II  $\lambda = 10.6$   
 X II Y = 07



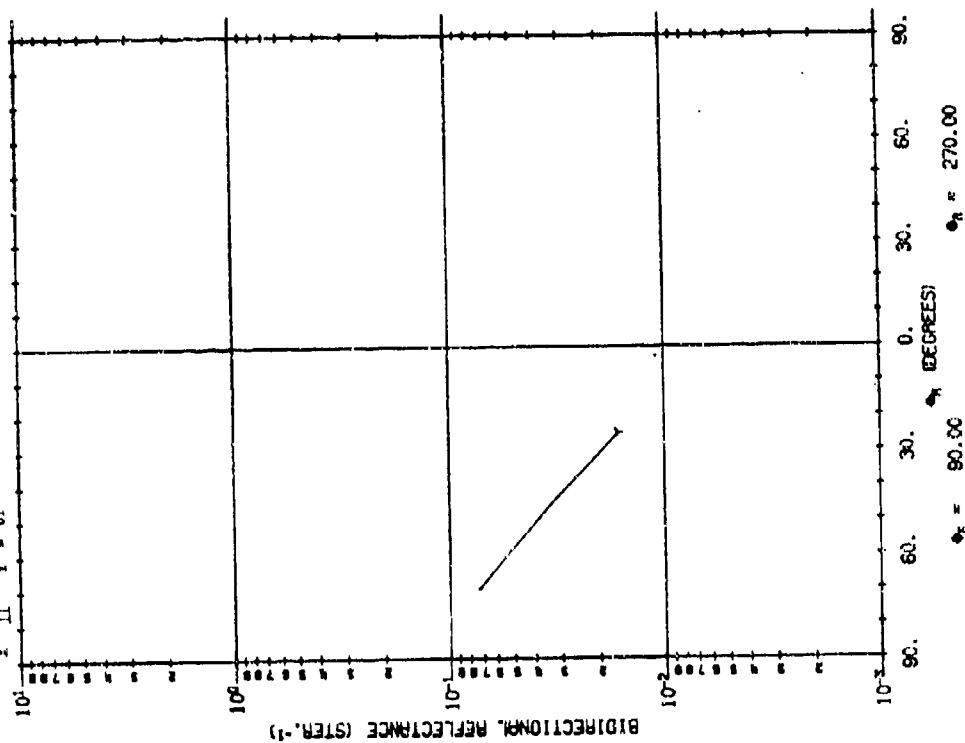
ASPHALT AND CONCRETE



R01530 002

Fine Textured Concrete

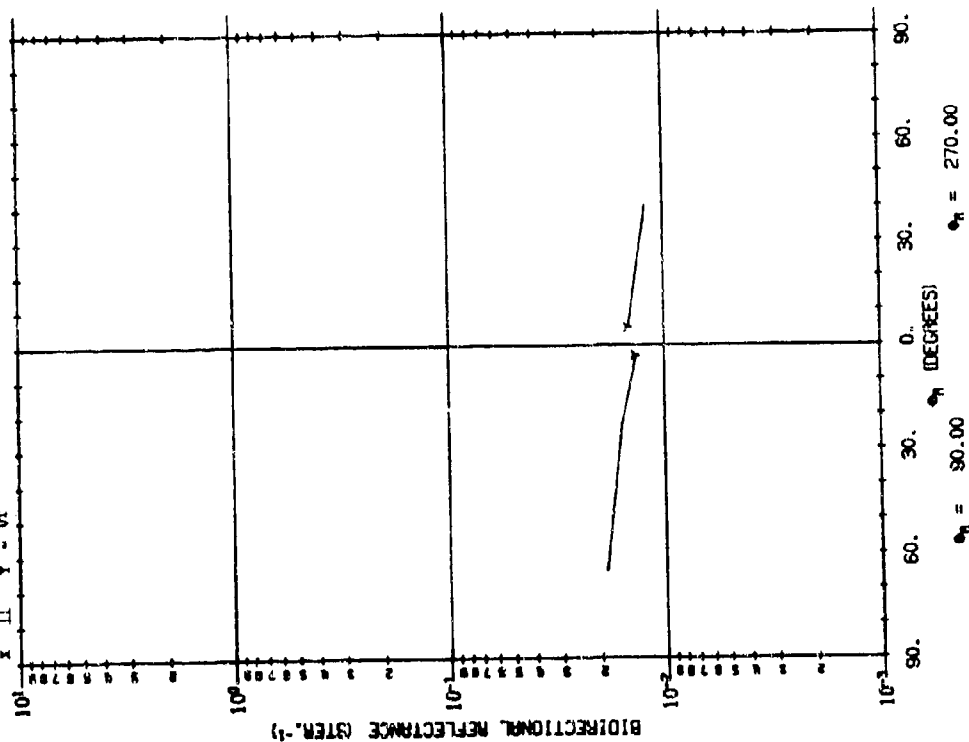
0 ||  $\phi_1 = 50.0$   
 + ||  $\phi_2 = 270.0$   
 A ||  $\lambda = 10.6$   
 X || Y = VT



R01530 002

Fine Textured Concrete

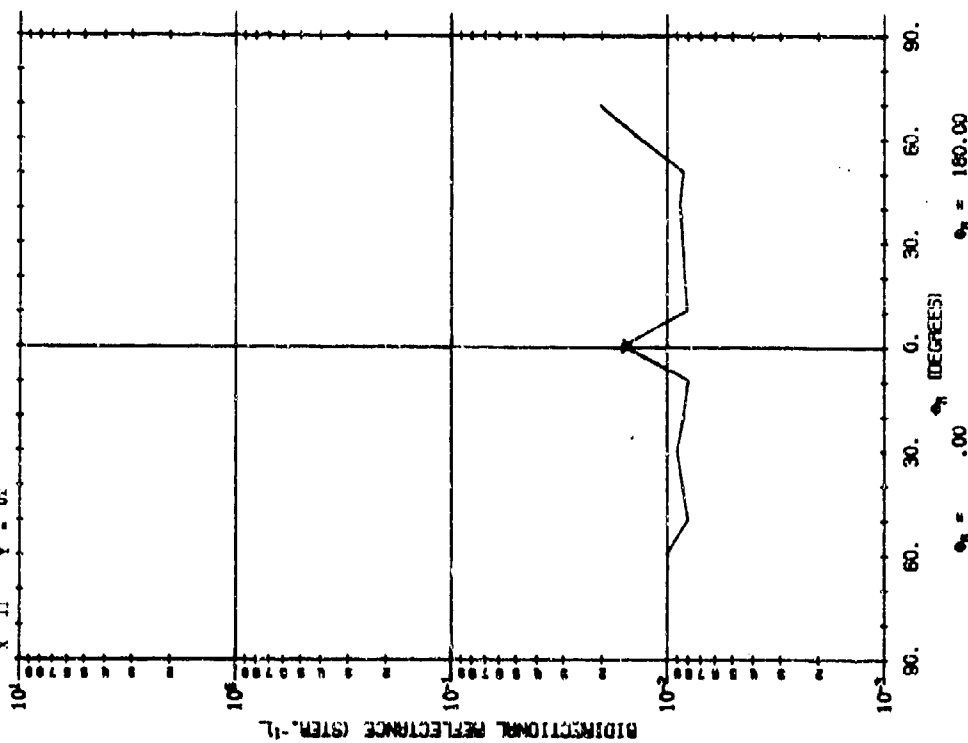
0 ||  $\phi_1 = 0.0$   
 + ||  $\phi_2 = 270.0$   
 A ||  $\lambda = 10.6$   
 X || Y = VT



A01537 002

Very Fine Concrete

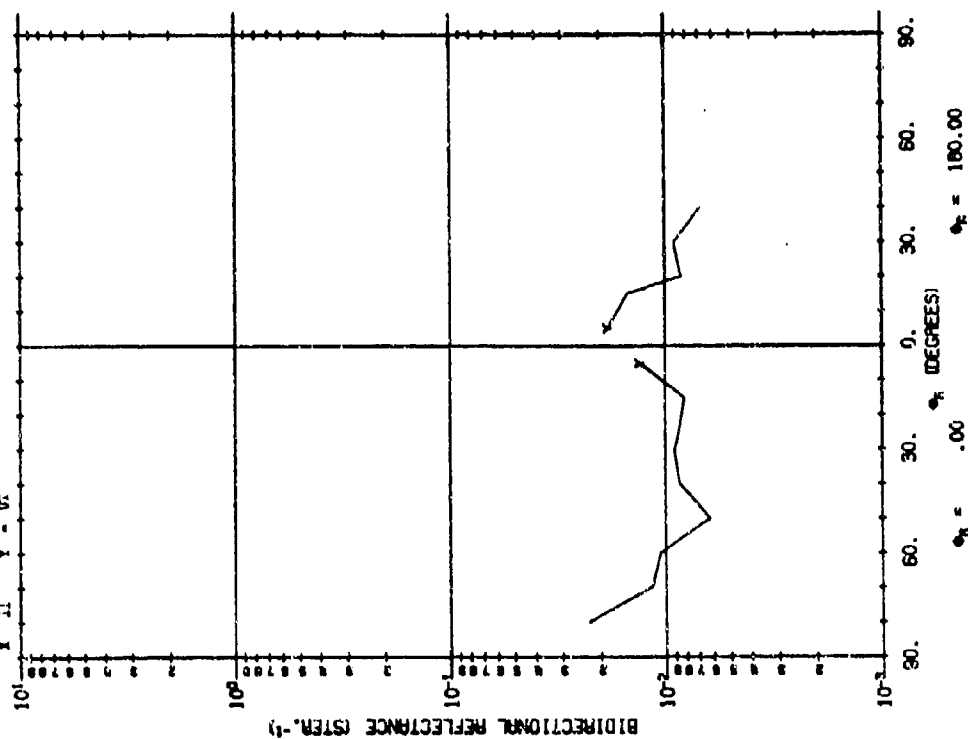
0 || 28 = 1.10  
+ ||  $\phi_1$  =  $\phi_r$   
A ||  $\lambda$  = 10.6  
X || Y =  $\sqrt{r}$



A01537 002

Very Fine Concrete

0 ||  $\phi_1$  = 0.6  
+ ||  $\phi_1$  = 180.0  
A ||  $\lambda$  = 10.6  
X || Y =  $\sqrt{r}$

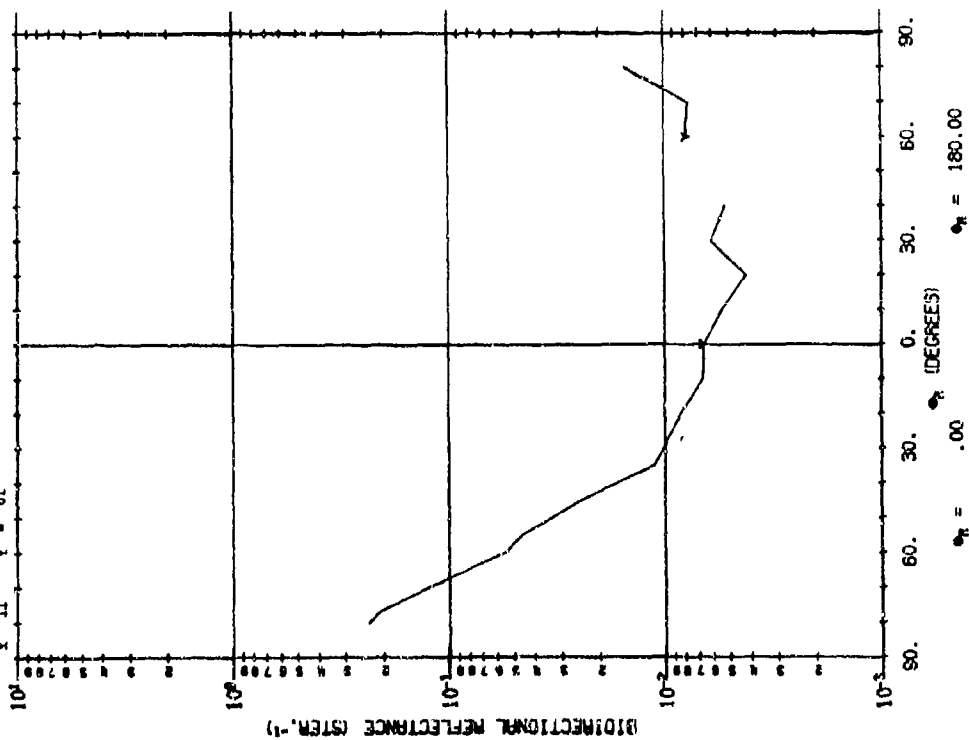


ASPHALT AND CONCRETE

R01537 002

Very Fine Concrete

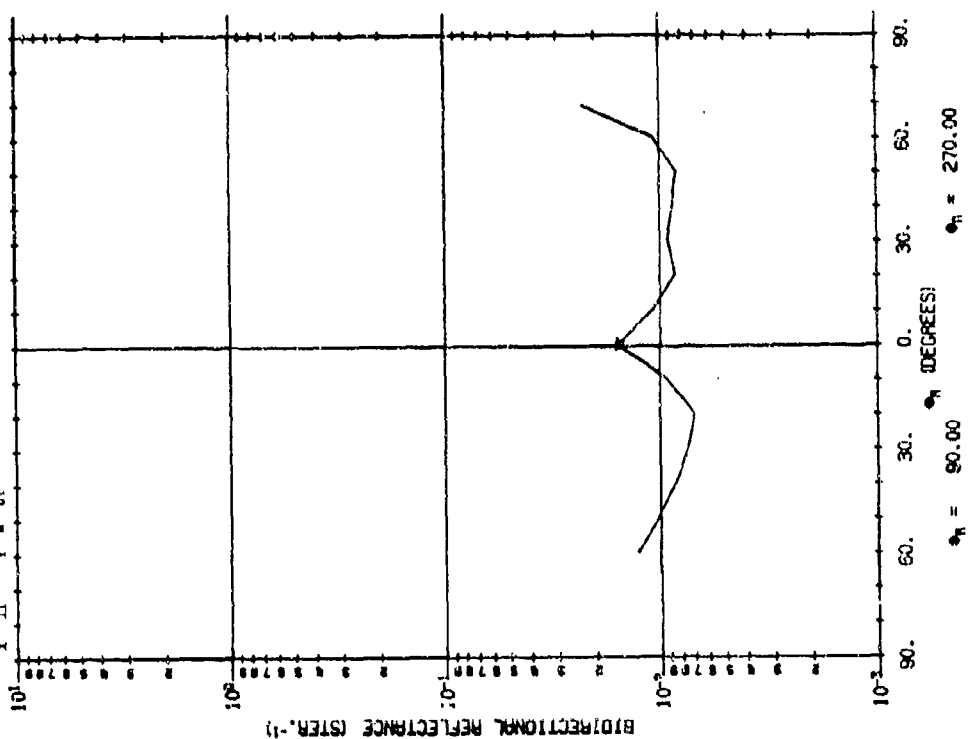
0 ||  $\theta_1 = 50.0$   
 + ||  $\phi_1 = 180.0$   
 x ||  $\lambda = 10.6$   
 Y = UT



R01537 002

Very Fine Concrete

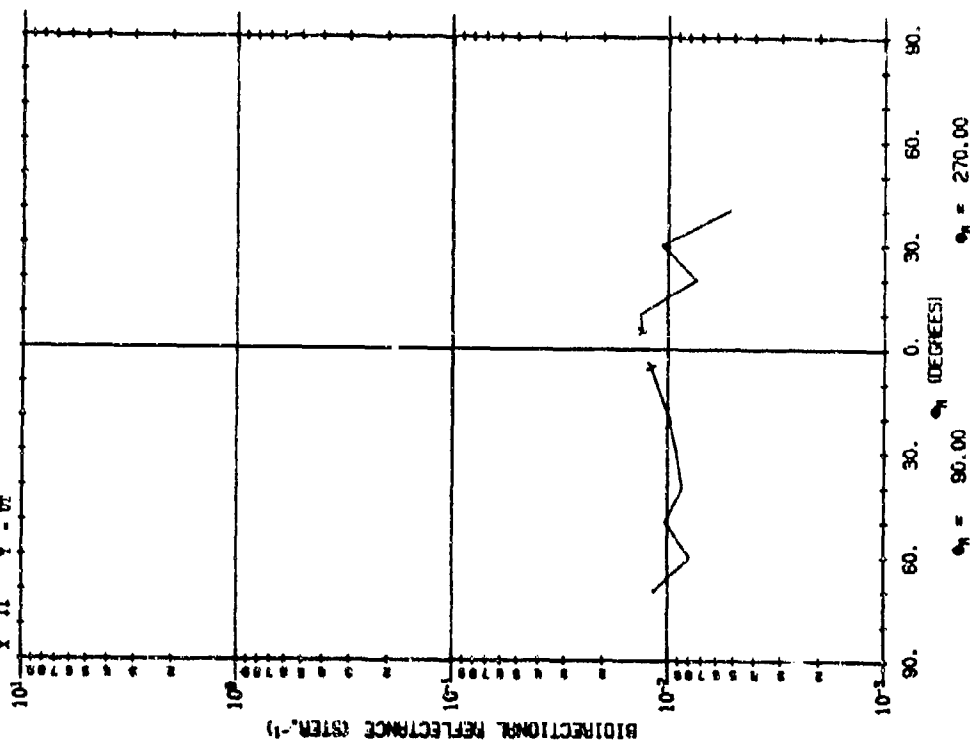
0 ||  $\theta_1 = 1.10$   
 + ||  $\phi_1 = 0$   
 x ||  $\lambda = 10.6$   
 Y = UT



R01537 002

Very Fine Concrete

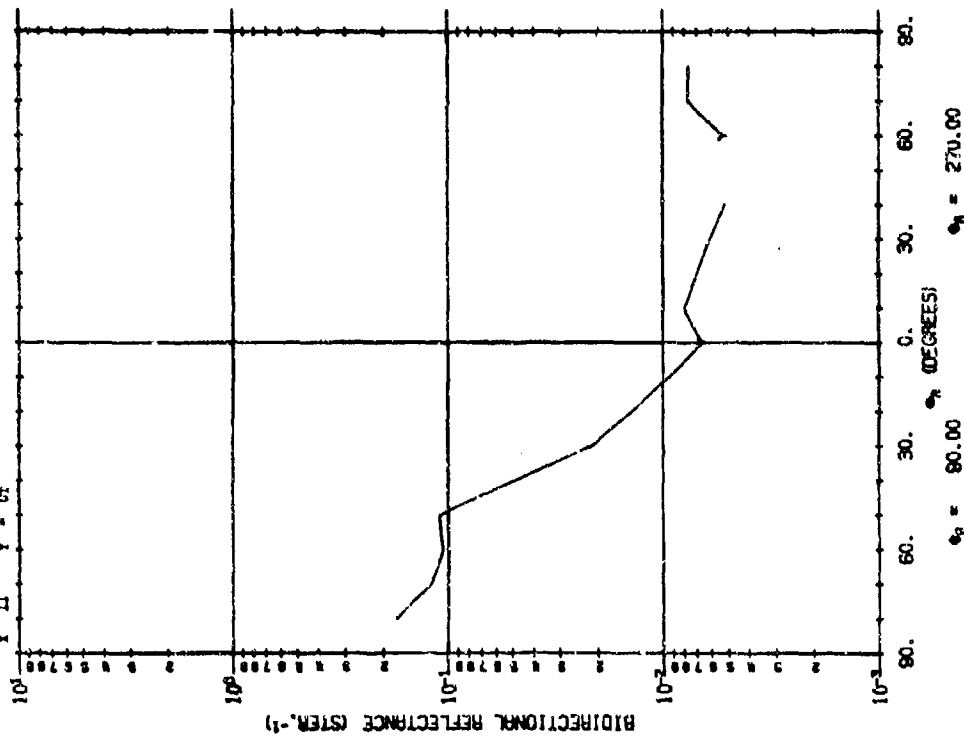
0 ||  $\phi_1 = 0.0$   
 + ||  $\phi_2 = 270.0$   
 Δ ||  $\lambda = 10.6$   
 X ||  $\gamma = 07$



R01537 002

Very Fine Concrete

0 ||  $\phi_1 = 56.0$   
 + ||  $\phi_2 = 270.0$   
 Δ ||  $\lambda = 10.6$   
 X ||  $\gamma = 07$

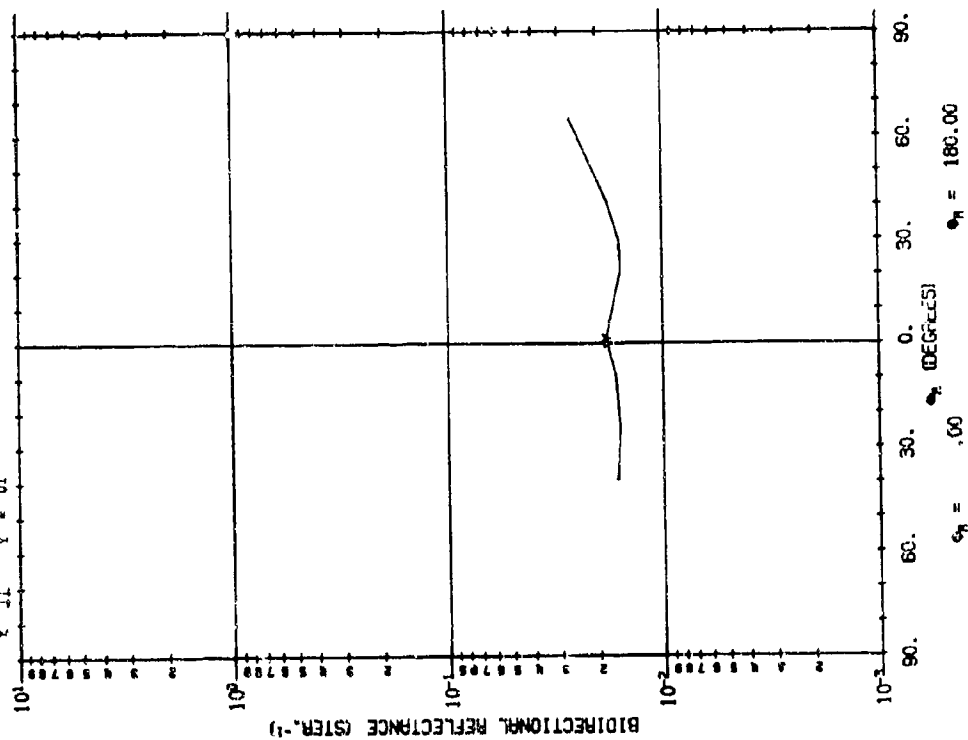


## ASPHALT AND CONCRETE

R01543 002

Medium Fine Asphalt

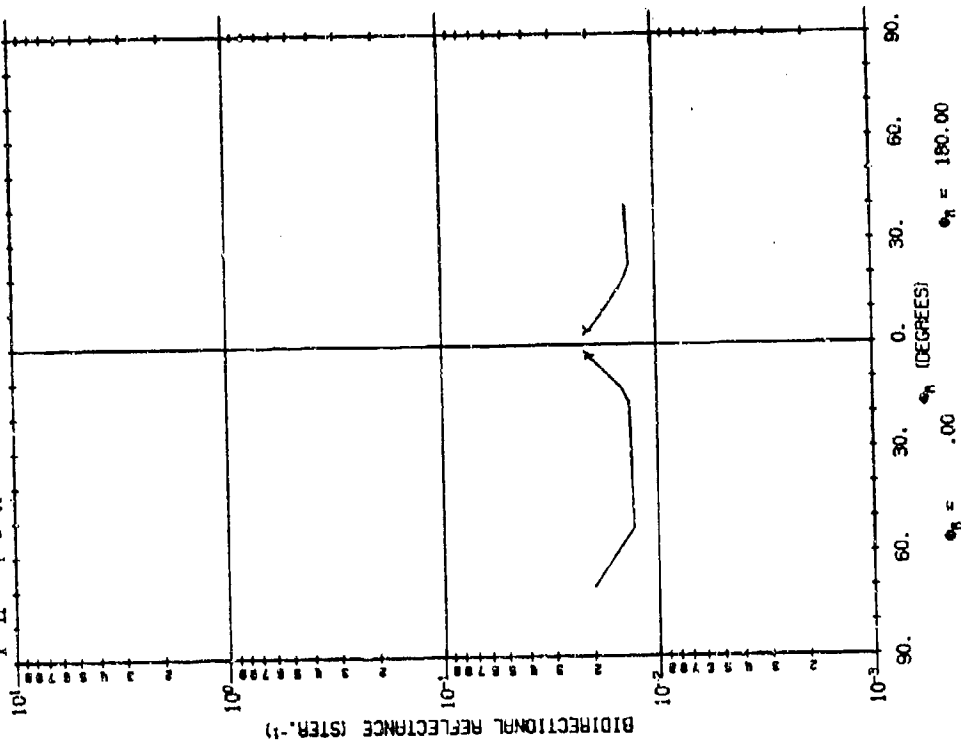
$\theta_i = 1.10$   
 $\theta_r = 0$   
 $\theta_t = 180.0$   
 $\lambda = 10.6$   
 $Y = 0T$



R01543 002

Medium Fine Asphalt

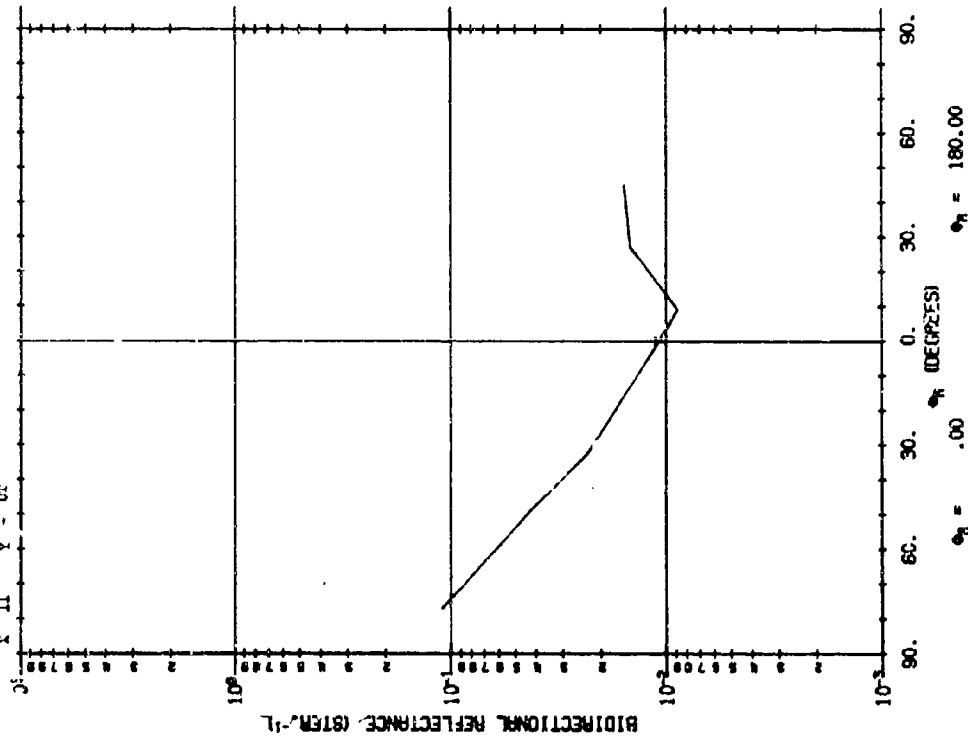
$\theta_i = 0.0$   
 $\theta_r = 0$   
 $\theta_t = 180.0$   
 $\lambda = 10.6$   
 $Y = 0T$



R01543 002

Medium Fine Asphalt

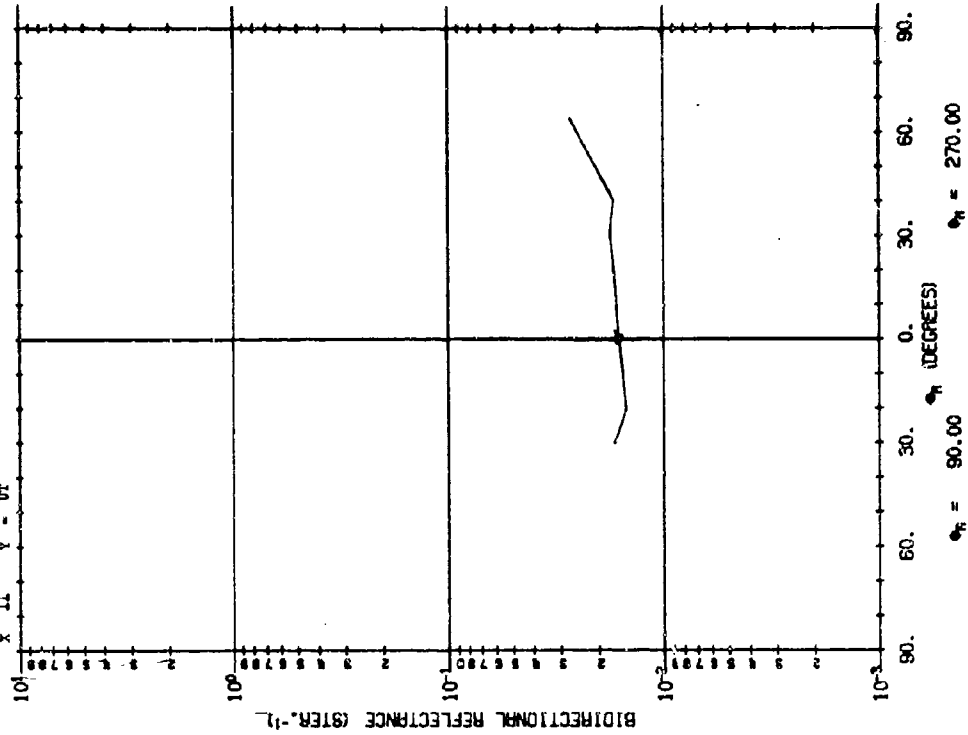
0 ||  $\theta_1 = 50.0$   
 + ||  $\phi_1 = 180.0$   
 A ||  $\lambda = 10.6$   
 X || Y = 0°



R01543 002

Medium Fine Asphalt

0 ||  $\theta_1 = 1.10$   
 + ||  $\phi_1 = 0$   
 A ||  $\lambda = 10.6$   
 X || Y = 0°

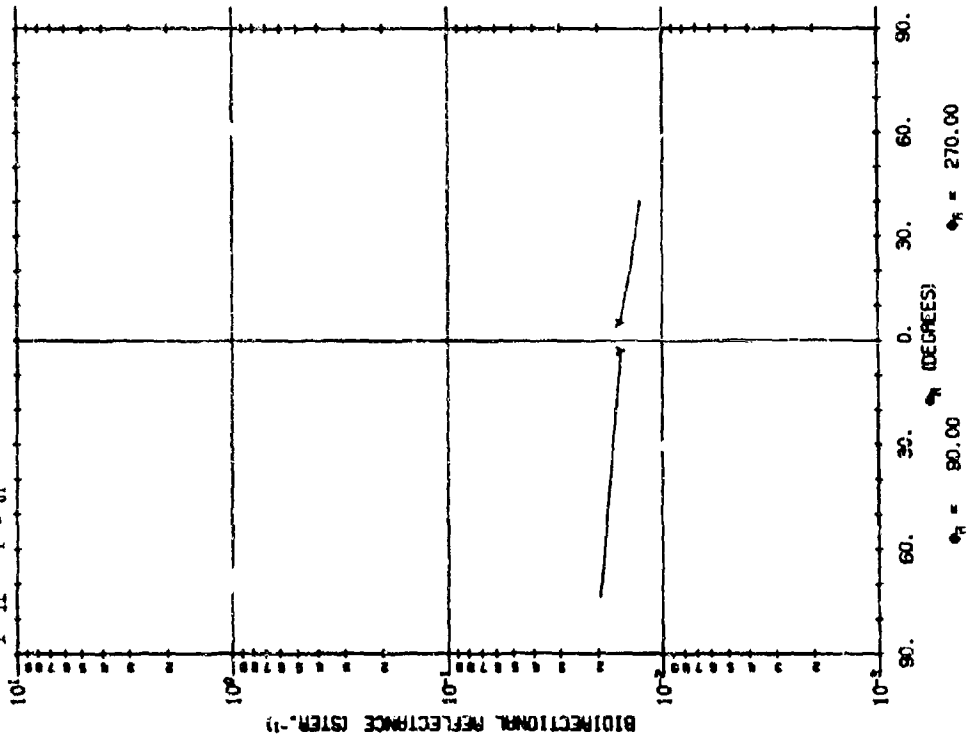


# ASPHALT AND CONCRETE

R01543 002

Medium Fine Asphalt

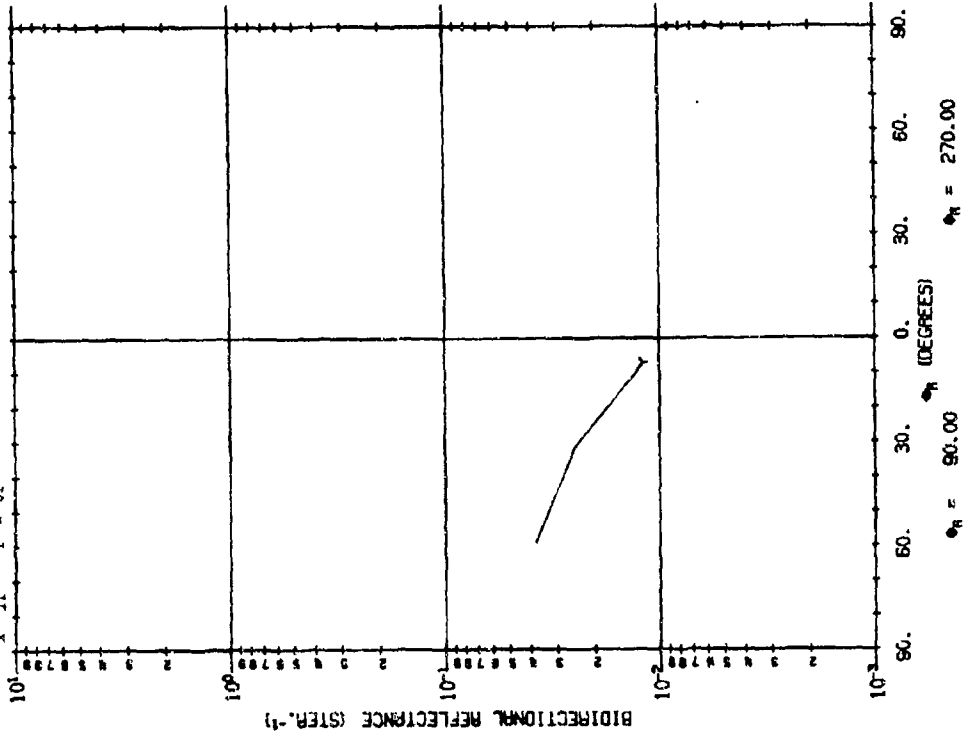
0 ||  $\theta_i = 0.0$   
 + ||  $\theta_t = 270.0$   
 x ||  $\lambda = 10.6$   
 x ||  $\gamma = \gamma_T$



R01543 002

Medium Fine Asphalt

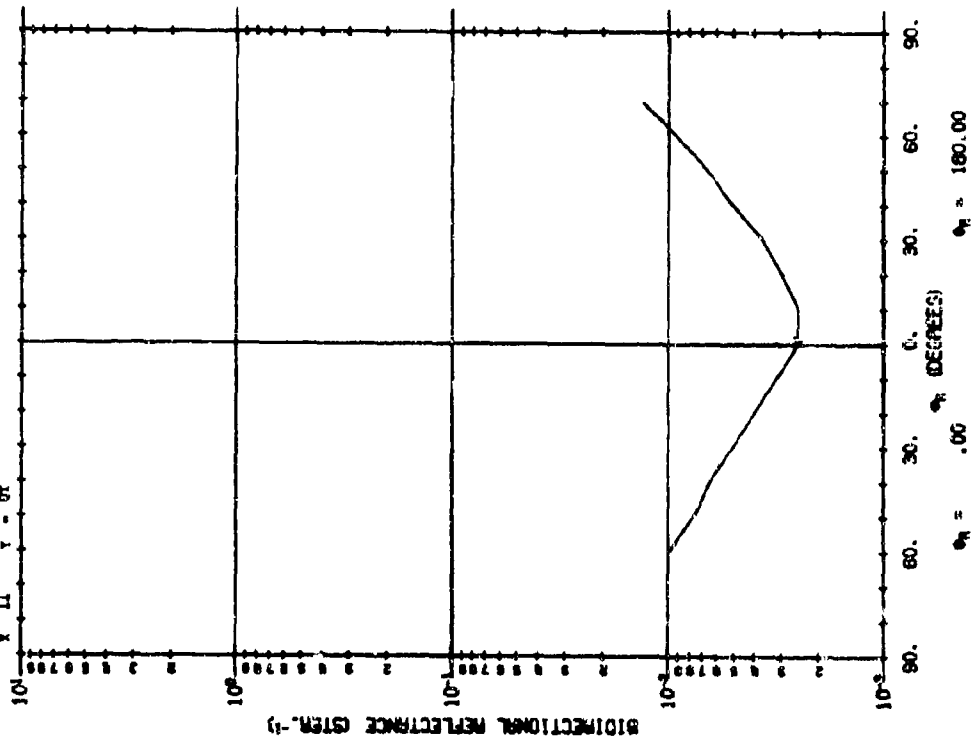
0 ||  $\theta_i = 50.0$   
 + ||  $\theta_t = 270.0$   
 x ||  $\lambda = 10.6$   
 x ||  $\gamma = \gamma_T$



R01546 002

Medium Fine Asphalt

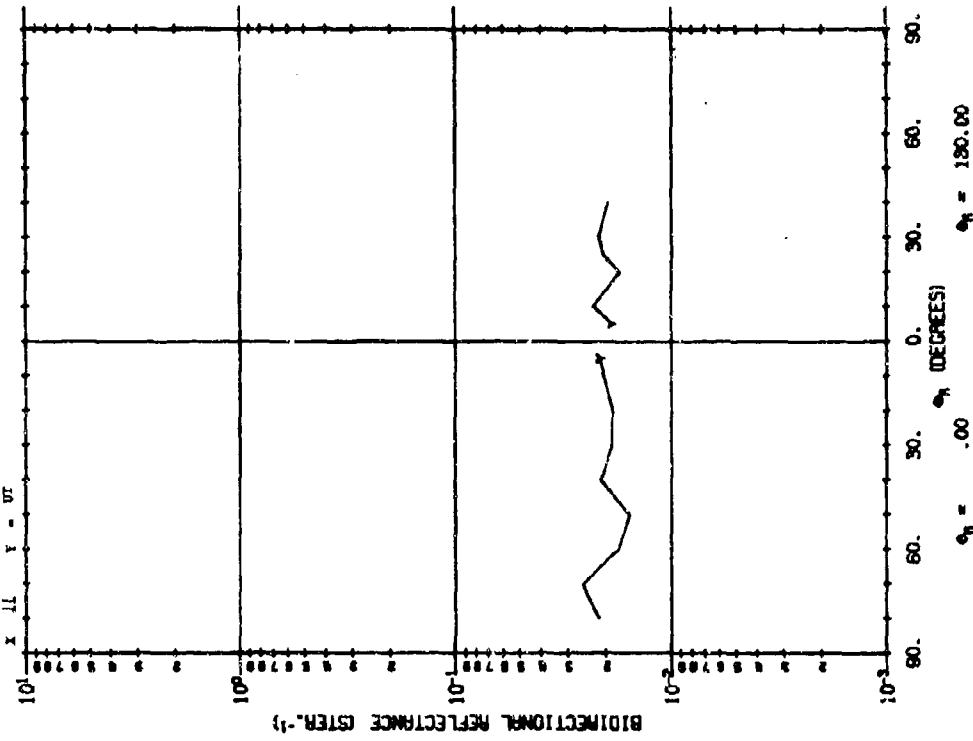
0 ||  $\theta_1 = 1.10$   
 + ||  $\theta_2 = \theta_1$   
 A ||  $\lambda = 10.6$   
 X ||  $\gamma = 0^\circ$



R01546 002

Medium Fine Asphalt

0 ||  $\theta_1 = 0.0$   
 + ||  $\theta_2 = 180.0$   
 A ||  $\lambda = 10.6$   
 X ||  $\gamma = 0^\circ$



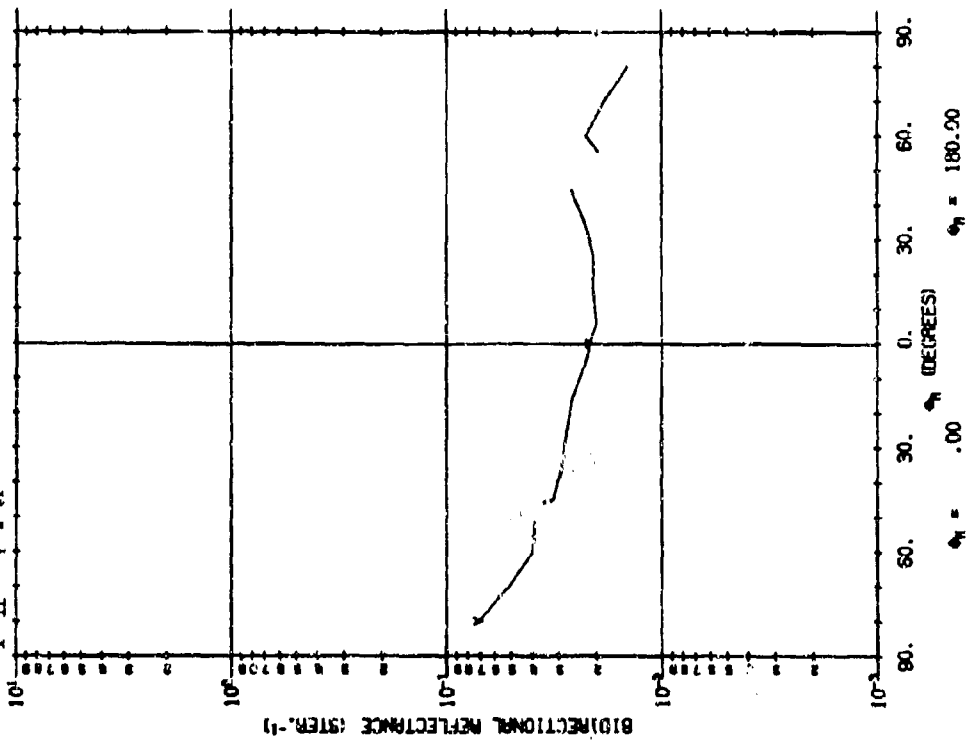
ASPHALT AND CONCRETE



R01546 002

Medium Fine Asphalt

0 //  $\theta_1 = 35.0$   
 + //  $\theta_2 = 180.0$   
 A //  $\lambda = 10.6$   
 X //  $\gamma = 0^\circ$

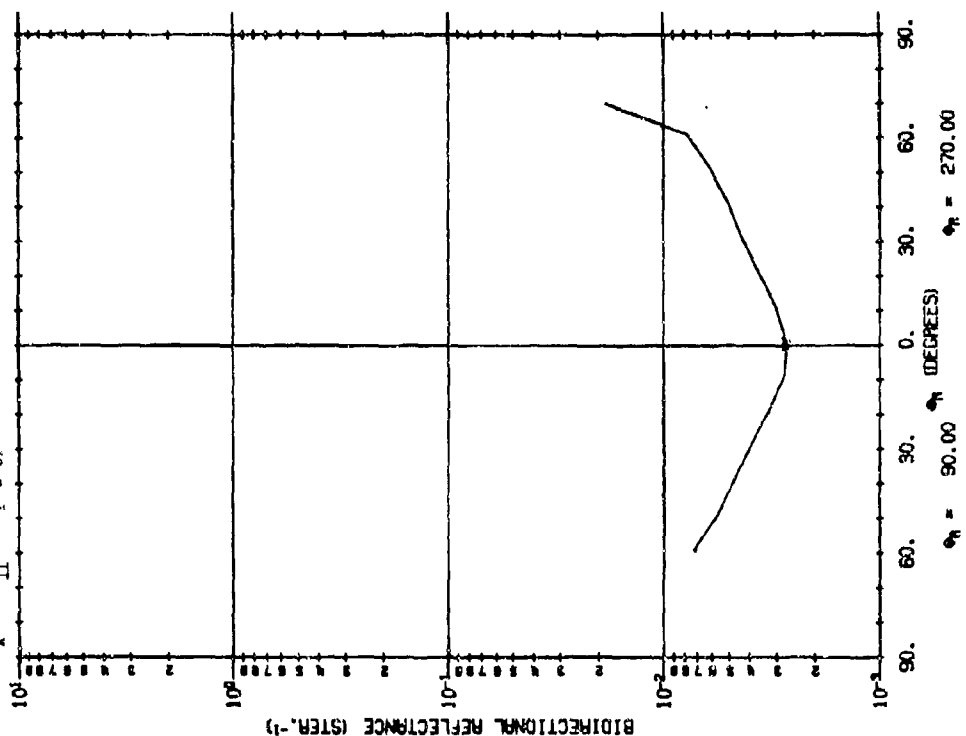


R01546

002

Medium Fine Textured Asphalt

0 //  $\theta_1 = 1.10$   
 + //  $\theta_2 = 0^\circ$   
 A //  $\lambda = 10.6$   
 X //  $\gamma = 0^\circ$



9H510H 002

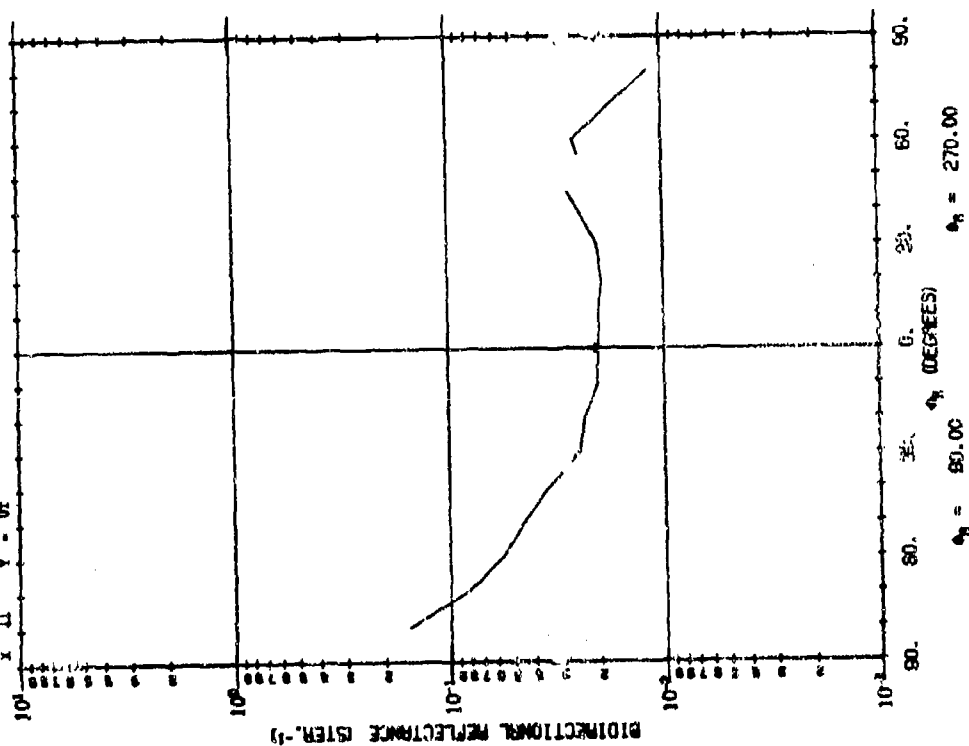
Medium Fine Asphalt

0. = 50.0

 $\theta_x = 270.0$ 

$\lambda = 10.6$

5.



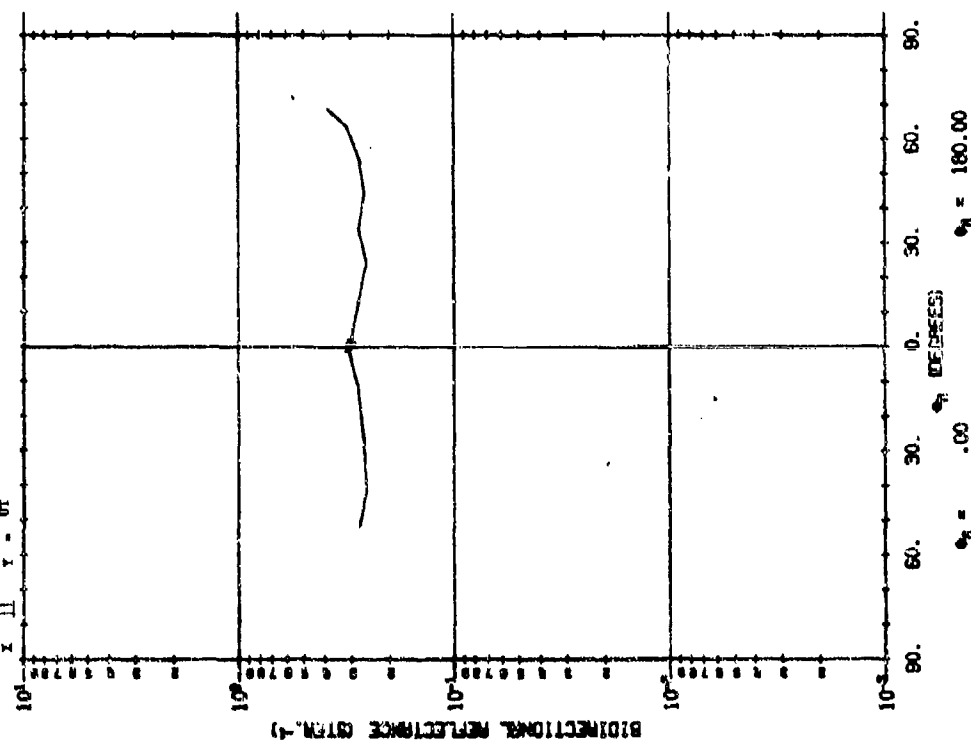
25

# REFLECTANCE STANDARDS MATERIAL

P01094 001

Flame Sprayed Aluminum Panel

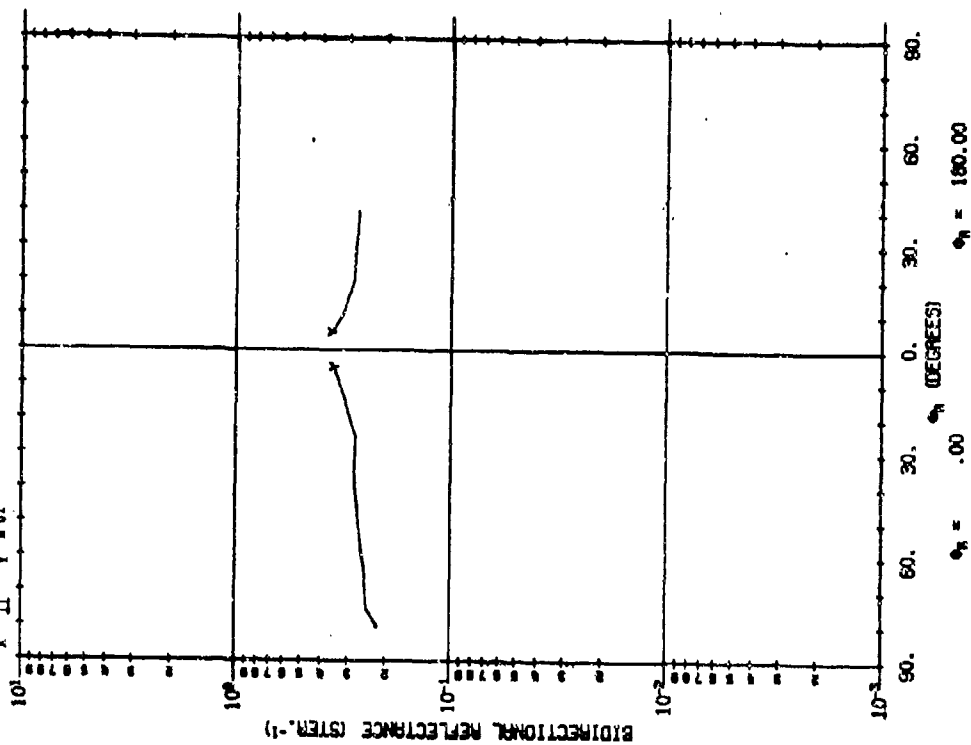
0 || 22 = 1.10  
+ ||  $\theta_1$  = 4°  
A ||  $\lambda$  = 10.6  
X || Y = UT



P01094 001

Flame Sprayed Aluminum Panel

0 ||  $\theta_1$  = 0.0  
+ ||  $\theta_2$  = 180.0  
A ||  $\lambda$  = 10.6  
X || Y = UT

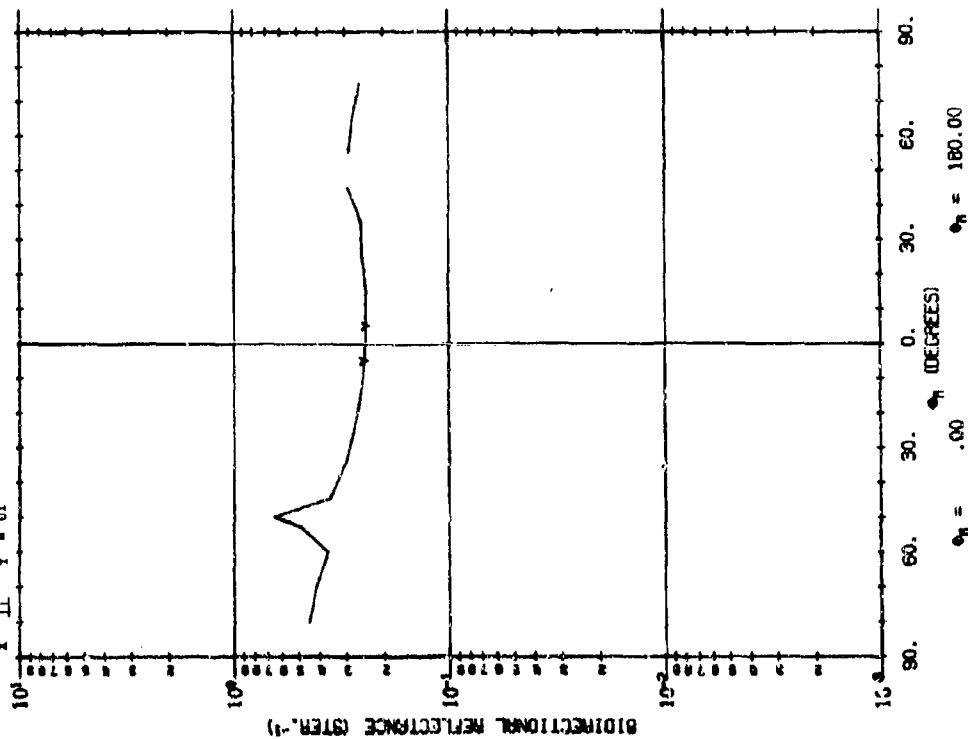


REFLECTANCE STANDARDS MATERIAL

A01094 001

Flame Sprayed Aluminum Panel

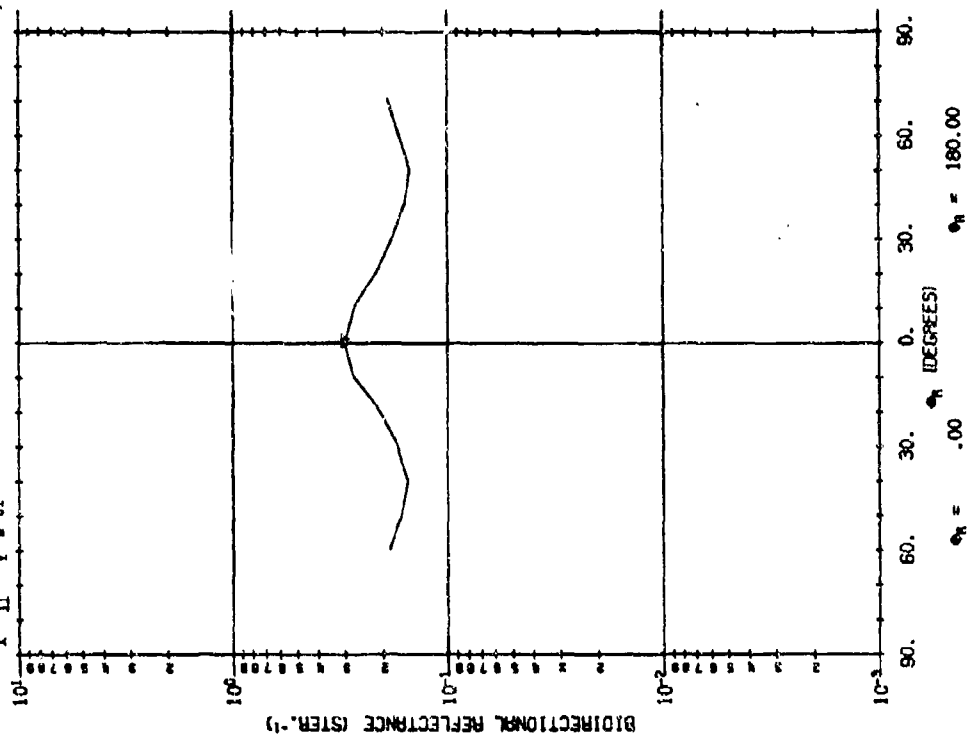
0 ||  $\theta_1 = 50.0$   
 + ||  $\phi_1 = 180.0$   
 Δ ||  $\lambda = 10.6$   
 X || Y = UT



A01095 001

Flame Sprayed Copper Panel

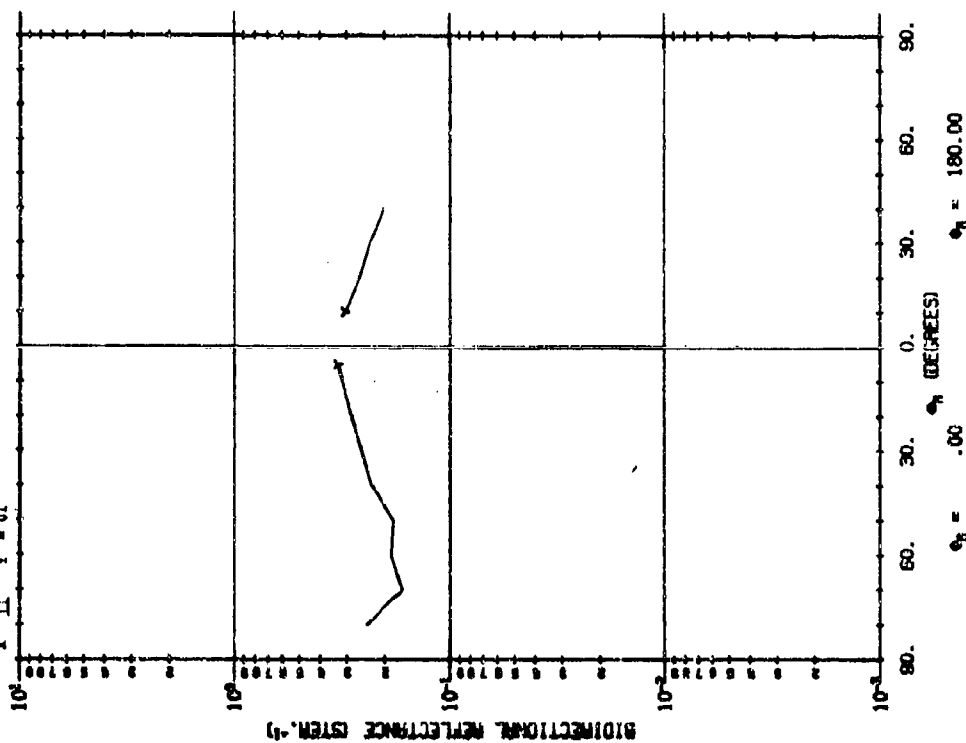
0 ||  $2\theta = 1.10$   
 + ||  $\phi_1 = 4r$   
 Δ ||  $\lambda = 10.6$   
 X || Y = UT



R01095 001

Flame Sprayed Copper Panel

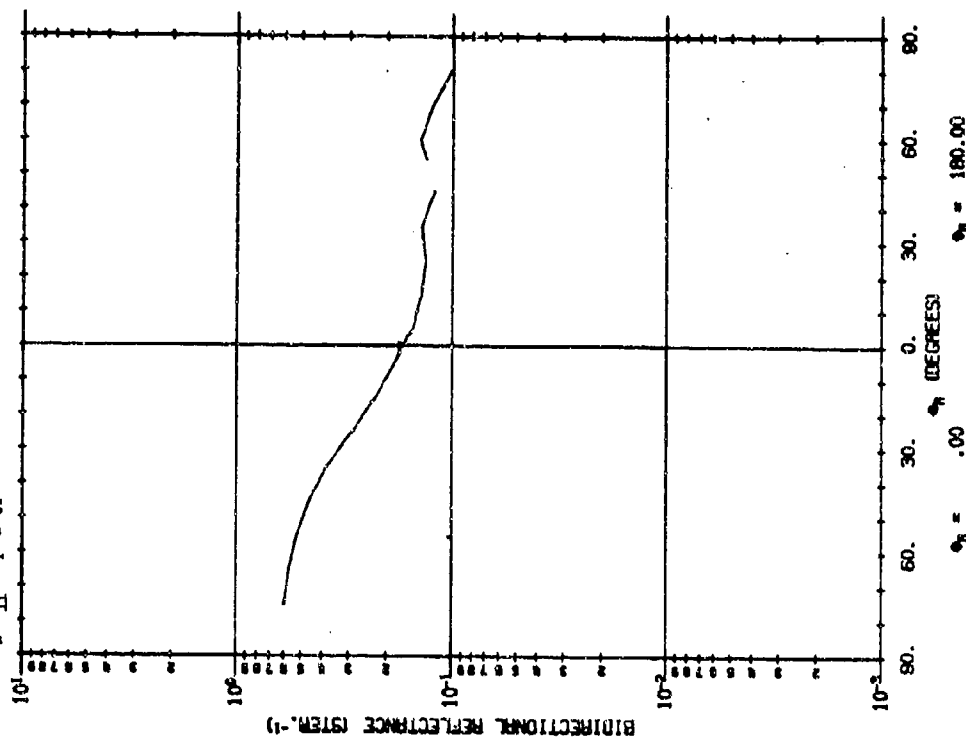
0 ||  $\phi_1 = 0.0$   
 + ||  $\phi_2 = 180.0$   
 x ||  $\lambda = 10.6$   
 Y = UT



R01095 001

Flame Sprayed Copper Panel

0 ||  $\phi_1 = 50.0$   
 + ||  $\phi_2 = 180.0$   
 x ||  $\lambda = 10.6$   
 Y = UT

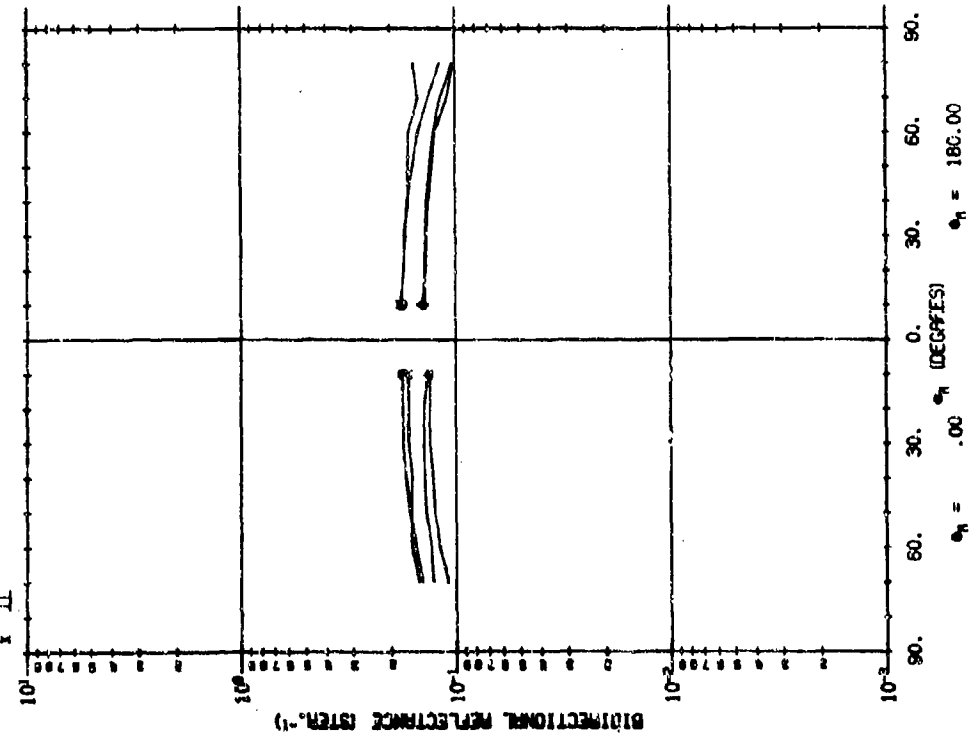


# REFLECTANCE STANDARDS MATERIAL

A01190 001

SHERED MAGNESIUM OXIDE  
ON ALUMINUM PLATE

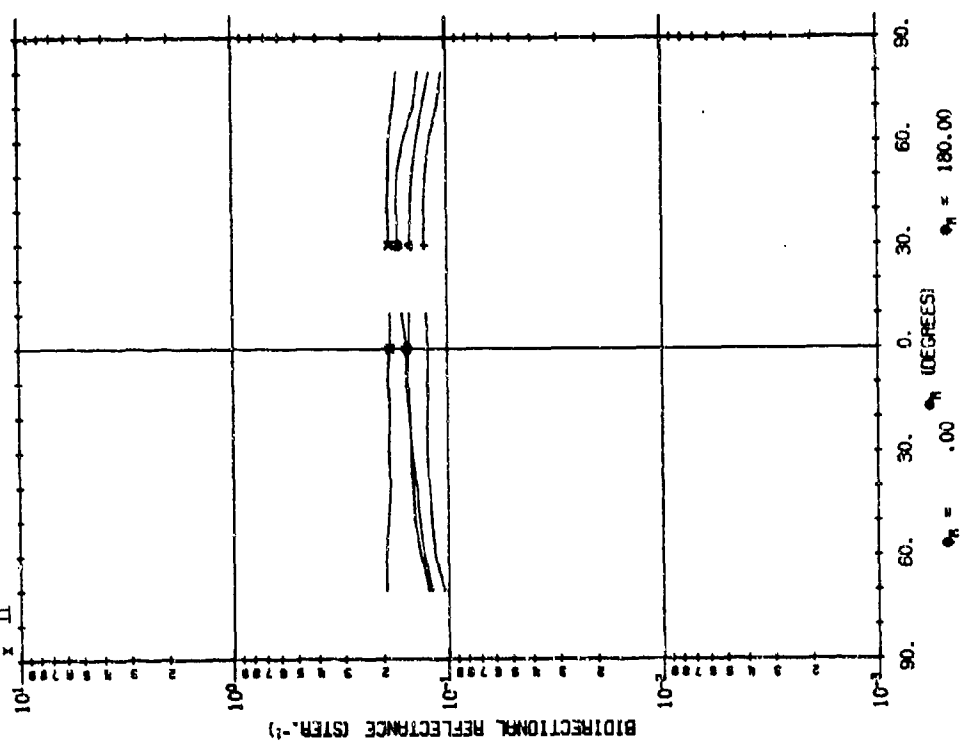
$\theta_1 = 0.0$   
 $\phi_1 = 180.0$   
 $\lambda = 0.63$

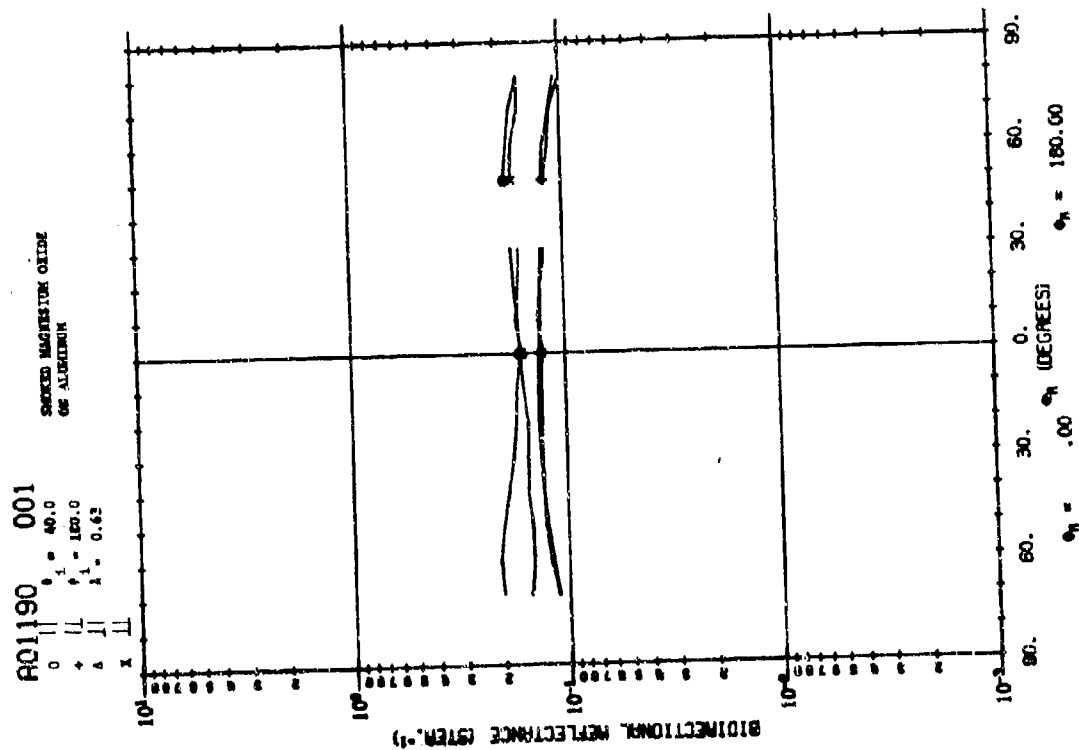
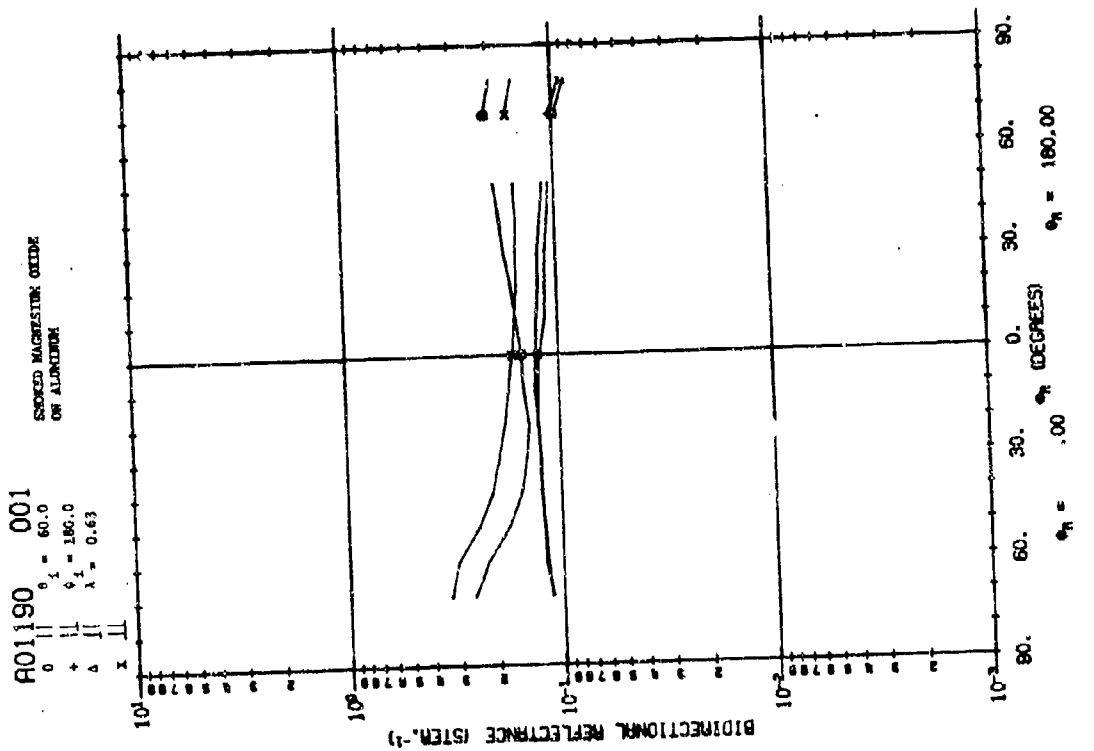


A01190 001

SHERED MAGNESIUM OXIDE  
ON ALUMINUM PLATE

$\theta_1 = 20.0$   
 $\phi_1 = 180.0$   
 $\lambda = 0.63$





REFLECTANCE STANDARDS MATERIAL



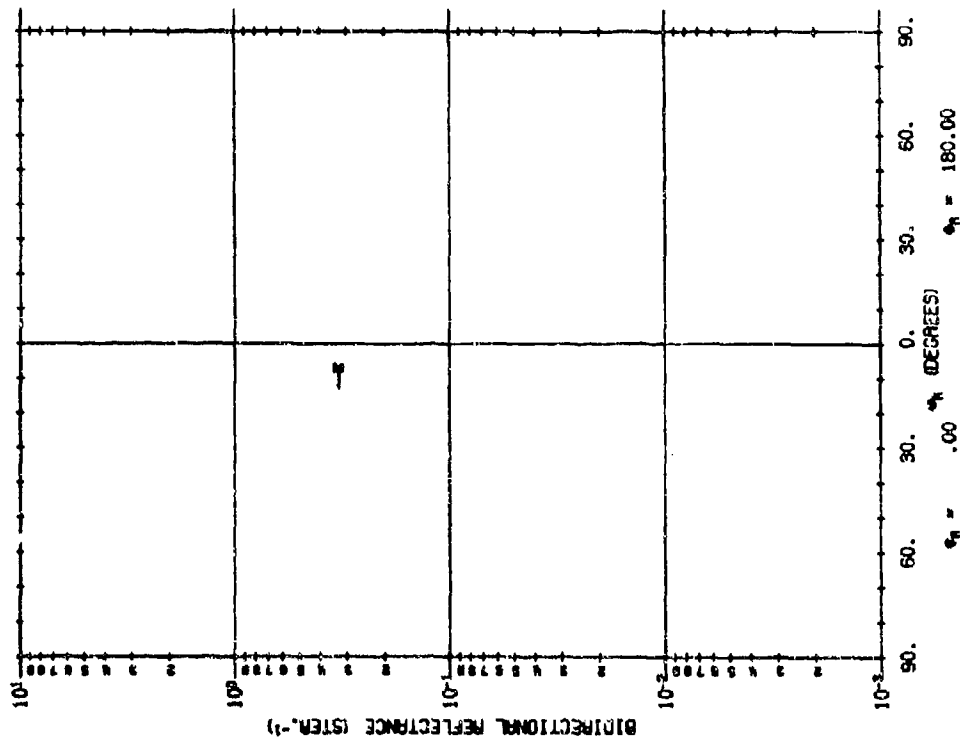
A01191 001

FIBERFAX TYPE 970 JR ON 1/4" PLYWOOD

X | Y |  $\theta_i = 0.0$

Z |  $\phi_i = 180.0$

$\lambda = 0.43$



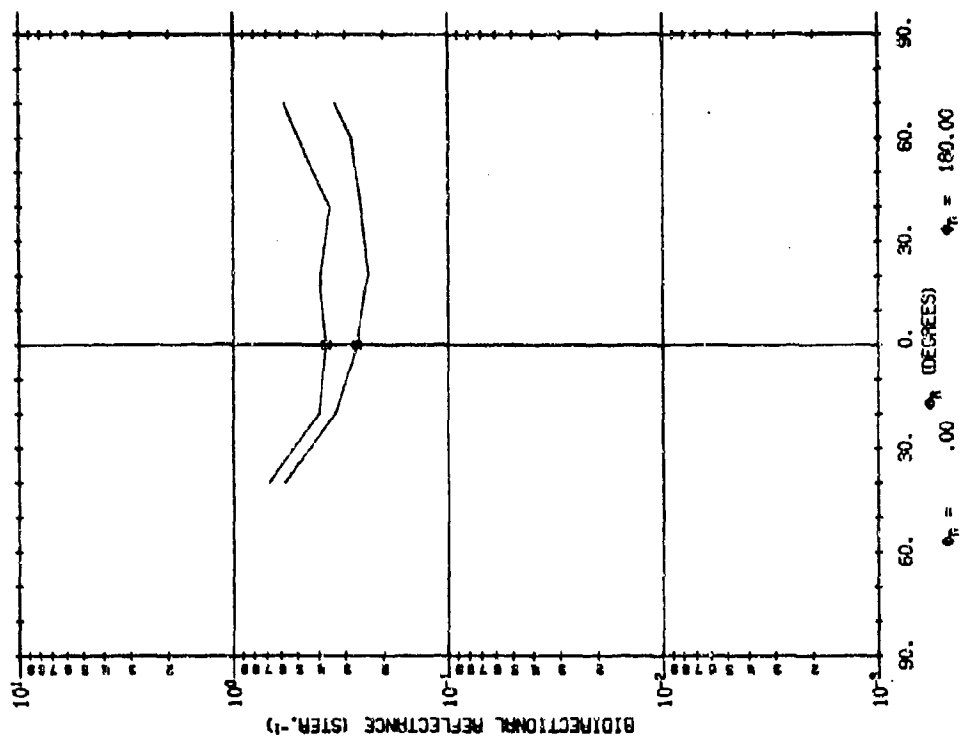
A01191 001

FIBERFAX TYPE 970 JR ON 1/4" PLYWOOD

X | Y |  $\theta_i = 0.0$

Z |  $\phi_i = 180.0$

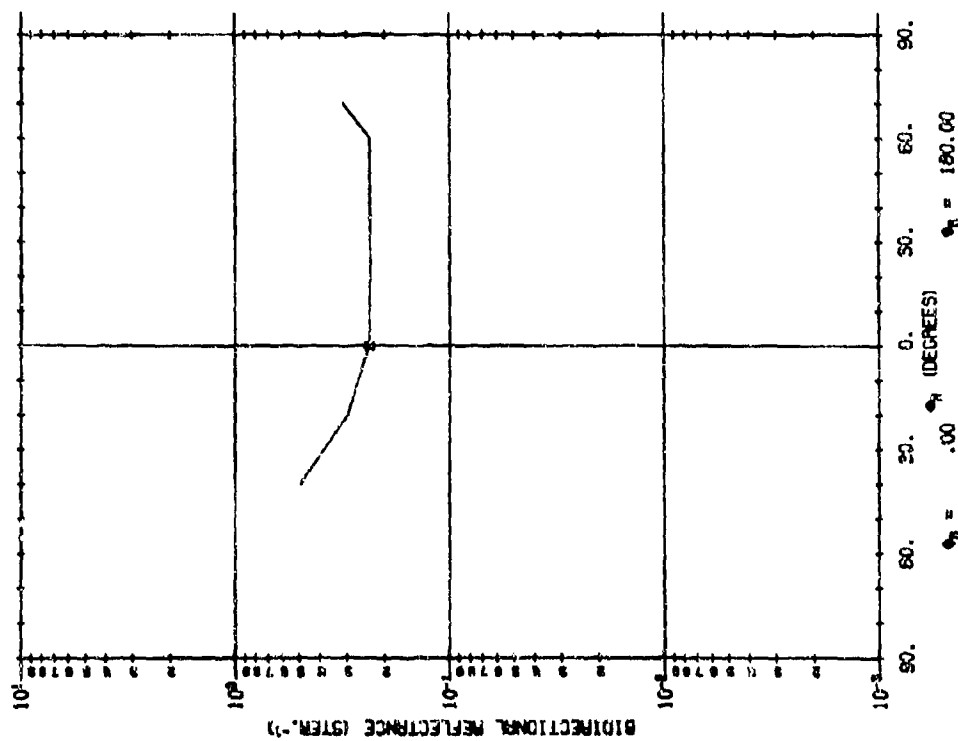
$\lambda = 0.43$



R01191 001

FIBREPLAX TYPE 970 JH ON 1/4" PLYWOOD

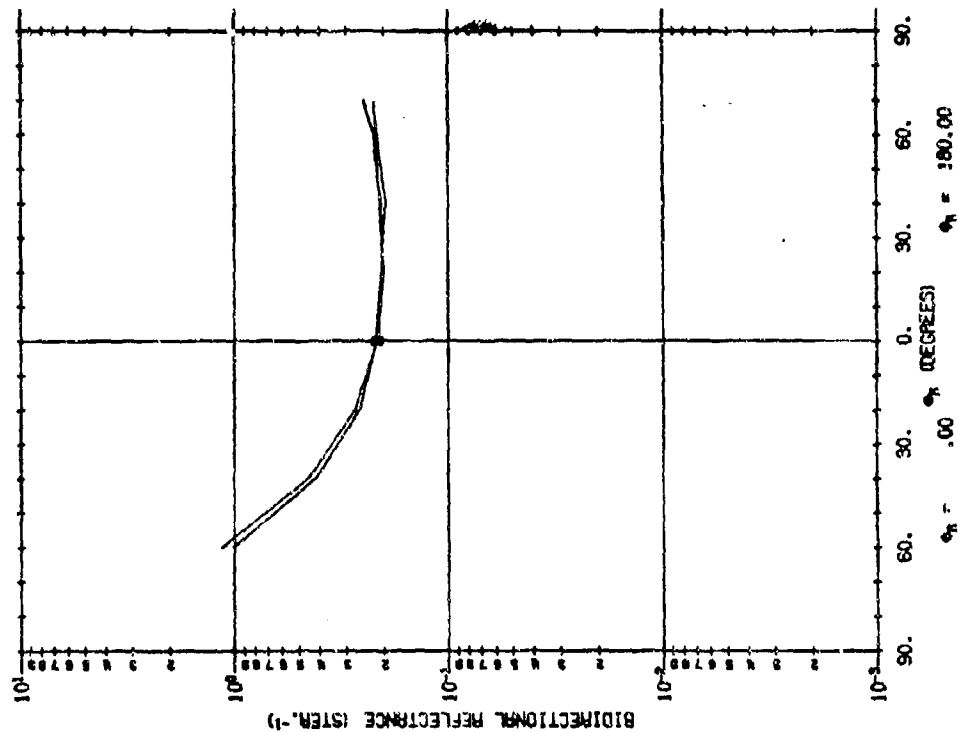
$\lambda = 0.55$   
 $\theta_i = 80.0$   
 $\theta_t = 180.0$



R01191 001

FIBREPLAX TYPE 970 JH ON 1/4" PLYWOOD

$\lambda = 0.75$   
 $\theta_i = 80.0$   
 $\theta_t = 180.0$

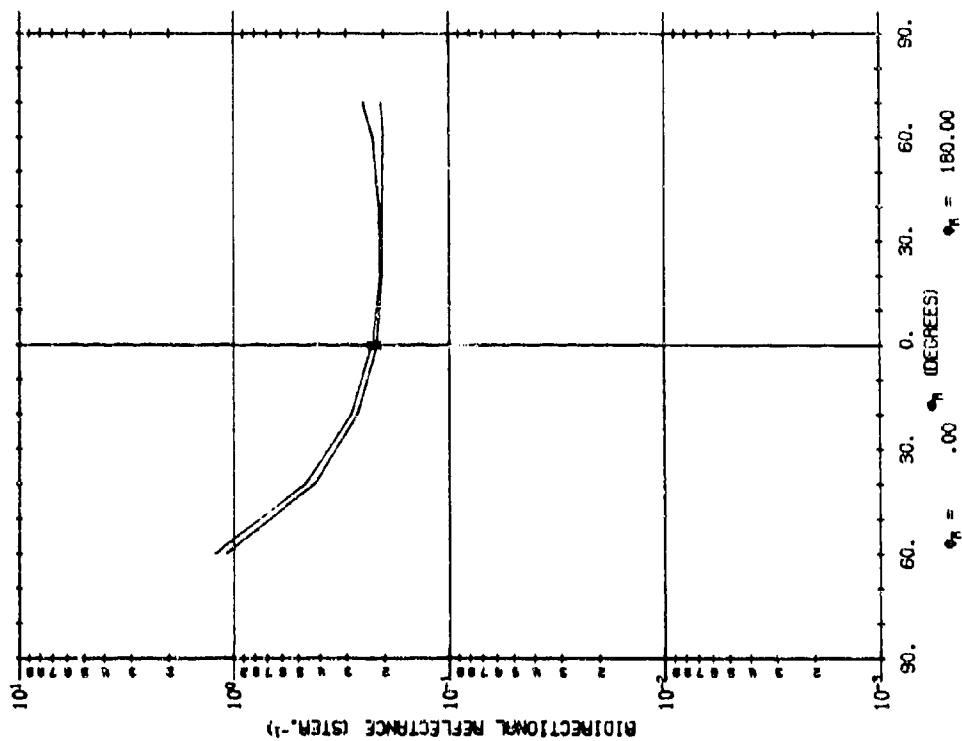


# REFLECTANCE STANDARDS MATERIAL

A01191 001

FIBERGLASS TYPE 970 JH ON 1/4" PLYWOOD

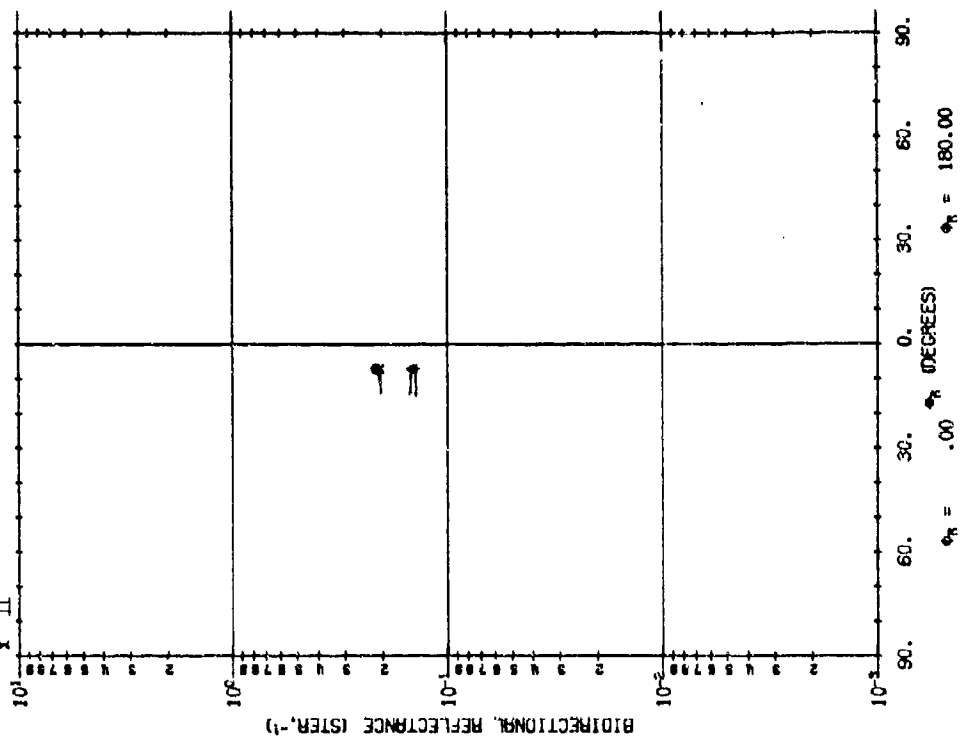
X ||  $\theta_i = 80.0$   
Z ||  $\phi_i = 180.0$   
 $\lambda = 1.10$



A01191 002

FIBERGLASS TYPE 970 JH ON 1/4" PLYWOOD

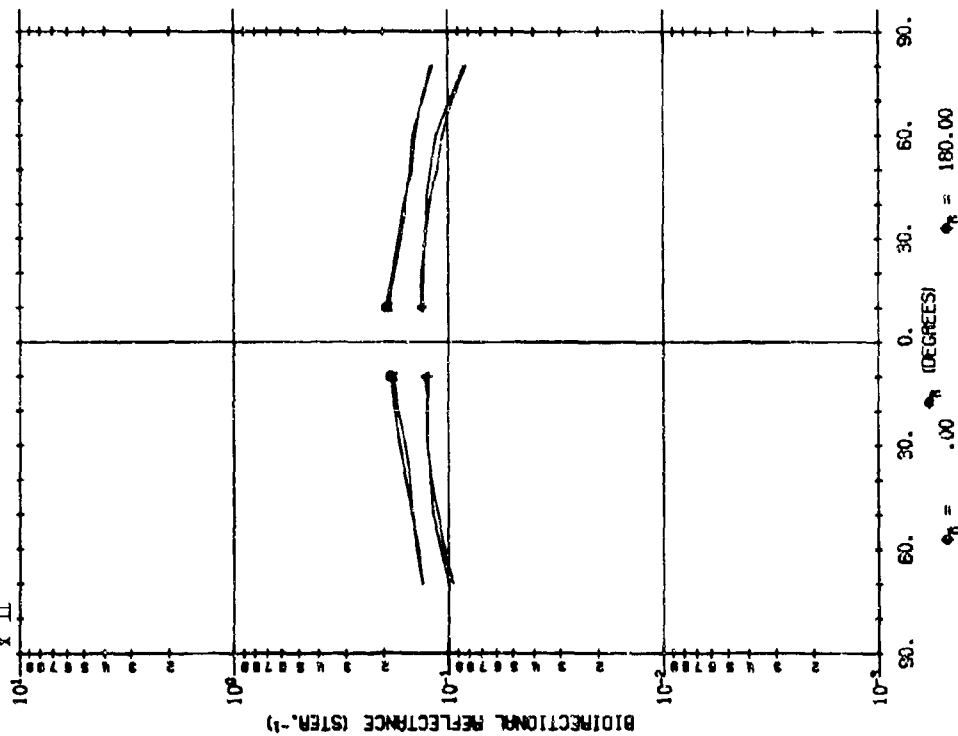
X ||  $\theta_i = 0.0$   
Z ||  $\phi_i = 180.0$   
 $\lambda = 0.55$



R01191 002

FIBERFLAX TYPE 970 JH ON 1/4" PLYWOOD

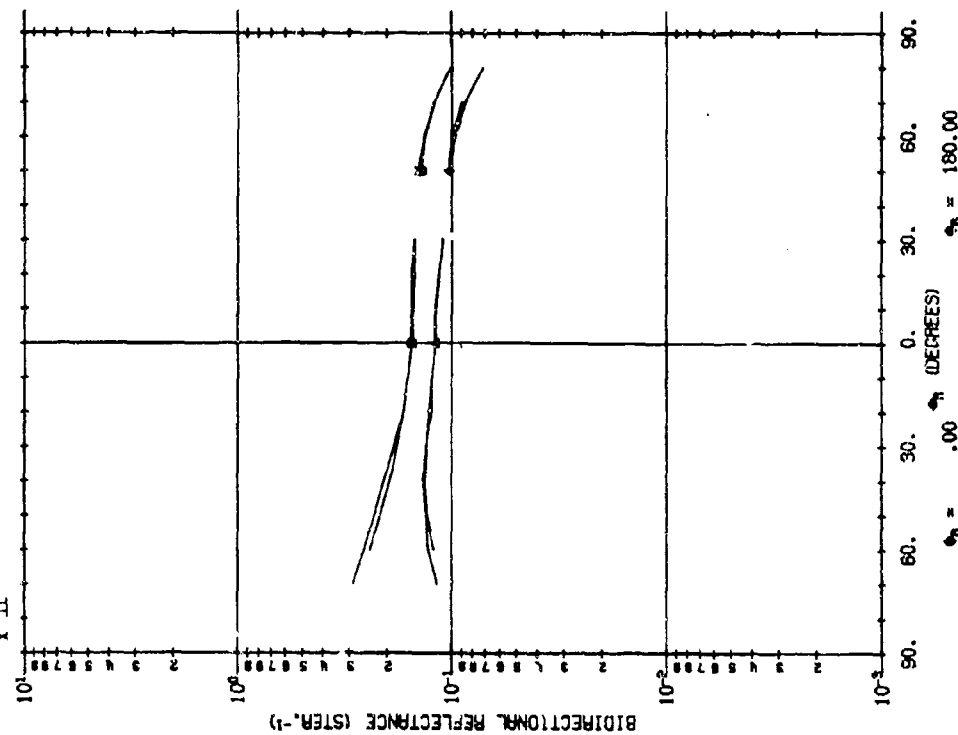
0 ||  $\theta_1 = 0.0$   
 + ||  $\theta_2 = 180.0$   
 Δ ||  $\lambda = 0.63$   
 x ||



R01191 002

FIBERFLAX TYPE 970 JH ON 1/4" PLYWOOD

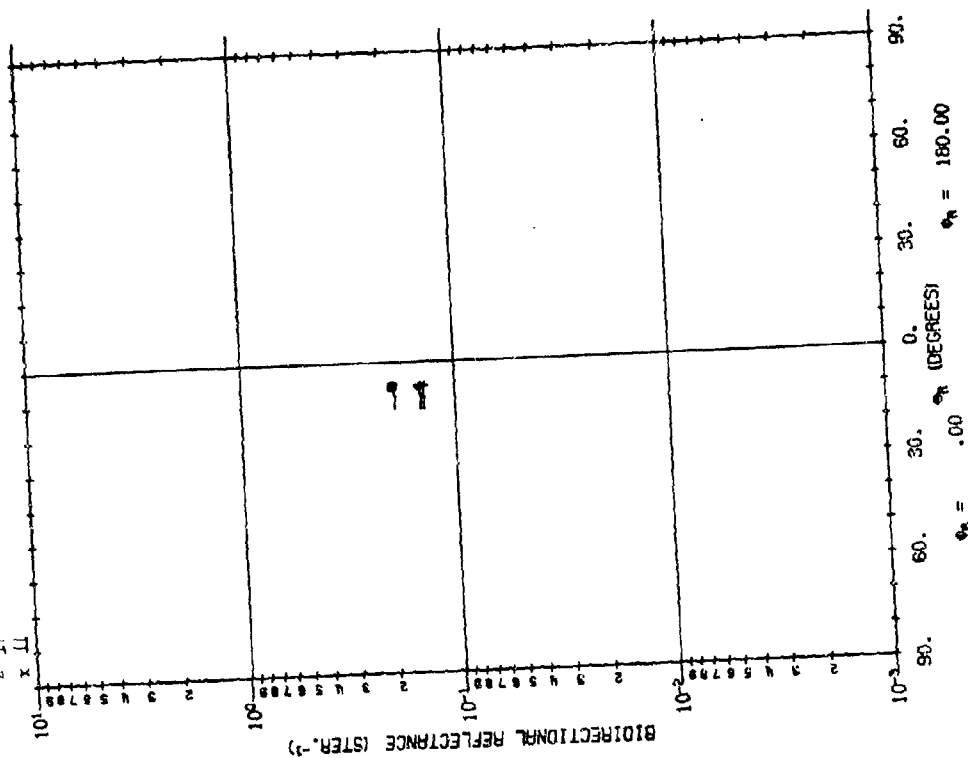
0 ||  $\theta_1 = 40.0$   
 + ||  $\theta_2 = 180.0$   
 Δ ||  $\lambda = 0.63$   
 x ||



REFLECTANCE STANDARDS MATERIAL

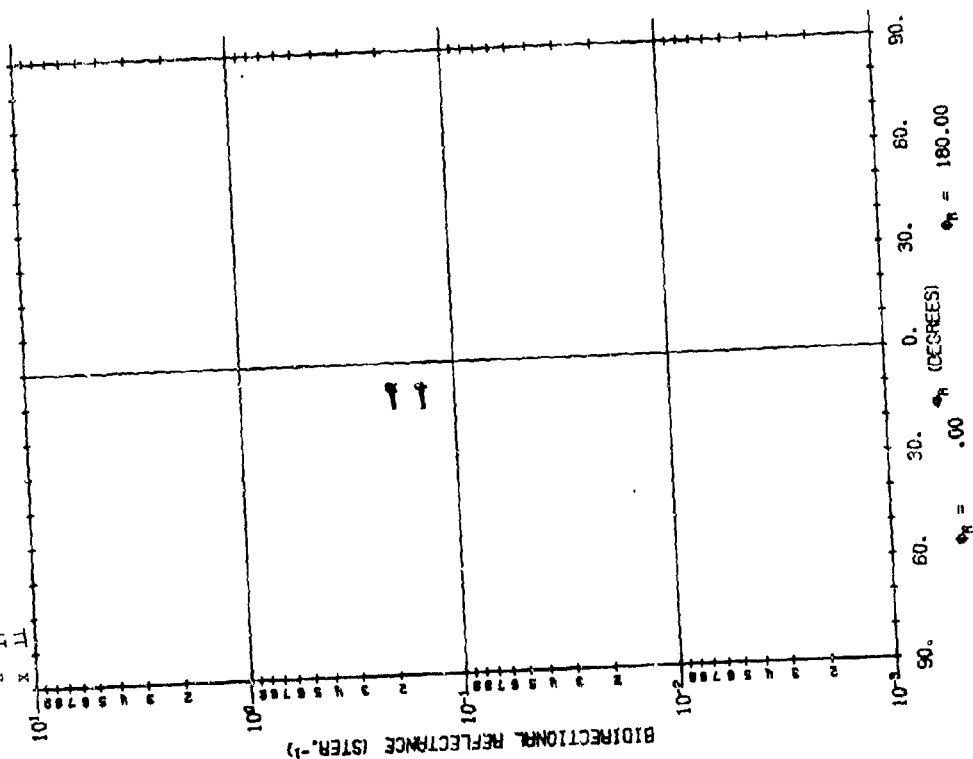
R01191 002  
FIBERFRAX TYPE 970 JH ON 1/4" PLYWOOD

$\theta_i = 0.0$   
 $\phi_i = 180.0$   
 $\lambda = 1.10$



R01191 002  
FIBERFRAX TYPE 970 JH ON 1/4" PLYWOOD

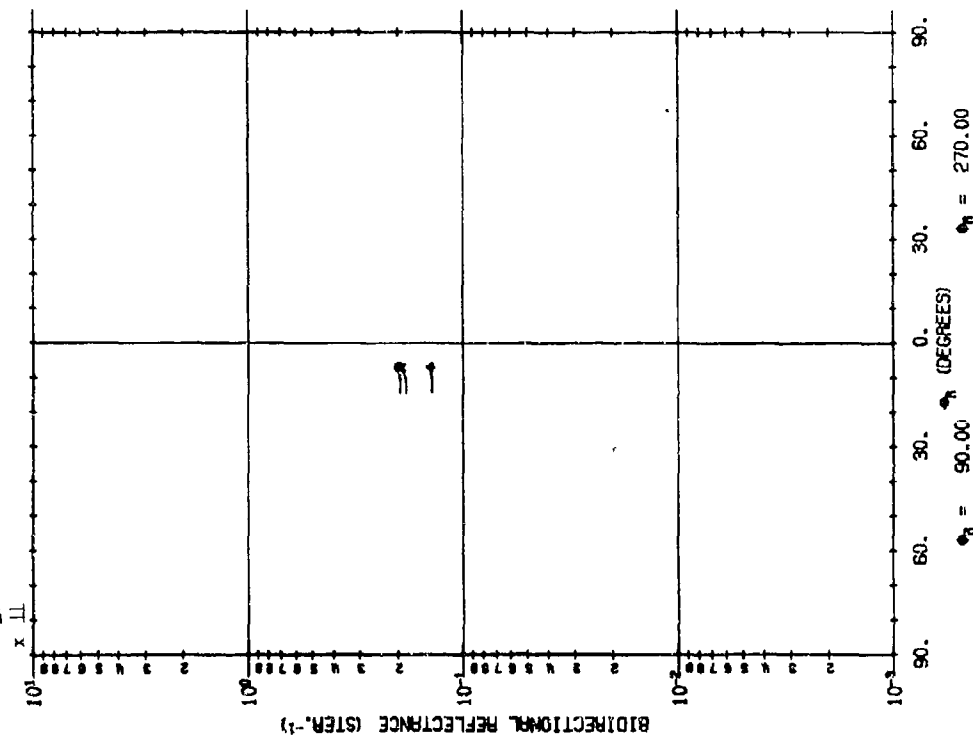
$\theta_i = 0.0$   
 $\phi_i = 180.0$   
 $\lambda = 0.75$



A01191 002

FIBERFRAX TYPE 970 JET ON 1/4" PLYWOOD

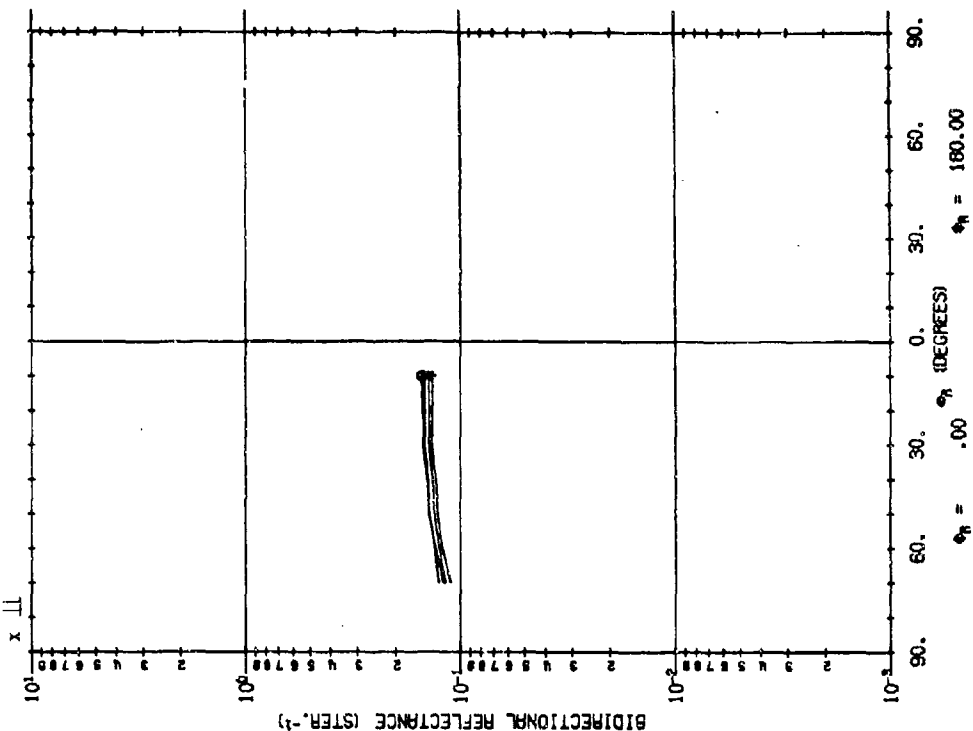
0 ||  $\phi_1 = 0.0$   
 + ||  $\phi_1 = 270.0$   
 Δ ||  $\lambda = 1.10$



A01192 001

FLOWERS OF SULFUR

0 ||  $\phi_1 = 0.0$   
 + ||  $\phi_1 = 180.0$   
 Δ ||  $\lambda = 0.63$

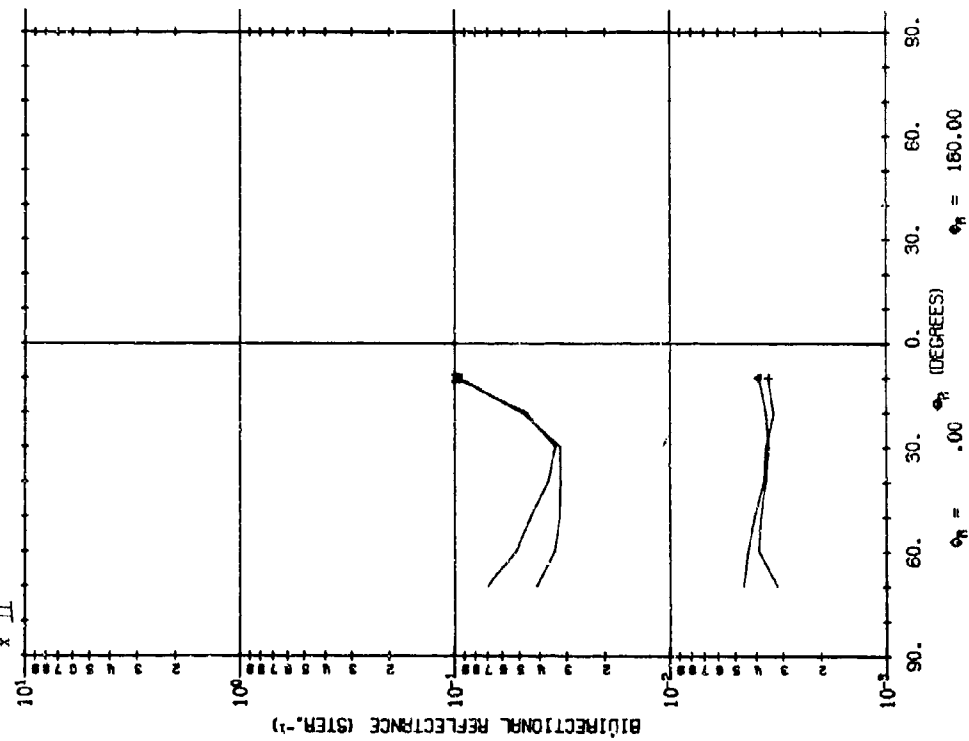


# REFLECTANCE STANDARDS MATERIAL

A01194 001

CHROME PLATED GLASS BEADS

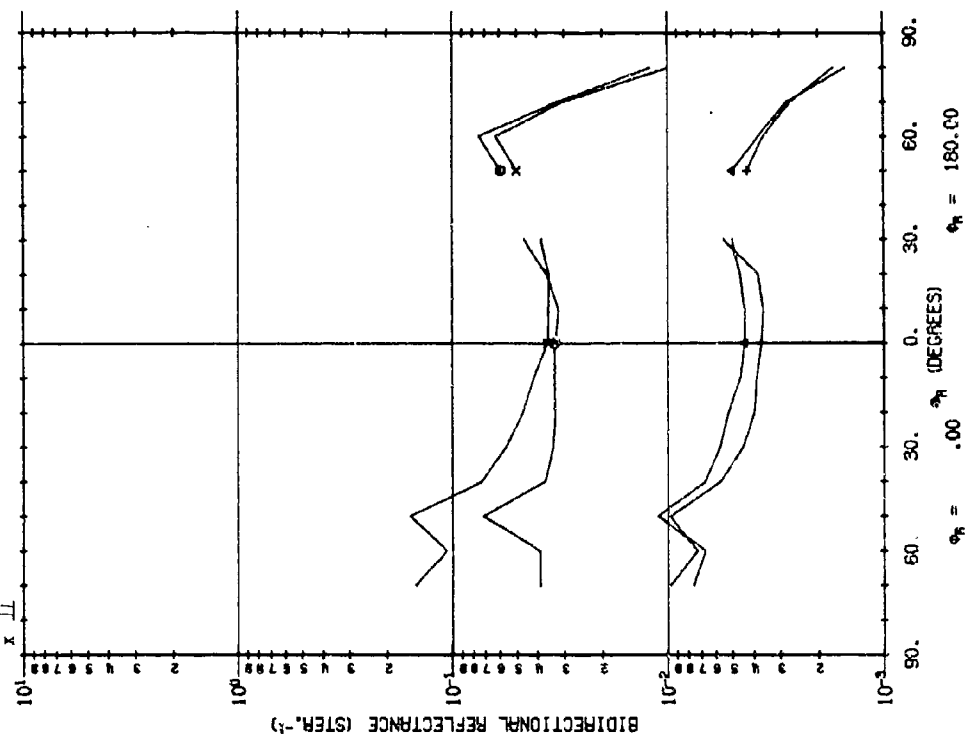
0 ||  $\phi_1 = 0.0$   
 + ||  $\phi_2 = 180.0$   
 Δ ||  $\lambda = 0.63$



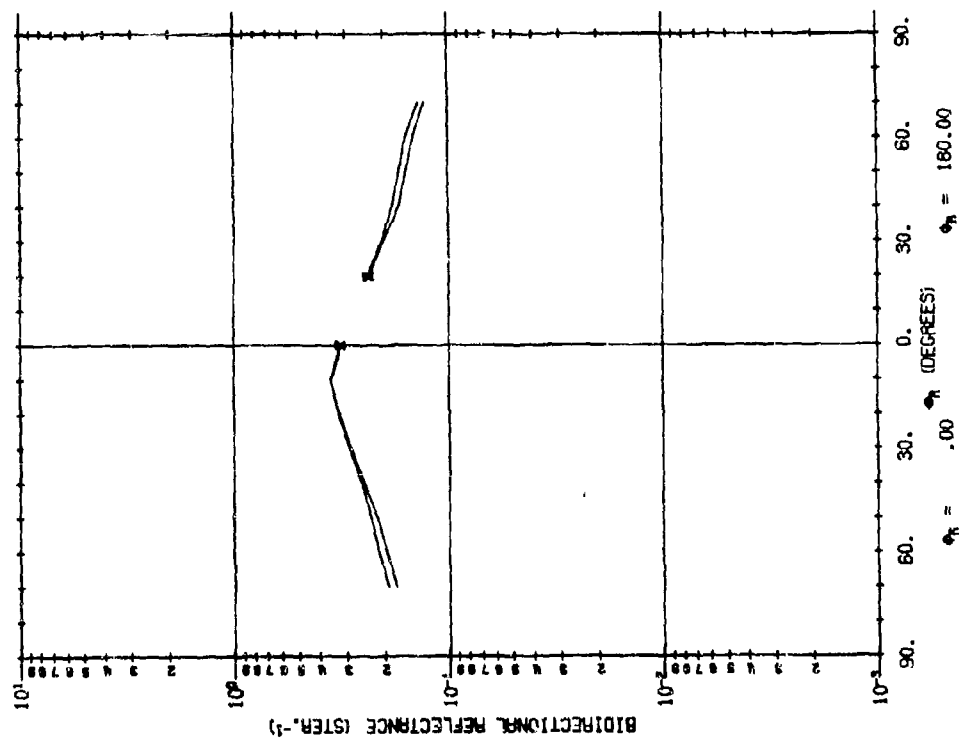
A01194 001

CHROME PLATED GLASS BEADS

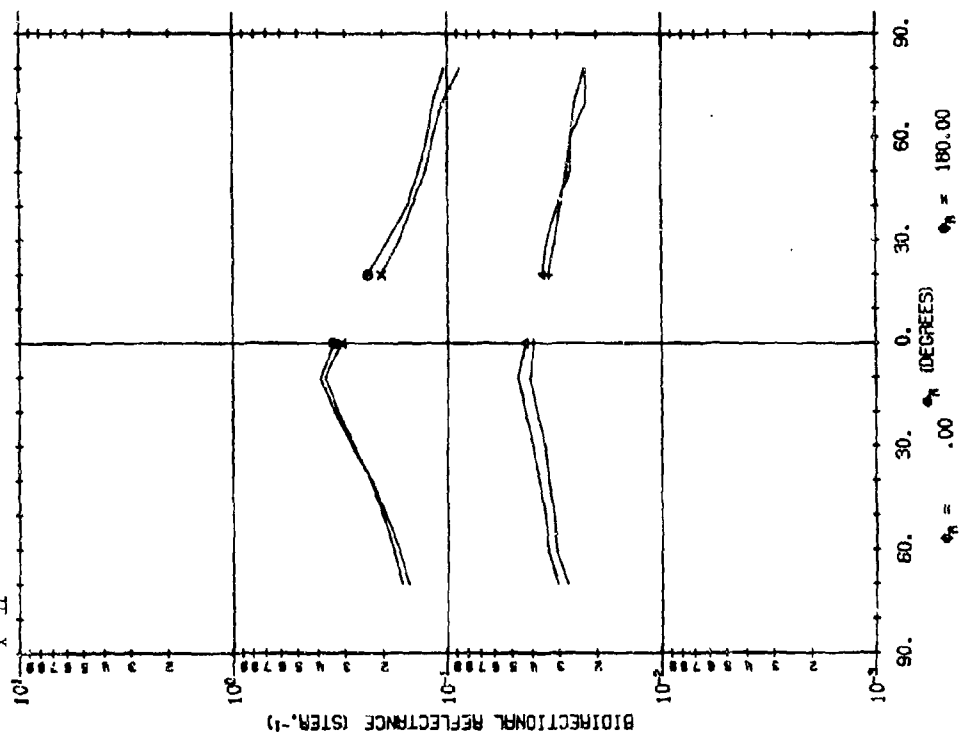
0 ||  $\phi_1 = 60.0$   
 + ||  $\phi_2 = 180.0$   
 Δ ||  $\lambda = 0.63$



R01197 001  
 SANDBLASTED ALUMINUM  
 $\theta_1 = 10.0$   
 $\phi_1 = 180.0$   
 $\lambda = 0.54$



R01197 002  
 SANDBLASTED ALUMINUM  
 $\theta_1 = 10.0$   
 $\phi_1 = 180.0$   
 $\lambda = 1.08$



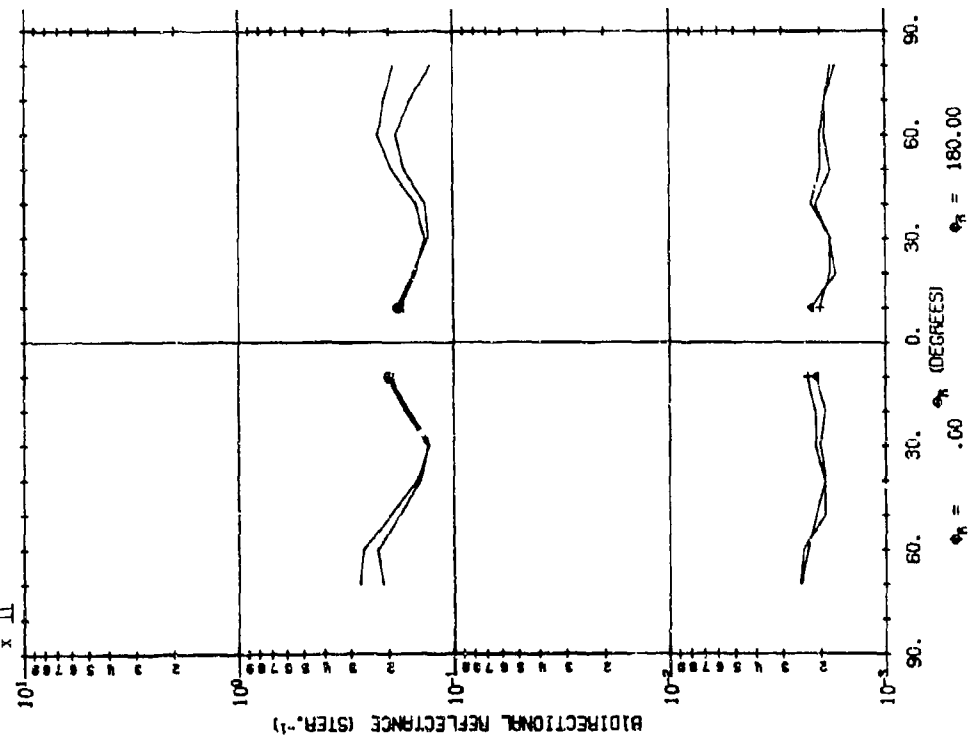
REFLECTANCE STANDARDS MATERIAL



R01272 001

CHROME PLATED GLASS BEADS

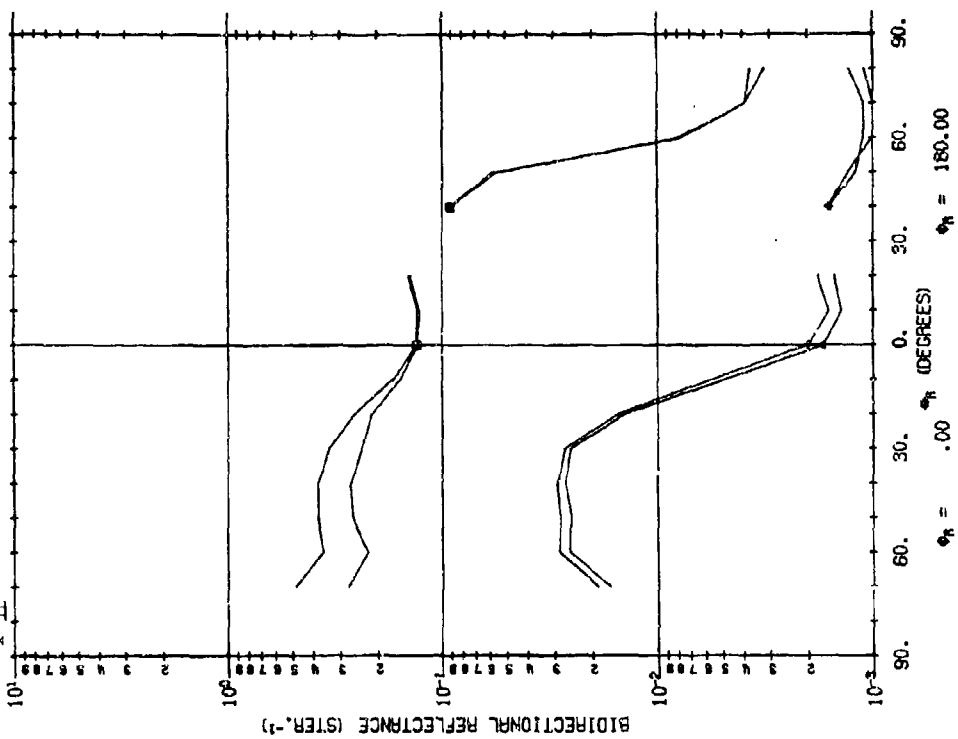
$\epsilon_1 = 0.0$   
 $\phi_1 = 180.0$   
 $\lambda = 1.06$



R01272 001

CHROME PLATED GLASS BEADS

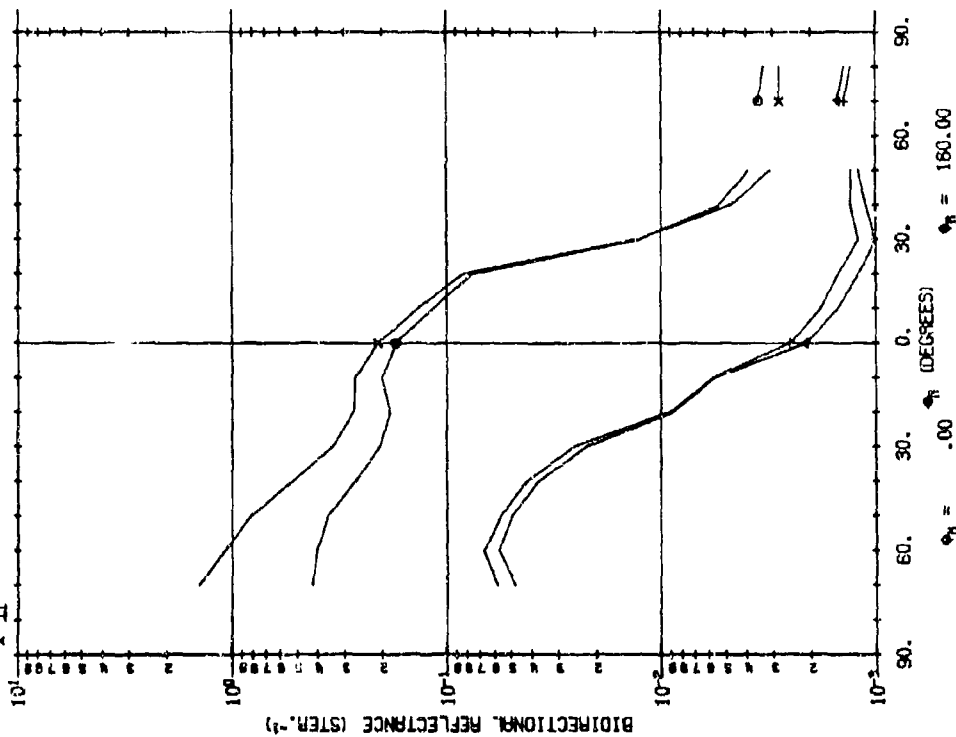
$\epsilon_1 = 30.0$   
 $\phi_1 = 180.0$   
 $\lambda = 1.06$



R01272 001

CHROME PLATED GLASS BEADS

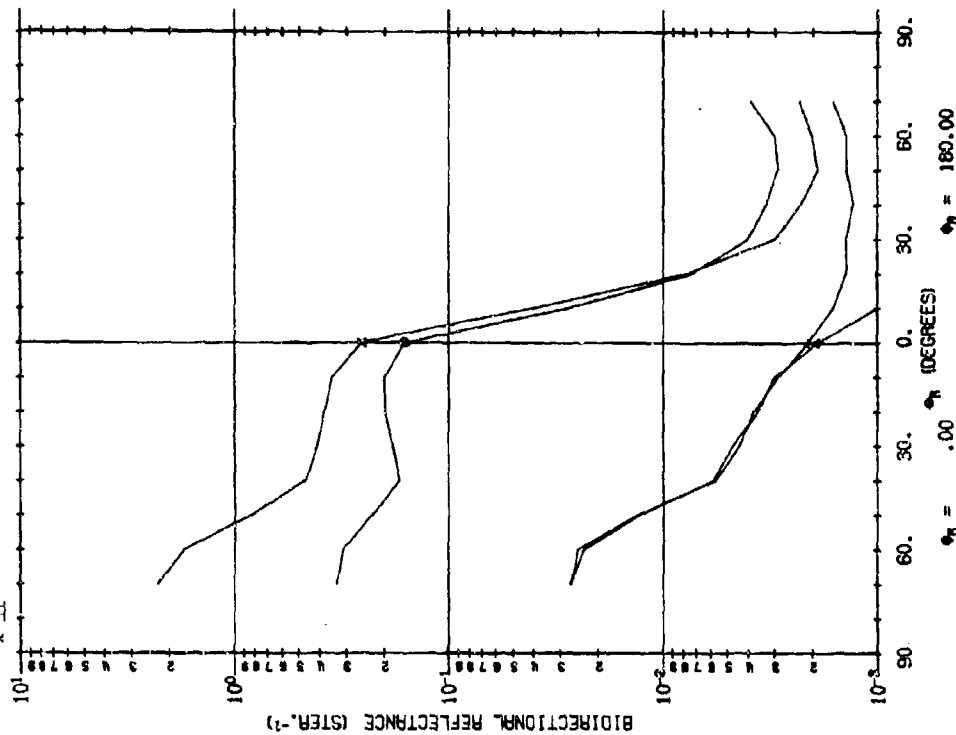
$\theta_i = 60.0$   
 $\phi_i = 180.0$   
 $\lambda = 1.06$



R01272 001

CHROME PLATED GLASS BEADS

$\theta_i = 80.0$   
 $\phi_i = 180.0$   
 $\lambda = 1.06$

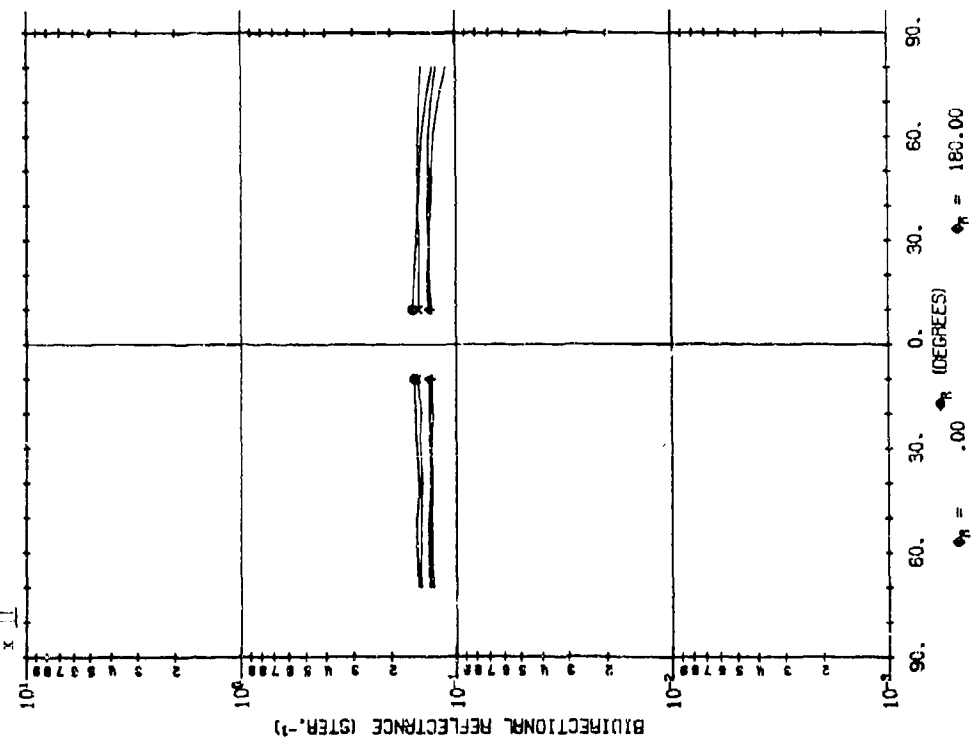


## REFLECTANCE STANDARDS MATERIAL

A01290 001

TWO COATS 3K WHITE PAINT ON ZINC  
CHROMATE PRIMER ON ANODIZED ALUMINUM

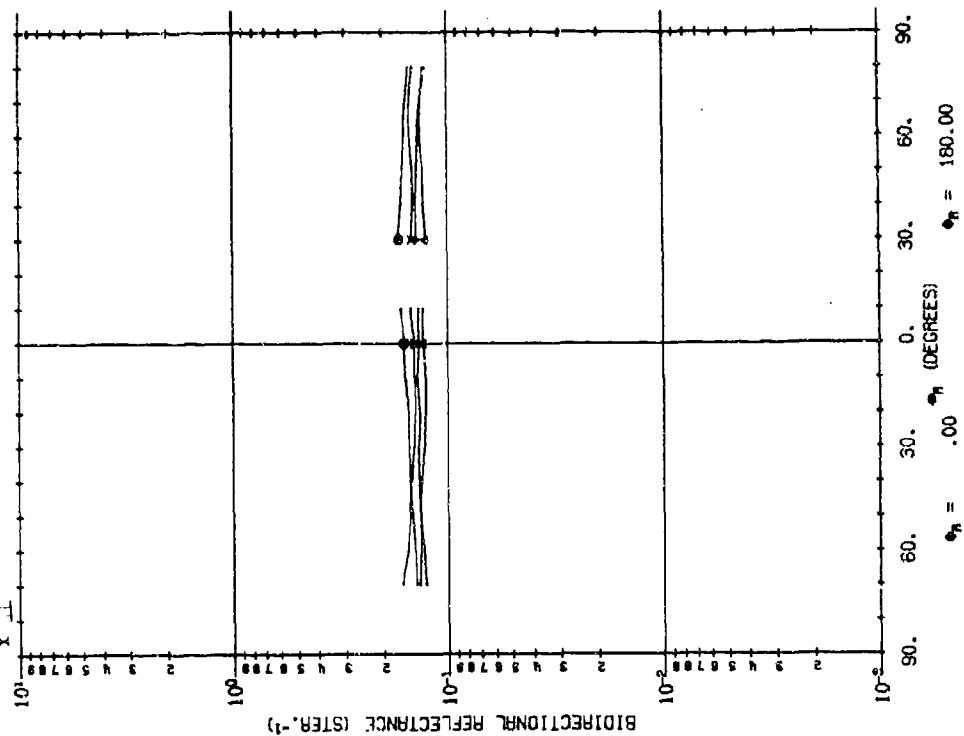
0 ||  $\phi_i = 0.0$   
+ ||  $\phi_i = 180.0$   
Δ ||  $\lambda = 1.06$



A01290 001

TWO COATS 3K WHITE PAINT ON ZINC  
CHROMATE PRIMER ON ANODIZED ALUMINUM

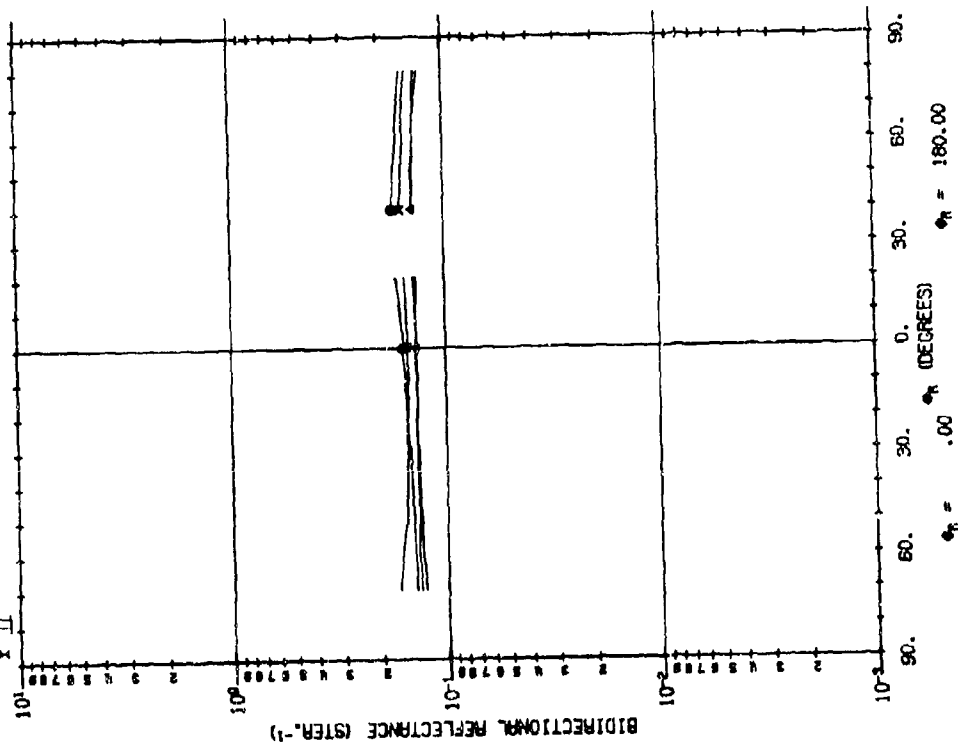
0 ||  $\phi_i = 20.0$   
+ ||  $\phi_i = 180.0$   
Δ ||  $\lambda = 1.06$



A01290 001

TWO COATS 2M WHITE PAINT ON ZINC  
CHROMATE PRIMER ON ANODIZED ALUMINUM

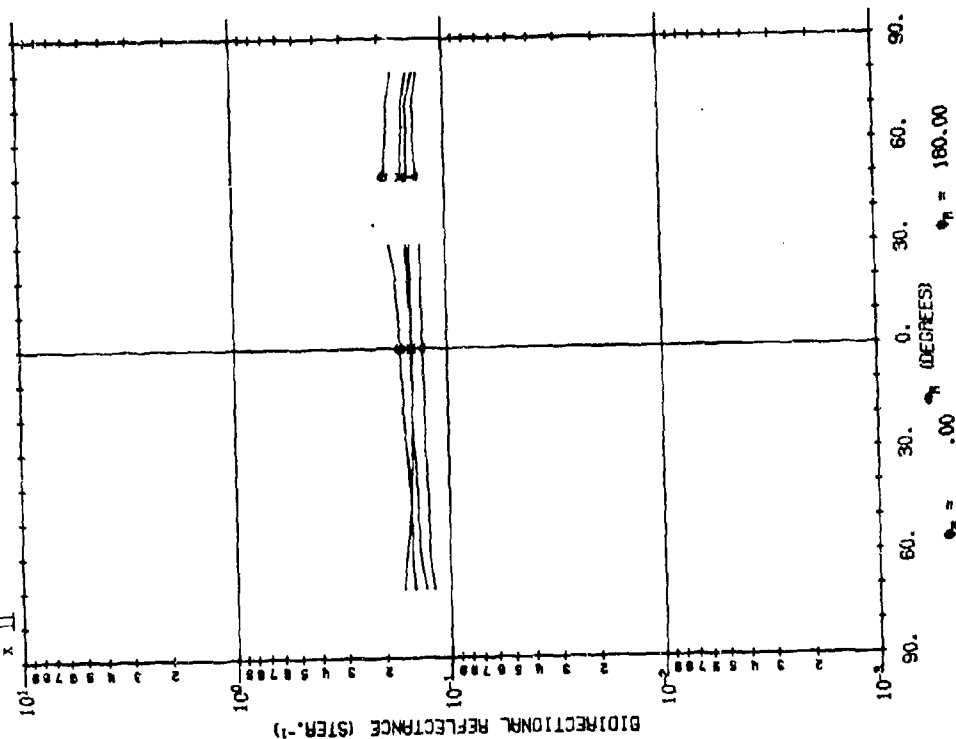
$\theta_i = 30.0$   
 $\phi_i = 180.0$   
 $\lambda = 1.06$



A01290 001

TWO COATS 3M WHITE PAINT ON ZINC  
CHROMATE PRIMER ON ANODIZED ALUMINUM

$\theta_i = 40.0$   
 $\phi_i = 180.0$   
 $\lambda = 1.06$

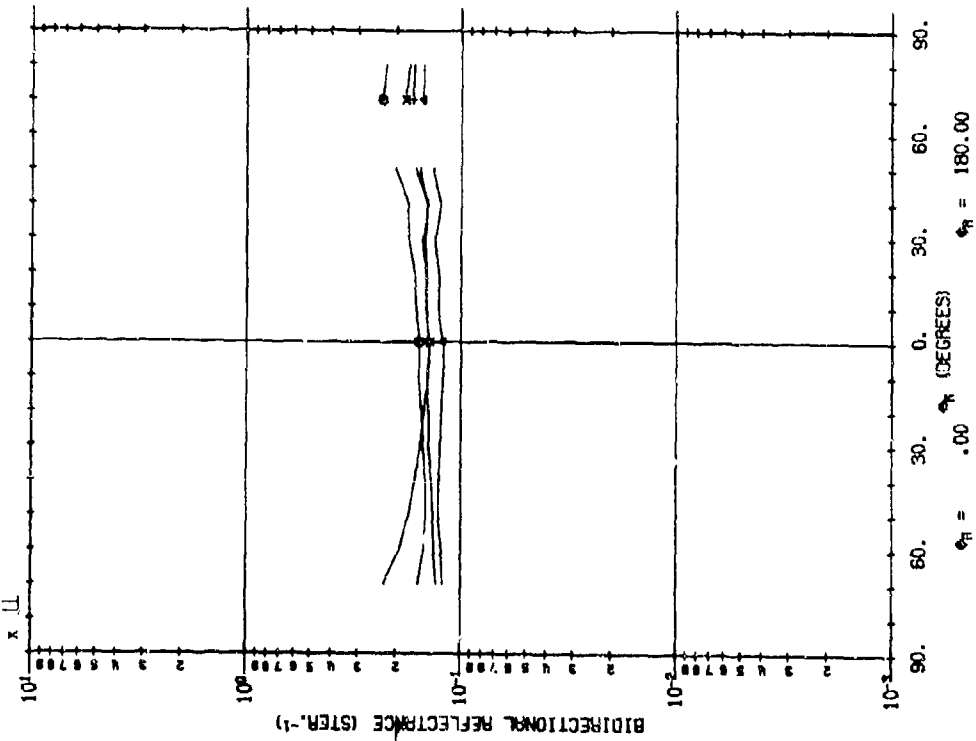


REFLECTANCE STANDARDS MATERIAL

R01230 001

TWO COATS 3M WHITE PAINT ON ZINC  
CHROMATE PRIMER ON ANODIZED ALUMINUM

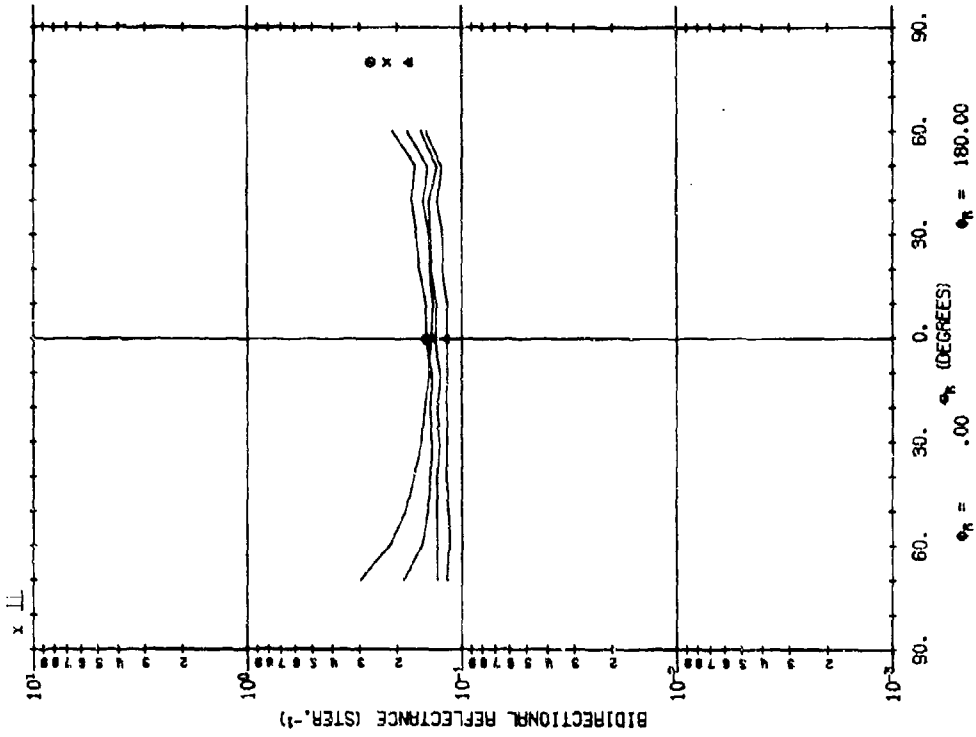
$\theta_1 = 60.0$   
 $\theta_2 = 180.0$   
 $\lambda = 1.06$



R01290 001

TWO COATS 3M WHITE PAINT ON ZINC  
CHROMATE PRIMER ON ANODIZED ALUMINUM

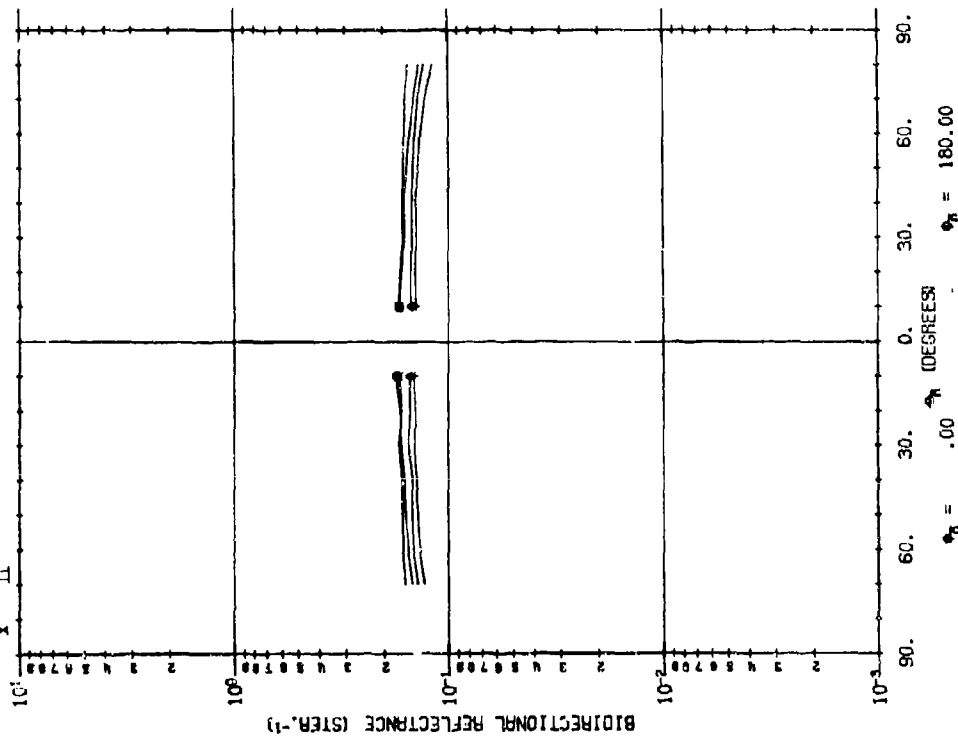
$\theta_1 = 70.0$   
 $\theta_2 = 180.0$   
 $\lambda = 1.06$



A01292 001

3M WHITE VELVET PAINT ON ALUMINUM

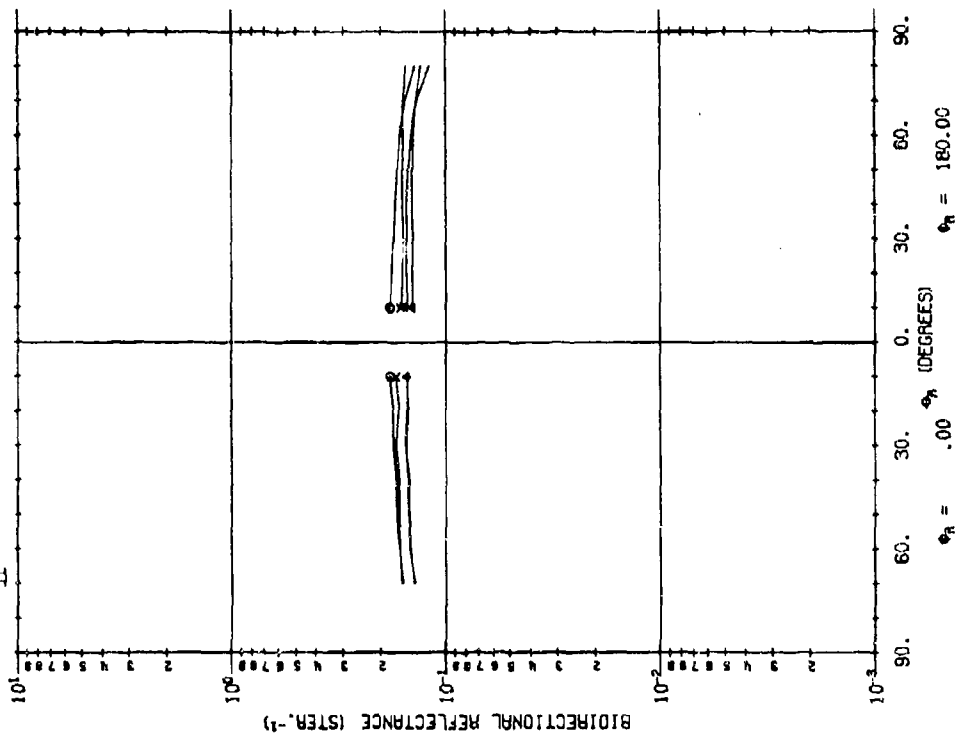
$\epsilon_1 = 0.0$   
 $\phi_1 = 180.0$   
 $\lambda = 1.06$



A01292 002

3M WHITE VELVET PAINT ON ALUMINUM

$\epsilon_1 = 0.0$   
 $\phi_1 = 180.0$   
 $\lambda = 1.06$

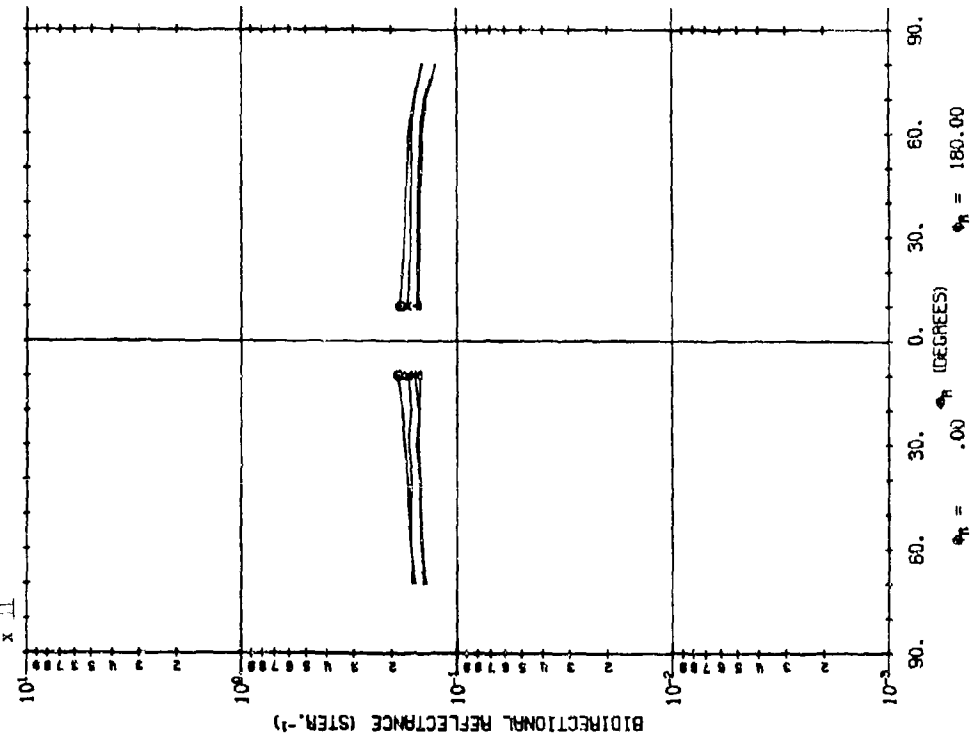


REFLECTANCE STANDARDS MATERIAL

R01292 003

100 COATS 1M WHITE PAINT ON ZINC  
CHROMATE PRIMER ON ANODIZED ALUMINUM

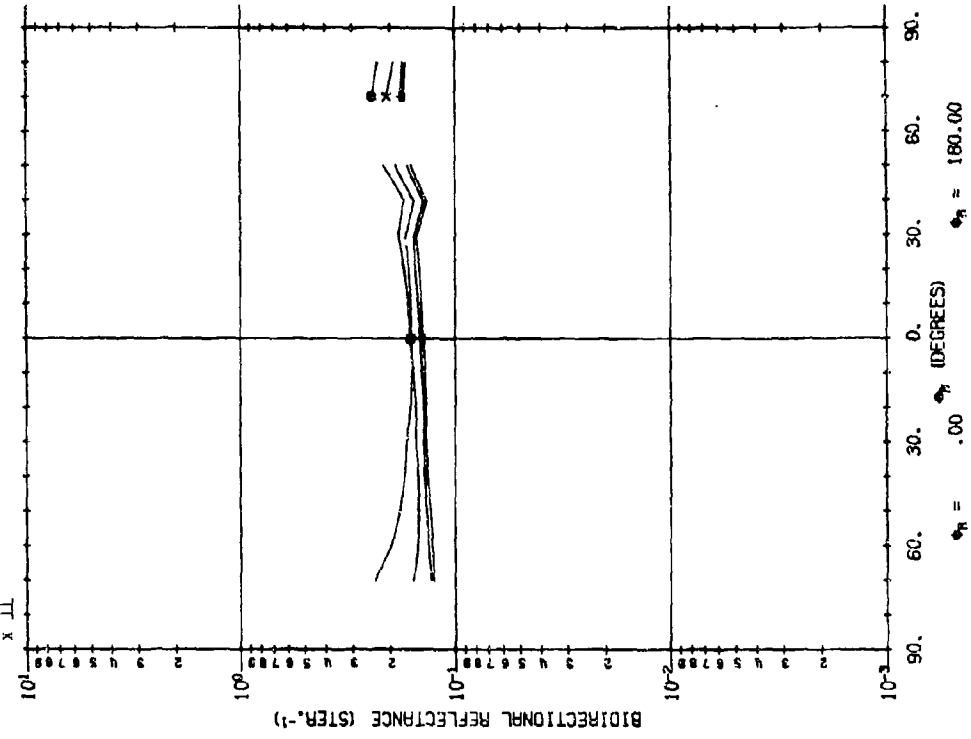
$\phi_i = 0.0$   
 $\phi_r = 180.0$   
 $\lambda = 1.06$



R01292 003

100 COATS 1M WHITE PAINT ON ZINC  
CHROMATE PRIMER ON ANODIZED ALUMINUM

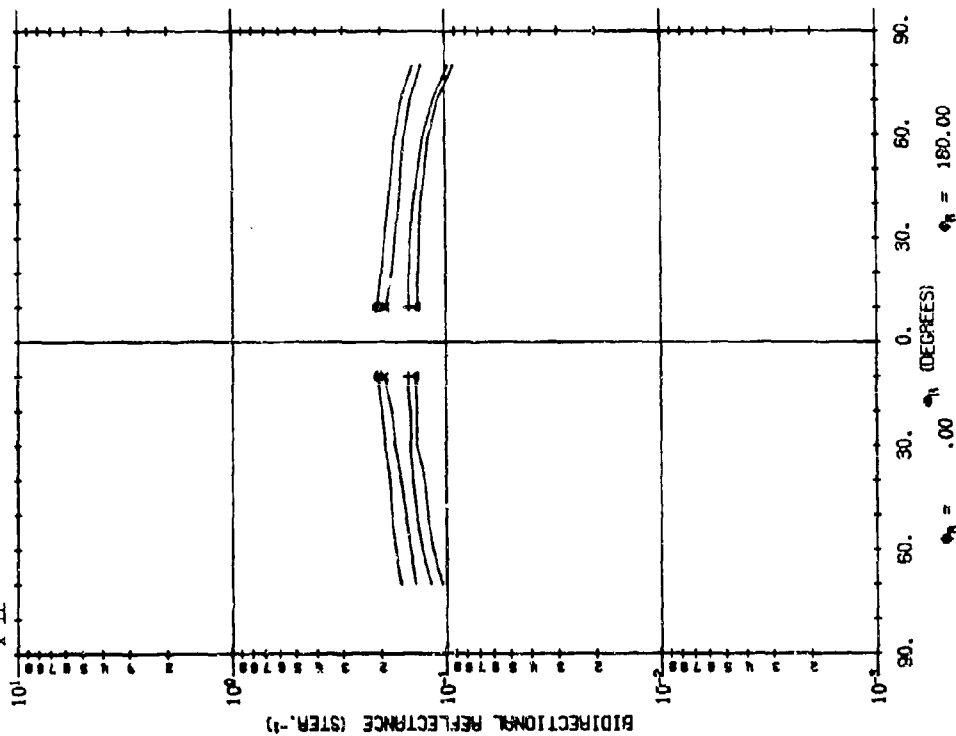
$\phi_i = 60.0$   
 $\phi_r = 180.0$   
 $\lambda = 1.06$



A01293 001

FIBERFRAX TYPE 970 JR ON 1/4" PLYWOOD

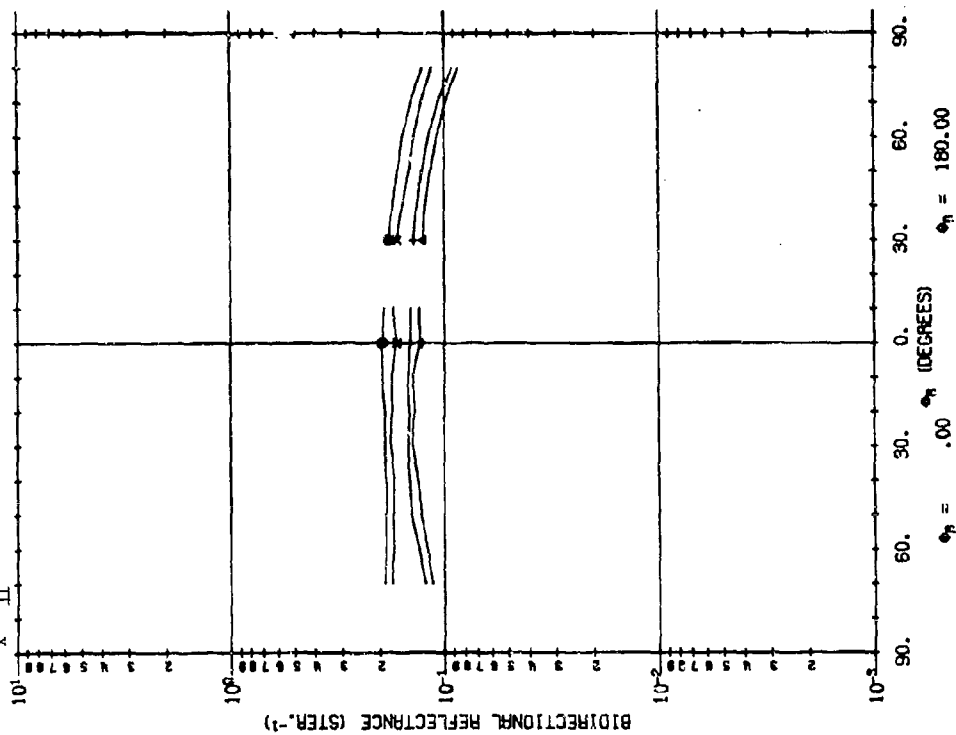
0 ||  $\theta_1 = 0.0$   
 + ||  $\theta_2 = 180.0$   
 x ||  $\lambda = 1.06$



A01293 001

FIBERFRAX TYPE 970 JS ON 1/4" PLYWOOD

0 ||  $\theta_1 = 20.0$   
 + ||  $\theta_2 = 180.0$   
 x ||  $\lambda = 1.06$

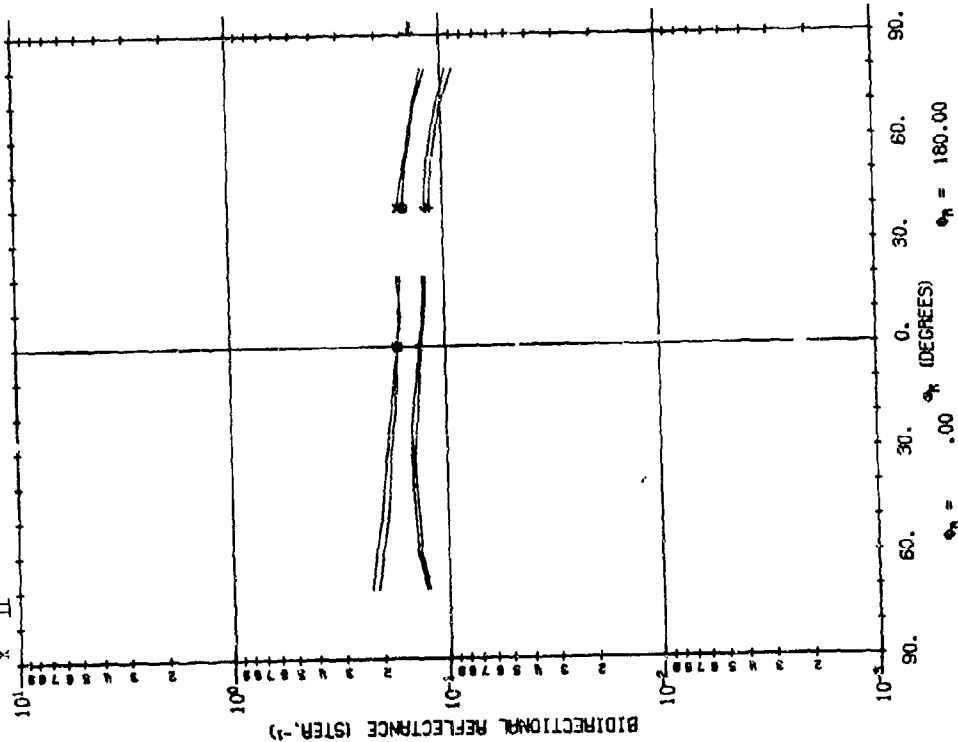


# REFLECTANCE STANDARDS MATERIAL



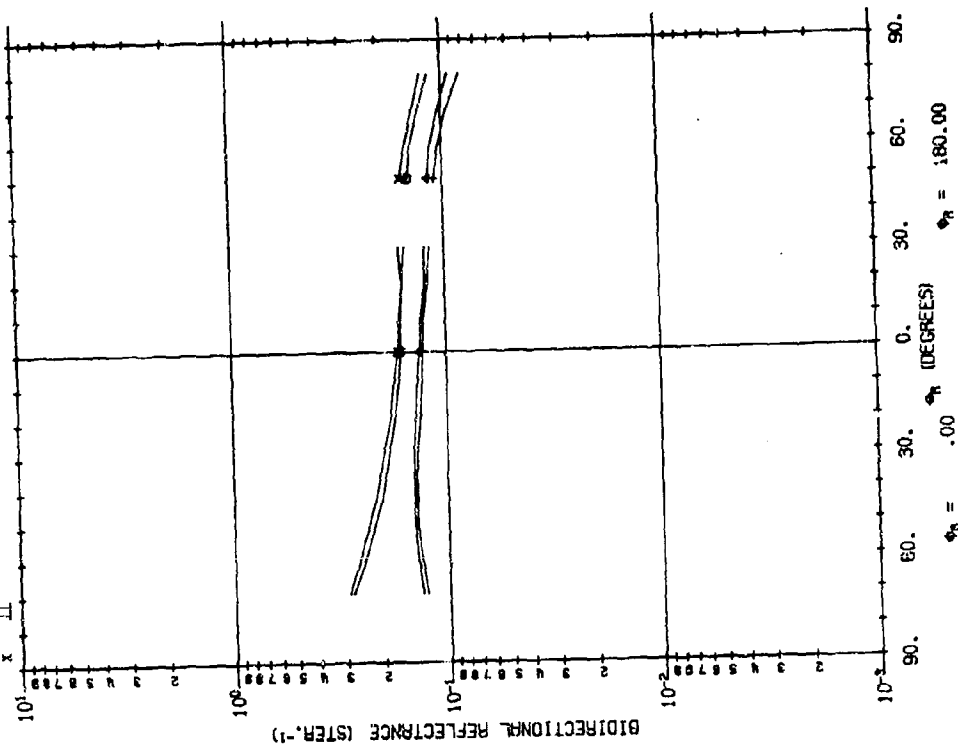
R01293 001  
 $\theta_1 = 30.0$   
 $\phi_1 = 180.0$   
 $\lambda = 1.06$

FIBERFRAX TYPE 970 JH ON 1/4" PLYWOOD



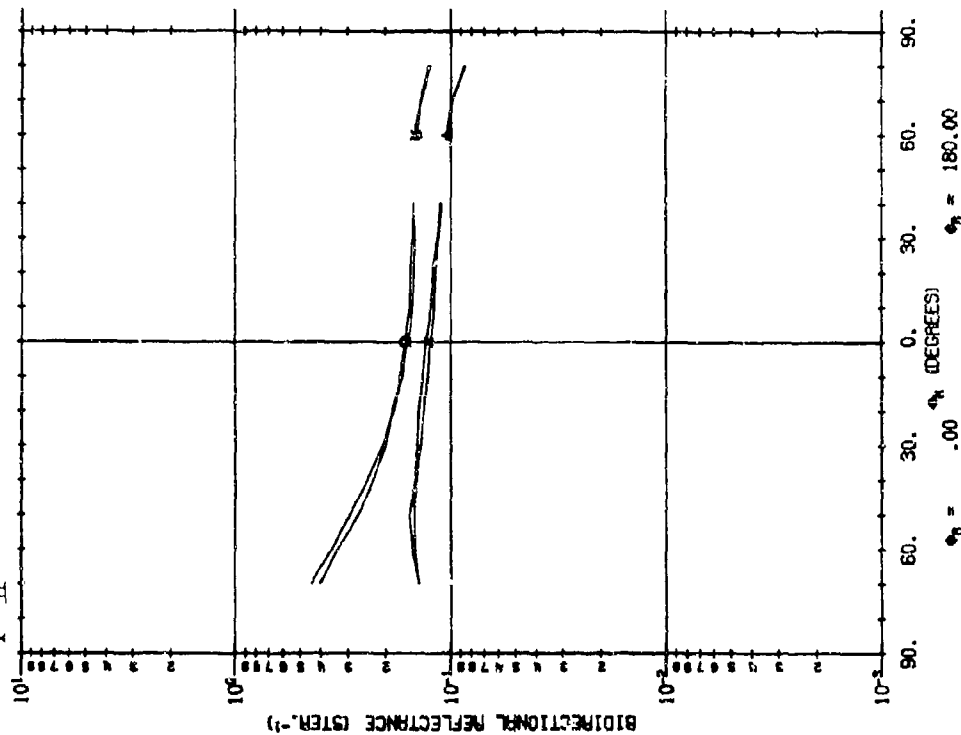
R01293 001  
 $\theta_1 = 40.0$   
 $\phi_1 = 180.0$   
 $\lambda = 1.06$

FIBERFRAX TYPE 970 JH ON 1/4" PLYWOOD



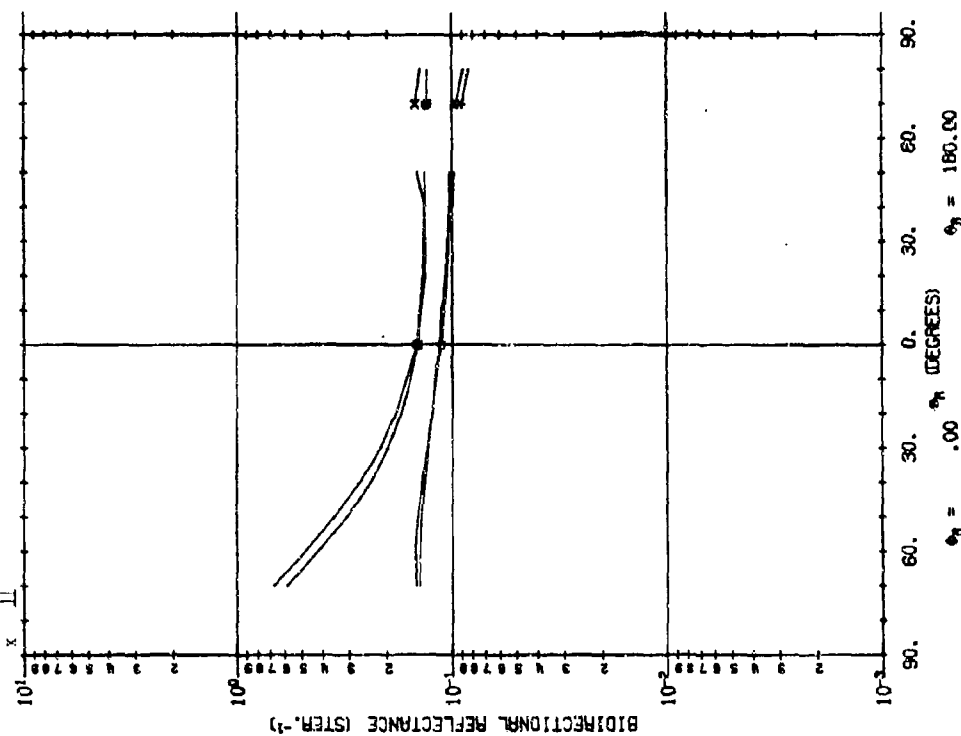
A01293 001  
 0 ||  $\theta_i = 50.0$   
 + ||  $\theta_i = 180.0$   
 Δ ||  $\lambda = 1.06$   
 x ||

FIBERTRAX TYPE 970 JH ON 1/4" PLYWOOD



A01293 001  
 0 ||  $\theta_i = 60.0$   
 + ||  $\theta_i = 180.0$   
 Δ ||  $\lambda = 1.06$   
 x ||

FIBERTRAX TYPE 970 JH ON 1/4" PLYWOOD

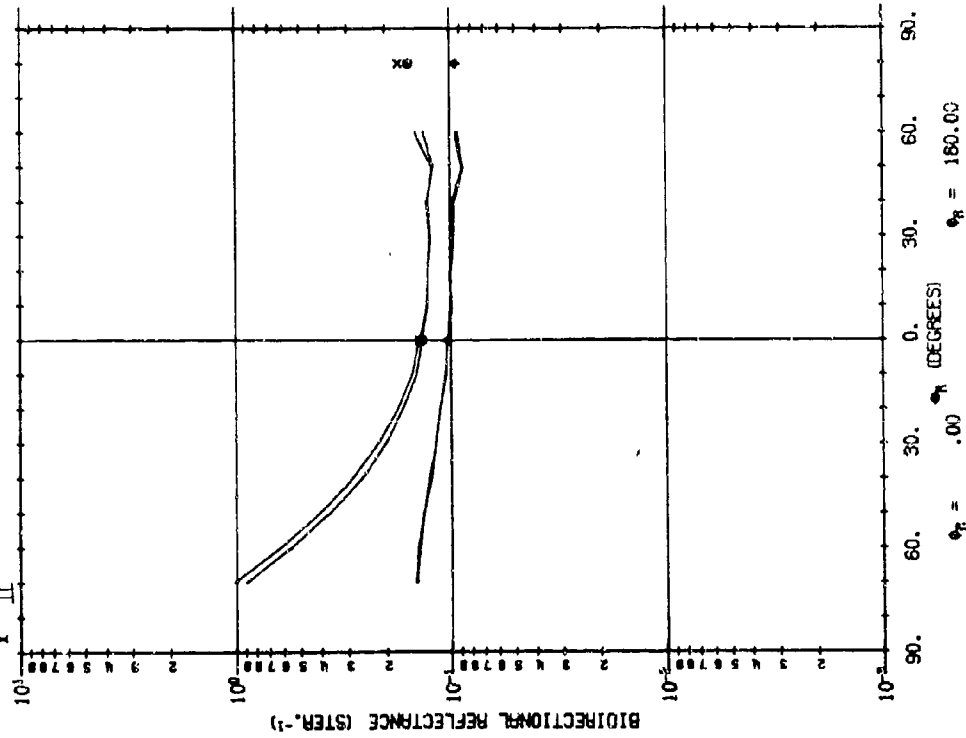


REFLECTANCE STANDARDS MATERIAL

B01293 001

FIBERGLASS TYPE 970 JH ON 1/4" PLYWOOD

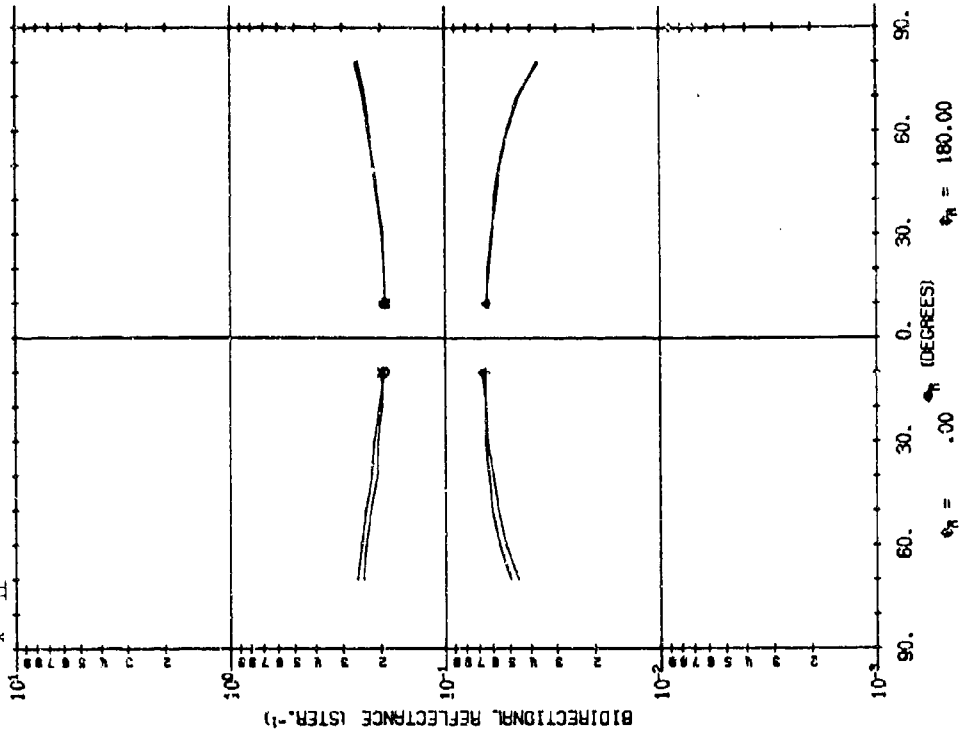
0 ||  $\phi_1 = 70.0$   
 + ||  $\phi_1 = 180.0$   
 Δ ||  $\lambda = 1.06$



B01296 001

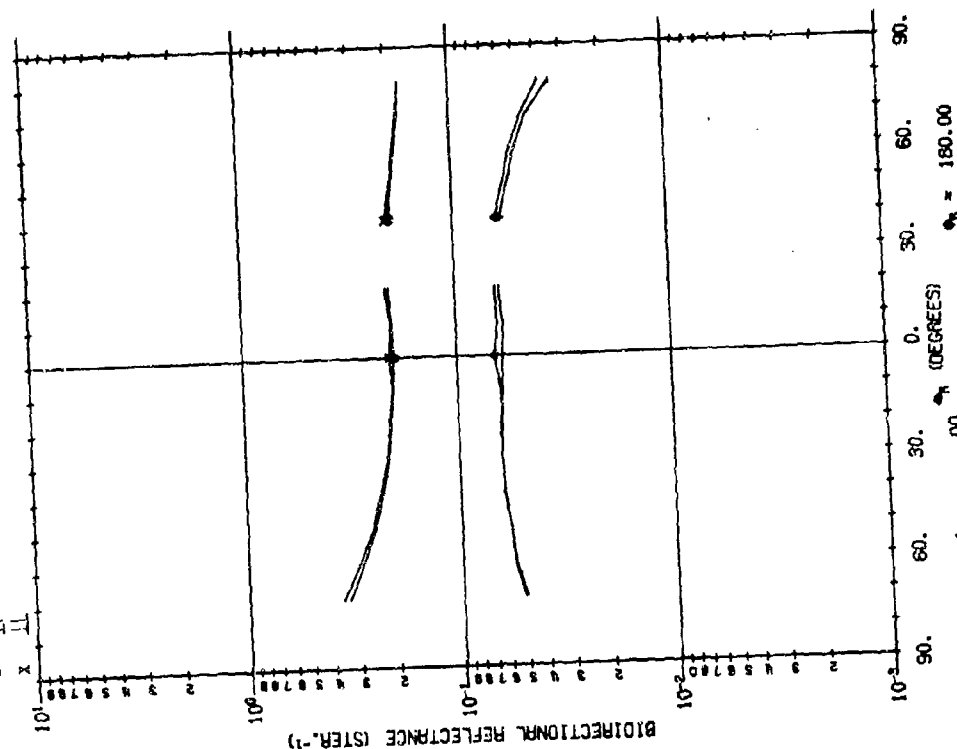
SANDBLASTED COPPER PLATED STAINLESS STEEL

0 ||  $\phi_1 = 0.0$   
 + ||  $\phi_1 = 180.0$   
 Δ ||  $\lambda = 1.06$



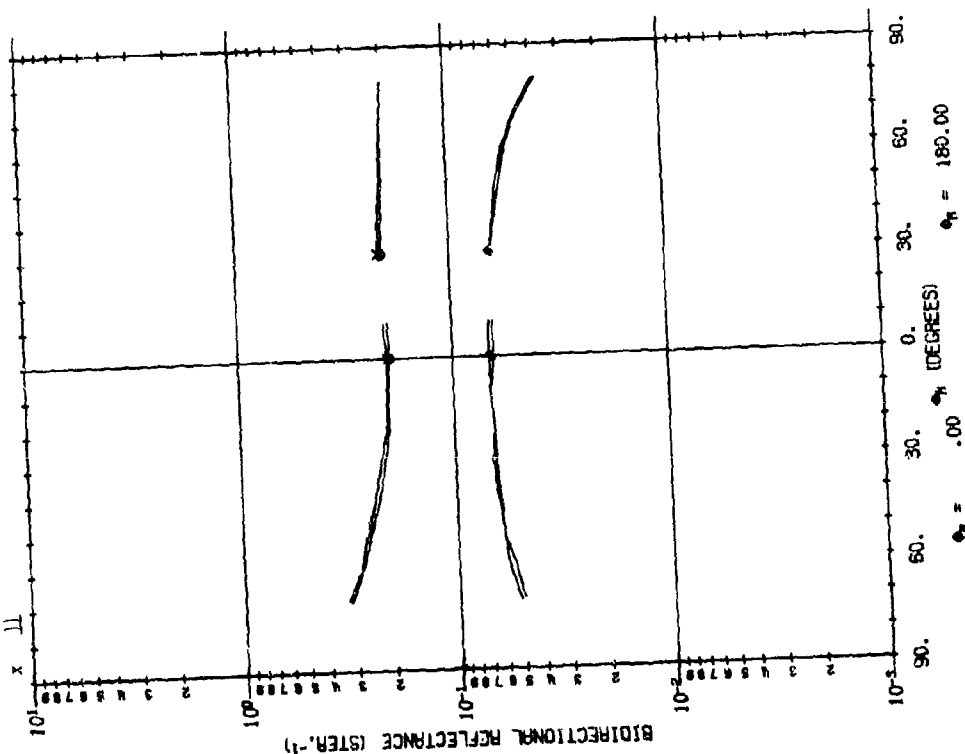
A01296 001  
SANDBLASTED COPPER PLATED STAINLESS STEEL

$\theta_i = 30.0$   
 $\phi_i = 180.0$   
 $\lambda = 1.06$



A01296 001  
SANDBLASTED COPPER PLATED STAINLESS STEEL

$\theta_i = 20.0$   
 $\phi_i = 180.0$   
 $\lambda = 1.06$

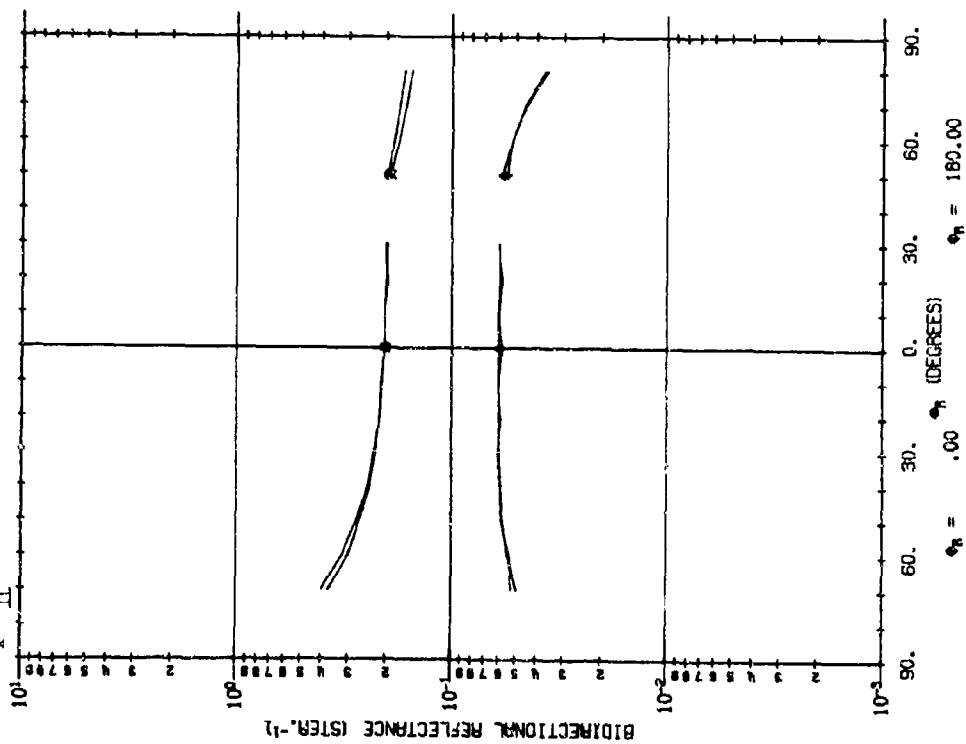


REFLECTANCE STANDARDS MATERIAL

A01296 001

SANDBLASTED COPPER PLATED STAINLESS STEEL

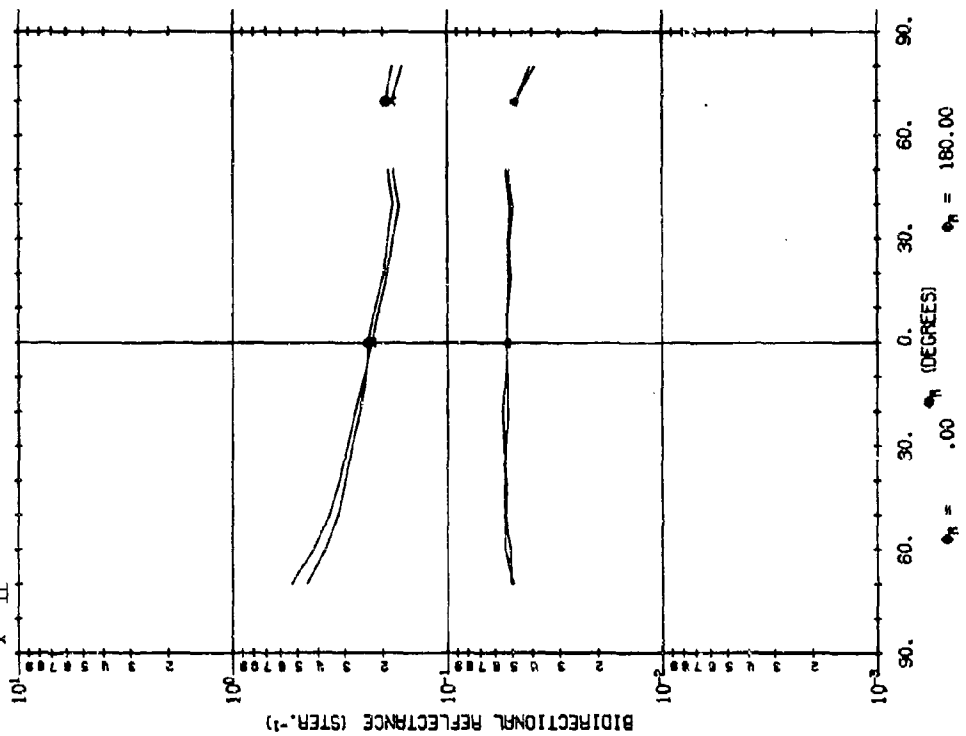
0 ||  $\theta_1 = 40.0$   
 + ||  $\phi_1 = 180.0$   
 x ||  $\lambda = 1.06$



A01296 001

SANDBLASTED COPPER PLATED STAINLESS STEEL

0 ||  $\theta_1 = 60.0$   
 + ||  $\phi_1 = 180.0$   
 x ||  $\lambda = 1.06$



R01296 001

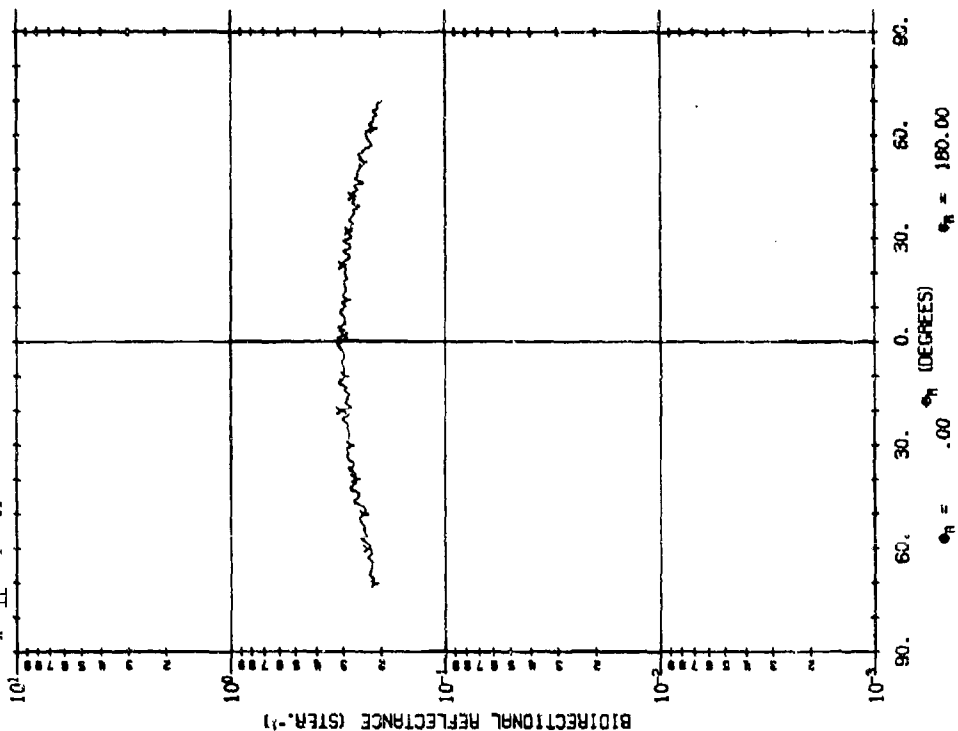
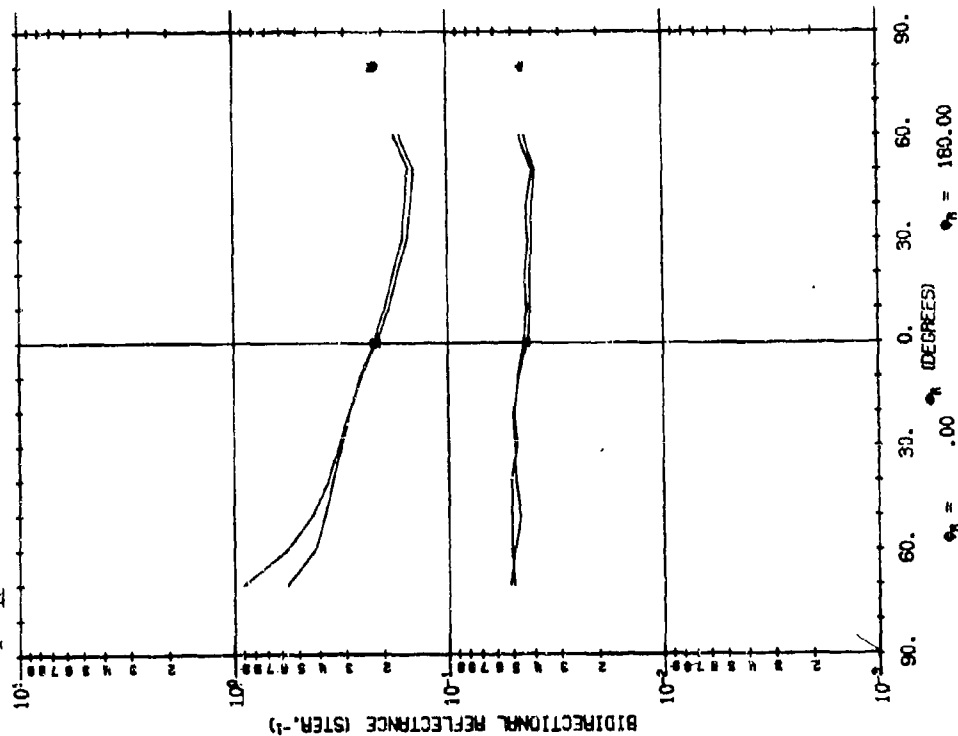
SANDBLASTED COPPER PLATED STAINLESS STEEL

$\theta_1 = 70.0$   
 $\phi_1 = 180.0$   
 $\lambda = 1.06$

R01296 101

SANDBLASTED COPPER PLATED STAINLESS STEEL

$\theta_1 = 2.0$   
 $\phi_1 = 0$   
 $\lambda = 10.6$   
 $\gamma = 0$

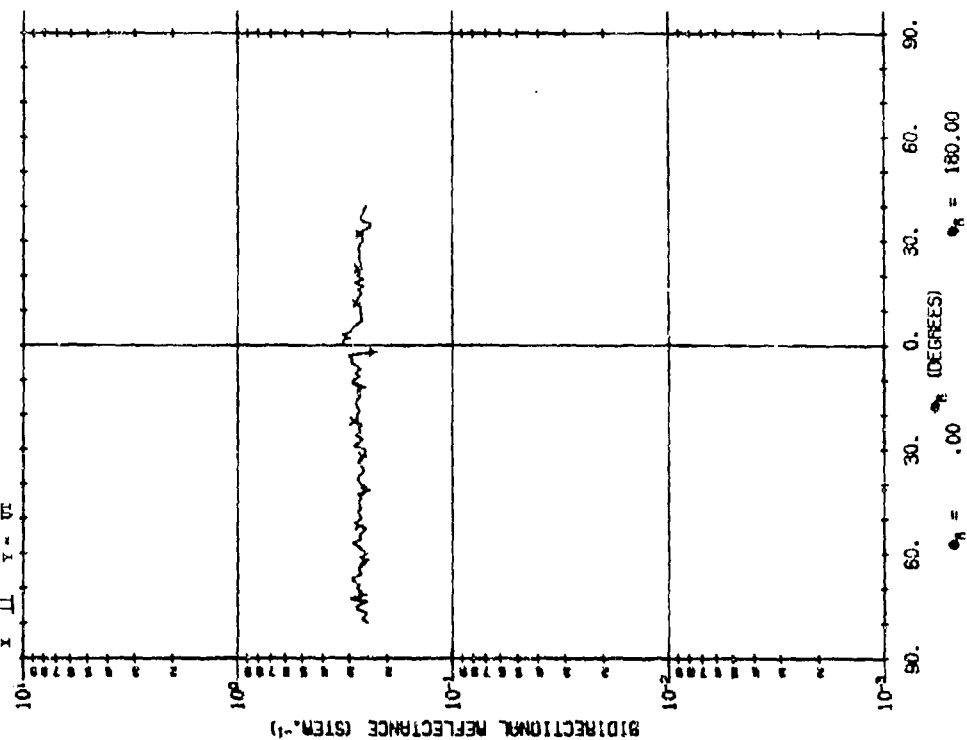


# REFLECTANCE STANDARDS MATERIAL

R01296 101

SANDBLASTED COPPER PLATED STAINLESS STEEL

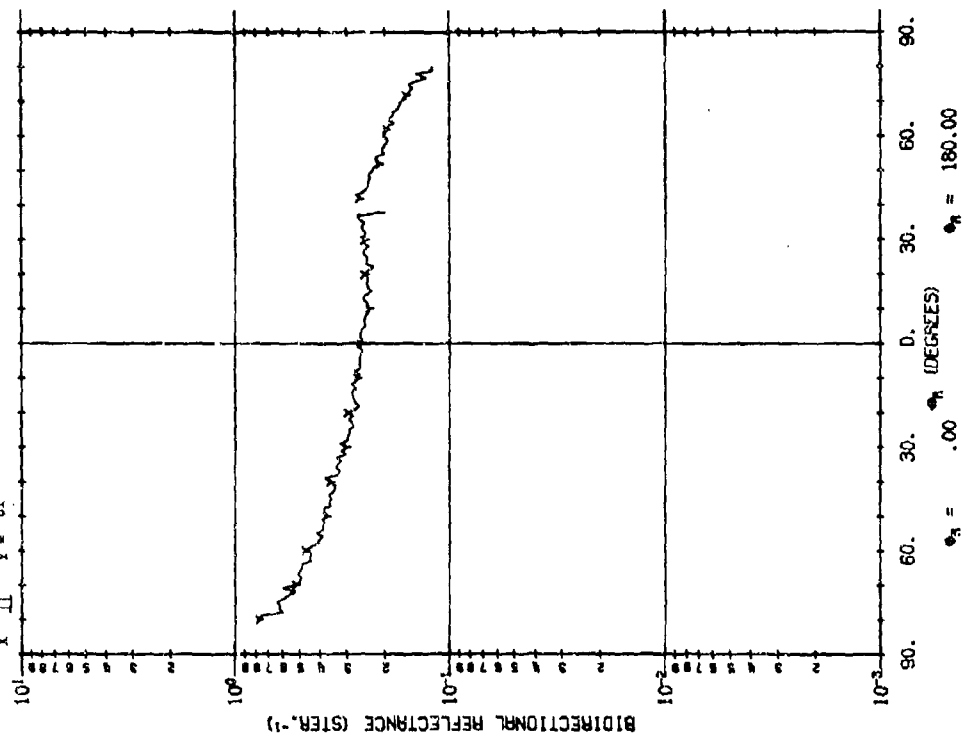
0 ||  $\epsilon_1 = 0.0$   
 + ||  $\phi_1 = 180.0$   
 Δ ||  $\lambda = 10.6$   
 X || Y = VT



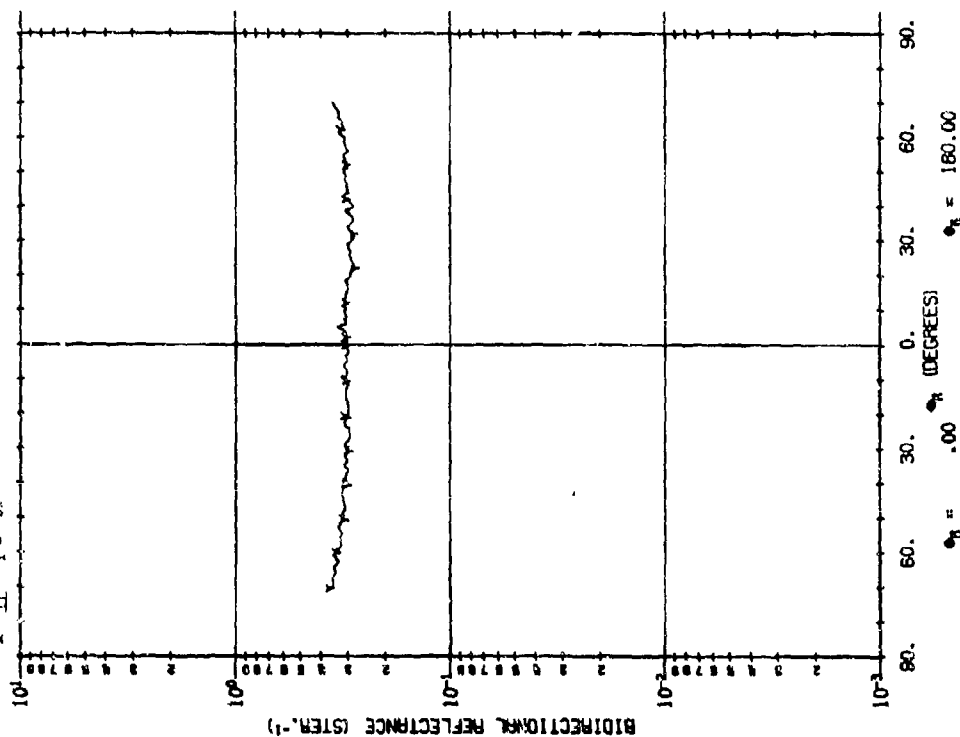
R01296 101

SANDBLASTED COPPER PLATED STAINLESS STEEL

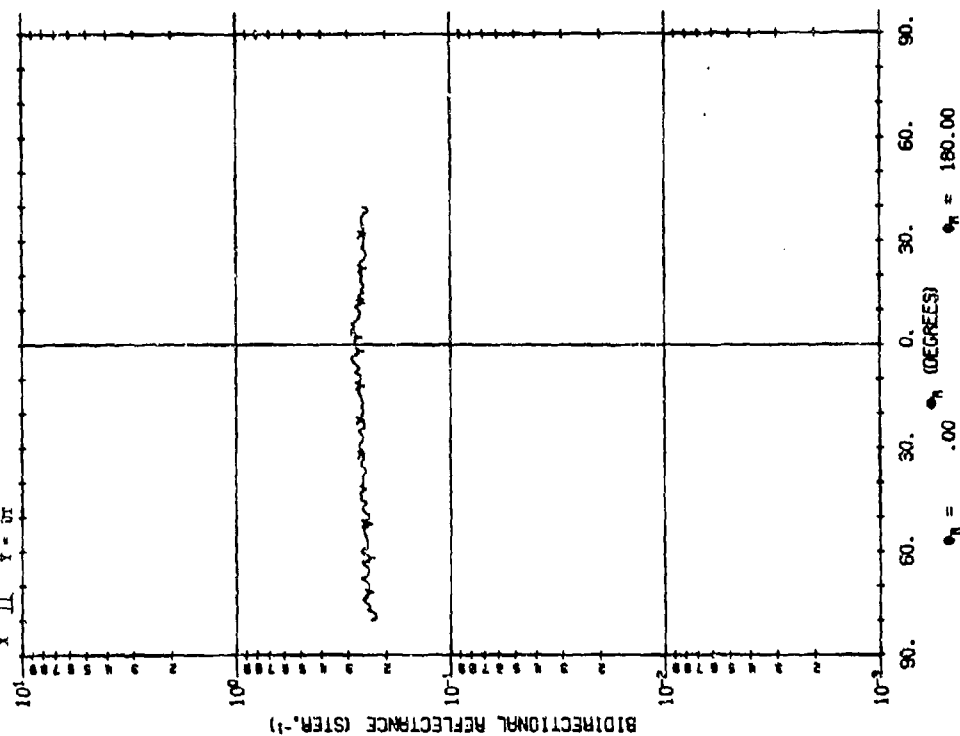
0 ||  $\epsilon_1 = 40.0$   
 + ||  $\phi_1 = 180.0$   
 Δ ||  $\lambda = 10.6$   
 X || Y = VT



R01297 101  
 WHITE SALT STANDARD  
 0 ||  $\theta_i = 2.0$   
 + ||  $\theta_r = 0$   
 Δ ||  $\theta_t = 180.0$   
 X ||  $\lambda = 10.6$   
 Y = DT



R01297 101  
 WHITE SALT STANDARD  
 0 ||  $\theta_i = 0.0$   
 + ||  $\theta_r = 0$   
 Δ ||  $\theta_t = 180.0$   
 X ||  $\lambda = 10.6$   
 Y = DT



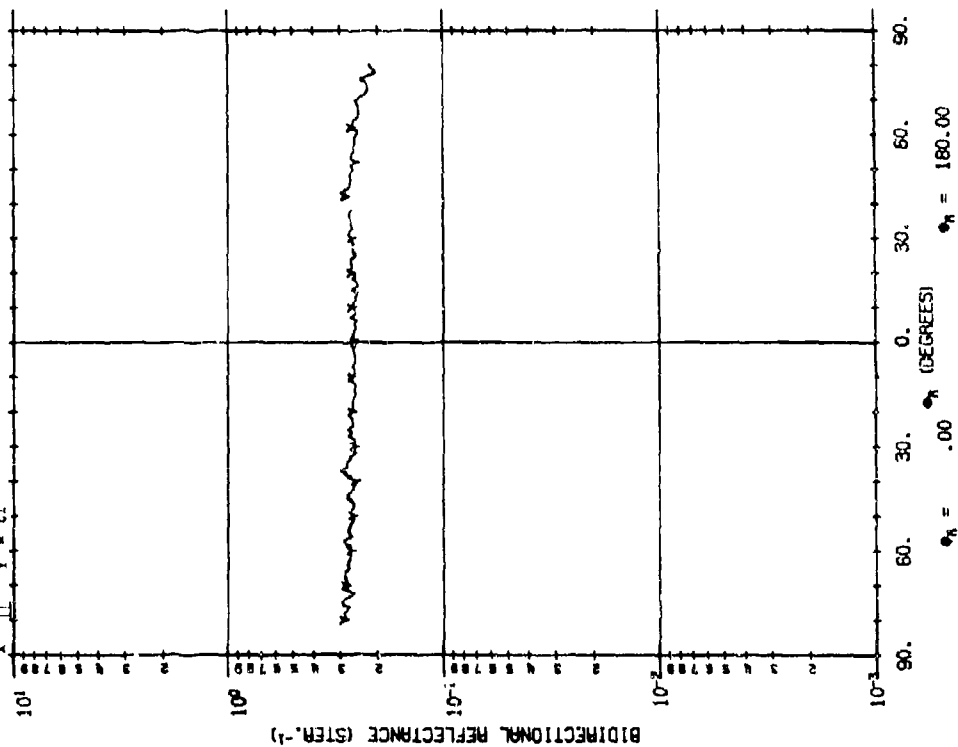
# REFLECTANCE STANDARDS MATERIAL



R01297 101

WHITE SALT STANDARD

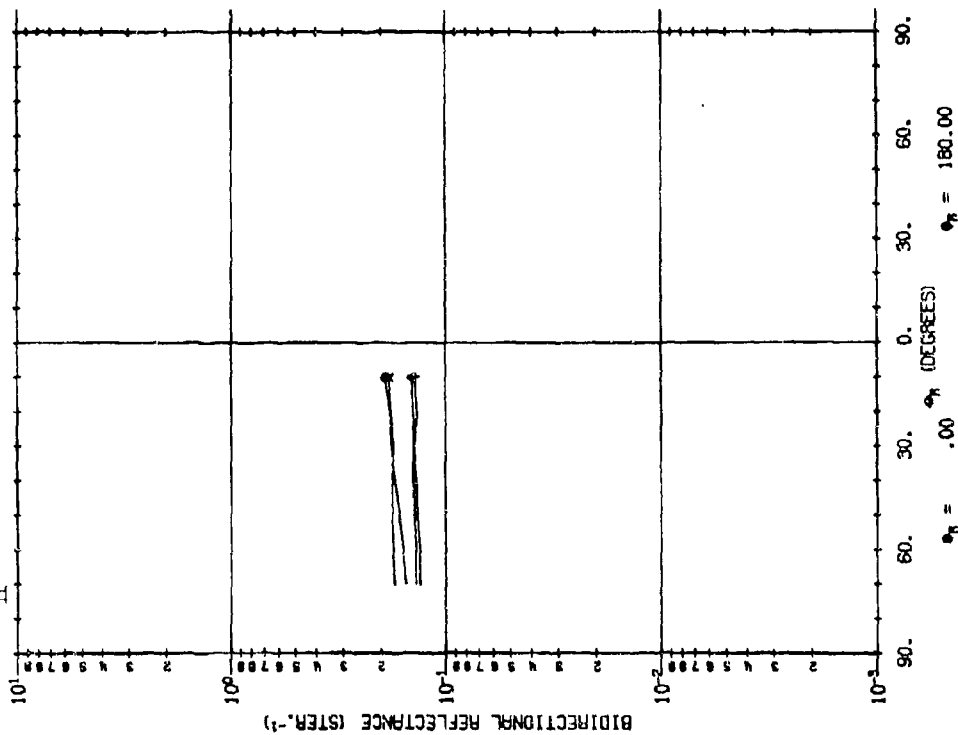
0 ||  $\theta_1 = 40.0$   
 + ||  $\theta_2 = 180.0$   
 Δ ||  $\lambda = 10.6$   
 X || Y = VT



R01317 001

PRESSED MAGNESIUM OXIDE

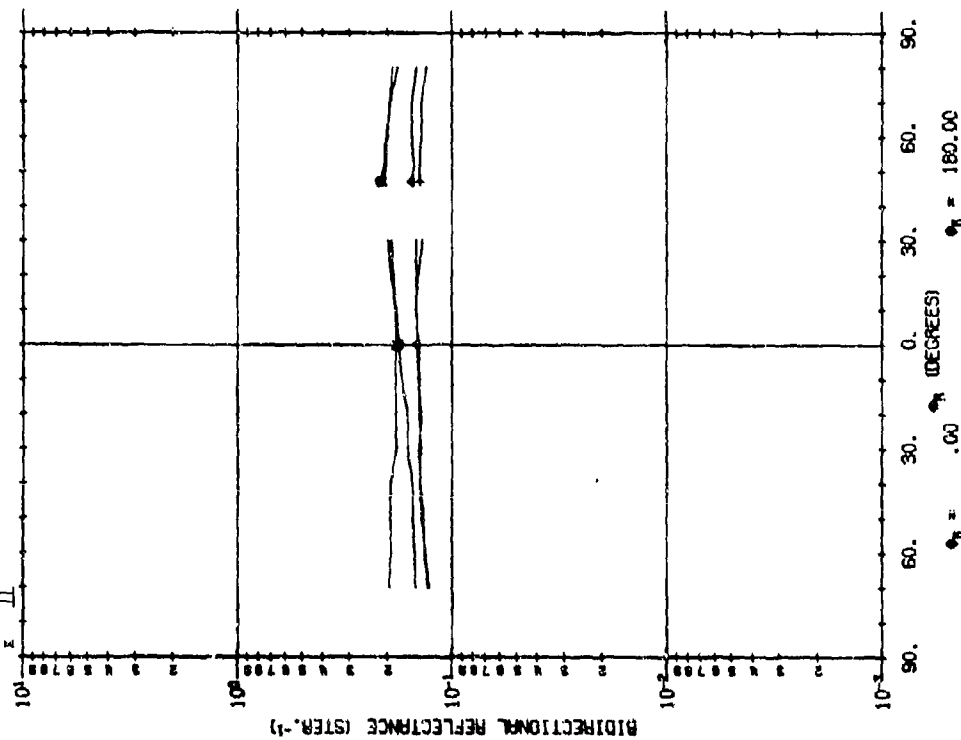
0 ||  $\theta_1 = 0.0$   
 + ||  $\theta_2 = 180.0$   
 Δ ||  $\lambda = 0.63$   
 X ||



A01317 001

PRESSED MAGNESIUM OXIDE

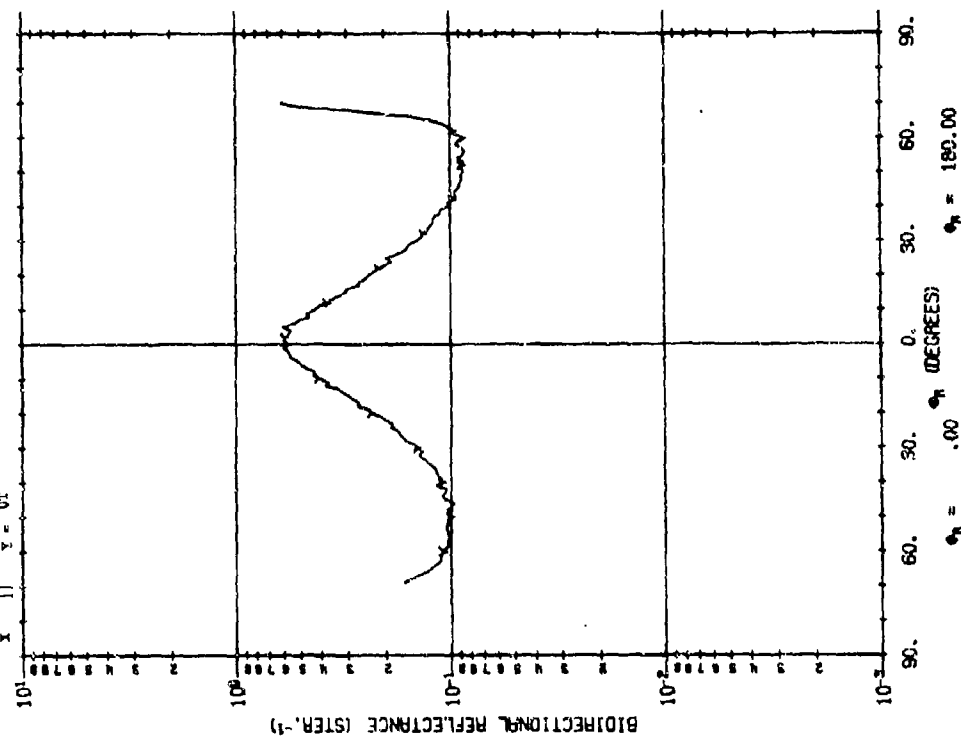
0 ||  $\theta_i = 40.0$   
 + ||  $\theta_r = 180.0$   
 Δ ||  $\lambda = 0.63$



A01331 101

GOLD PLATED SILICON CARBIDE PAPER

0 ||  $2\theta = 2.0$   
 + ||  $\theta_i = \theta_r$   
 Δ ||  $\lambda = 10.6$   
 X ||  $\gamma = 0^\circ$

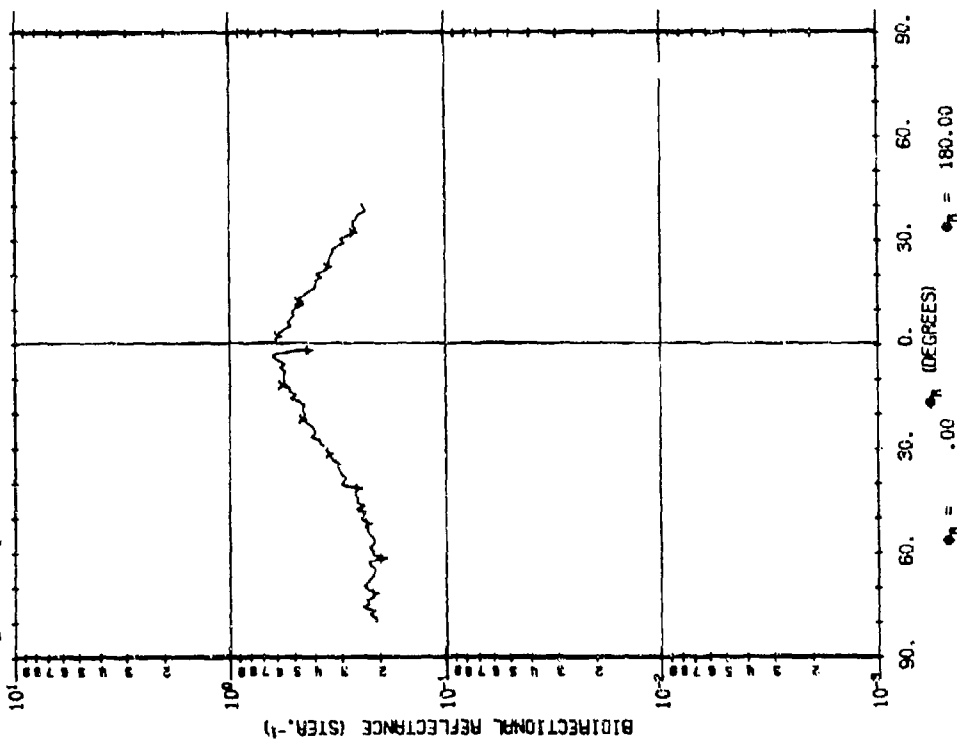


# REFLECTANCE STANDARDS MATERIAL

R01331 101

GOLD PLATED SILICON CARBIDE PAPER

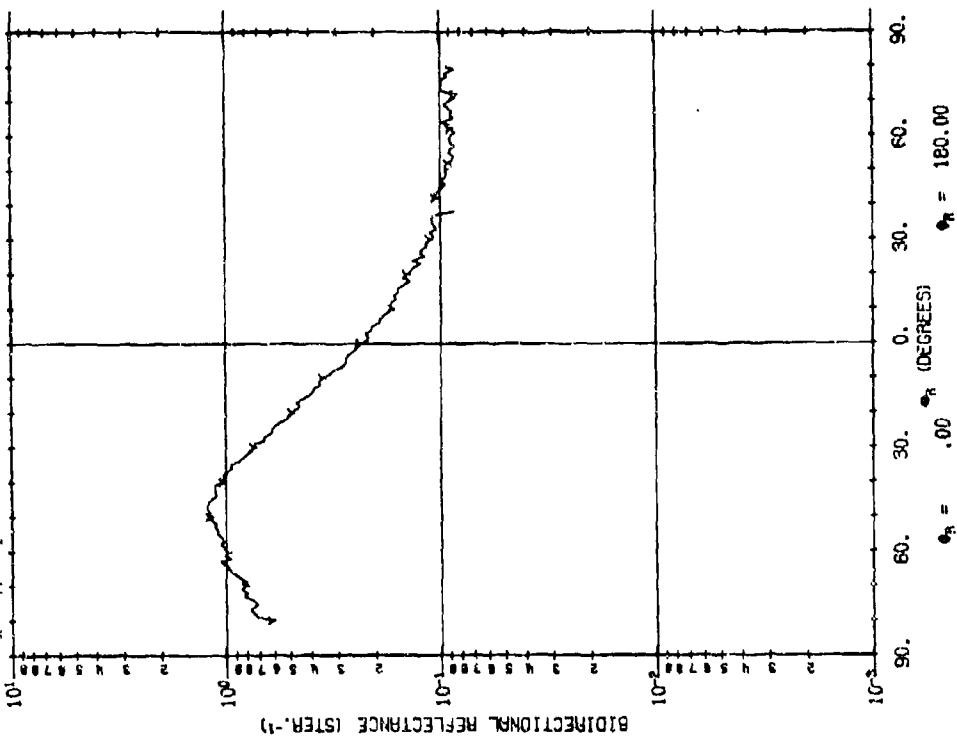
0 ||  $\theta_1 = 0.0$   
 + ||  $\phi_1 = 180.0$   
 x ||  $\lambda = 10.6$   
 || Y = UT



R01331 101

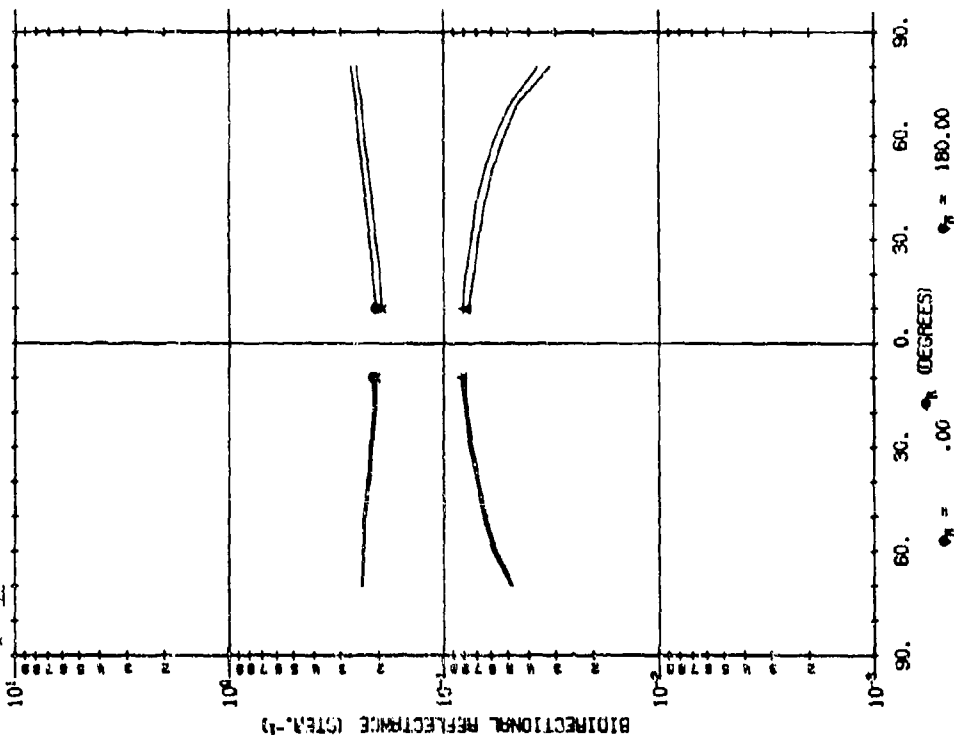
GOLD PLATED SILICON CARBIDE PAPER

0 ||  $\theta_1 = 40.0$   
 + ||  $\phi_1 = 180.0$   
 x ||  $\lambda = 10.6$   
 || Y = UT



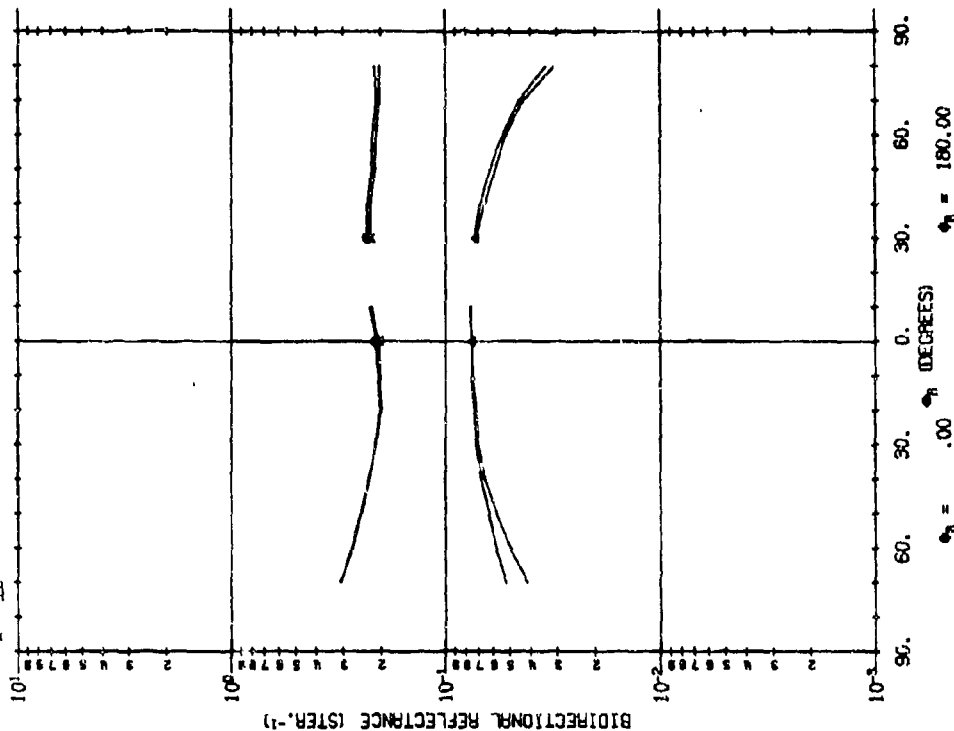
R01332 001  
 $\theta_1 = 0.0$   
 $\phi_1 = 180.0$   
 $\lambda = 1.06$

COPPER PLATED STAINLESS STEEL



R01332 001  
 $\theta_1 = 20.0$   
 $\phi_1 = 180.0$   
 $\lambda = 1.06$

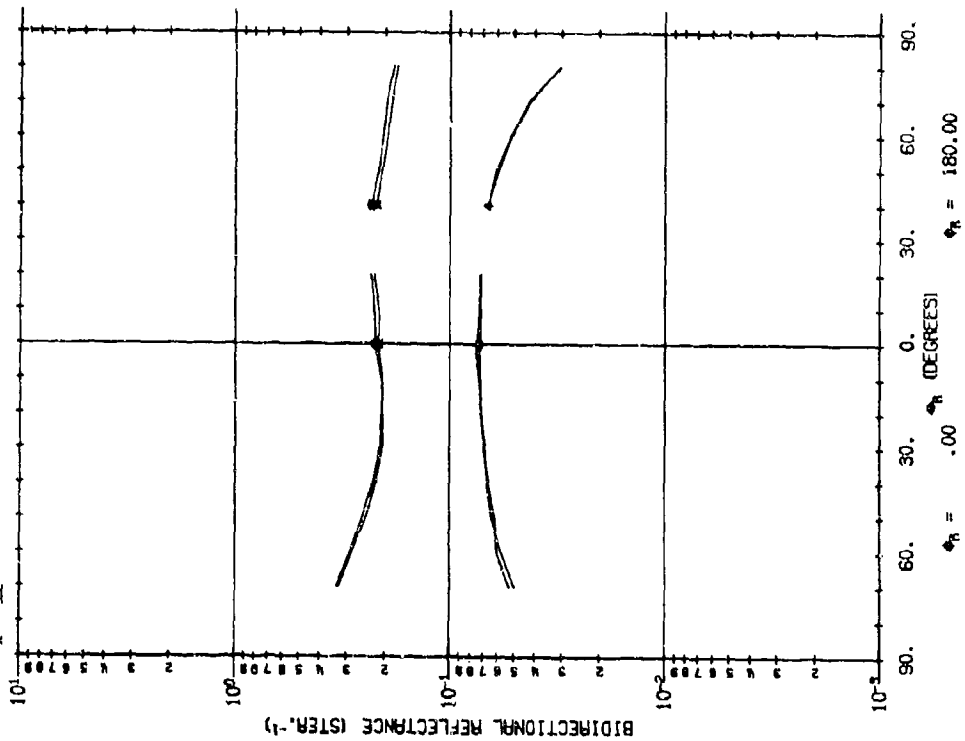
COPPER PLATED STAINLESS STEEL



# REFLECTANCE STANDARDS MATERIAL

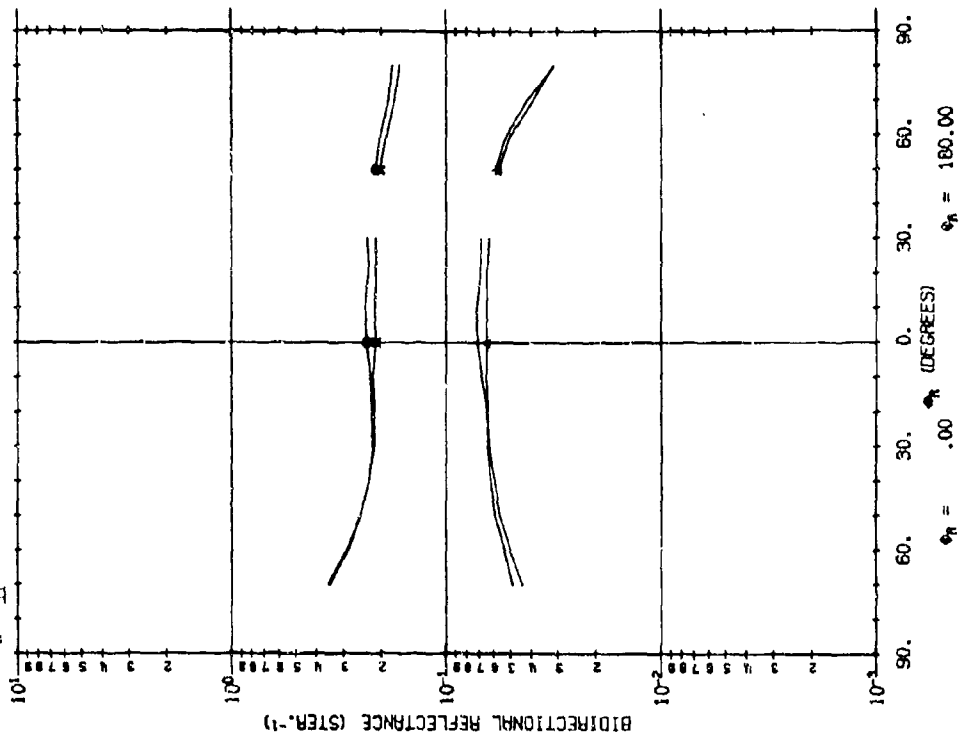
A01332 001  
 $\theta_1 = 30.0$   
 $\phi_1 = 180.0$   
 $\lambda = 1.06$

COPPER PLATED STAINLESS STEEL



A01332 001  
 $\theta_1 = 40.0$   
 $\phi_1 = 180.0$   
 $\lambda = 1.06$

COPPER PLATED STAINLESS STEEL

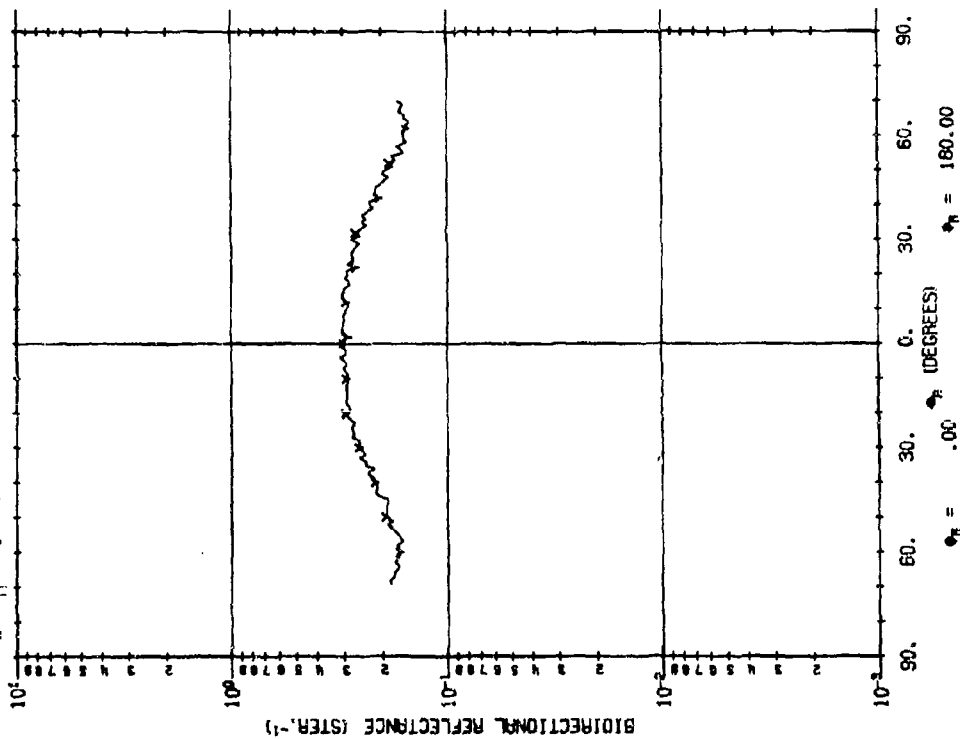




R01435 101

ELECTRO-PLATED COPPER ON SANDBLASTED  
STAINLESS STEEL

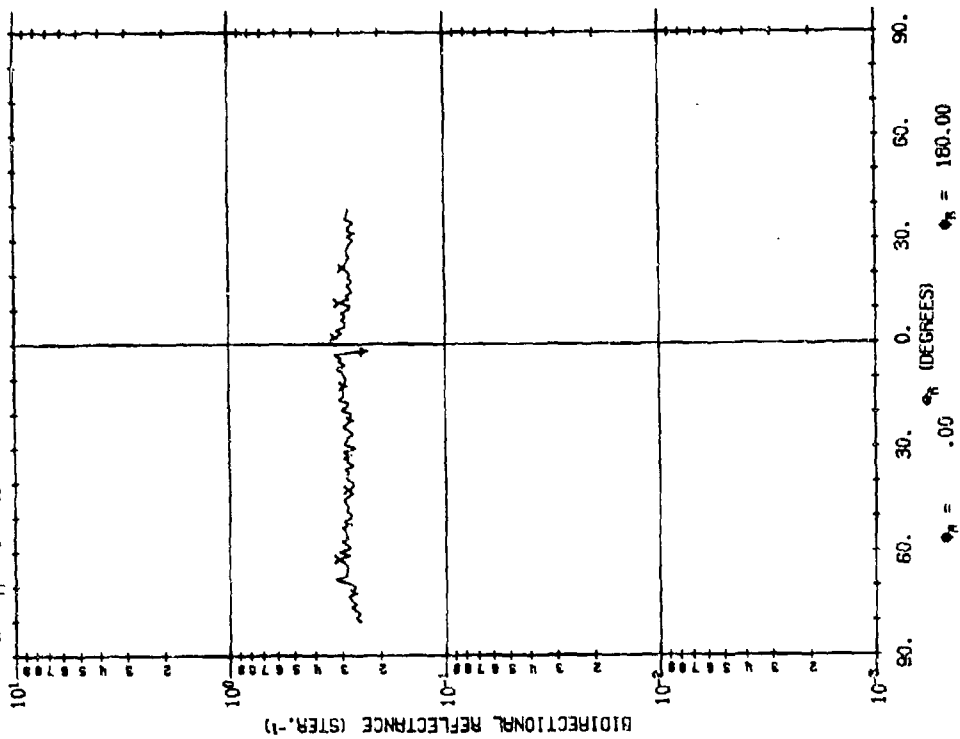
0 ||  $\theta_i = 2.0$   
+ ||  $\theta_r = \theta_i$   
Δ ||  $\lambda = 10.6$   
X ||  $\gamma = 0^\circ$



R01435 101

ELECTRO-PLATED COPPER ON SANDBLASTED  
STAINLESS STEEL

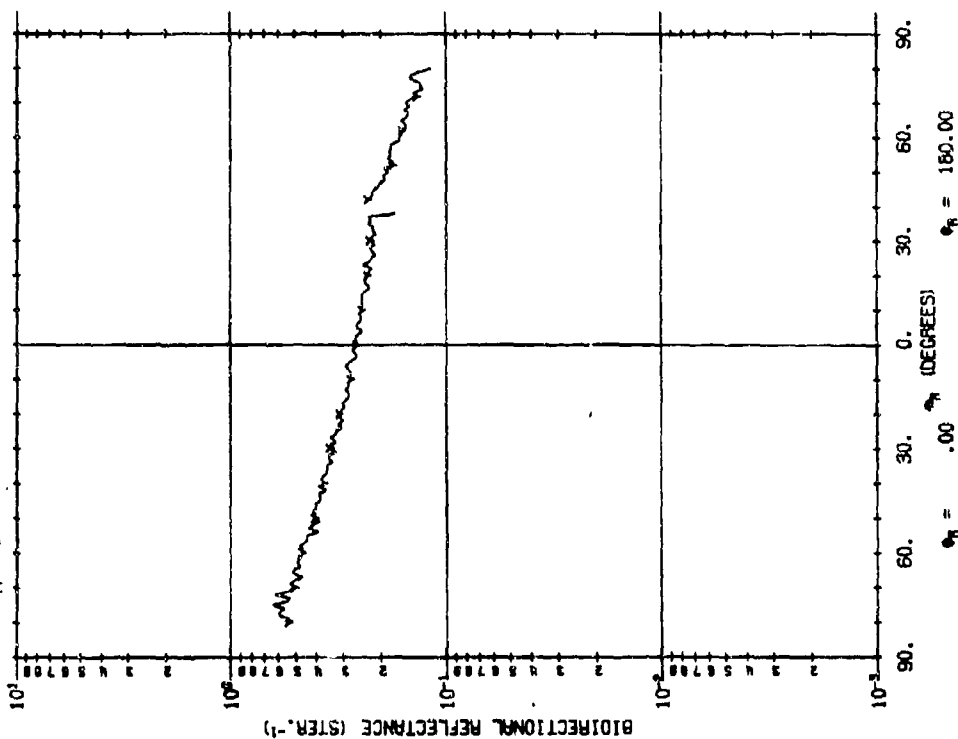
0 ||  $\theta_i = 0.0$   
+ ||  $\theta_r = 180.0$   
Δ ||  $\lambda = 10.6$   
X ||  $\gamma = 7^\circ$



R01435 101

ELECTRO-PLATED COPPER ON SANDBLASTED  
STAINLESS STEEL

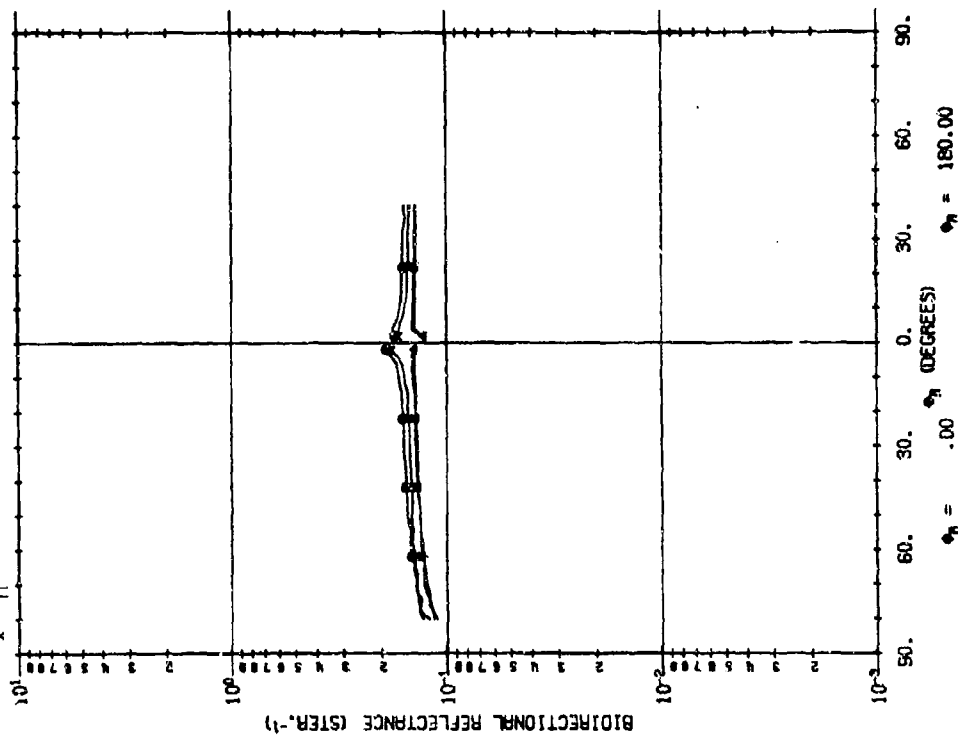
$\theta_1 = 40.0$   
 $\phi_1 = 180.0$   
 $\lambda = 10.6$   
 $\gamma = \text{UT}$



R01460 401

3M WHITE VELVET ON ANODIZED ALUMINUM

$\theta_1 = 0.0$   
 $\phi_1 = 180.0$   
 $\lambda = 0.63$



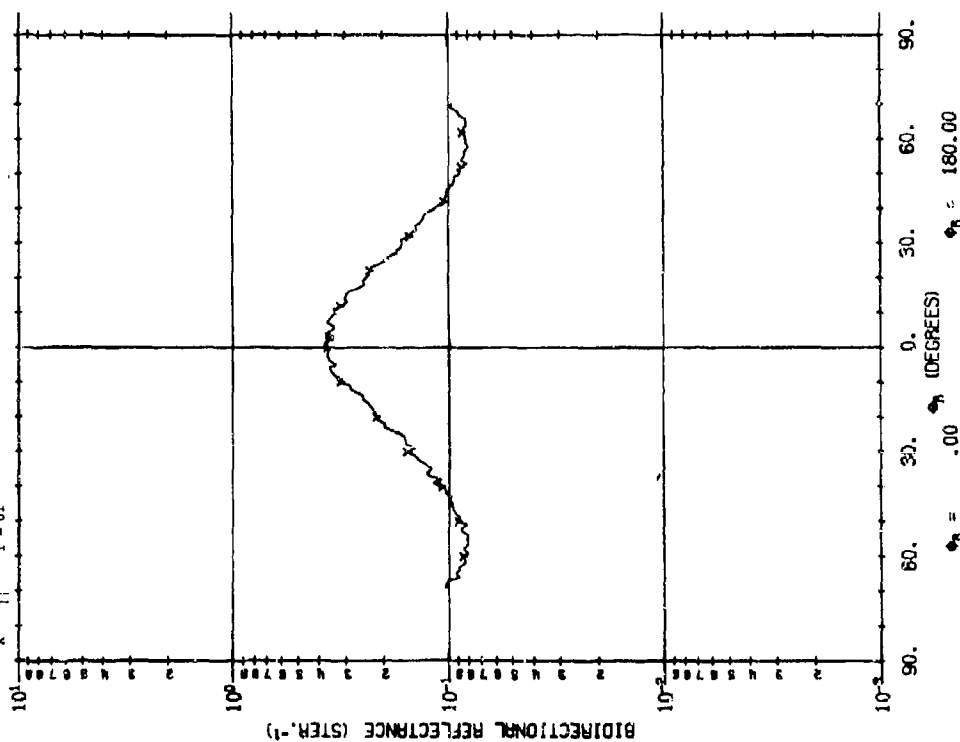
REFLECTANCE STANDARDS MATERIAL



A01598 101

GOLD PLATED, SANDBLASTED STAINLESS STEEL

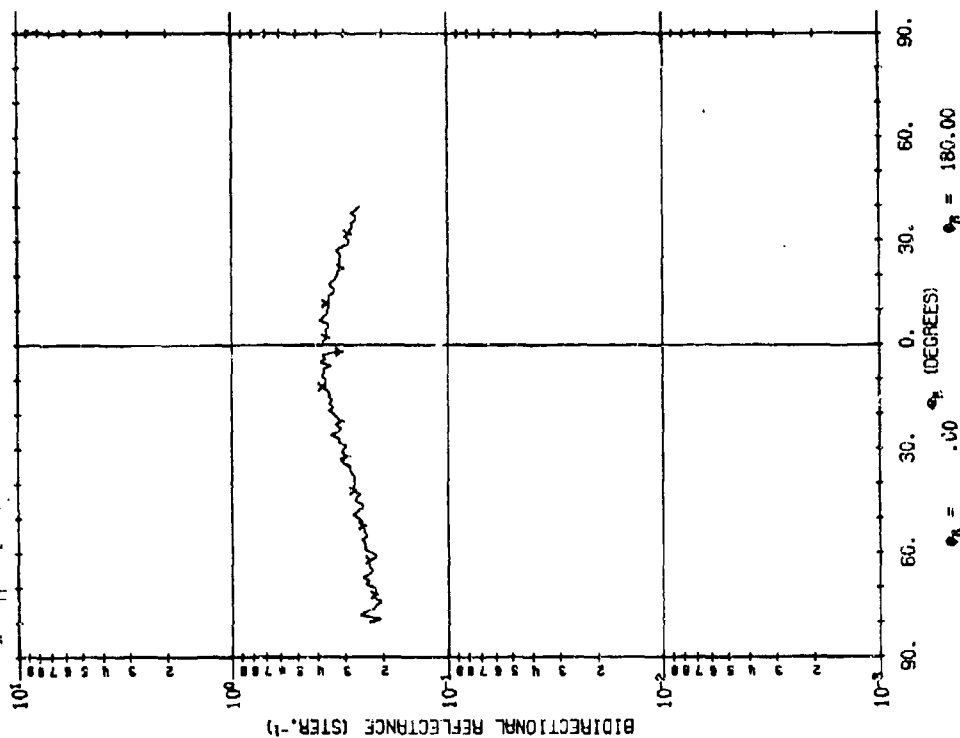
0 || 25 = 2.0  
+ ||  $\phi_1 = \phi_2$   
Δ ||  $\lambda = 10.6$   
X || Y = UT



A01598 101

GOLD PLATED, SANDBLASTED STAINLESS STEEL

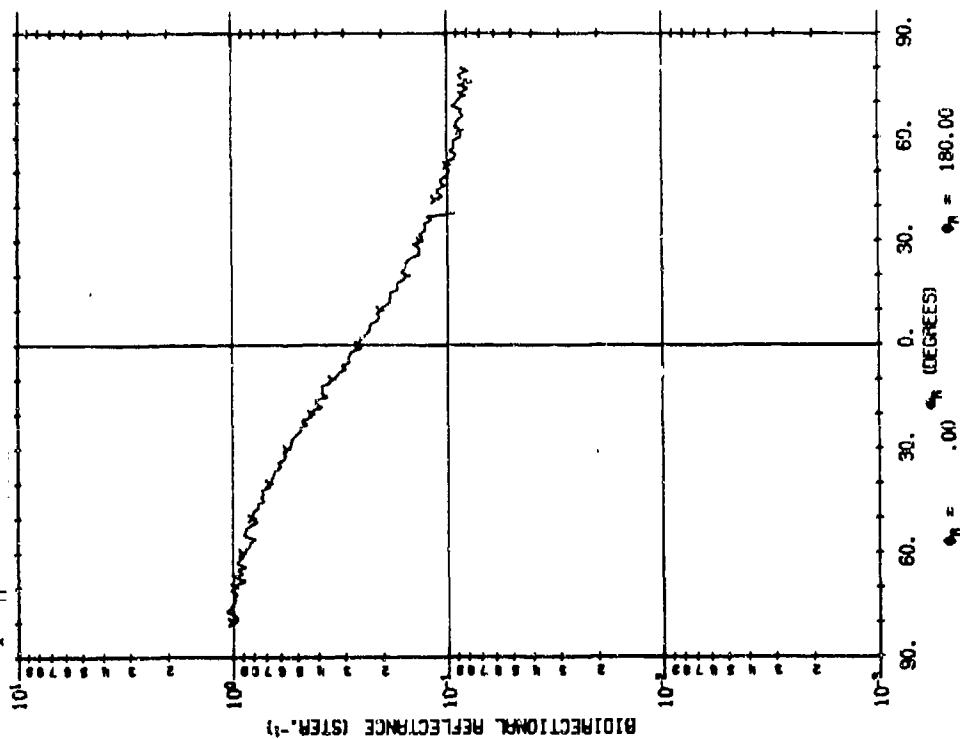
0 ||  $\theta_1 = 0.0$   
+ ||  $\phi_1 = 180.0$   
Δ ||  $\lambda = 10.6$   
X || Y = UT



R01598 101

GOLD PLATED, SANDBLASTED STAINLESS STEEL

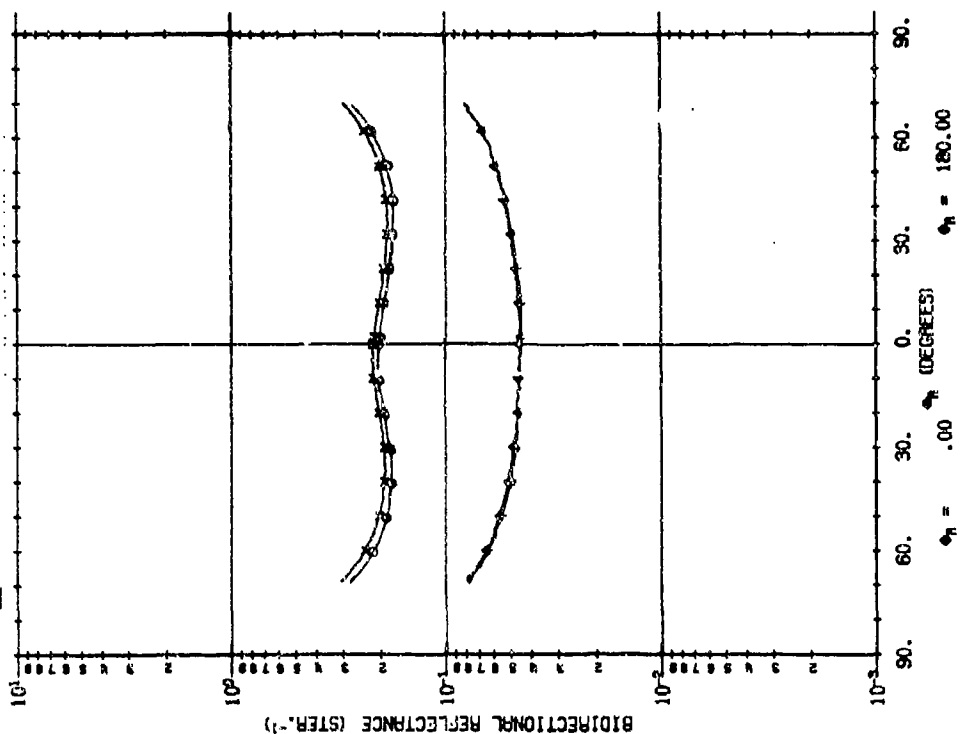
0 ||  $\phi_1 = 40.0$   
 + ||  $\phi_1 = 180.0$   
 Δ ||  $\lambda = 10.6$   
 X || Y = UT



R01683 102

FLAME-SPRAYED ALUMINUM .03" THICK  
 ON .25" ALUMINUM SUBSTRATE

0 ||  $2\theta = 2.0$   
 + ||  $\phi_1 = \phi_r$   
 Δ ||  $\lambda = 0.63$   
 X ||

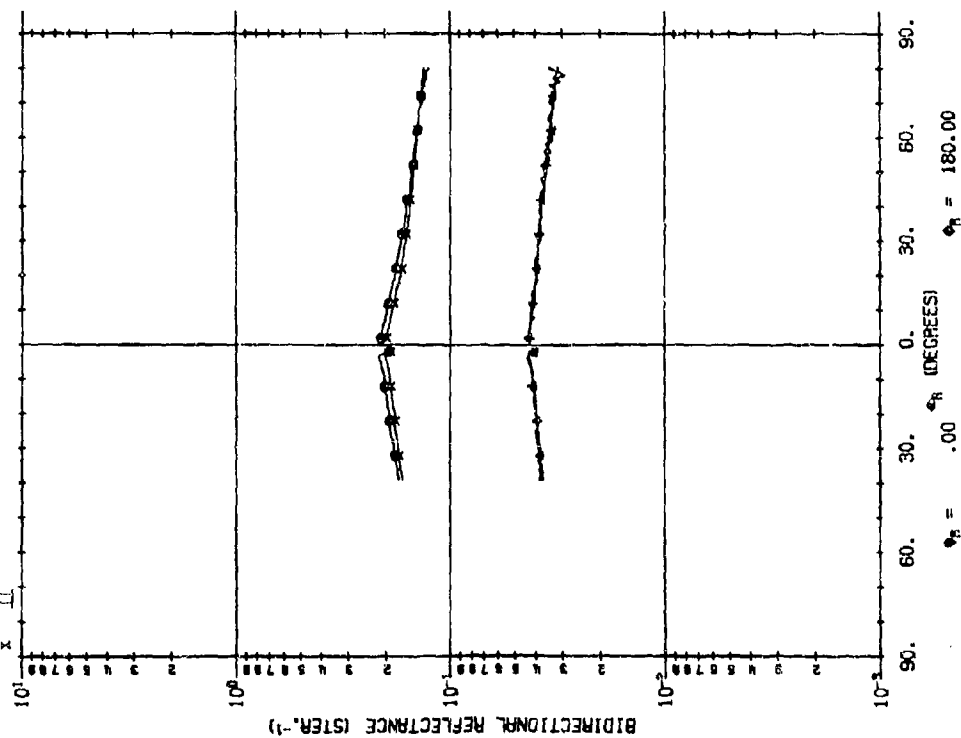


# REFLECTANCE STANDARDS MATERIAL

R01683 102

FLAME-SPRAYED ALUMINUM .03" THICK  
ON .25" ALUMINUM SUBSTRATE

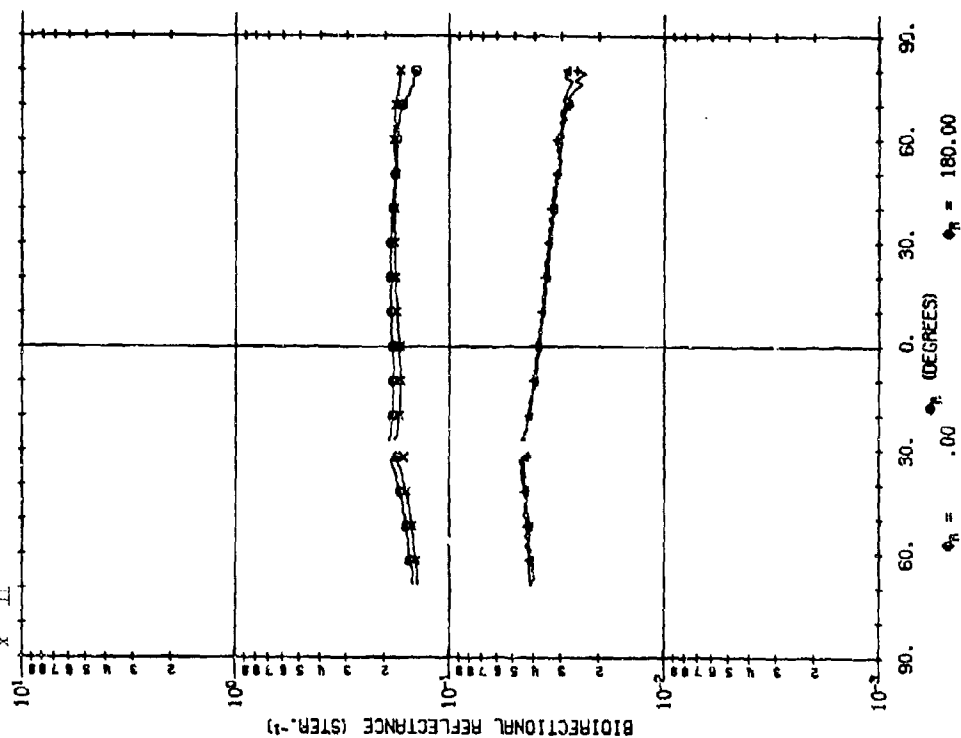
$\theta_1 = 0.0$   
 $\phi_1 = 0.0$   
 $\lambda = 0.63$



R01683 102

FLAME-SPRAYED ALUMINUM .03" THICK  
ON .25" ALUMINUM SUBSTRATE

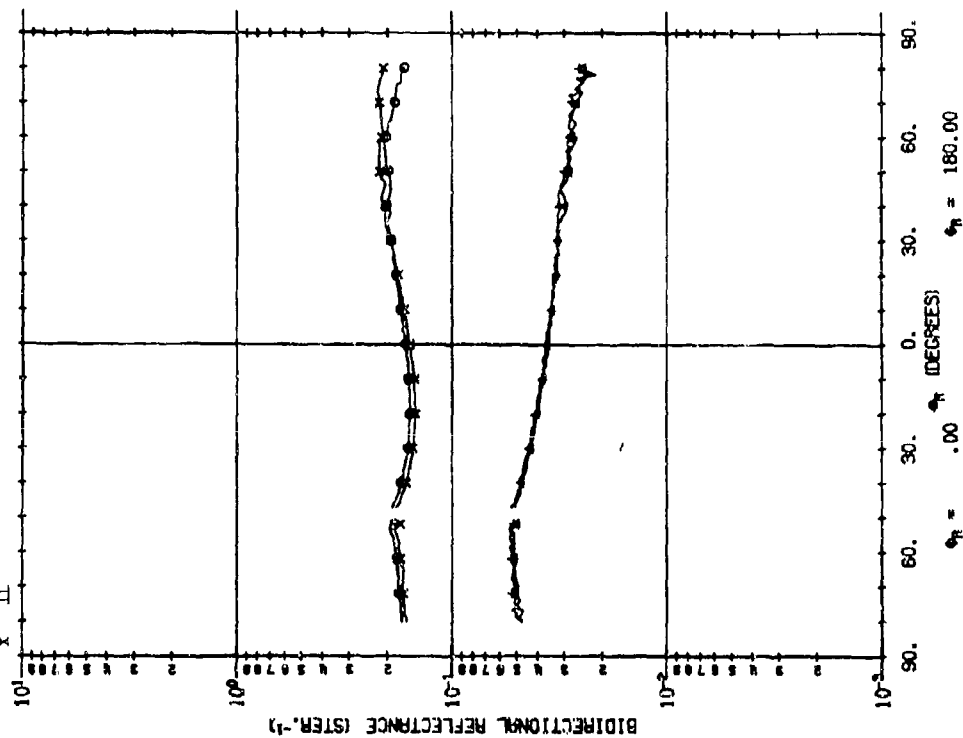
$\theta_1 = 30.0$   
 $\phi_1 = 0.0$   
 $\lambda = 0.63$



R01683 102

FLAME-SPRAYED ALUMINUM .03" THICK  
ON .25" ALUMINUM SUBSTRATE

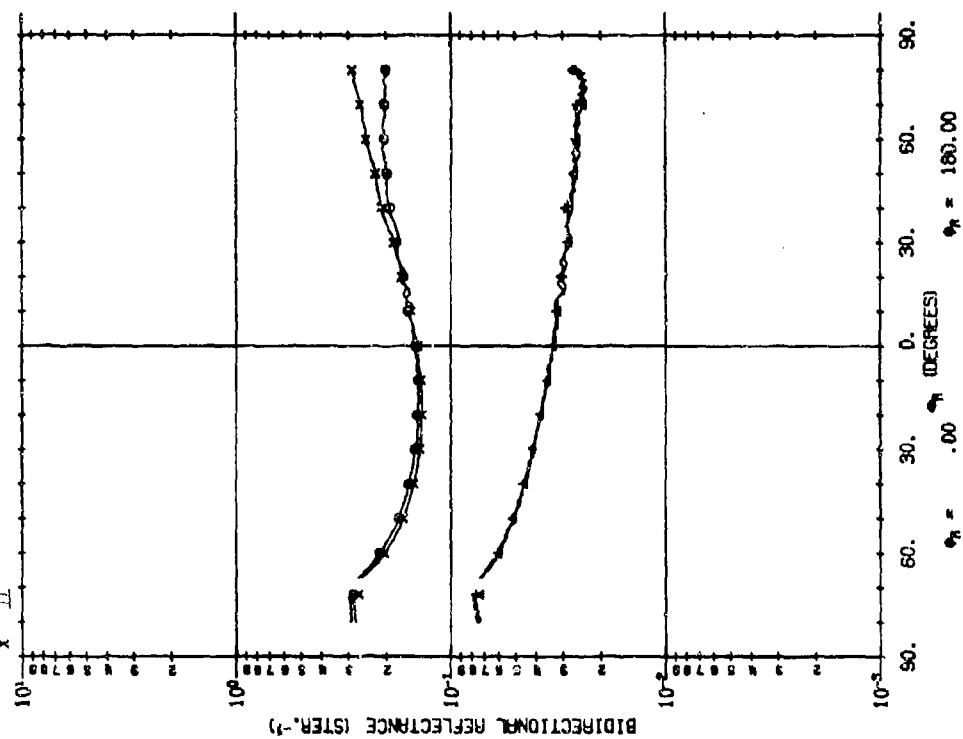
0 ||  $\theta_1 = 50.0$   
+ ||  $\theta_2 = 0.0$   
Δ ||  $\lambda = 0.63$   
x ||



R01683 102

FLAME-SPRAYED ALUMINUM .03" THICK  
ON .25" ALUMINUM SUBSTRATE

0 ||  $\theta_1 = 70.0$   
+ ||  $\theta_2 = 0.0$   
Δ ||  $\lambda = 0.63$   
x ||



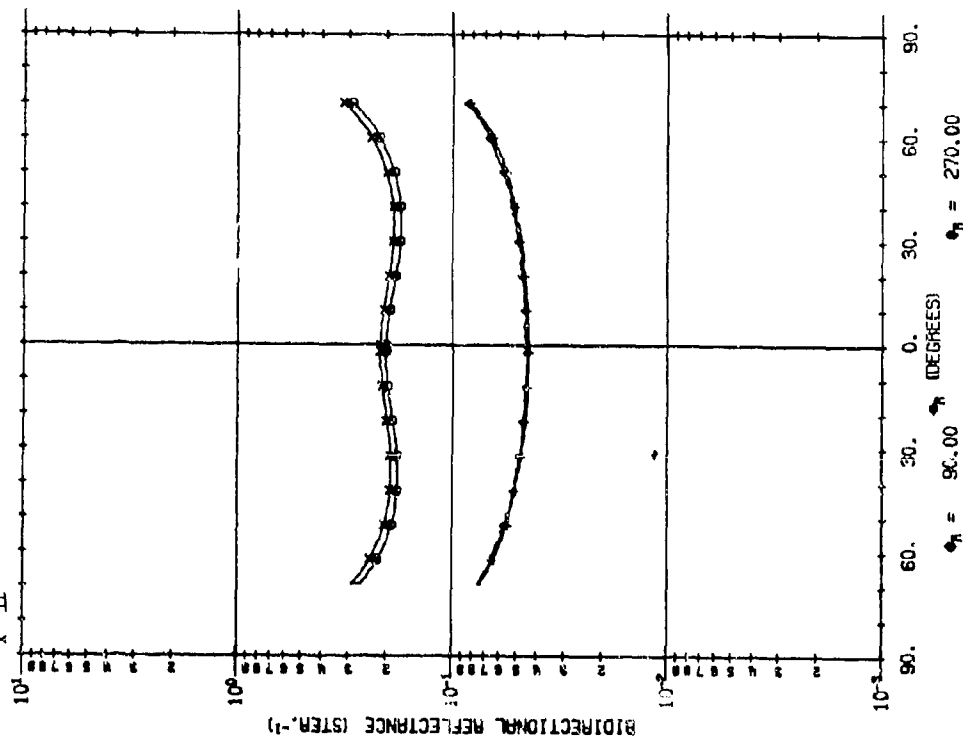
## REFLECTANCE STANDARDS MATERIAL

R01683 102

FLAME-SPRAYED ALUMINUM .03" THICK  
ON .25" ALUMINUM SUBSTRATE

$\phi_1 = 2.0$   
 $\phi_2 = \phi_3$   
 $\lambda = 0.63$

0 ||  
+ ||  
Δ ||  
x ||

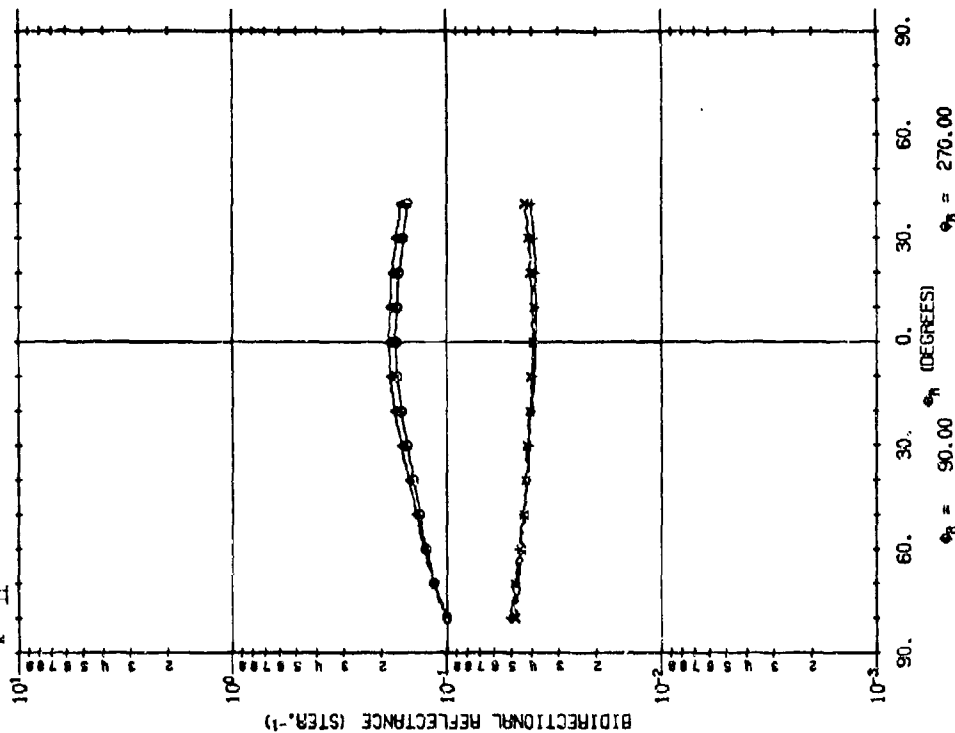


R01683 102

FLAME-SPRAYED ALUMINUM .03" THICK  
ON .25" ALUMINUM SUBSTRATE

$\phi_1 = 30.0$   
 $\phi_2 = \phi_3$   
 $\lambda = 0.63$

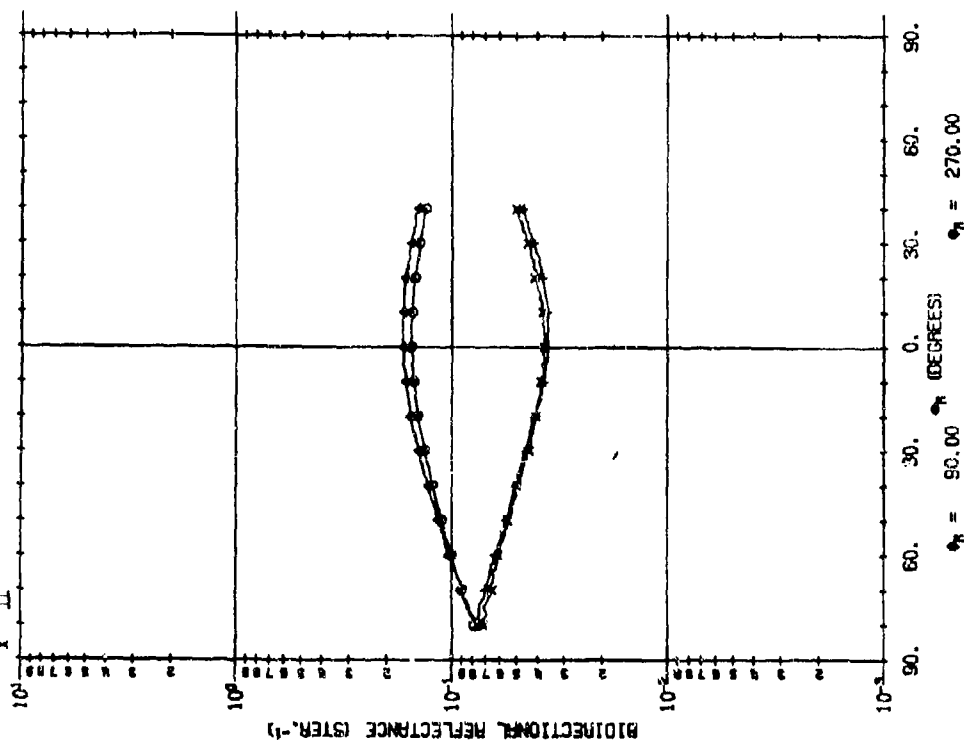
0 ||  
+ ||  
Δ ||  
x ||



R01683 102

FLAME-SPRAYED ALUMINUM .03" THICK  
ON .25" ALUMINUM SUBSTRATE

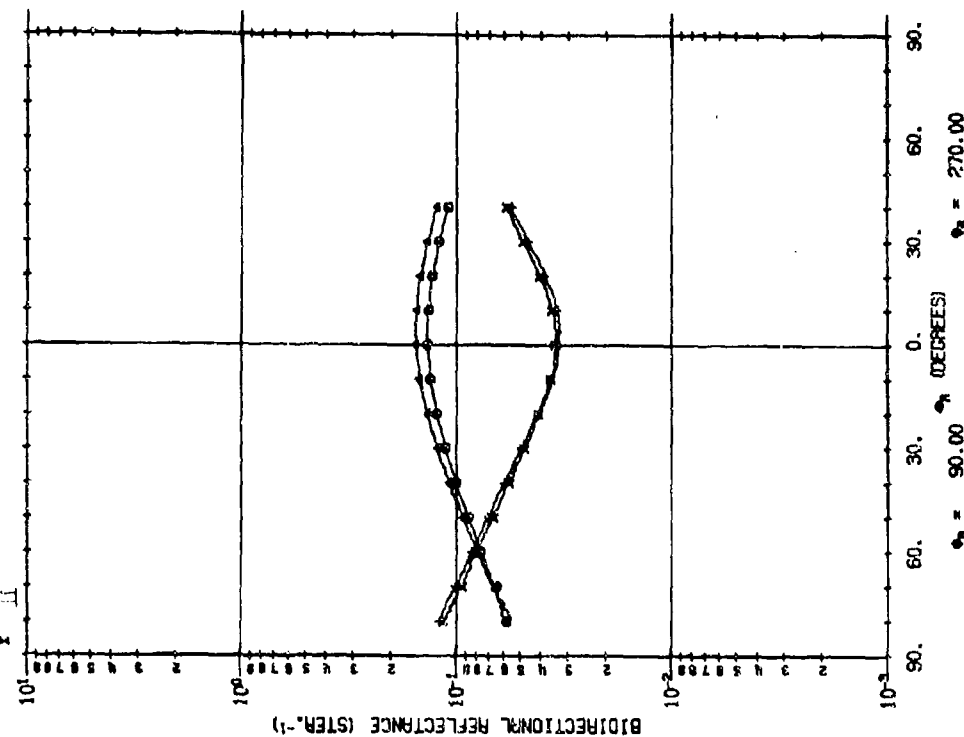
0 ||  $\phi_1 = 50.0$   
+ ||  $\phi_2 = 0.0$   
Δ ||  $\lambda = 0.63$   
X ||



R01683 102

FLAME-SPRAYED ALUMINUM .03" THICK  
ON .25" ALUMINUM SUBSTRATE

0 ||  $\phi_1 = 70.0$   
+ ||  $\phi_2 = 0.0$   
Δ ||  $\lambda = 0.63$   
X ||

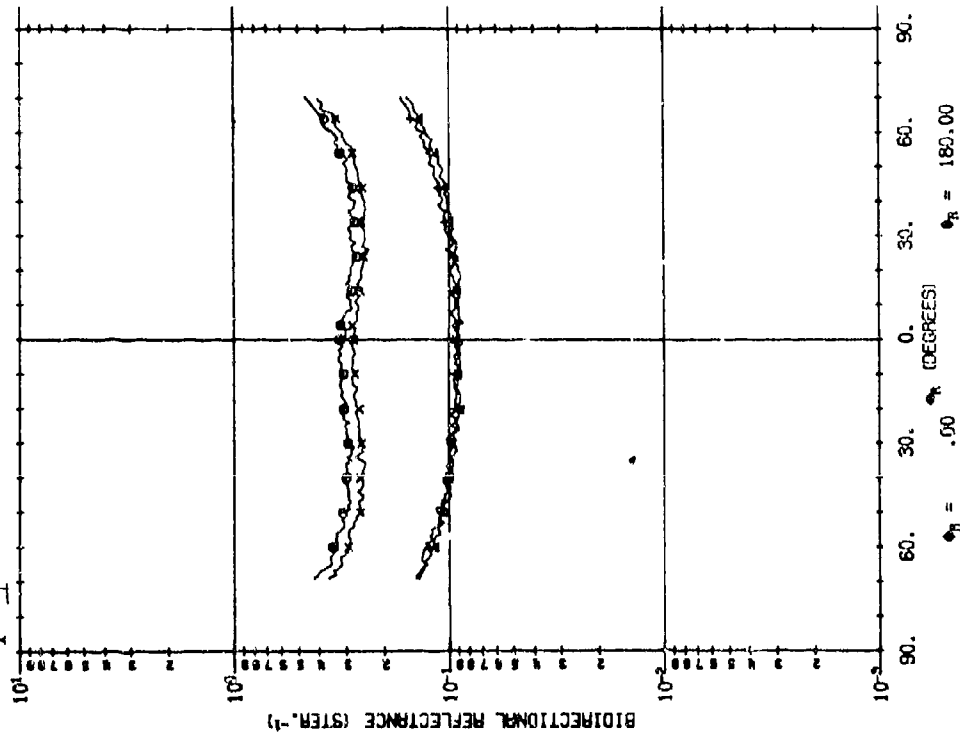


REFLECTANCE STANDARDS MATERIAL

R01683 101

FLAME-SPRAYED ALUMINUM .03" THICK  
OF .75" ALUMINUM SUBSTRATE

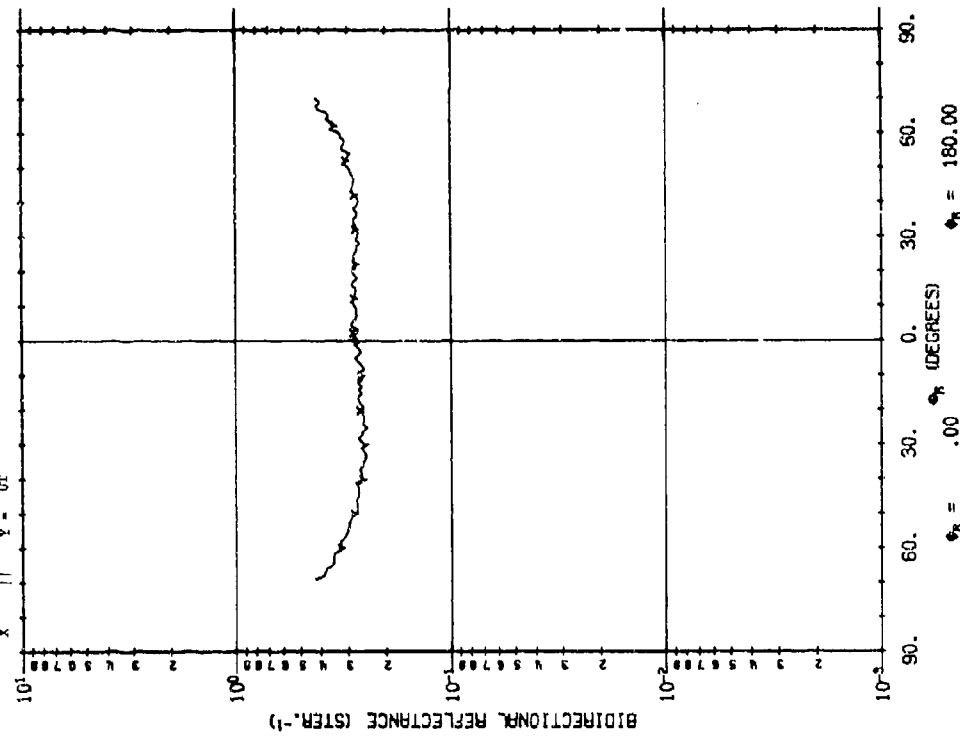
$2\theta = 4.0$   
 $\phi_s = \phi_r$   
 $\lambda = 10.6$



R01684 101

FLAME SPRAYED ALUMINUM ON  
1/4" THICK ALUMINUM

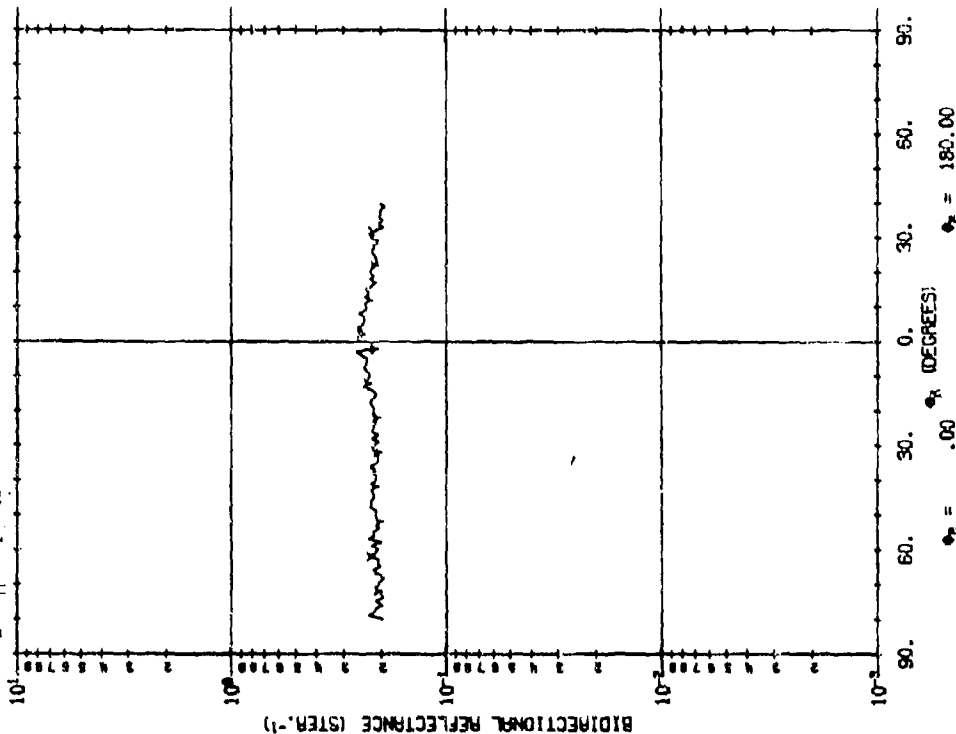
$2\theta = 2.0$   
 $\phi_s = \phi_r$   
 $\lambda = 10.6$



A01684 101

FLAME SPRAYED ALUMINUM ON 1/4" THICK ALUMINUM

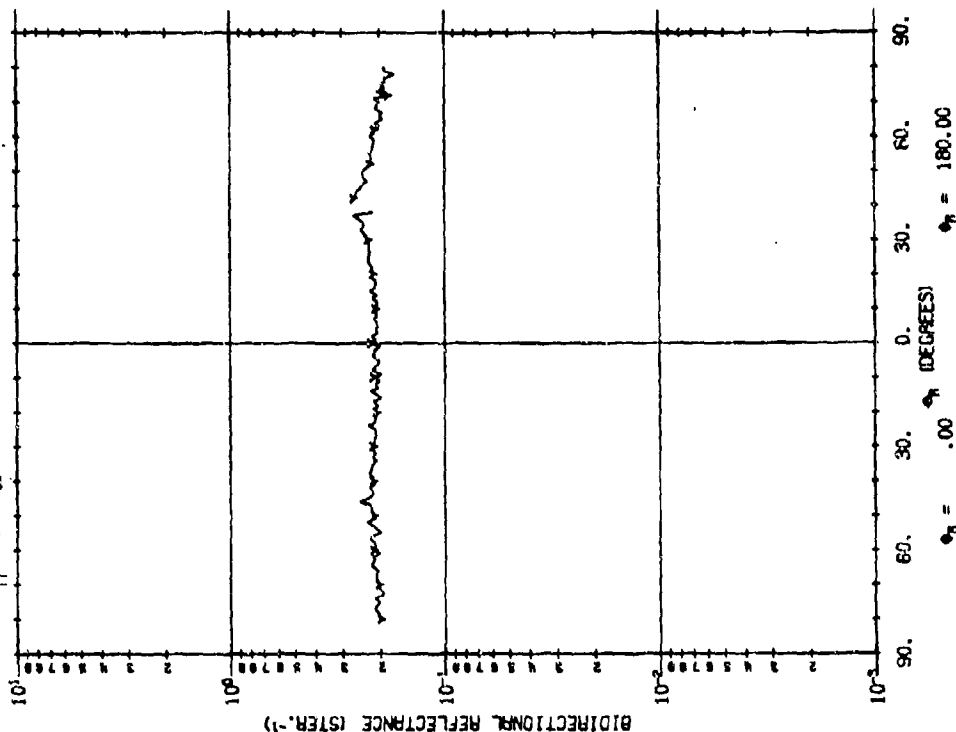
0 ||  $\theta_1 = 0.0$   
+ ||  $\theta_2 = 180.0$   
Δ ||  $\lambda = 10.6$   
X || Y = 0°



A01684 101

FLAME SPRAYED ALUMINUM ON 1/4" THICK ALUMINUM

0 ||  $\theta_1 = 40.0$   
+ ||  $\theta_2 = 180.0$   
Δ ||  $\lambda = 10.6$   
X || Y = 0°



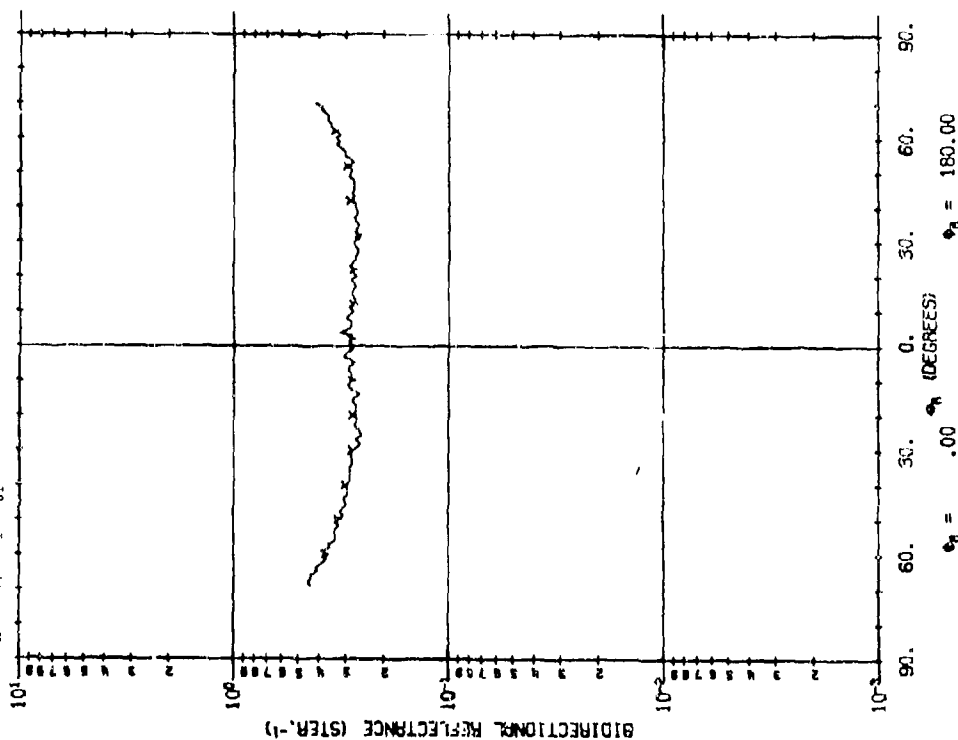
REFLECTANCE STANDARDS MATERIAL



RQ1688 101

FLAME SPRAYED ALUMINUM ON  
1/4" THICK ALUMINUM

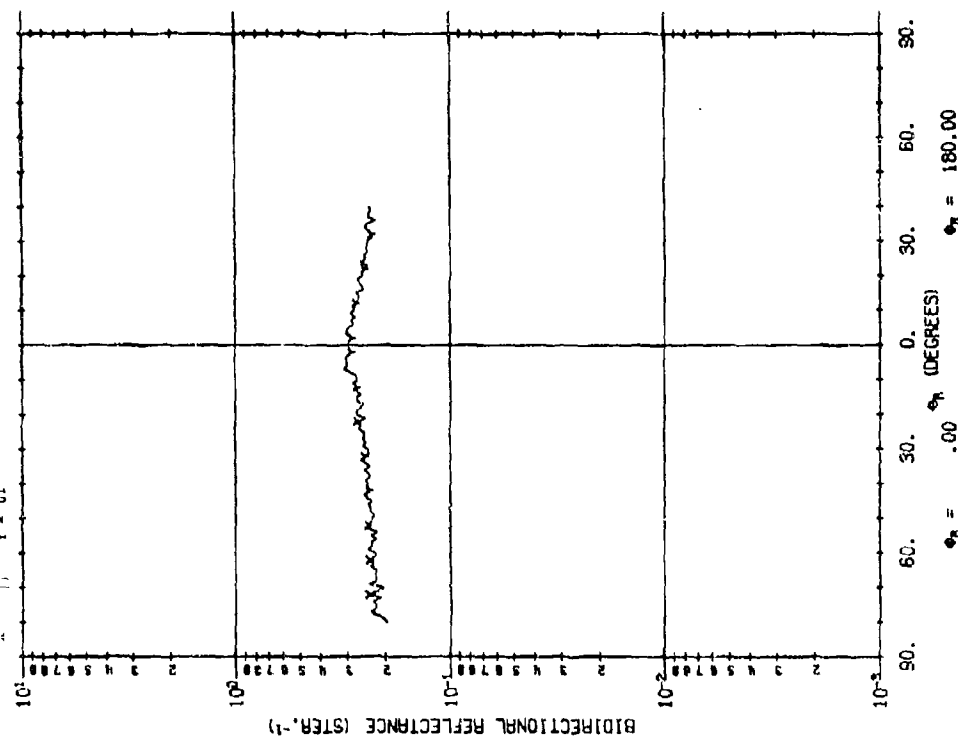
$\theta_1 = 2.0$   
 $\theta_2 = \theta_r$   
 $\lambda = 10.6$   
 $\gamma = \text{UT}$



RQ1688 101

FLAME SPRAYED ALUMINUM ON  
1/4" THICK ALUMINUM

$\theta_1 = 0.0$   
 $\theta_2 = 180.0$   
 $\lambda = 10.6$   
 $\gamma = \text{UT}$

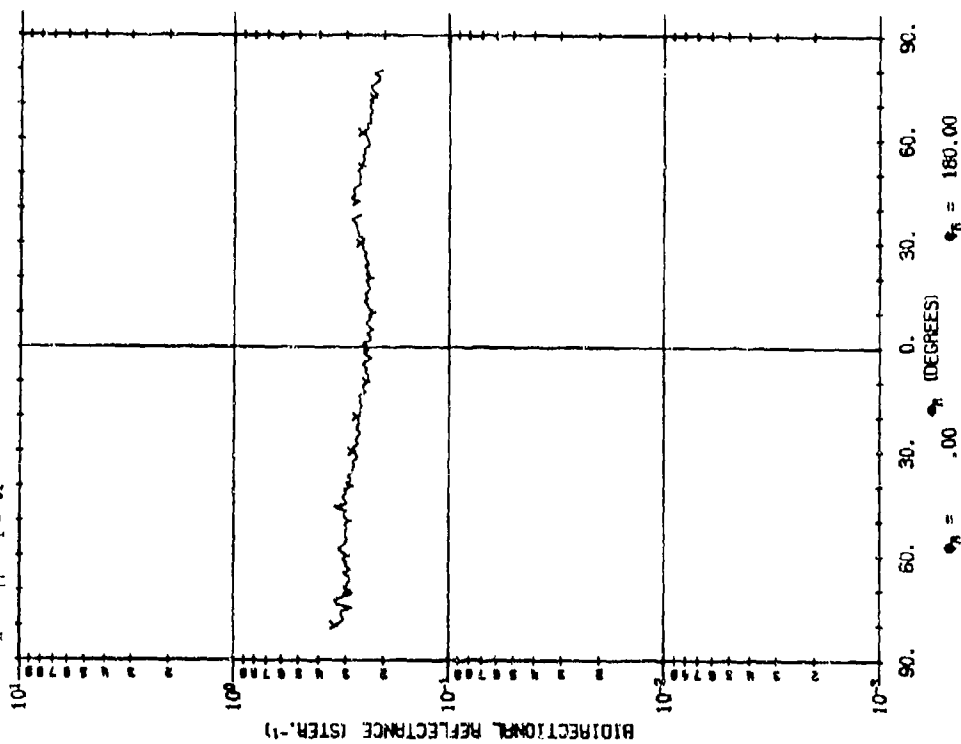


R01688 101

FLAME SPRAYED ALUMINUM ON  
1/4" THICK ALUMINUM

$\phi_1 = 40.0$   
 $\phi_2 = 180.0$   
 $\lambda = 10.6$

X Y = UT

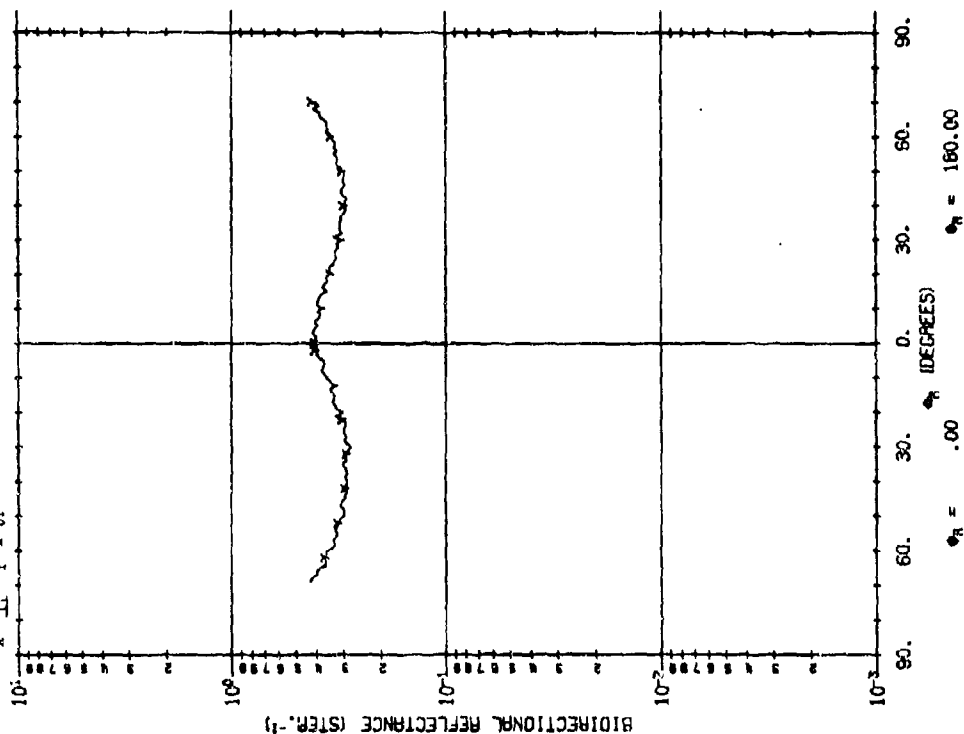


R01894 101

FLAME SPRAYED ALUMINUM OVER  
SANDBLASTED ALUMINUM PLATE

$\phi_1 = 22$   $\phi_2 = 2.0$   
 $\phi_3 = \phi_4$   
 $\lambda = 10.6$

X Y = UT

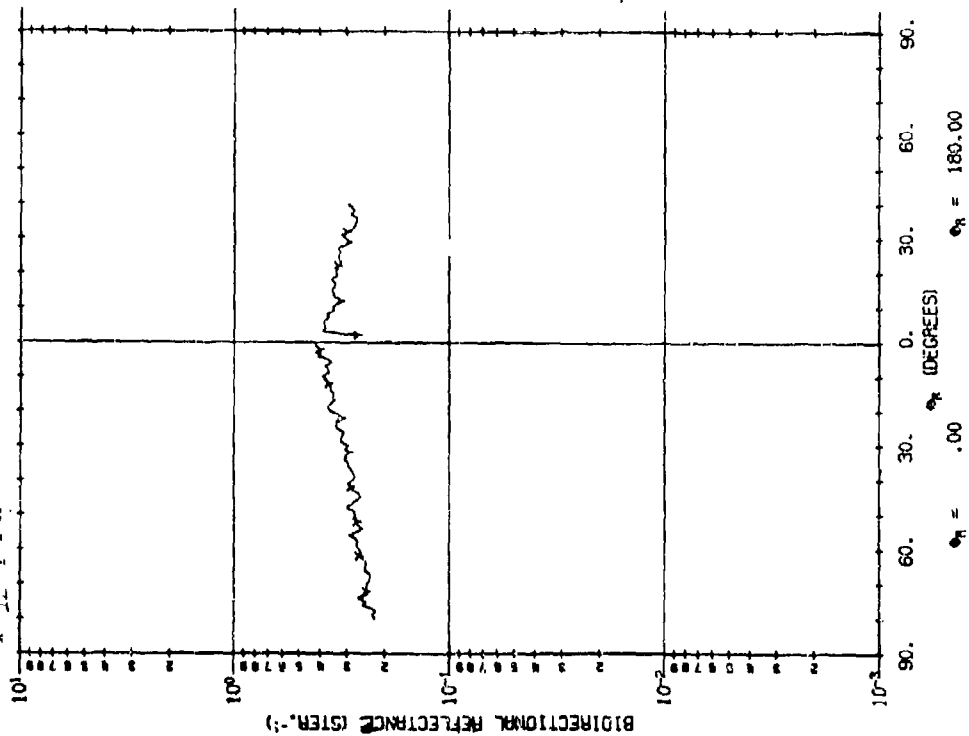


## REFLECTANCE STANDARDS MATERIAL

R01894 101

Flame Sprayed Aluminum over Sandblasted  
Aluminum Plate

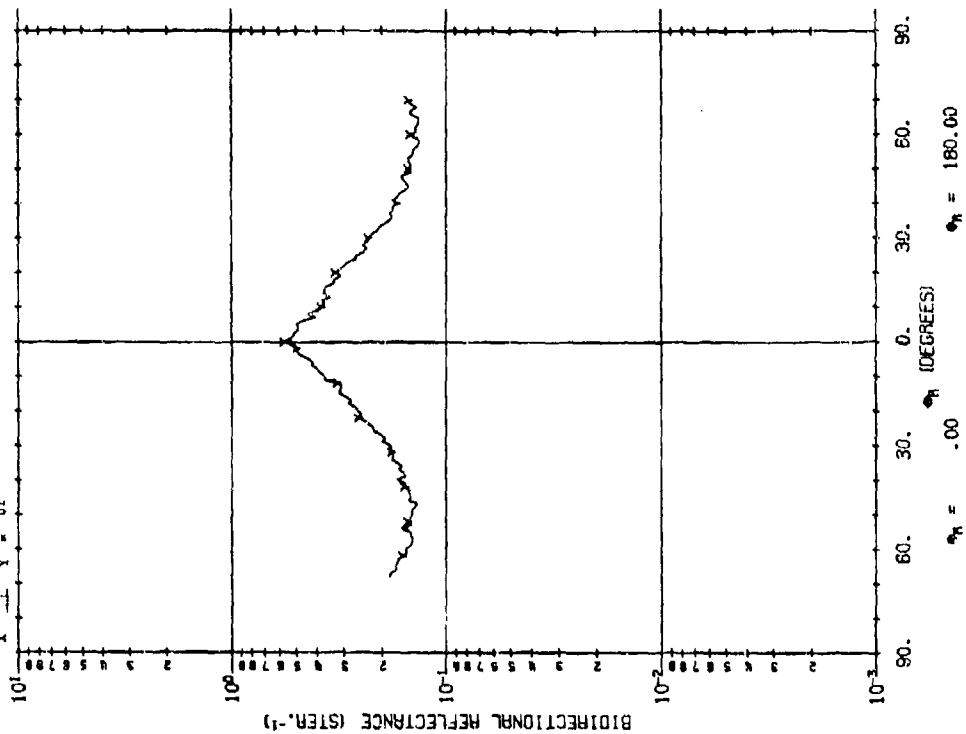
0 //  $\epsilon_1 = 0.0$   
+ //  $\epsilon_2 = 180.0$   
2 //  $\lambda = 10.5$   
X // Y = UT



R01895 101

Sandblasted Aluminum

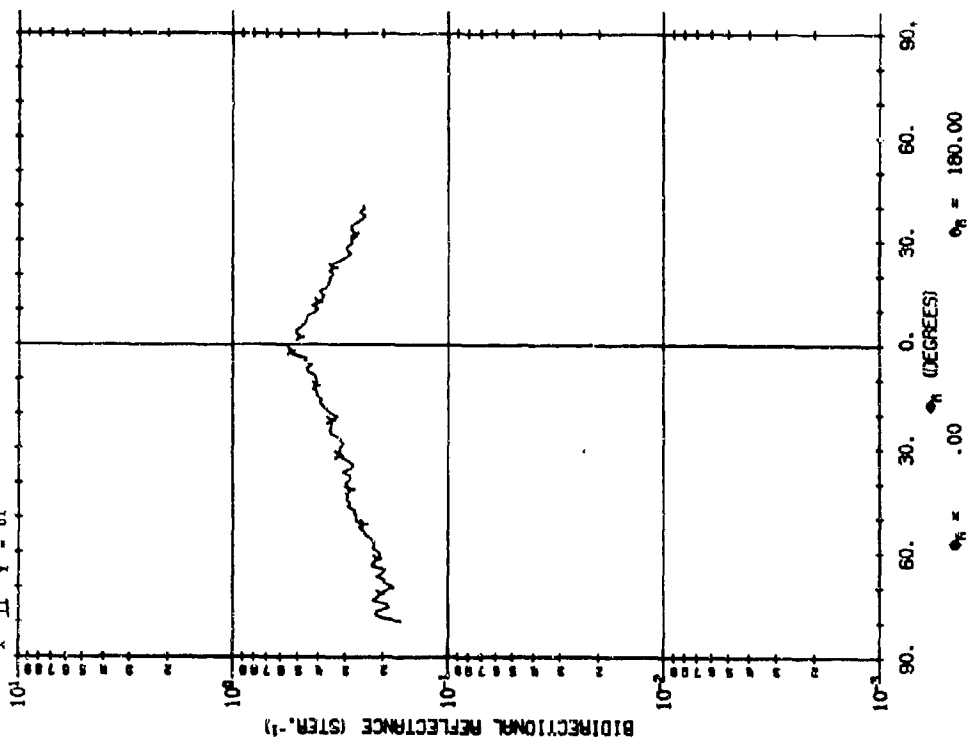
0 //  $\epsilon_1 = 2.0$   
+ //  $\epsilon_2 = 180.0$   
2 //  $\lambda = 10.6$   
X // Y = UT



R01895 101

Sandblasted Aluminum

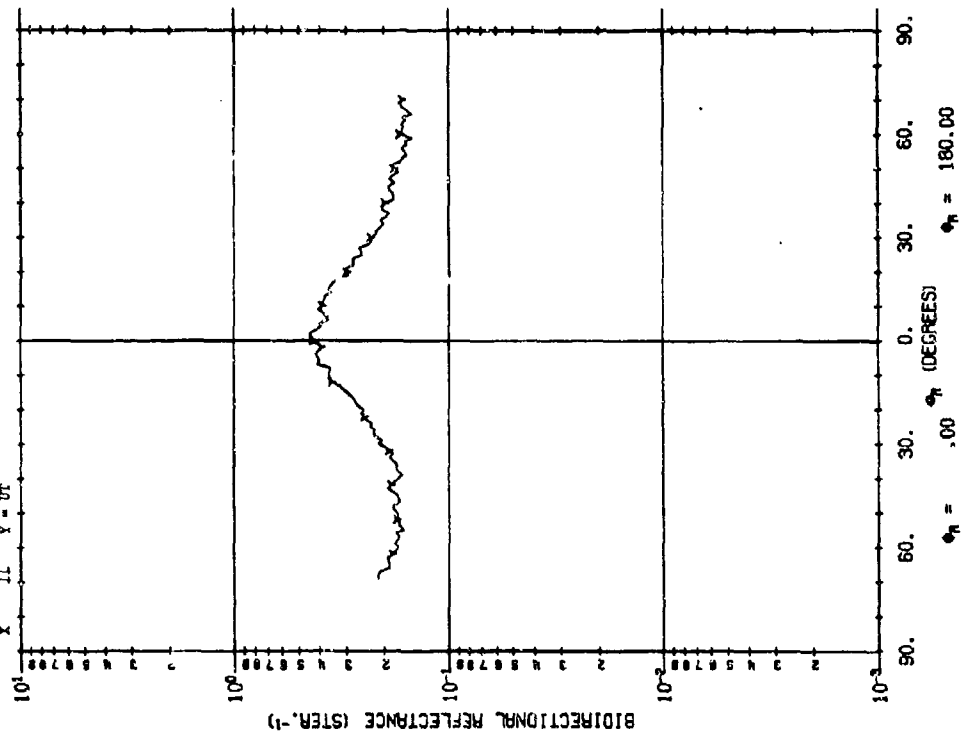
0 //  $\phi_i = 0.0$   
 + //  $\phi_i = 180.0$   
 Δ //  $\lambda = 10.6$   
 X // Y = UT



R01895 201

SANDBLASTED ALUMINUM

0 //  $2\theta = 2.0$   
 + //  $\phi_i = \phi_r$   
 Δ //  $\lambda = 10.6$   
 X // Y = UT

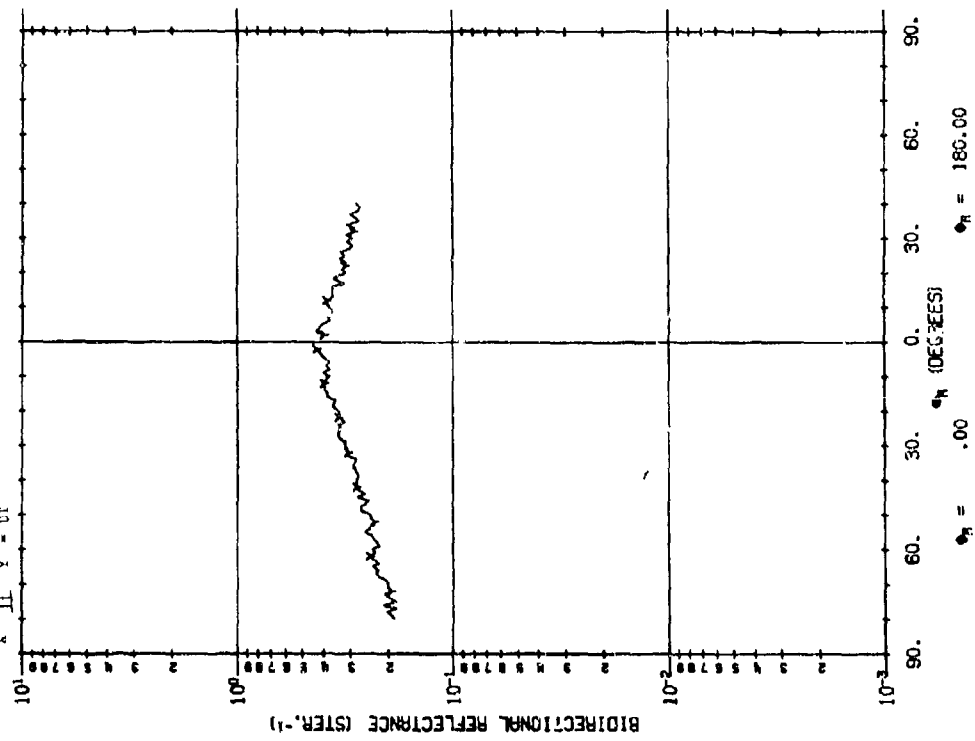


REFLECTANCE STANDARDS MATERIAL

R01895 201

Sandblasted Aluminum

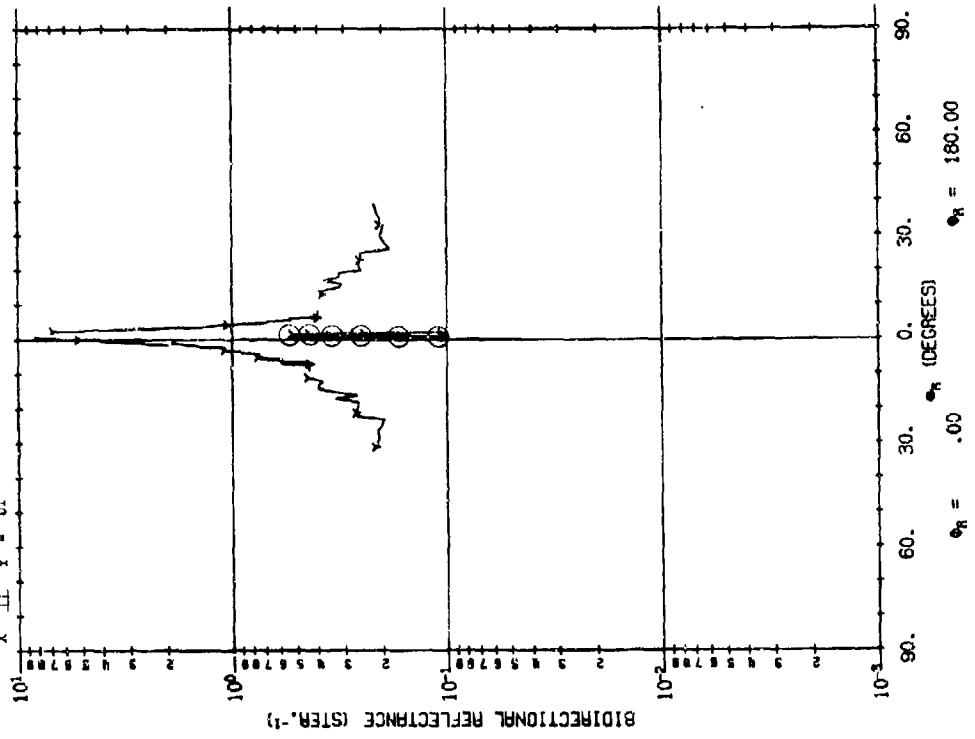
0 ||  $\phi_1 = 0.0$   
 + ||  $\phi_1 = 180.0$   
 5 ||  $\lambda = 10.6$   
 X || Y = UT



R01895 301

Sandblasted Aluminum

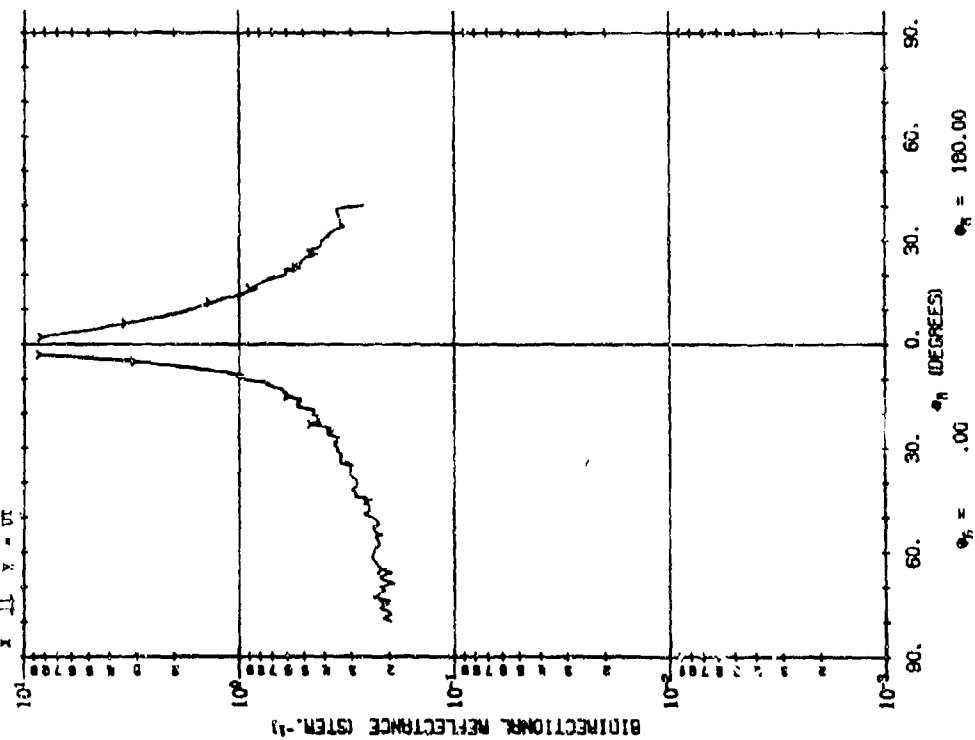
0 ||  $2\theta = 2.0$   
 + ||  $\phi_1 = \phi_r$   
 5 ||  $\lambda = 10.6$   
 X || Y = UT



R01895 301

Sandblasted Aluminum

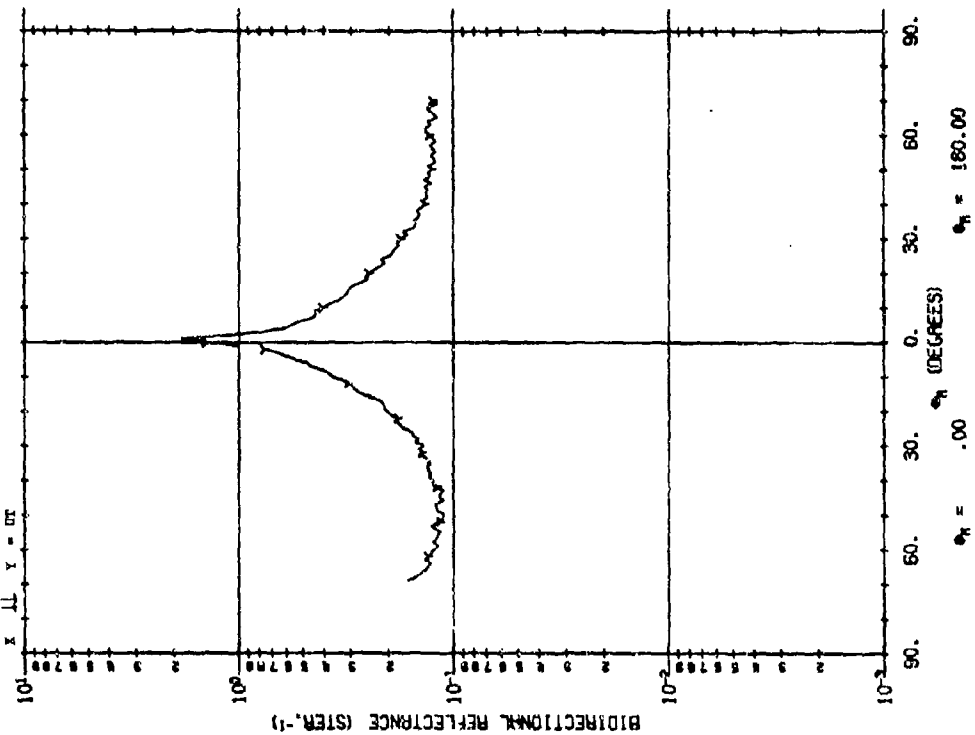
$\theta_i = 0.0$   
 $\theta_r = 180.0$   
 $\lambda = 10.6$   
 $Y = UT$



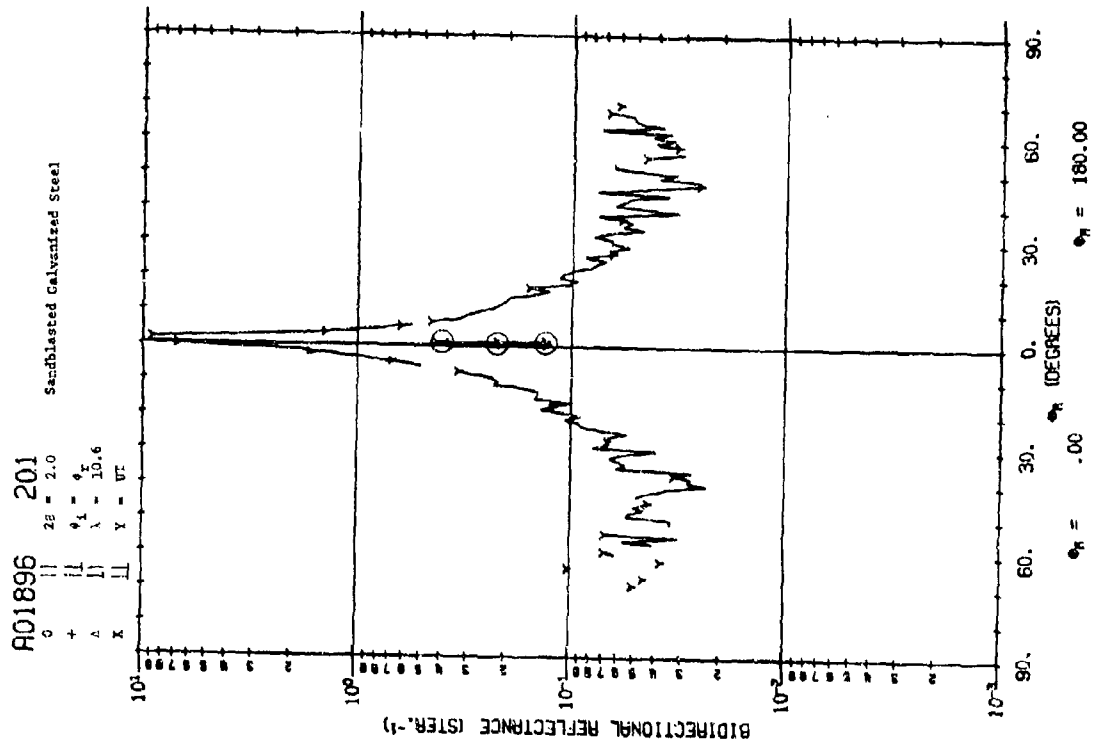
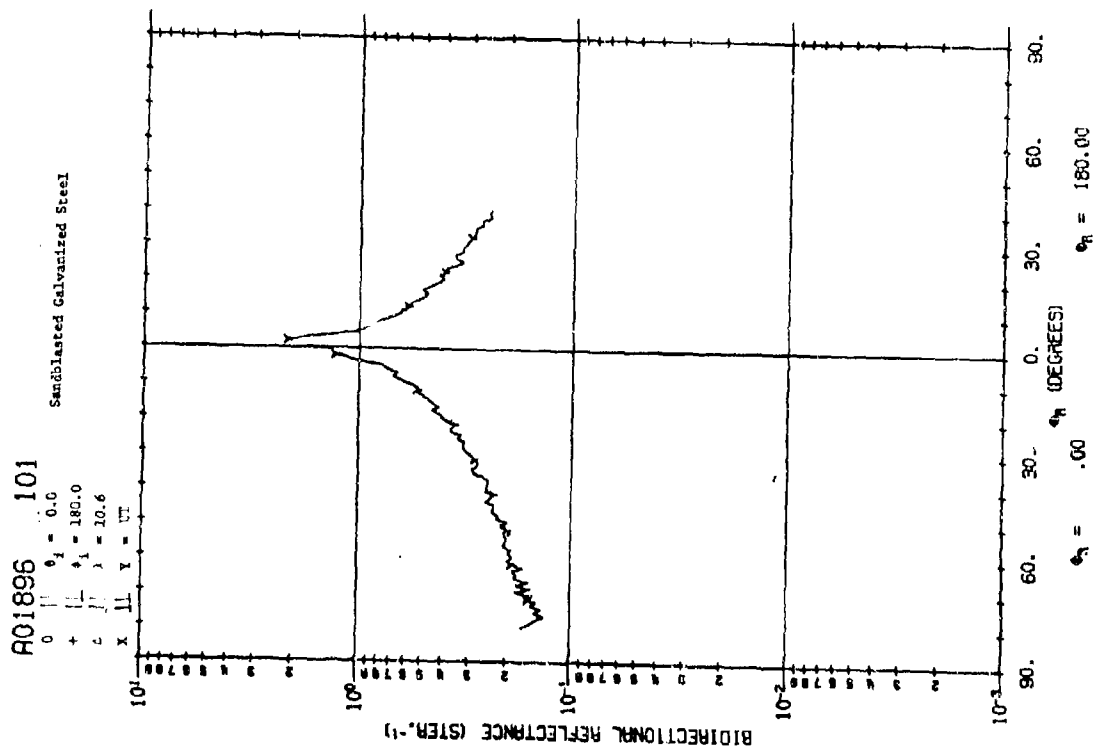
R01896 101

Sandblasted Galvanized Steel

$\theta_i = 2.0$   
 $\theta_r = 180.0$   
 $\lambda = 10.6$   
 $Y = UT$



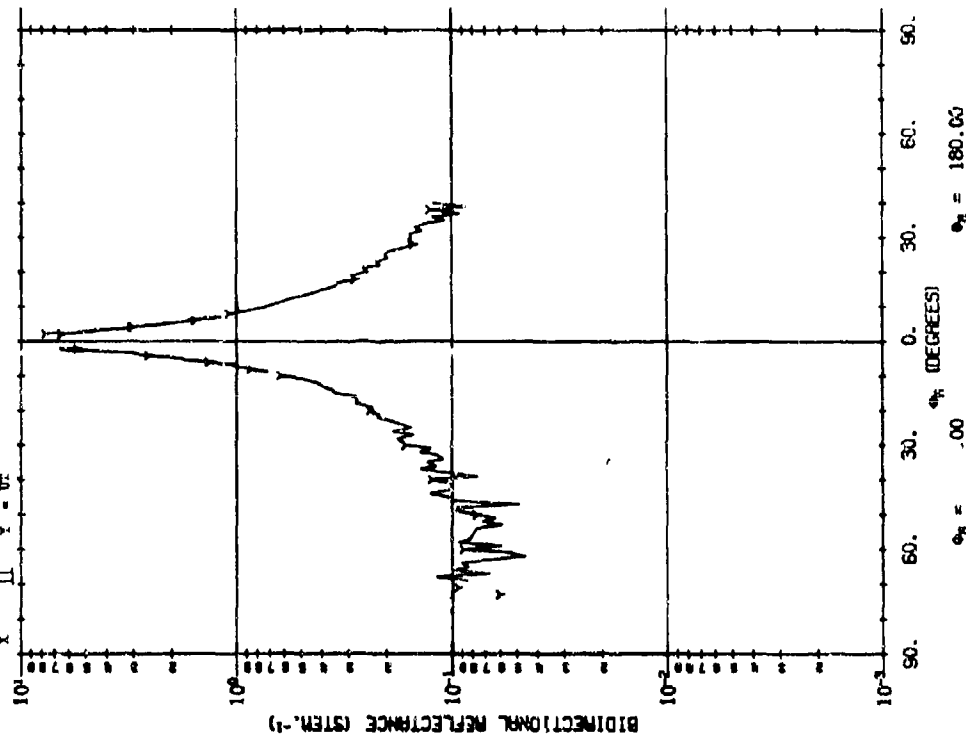
# REFLECTANCE STANDARDS MATERIAL



R01896 201

Sandblasted Galvanized Steel

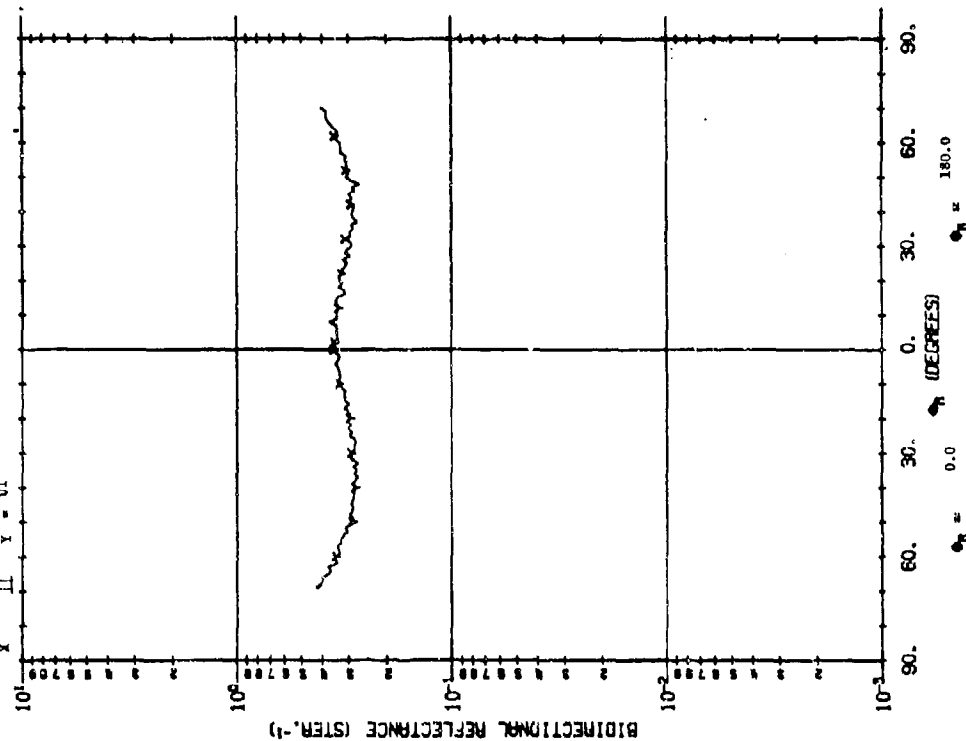
0 ||  $\phi_1 = 0.0$   
 + ||  $\phi_1 = 180.0$   
 Δ ||  $\lambda = 10.6$   
 X ||  $Y = VT$



R01915 101

Flame Sprayed Aluminum on Aluminum Substrate

0 ||  $2\theta = 2.0$   
 + ||  $\phi_1 = \phi_2$   
 Δ ||  $\lambda = 10.6$   
 X ||  $Y = VT$



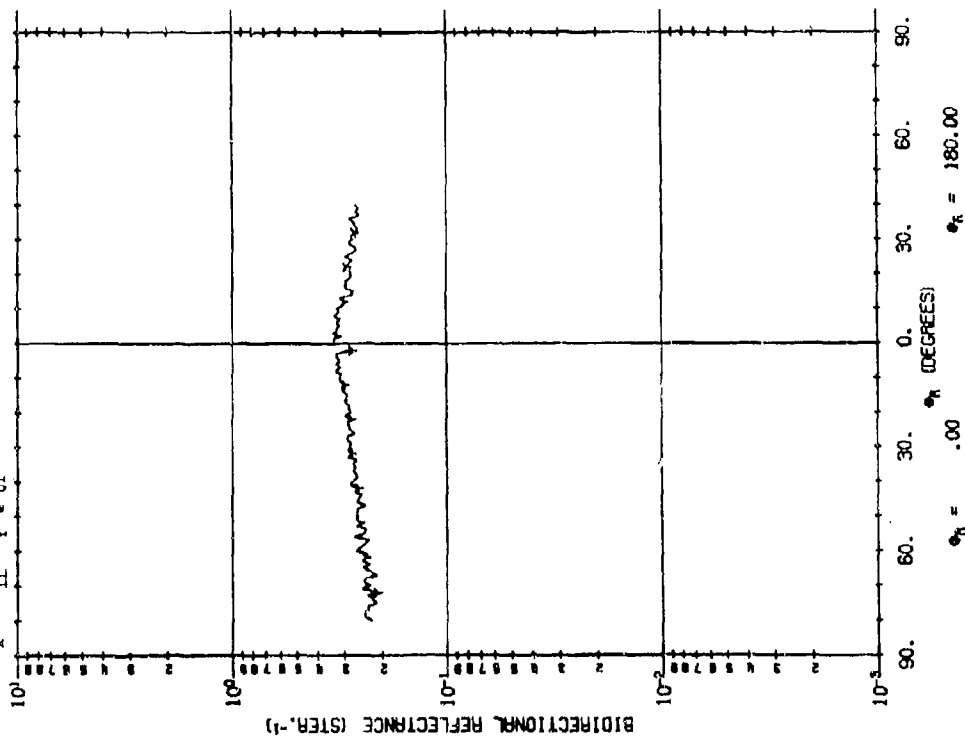
# REFLECTANCE STANDARDS MATERIAL



A01915 101

Flame Sprayed Aluminum on Aluminum

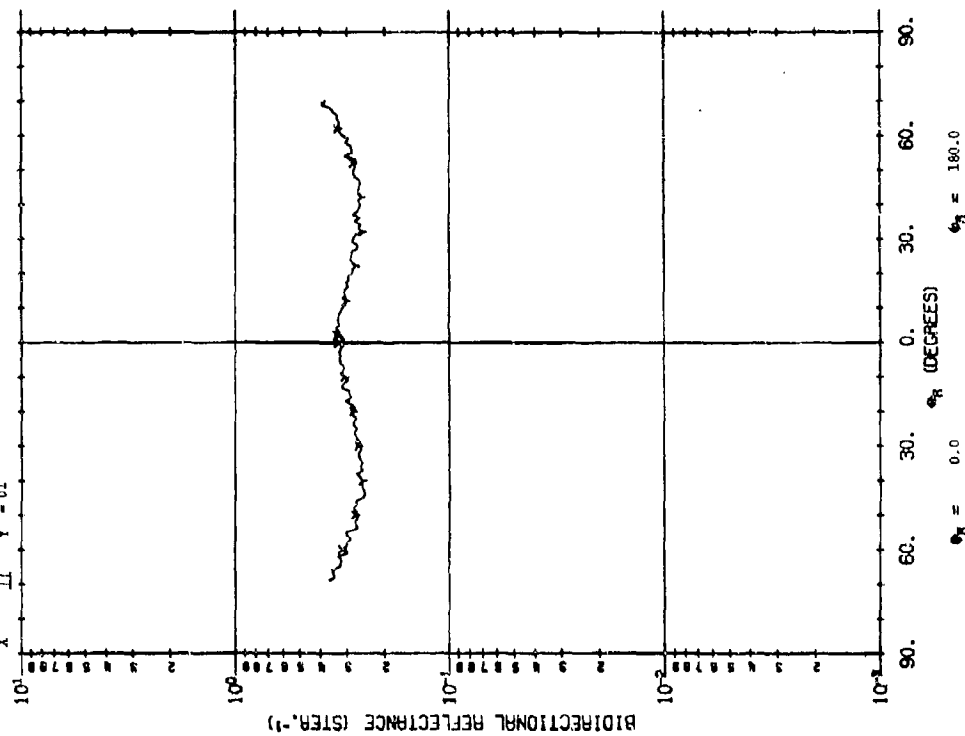
$\theta_i = 0.0$   
 $\phi_i = 180.0$   
 $\lambda = 10.6$   
 $Y = UT$



A01916 101

Flame Sprayed Aluminum on Aluminum

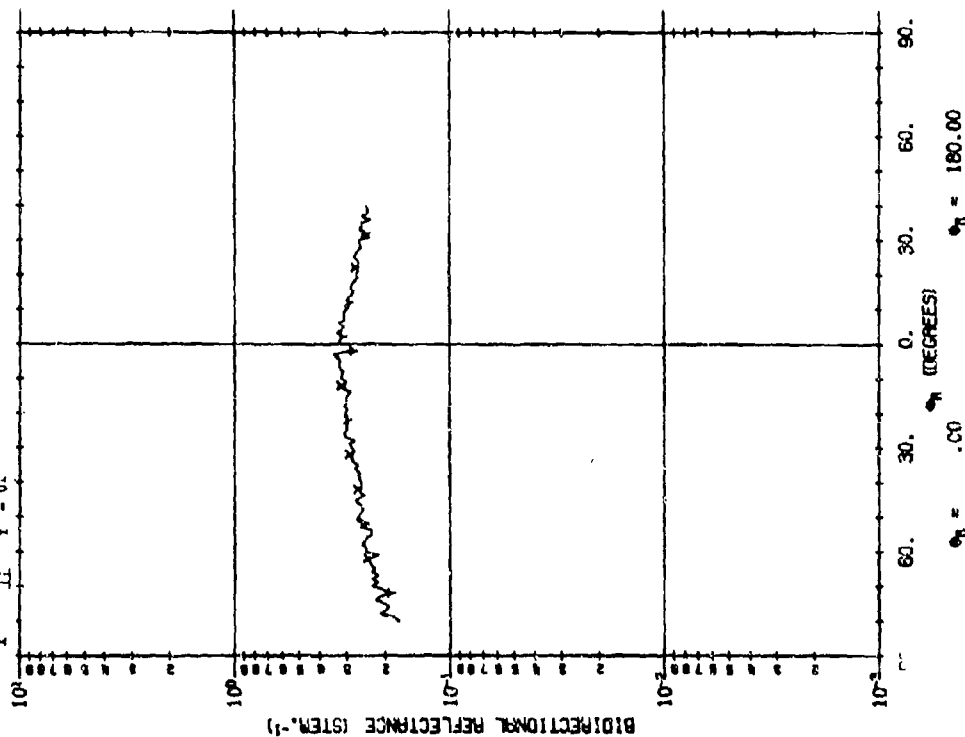
$\theta_i = 2.0$   
 $\phi_i = \phi_r$   
 $\lambda = 10.6$   
 $Y = UT$



R01916 101

Flame Sprayed Aluminum on Aluminum

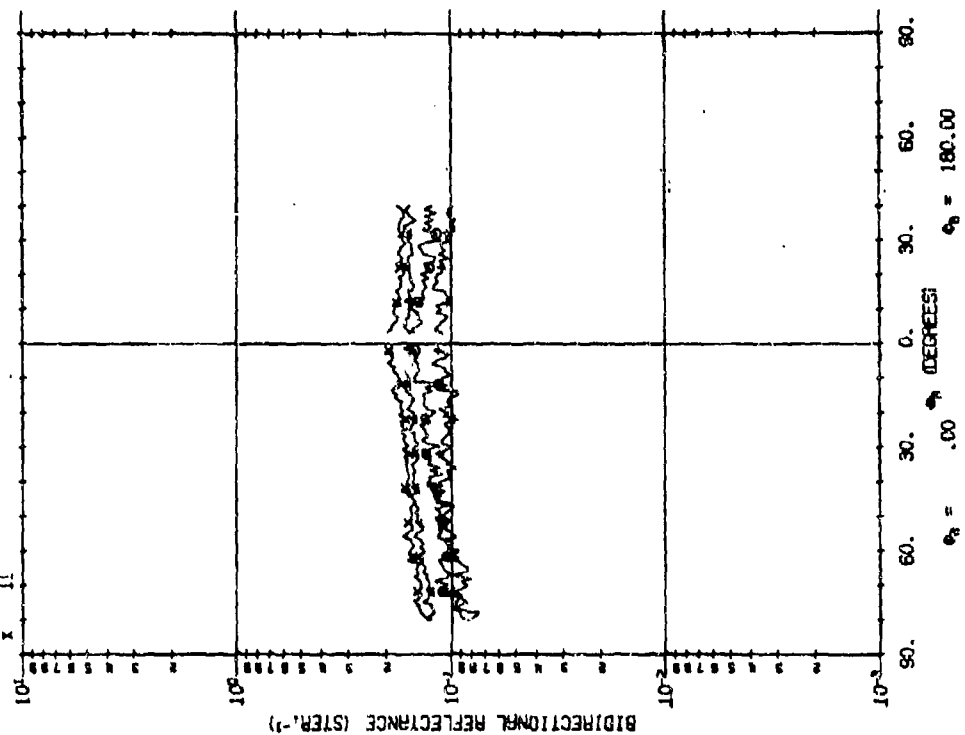
0 ||  $\theta_i = 0.0$   
 + ||  $\theta_r = 180.0$   
 Δ ||  $\lambda = 10.6$   
 X || Y - UT



R02003 101

3M White Paint on Fiberboard

0 ||  $\theta_i = 0.0$   
 + ||  $\theta_r = 180.0$   
 Δ ||  $\lambda = 1.06$   
 X ||

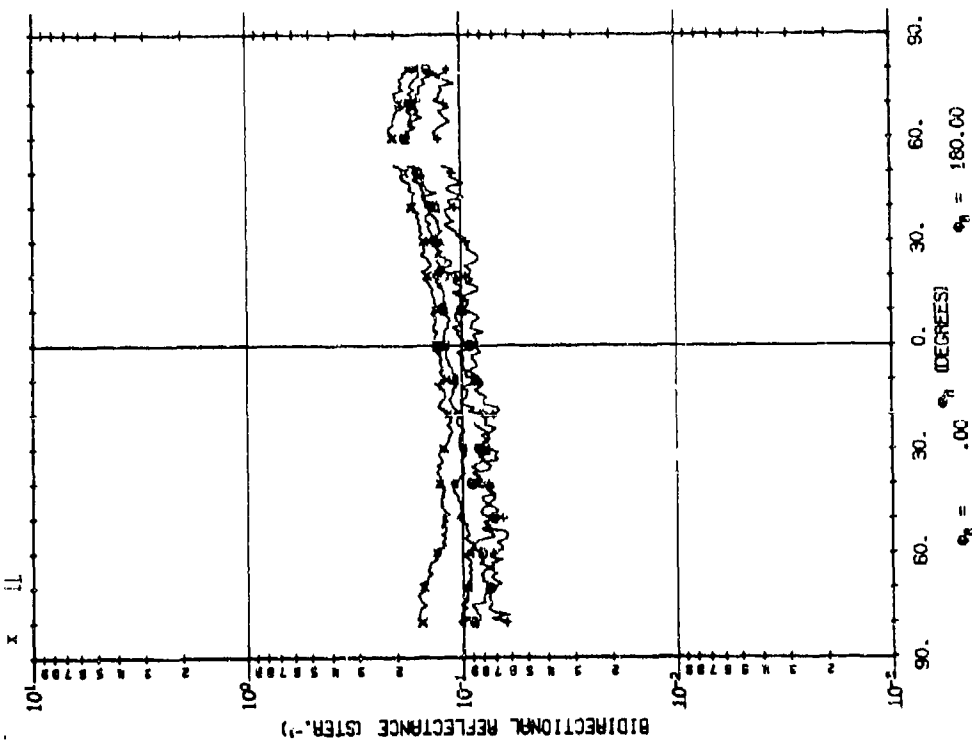


# REFLECTANCE STANDARDS MATERIAL

R02003 101

3M White Paint on Fiberboard

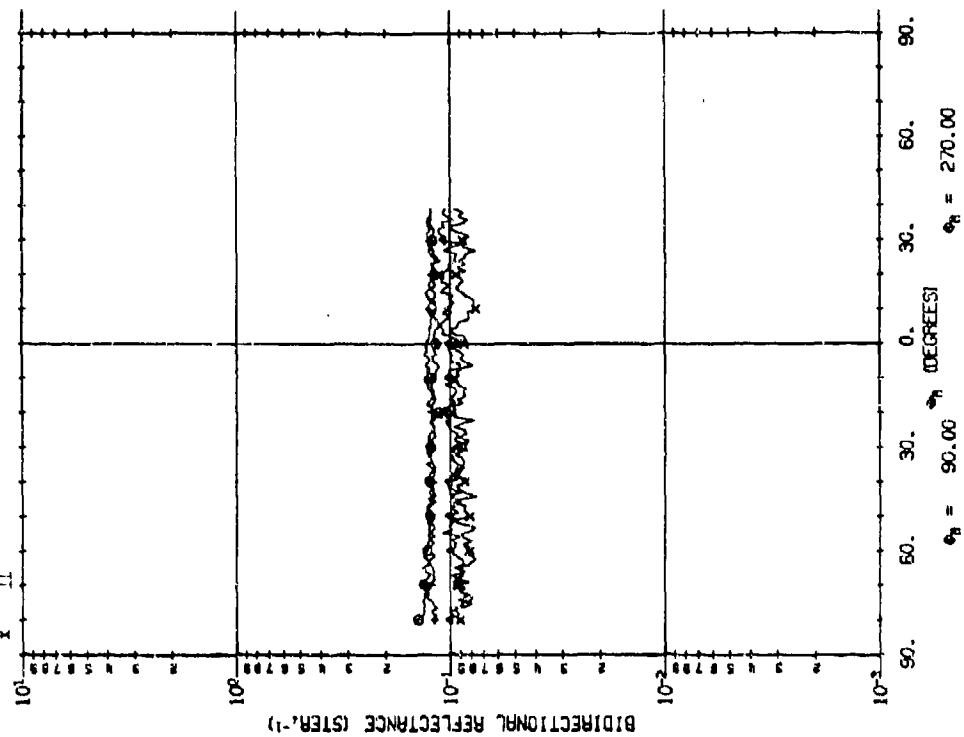
$\theta_i = 56.0$   
 $\phi_i = 180.0$   
 $\lambda = 1.06$



R02003 101

3M White Paint on Fiberboard

$\theta_i = 56.0$   
 $\phi_i = 180.0$   
 $\lambda = 1.06$

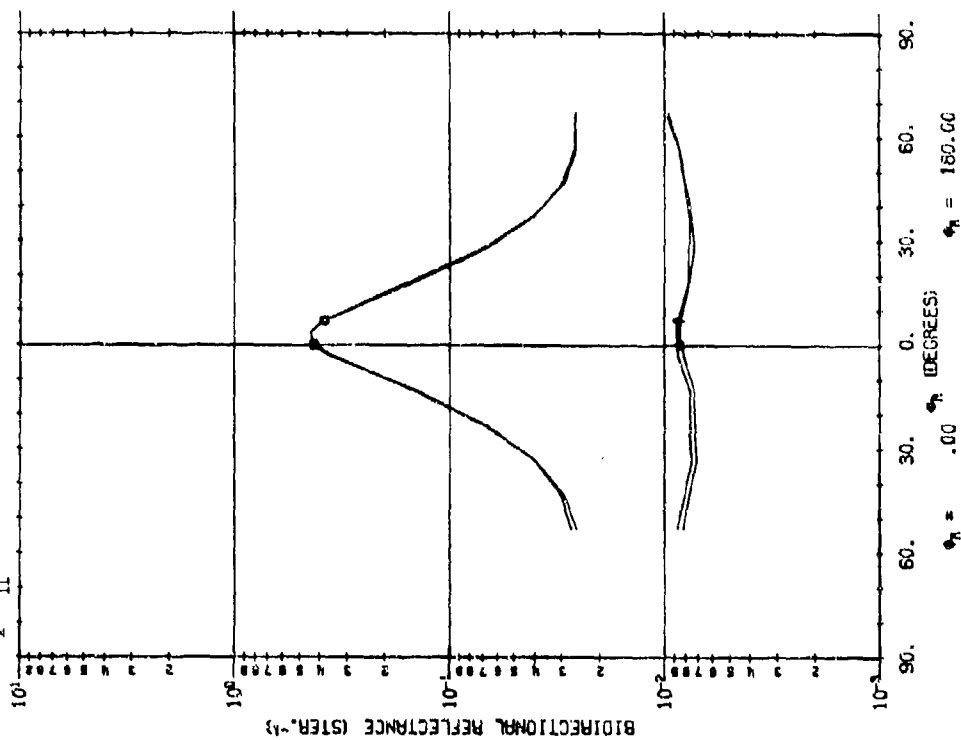


METAL

R01294 004

0 II 2E = 7.0 BARE METAL

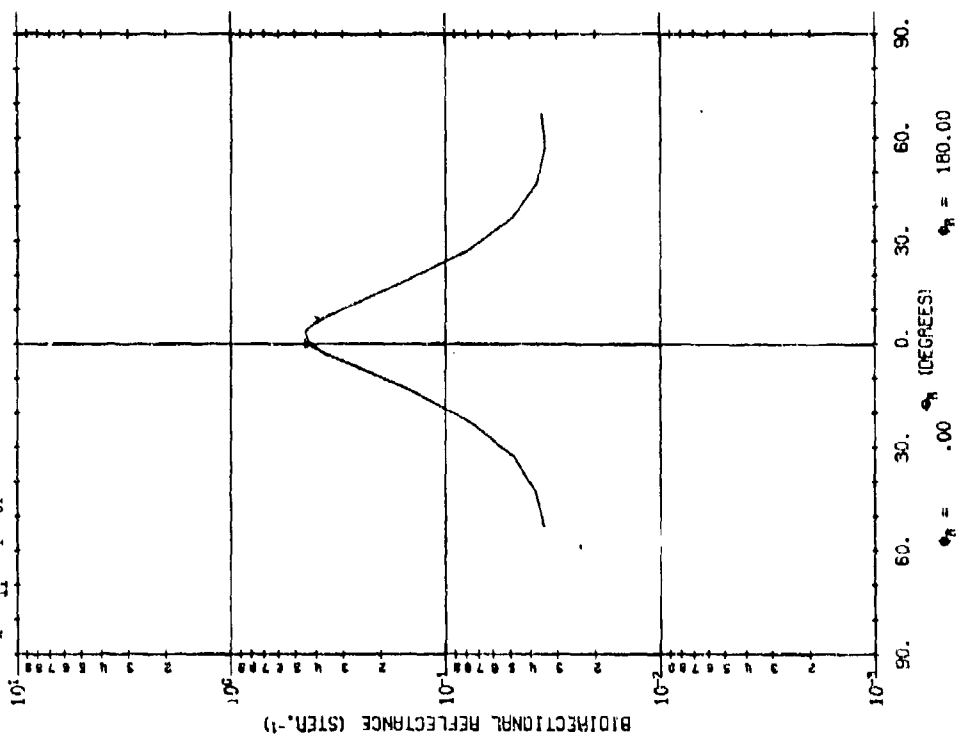
+ II  $\phi_1 = \phi_r$   
 $\Delta$  II  $\lambda = 0.63$   
 Z II



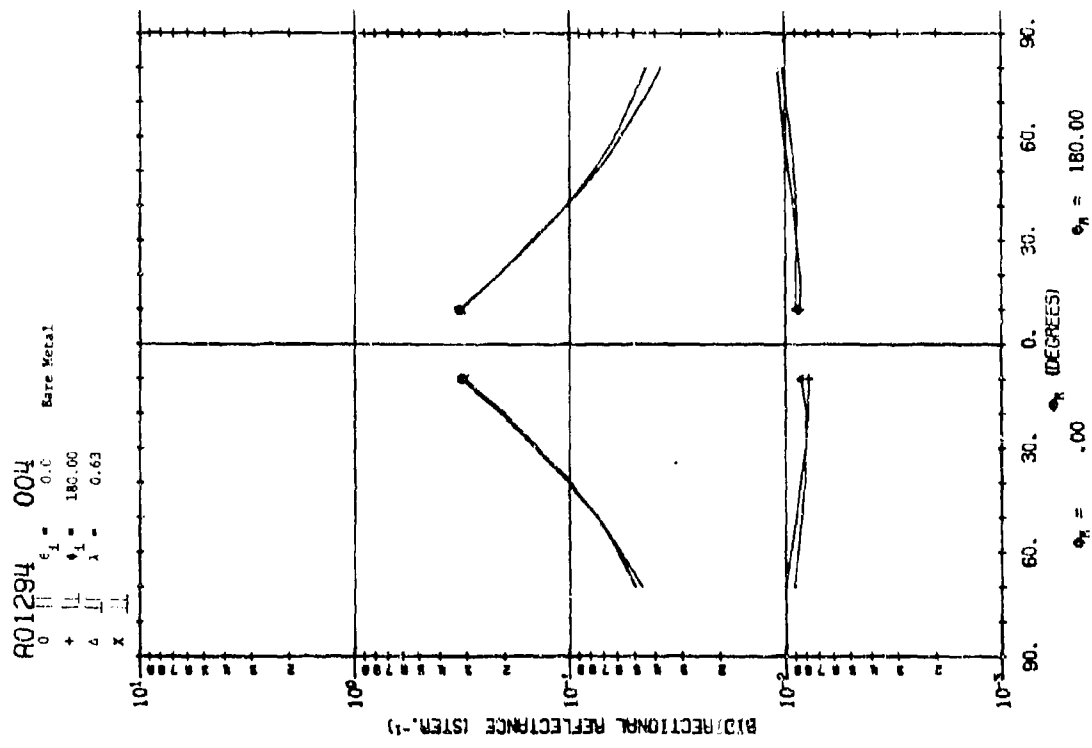
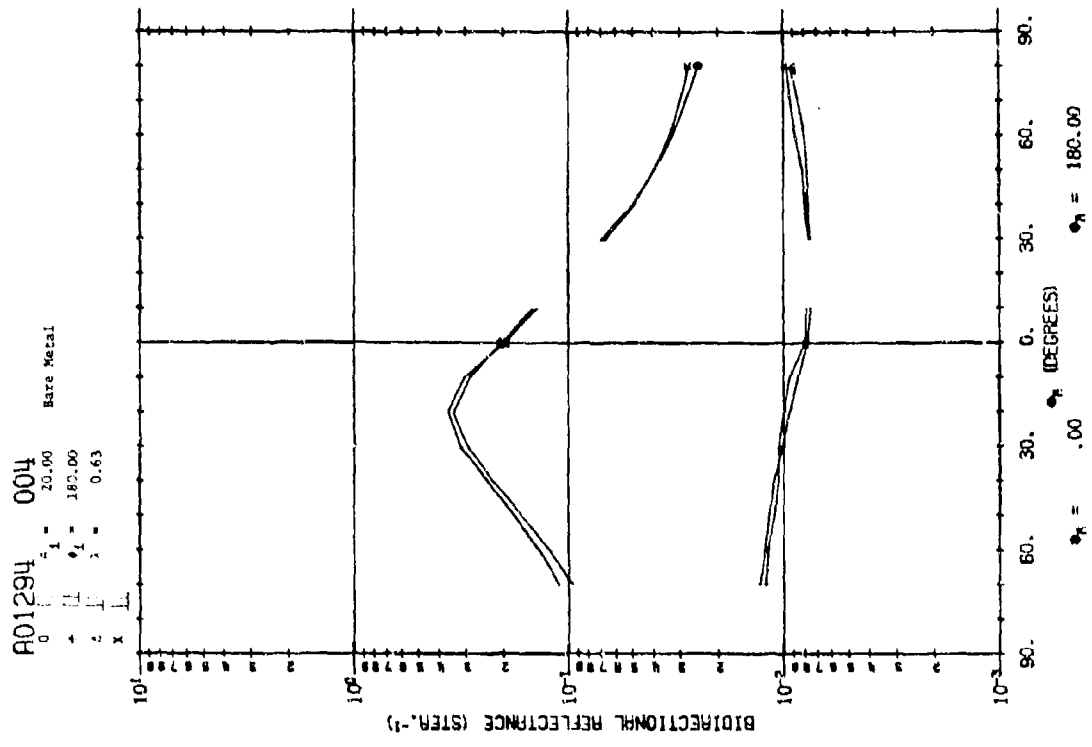
R01294 004

0 II 2E = 7.0 BARE METAL

+ II  $\phi_1 = \phi_r$   
 $\Delta$  II  $\lambda = 0.63$   
 X II Y = 0T

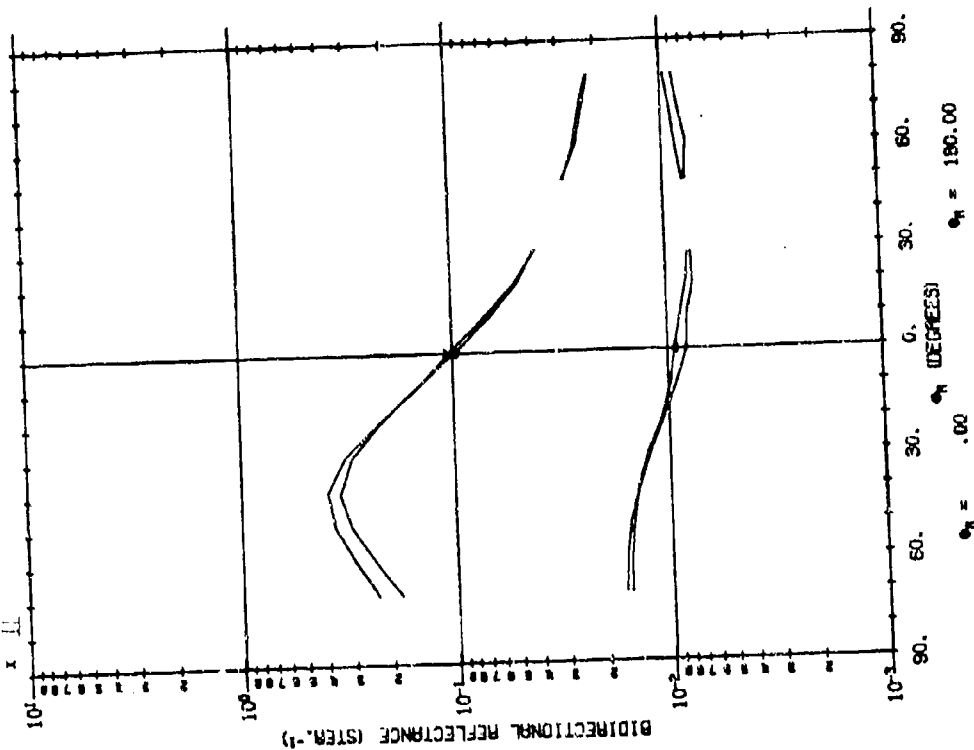


METAL



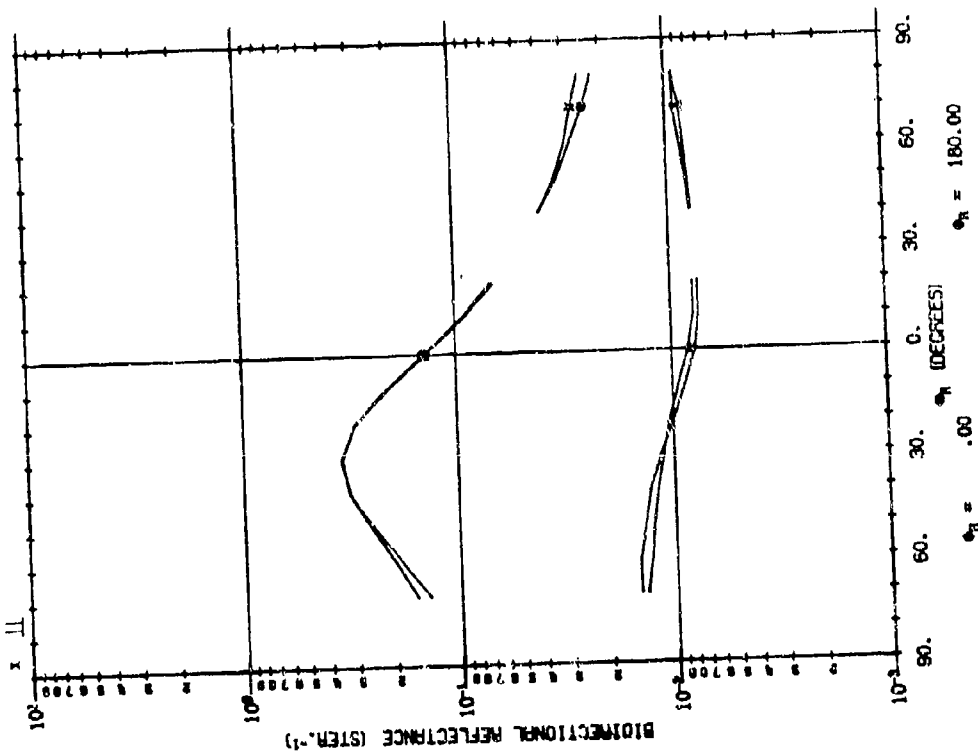
A01294 004 Bare Metal

$\epsilon_1 = 40.00$   
 $\phi_1 = 180.00$   
 $\lambda = 0.63$



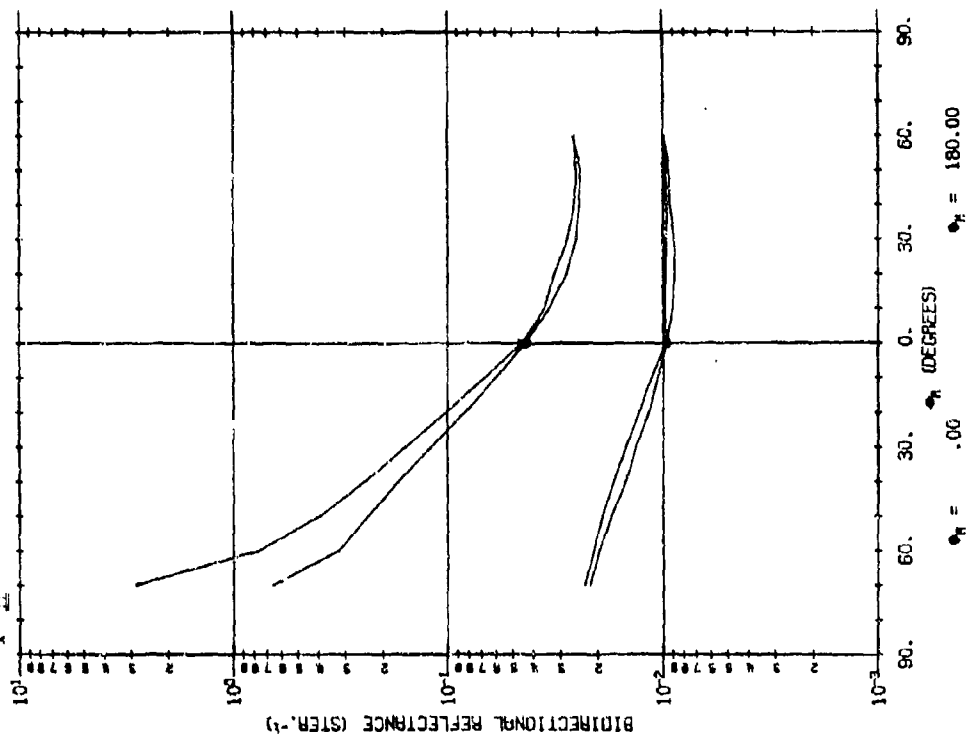
A01294 004 Bare Metal

$\epsilon_1 = 30.00$   
 $\phi_1 = 180.00$   
 $\lambda = 0.63$

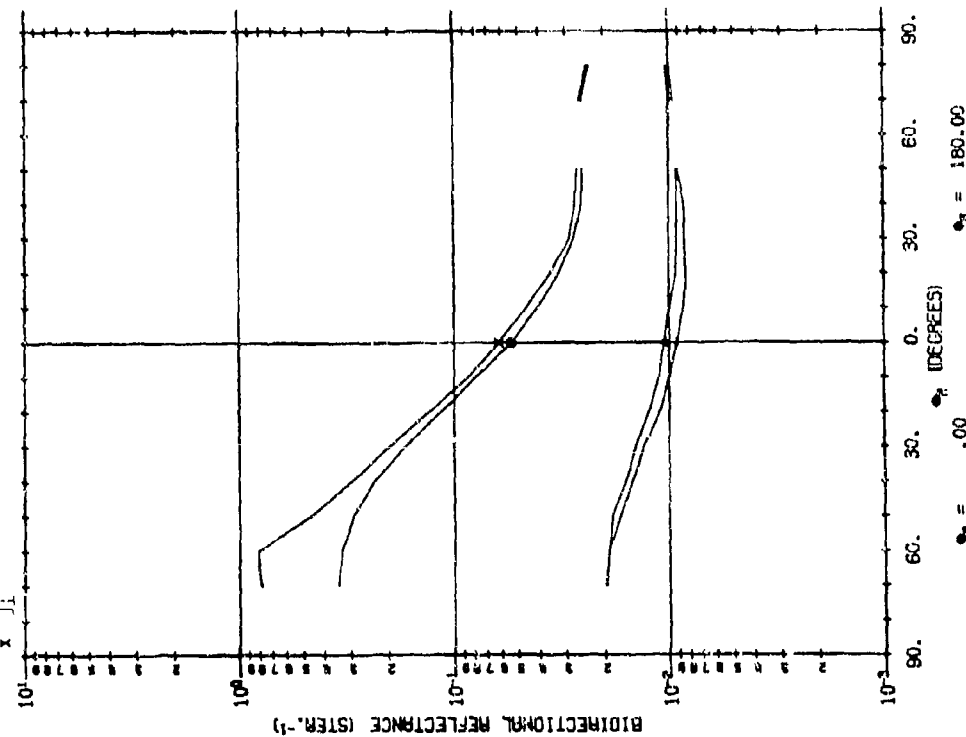


METAL

A01294 004 Bare Metal  
 $\epsilon_1 = 70.00$   
 $\epsilon_2 = 180.00$   
 $\phi_1 = 0.63$   
 $\phi_2 = 0.63$



A01294 004 Bare Metal  
 $\epsilon_1 = 50.00$   
 $\epsilon_2 = 180.00$   
 $\phi_1 = 0.63$   
 $\phi_2 = 0.63$

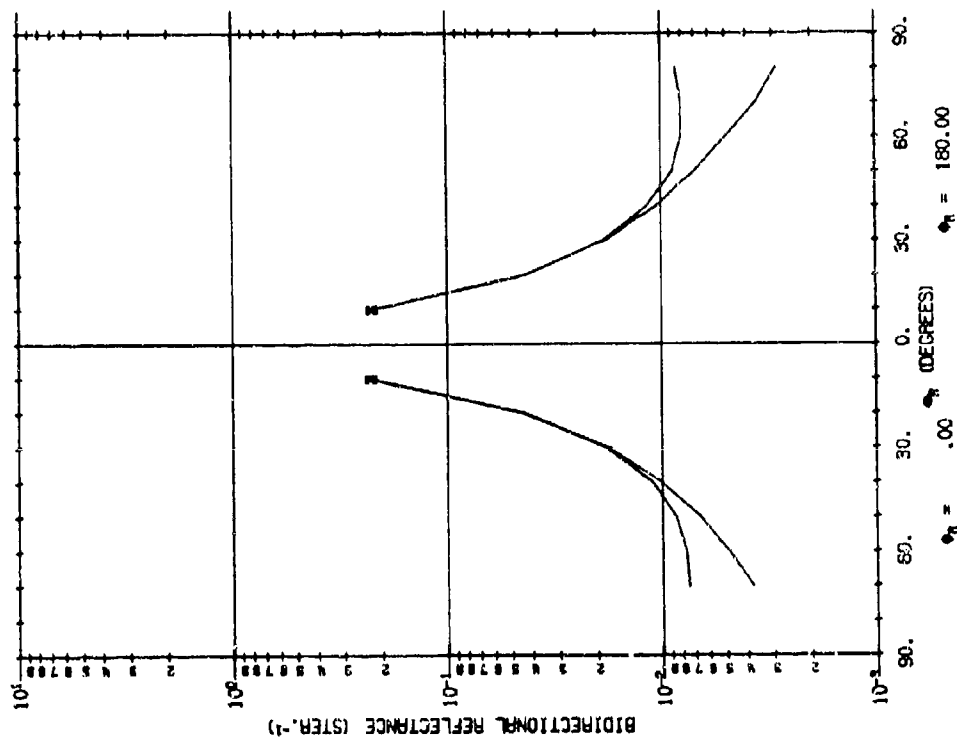




R01336 001

ALCLAD ALUMINUM PANEL

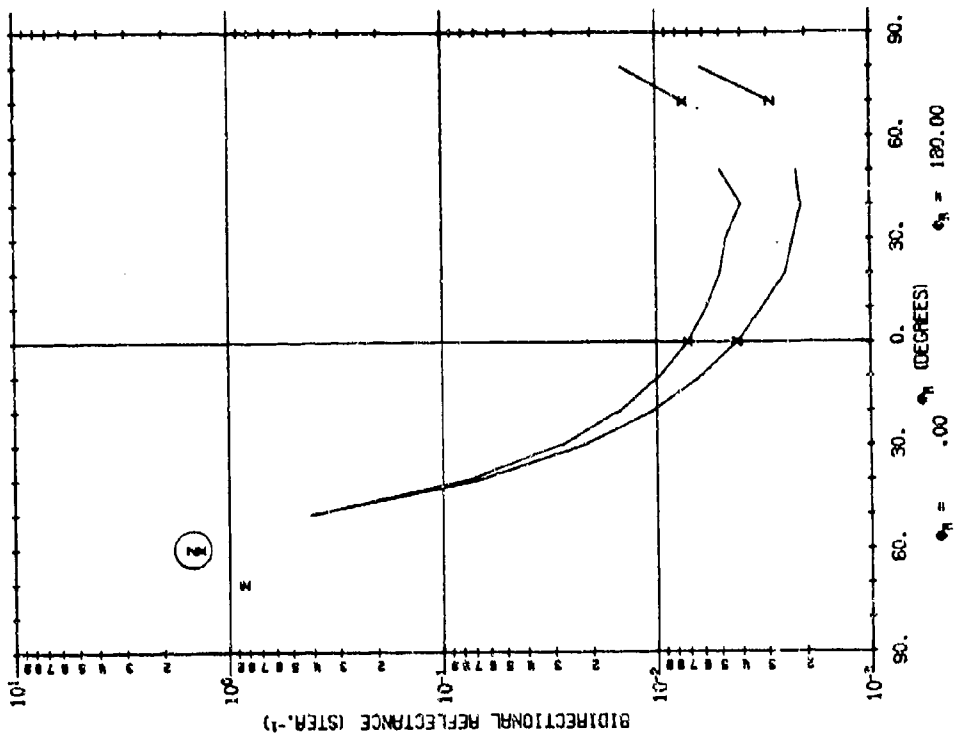
$\epsilon_1 = 0.0$   
 $\epsilon_2 = 180.0$   
 $\lambda = 1.06$



R01336 001

ALCLAD ALUMINUM PANEL

$\epsilon_1 = 60.0$   
 $\epsilon_2 = 180.0$   
 $\lambda = 1.06$

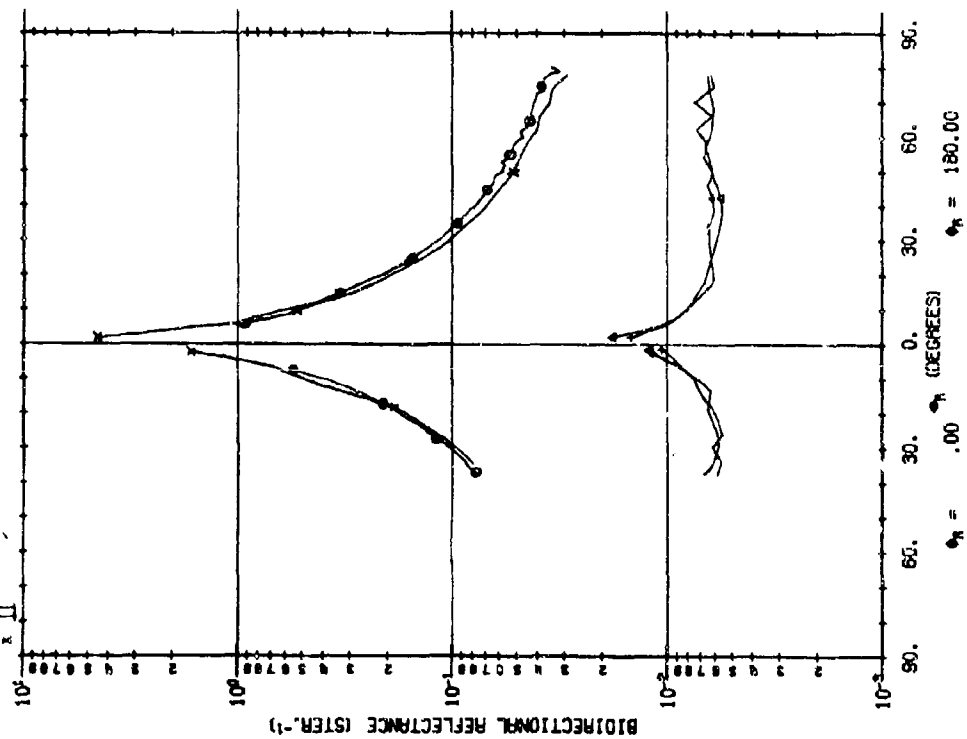


METAL

R01699 201

BARE METAL

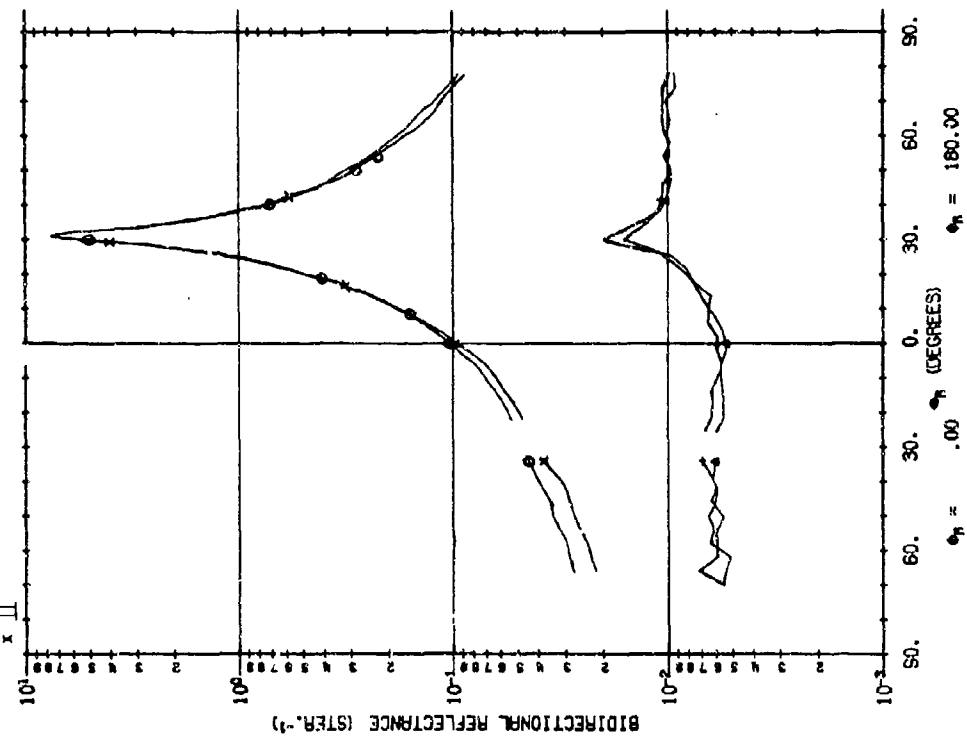
0 ||  $\theta_1 = 0.0$   
 + ||  $\theta_2 = 0.0$   
 Δ ||  $\theta_3 = 0.63$



R01699 201

BARE METAL

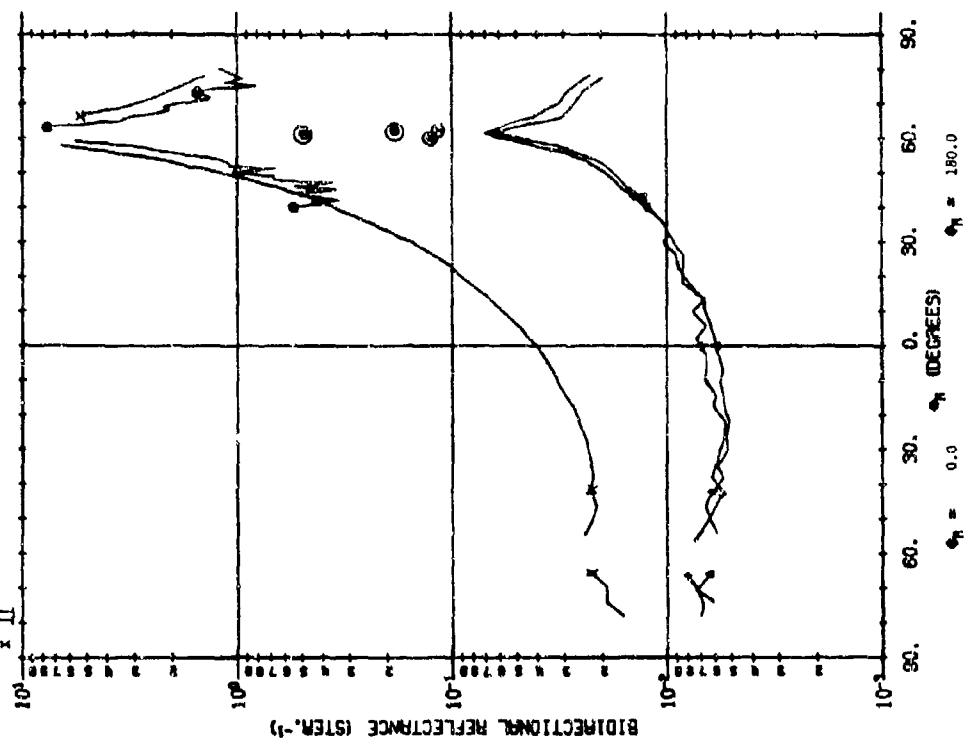
0 ||  $\theta_1 = 30.0$   
 + ||  $\theta_2 = 0.0$   
 Δ ||  $\theta_3 = 0.63$



A01699 201

BAKE METAL

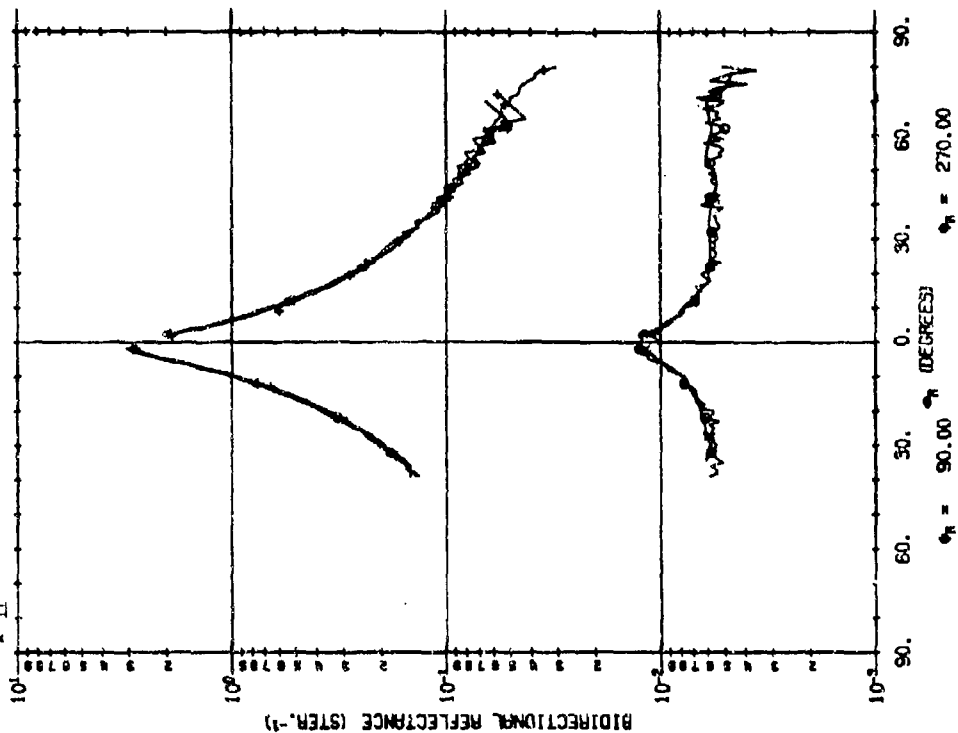
$\theta_i = 60.0$   
 $\phi_i = 0.0$   
 $\lambda = 0.63$



A01699 201

BAKE METAL

$\theta_i = 0.0$   
 $\phi_i = 0.0$   
 $\lambda = 0.63$

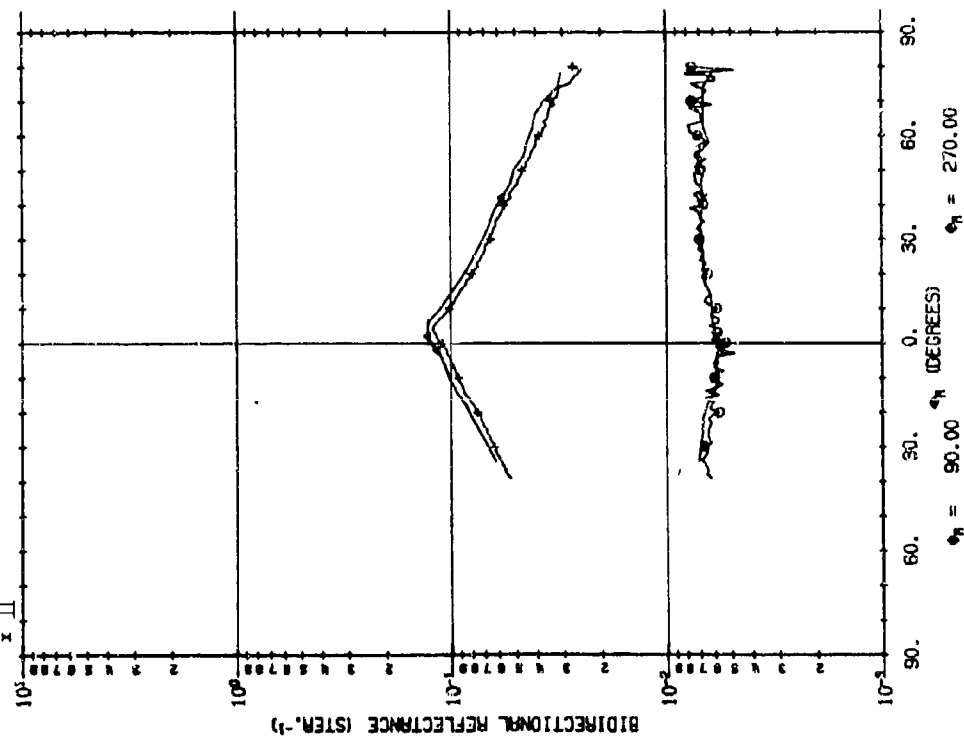


METAL

P01699 201

BARE METAL

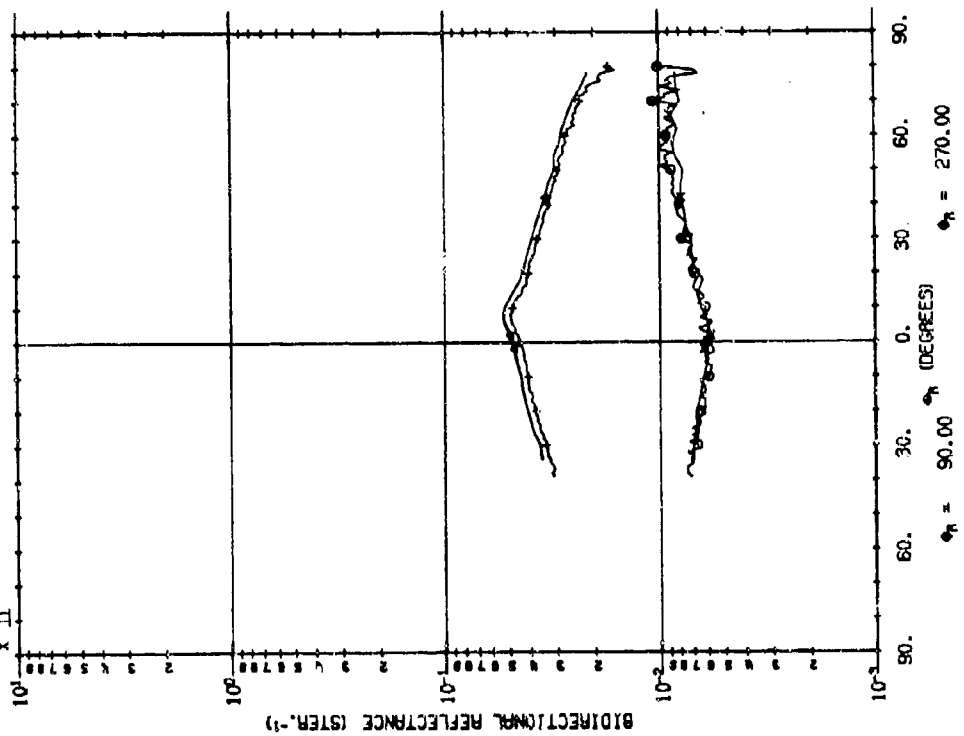
0 ||  $\theta_1 = 30.0$   
 + ||  $\phi_1 = 0.0$   
 Δ ||  $\lambda = 0.63$   
 x ||



P01699 201

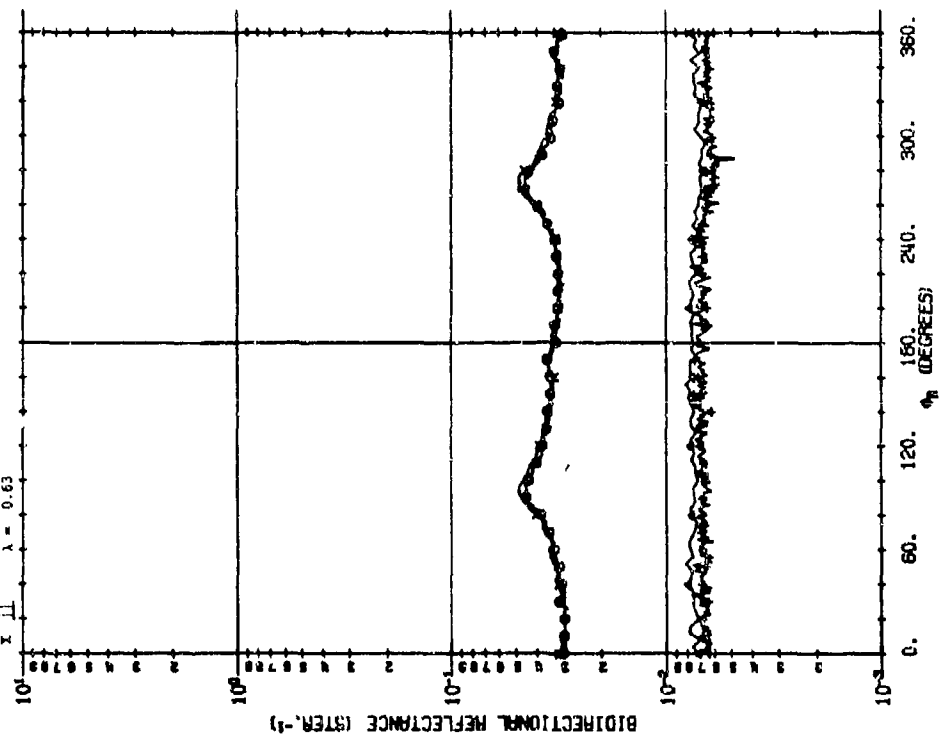
BARE METAL

0 ||  $\theta_1 = 60.0$   
 + ||  $\phi_1 = 0.0$   
 Δ ||  $\lambda = 0.63$   
 x ||



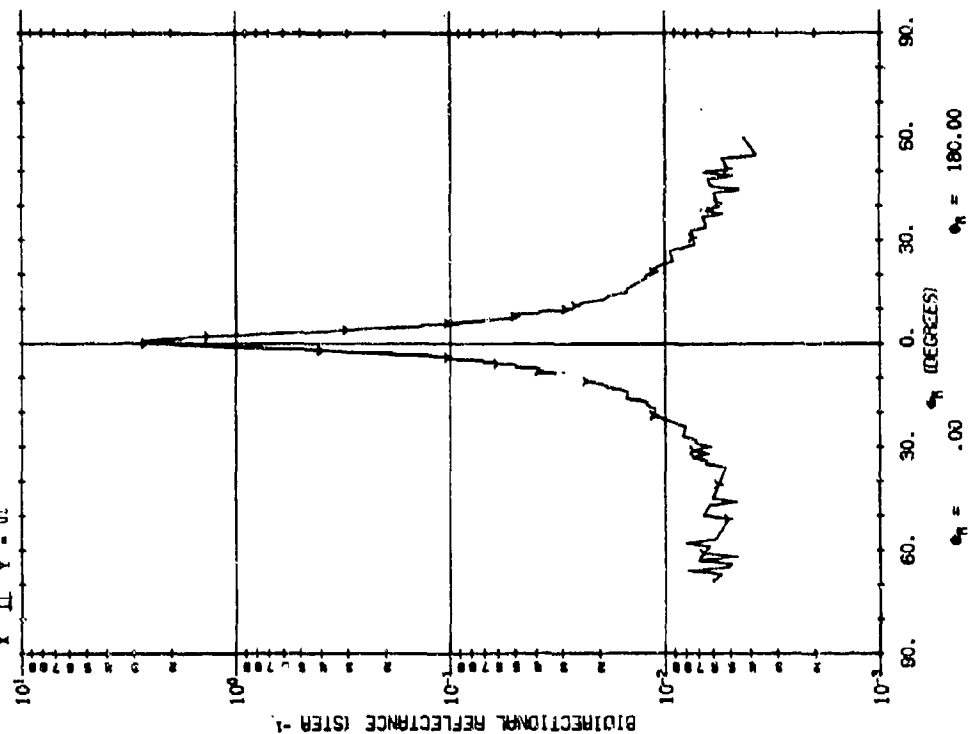
R01699 201

0 ||  $\theta_1 = 45.0$  BARE METAL  
 + ||  $\theta_1 = 47.0$ ,  $2\theta = 2.0$   
 Δ ||  $\theta_1 = \theta_r$   
 X ||  $\lambda = 0.63$



R01884 201

0 ||  $2\theta = 2.0$  Galvanized Pipe  
 + ||  $\theta_1 = \theta_r$  One and Five-Eighths Inch Diameter  
 Δ ||  $\lambda = 10.5$   
 X ||  $\gamma = \gamma_c$

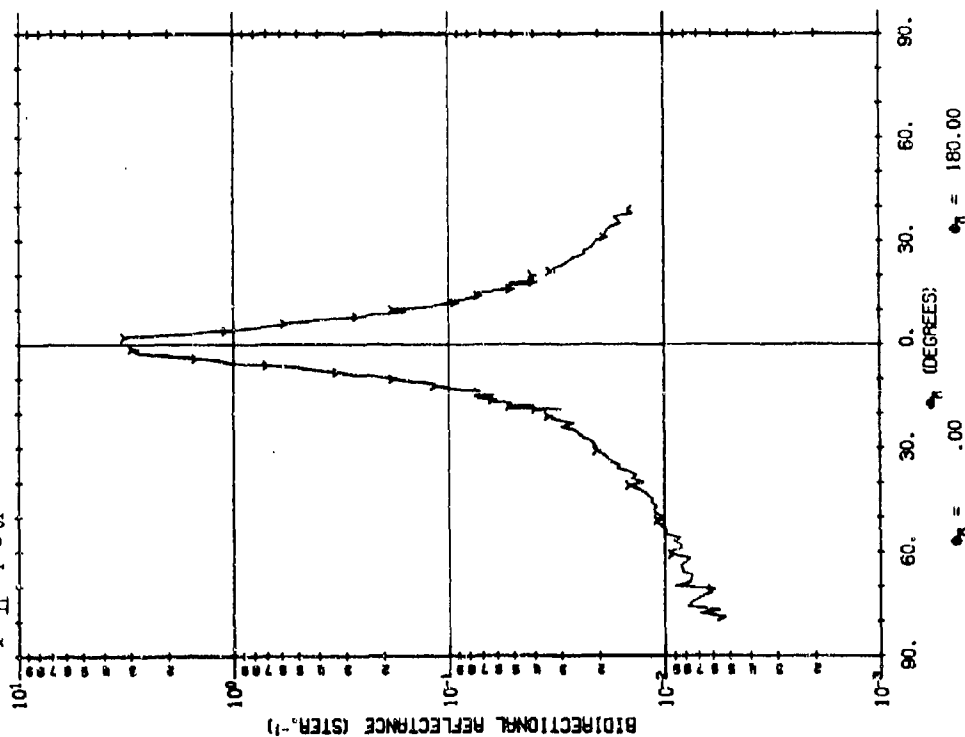


METAL

R01884 201

GALVANIZED PIPE  
One and Five-Eighths Inch Diameter

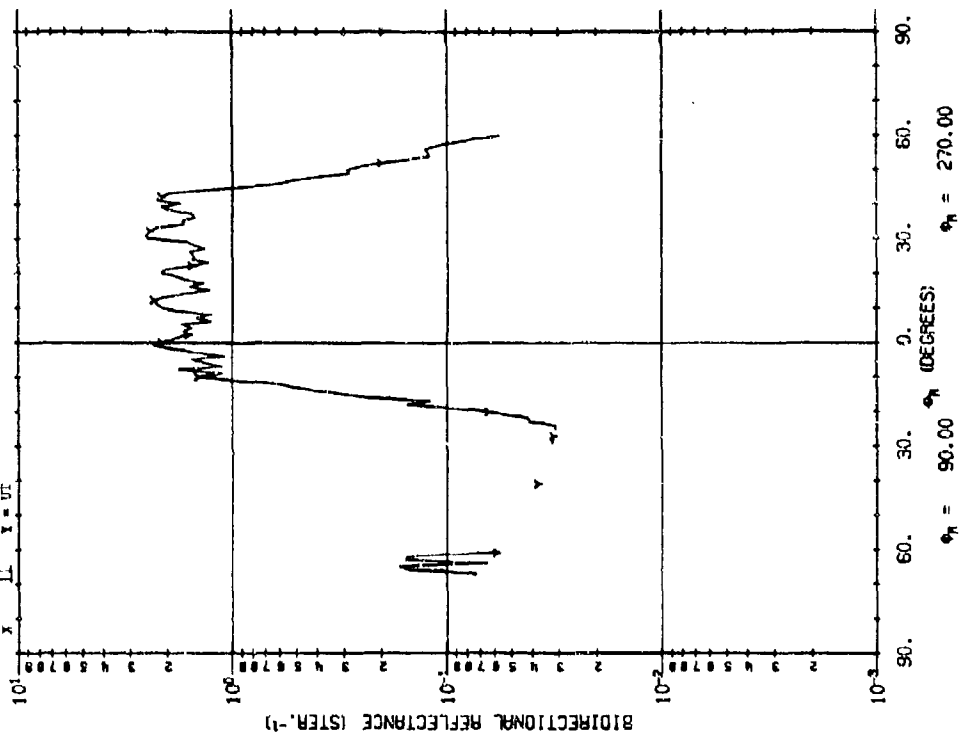
0 ||  $\phi_1 = 0.0$   
+ ||  $\phi_1 = 180.0$   
Δ ||  $\lambda = 10.6$   
X || Y = UT



R01884 201

GALVANIZED PIPE  
One and Five-Eighths Inch Diameter

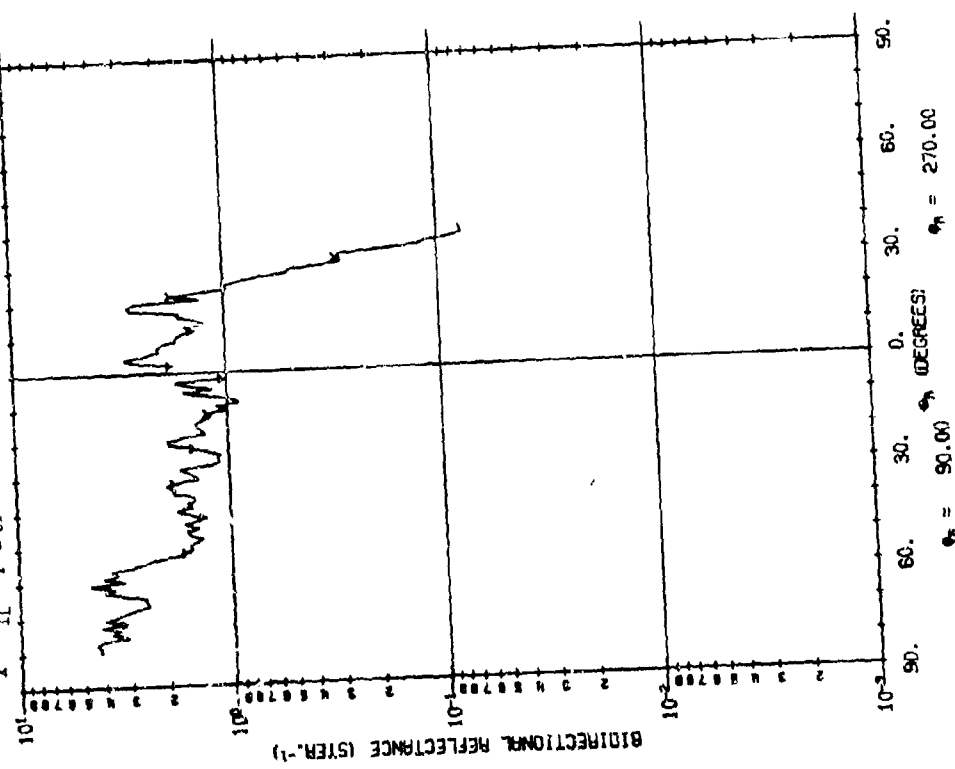
0 ||  $\phi_1 = 2.0$   
+ ||  $\phi_1 = 90.0$   
Δ ||  $\lambda = 10.6$   
X || Y = UT



AC1884 201

GALVANIZED PIPE  
One and Five-Eighths Inch Diameter

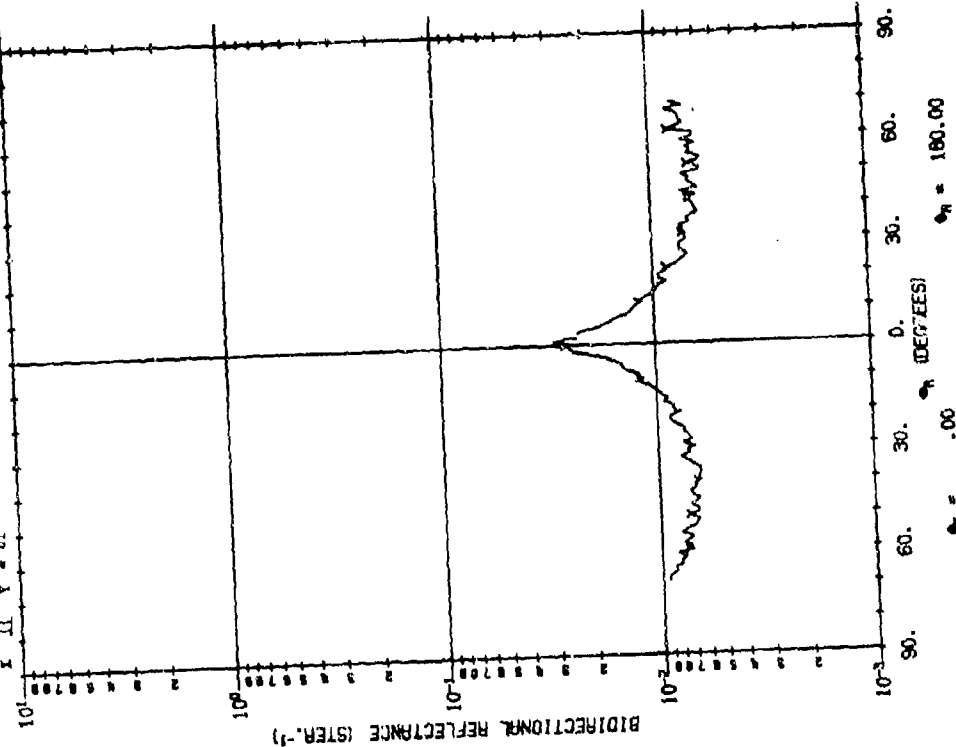
$\phi_1 = 0.0$   
 $\phi_2 = 0.0$   
 $\lambda = 10.6$   
 $\gamma = \text{UT}$



AC1885 201

GALVANIZED PIPE  
Two and Seven-Eighths Inch Diameter

$\phi_1 = 2.0$   
 $\phi_2 = 0.0$   
 $\lambda = 10.6$   
 $\gamma = \text{UT}$

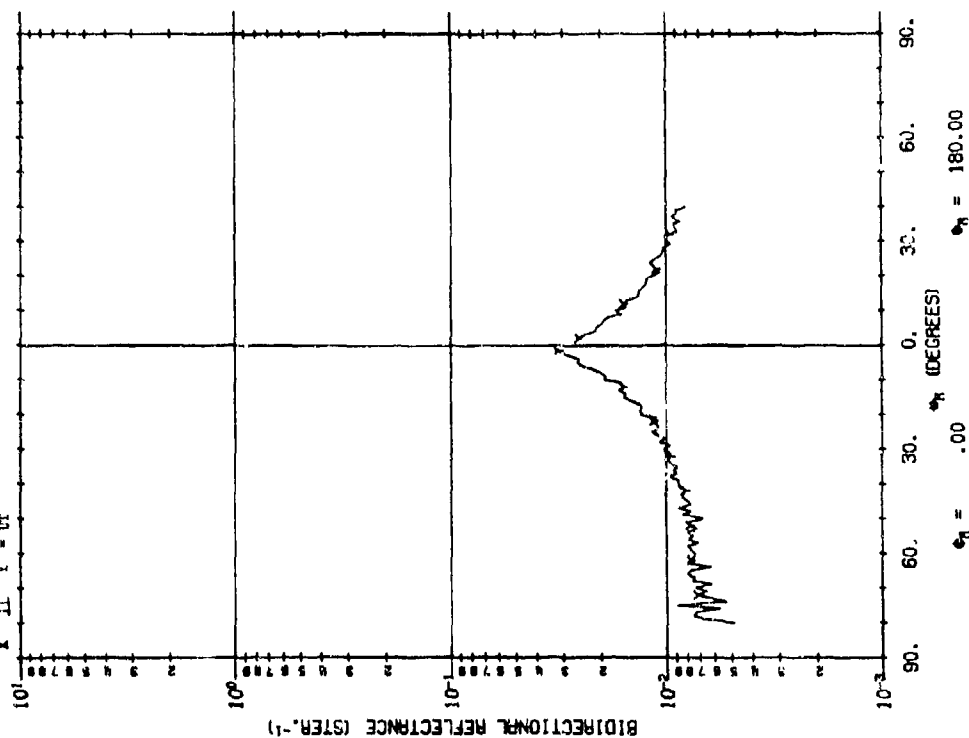


METAL

A01885 201

Galvanized Pipe  
Two and Seven-Eighths Inch Diameter

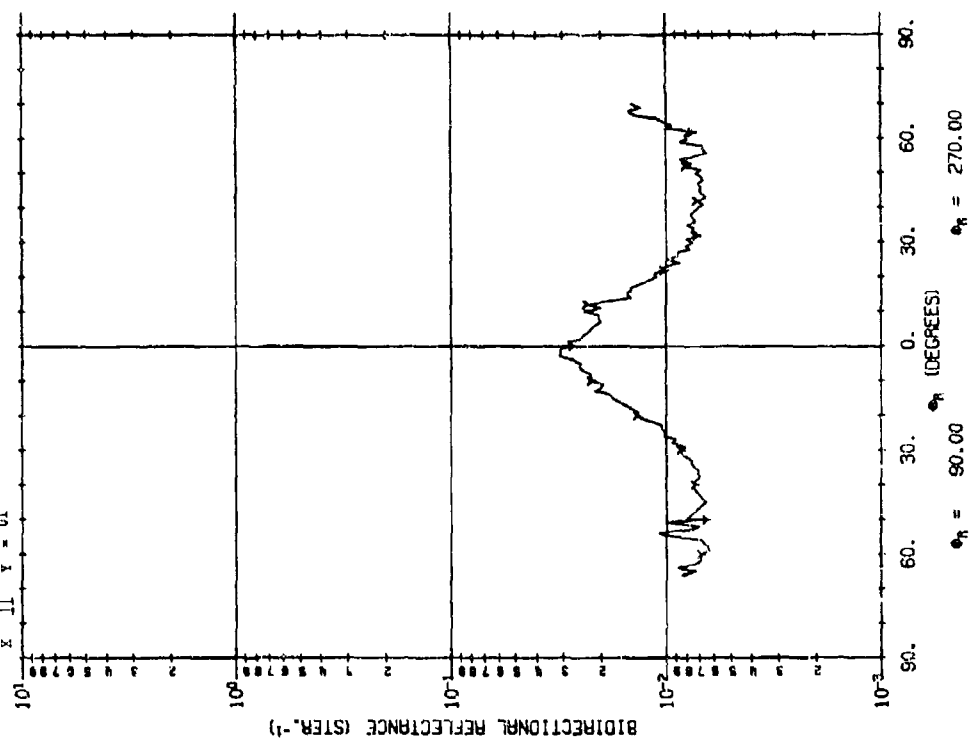
$\phi_1 = 0.0$   
 $\phi_2 = 180.0$   
 $\lambda = 10.6$   
 $X = Y = Z = UT$



A01885 201

Galvanized Pipe  
Two and Seven-Eighths Inch Diameter

$\phi_1 = 2.0$   
 $\phi_2 = 0$   
 $\lambda = 10.6$   
 $X = Y = Z = UT$

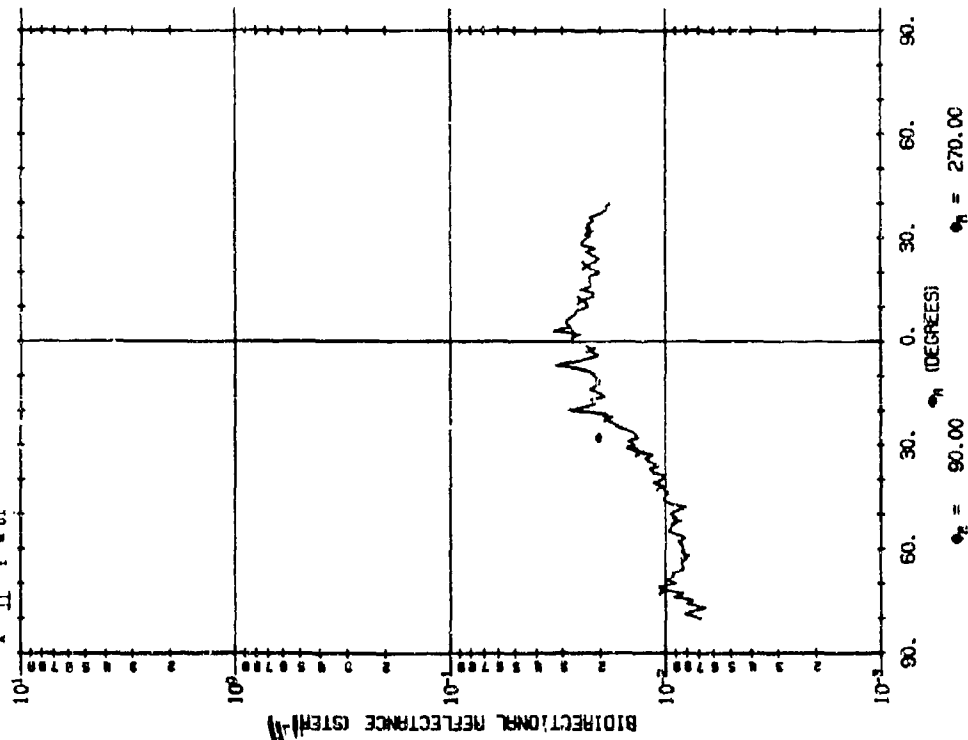




R01885 201

Galvanized Pipe  
Two and Seven-Eighths Inch Diameter

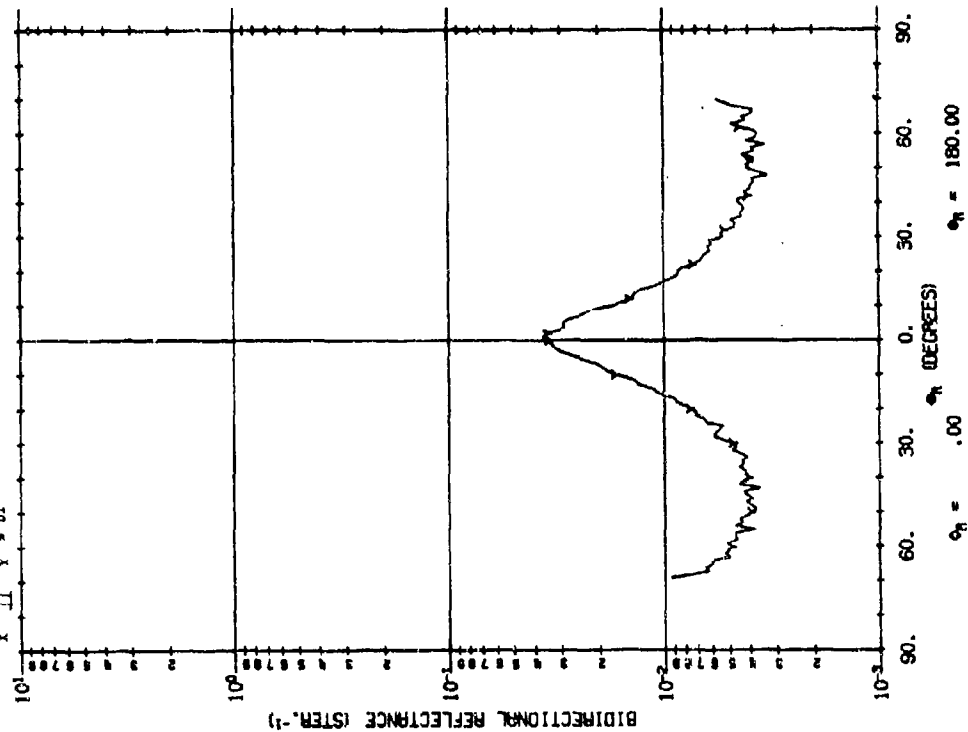
$\theta_1 = 0.0$   
+  $\theta_1 = 270.0$   
 $\Delta$   $\theta_1 = 10.6$   
X  $\theta_1 = 0.0$



R01886 201

Galvanized Pipe  
Three and One Half Inch Diameter

$\theta_1 = 2.0$   
+  $\theta_1 = 17$   
 $\Delta$   $\theta_1 = 10.6$   
X  $\theta_1 = 0.0$

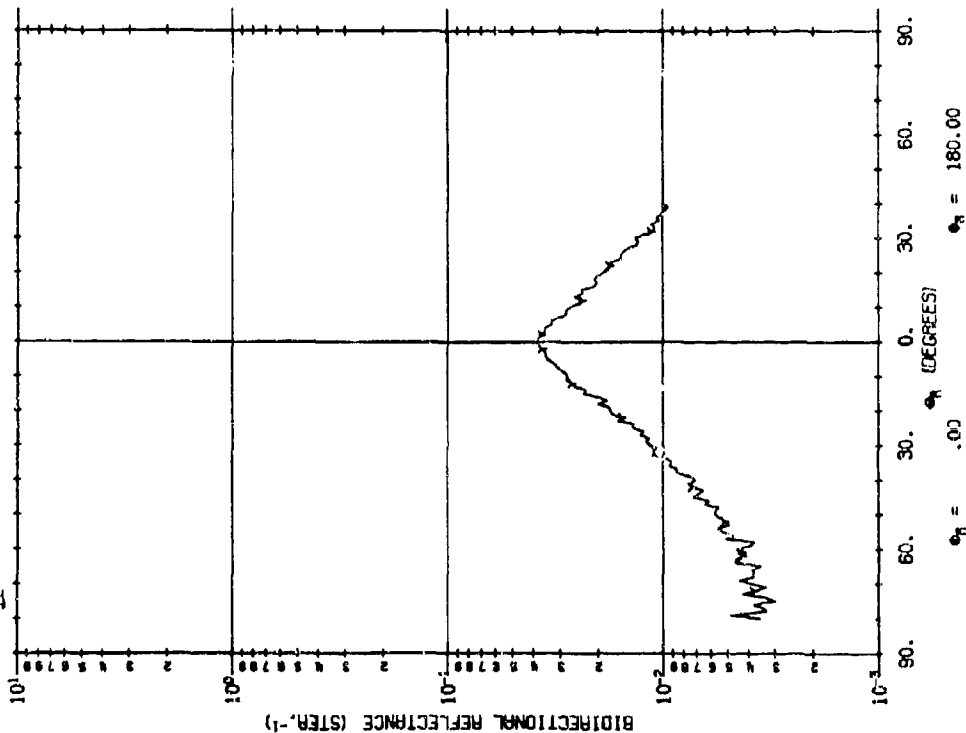


METAL

A01886 201

Galvanized Pipe  
Three and One Half Inch Diameter

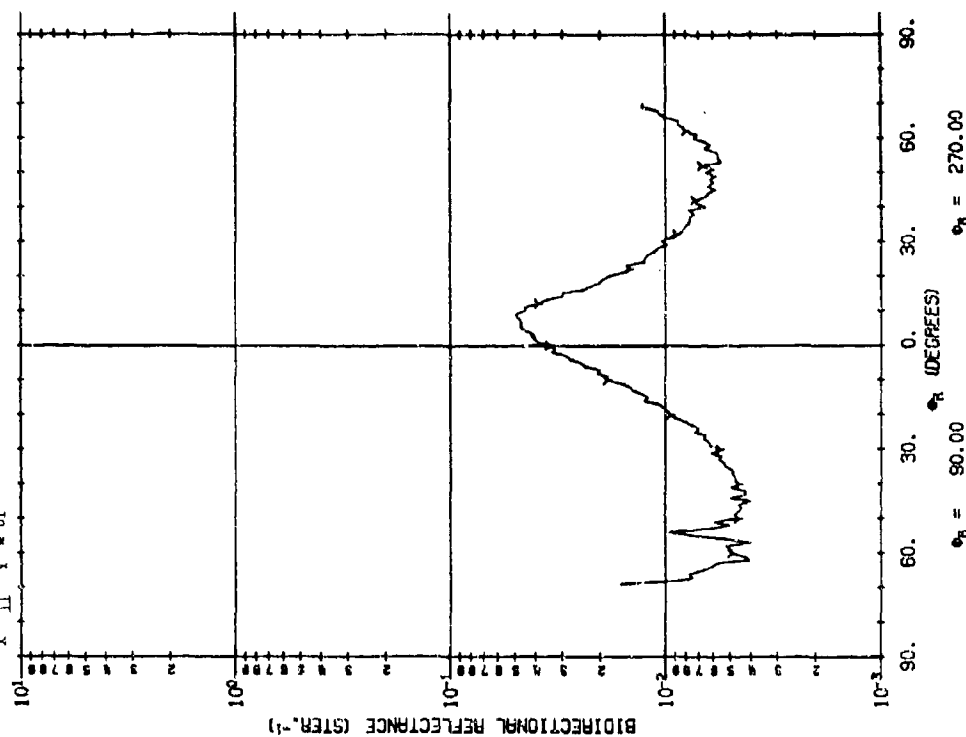
$\theta_i = 0.0$   
 $\phi_i = 120.0$   
 $\lambda = 10.6$   
X Y = UT



A01886 201

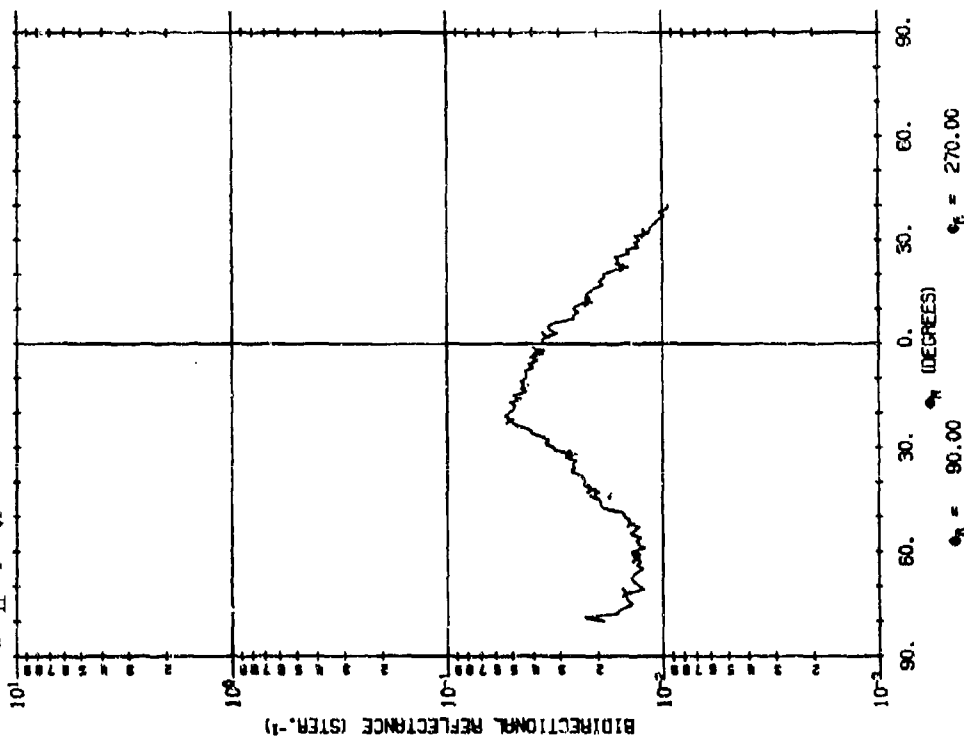
Galvanized Pipe  
Three and One Half Inch Diameter

$\theta_i = 2.0$   
 $\phi_i = 120.0$   
 $\lambda = 10.6$   
X Y = UT



R01886 201

Galvanized Pipe  
Three and One Half Inch Diameter  
0 ||  $\theta_1 = 0.0$   
+ ||  $\theta_2 = 270.0$   
x ||  $\lambda = 10.6$   
x || Y = VT



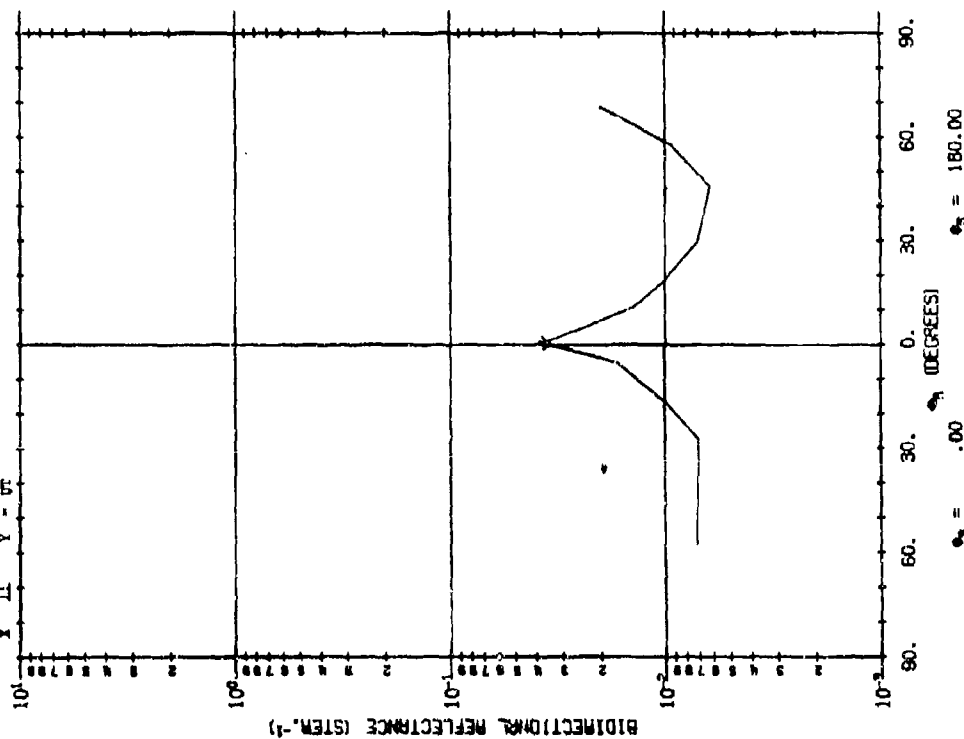
METAL

# MISCELLANEOUS

R01584 001

Cresote Treated Wood

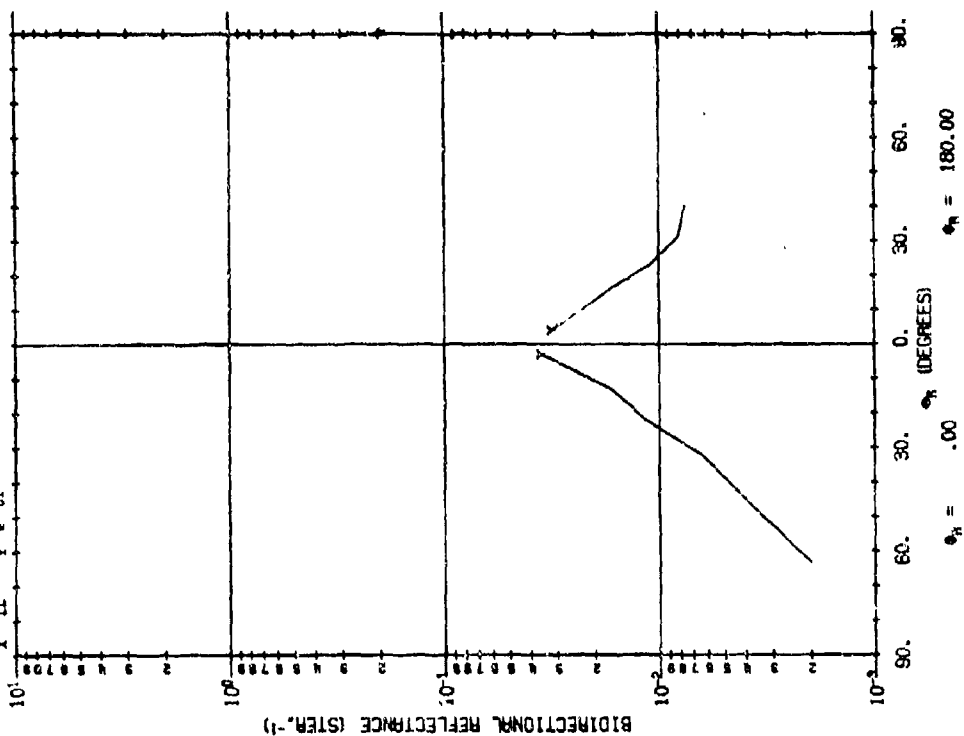
0 // 2 $\theta$  = 1.10  
+ //  $\theta_1$  =  $\theta_r$   
A //  $\lambda$  = 10.6  
X // Y = VT



R01584 001

Cresote Treated Wood

0 //  $\theta_1$  = 0.0  
+ //  $\theta_1$  = 180.0  
Z //  $\lambda$  = 10.6  
X // Y = VT

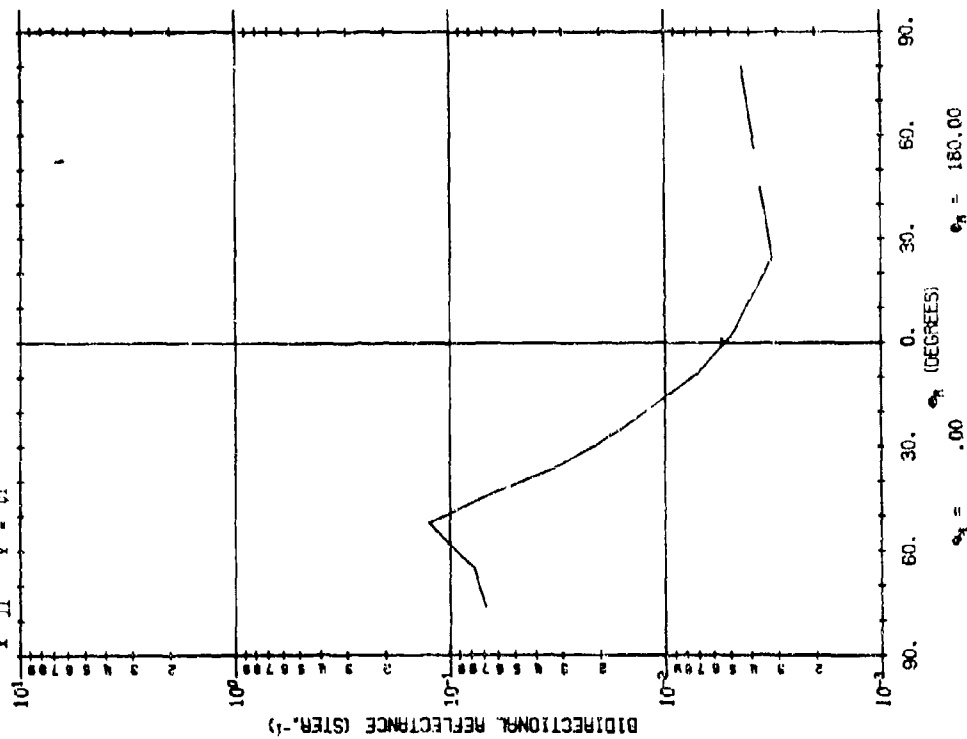


MISCELLANEOUS

R01584 001

Creosote Treated Wood

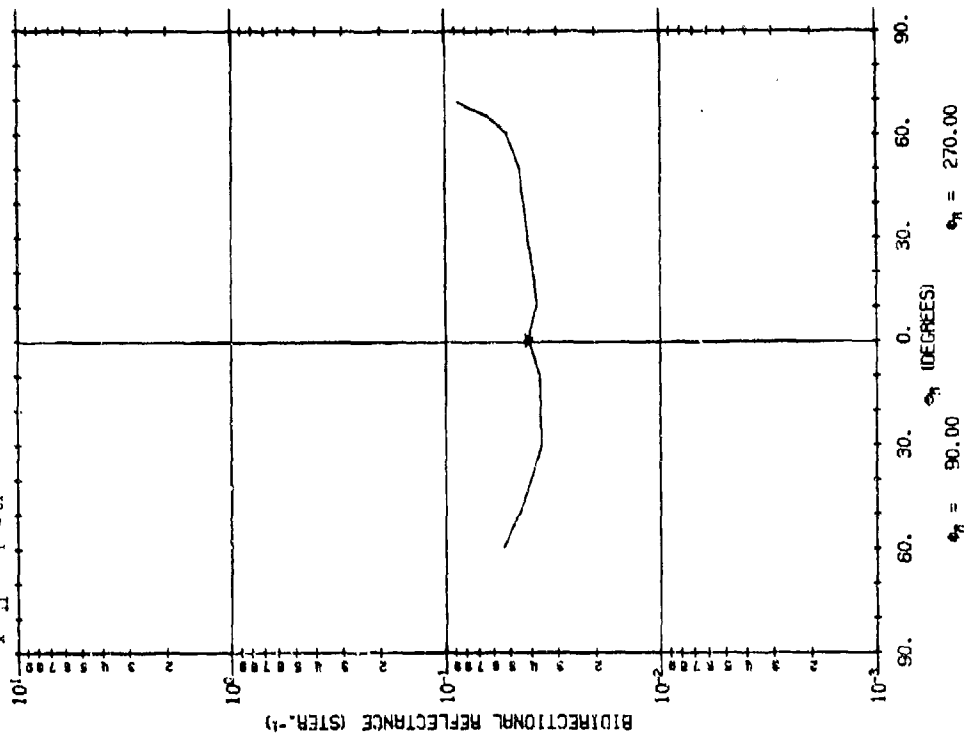
$\theta_1 = 50.0$   
 $\phi_1 = 180.0$   
 $\lambda = 10.6$   
 $\chi = 0.0$



R01584 001

Creosote Treated Wood

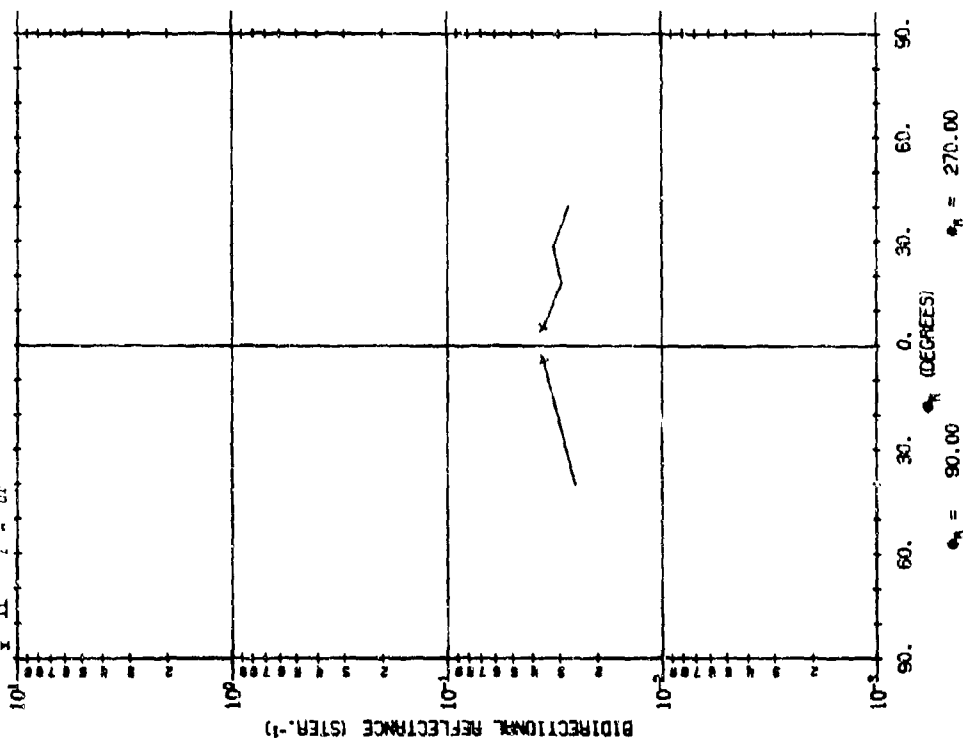
$\theta_1 = 1.10$   
 $\phi_1 = 0.0$   
 $\lambda = 10.6$   
 $\chi = 0.0$



R01584 001

Creosote Treated Wood

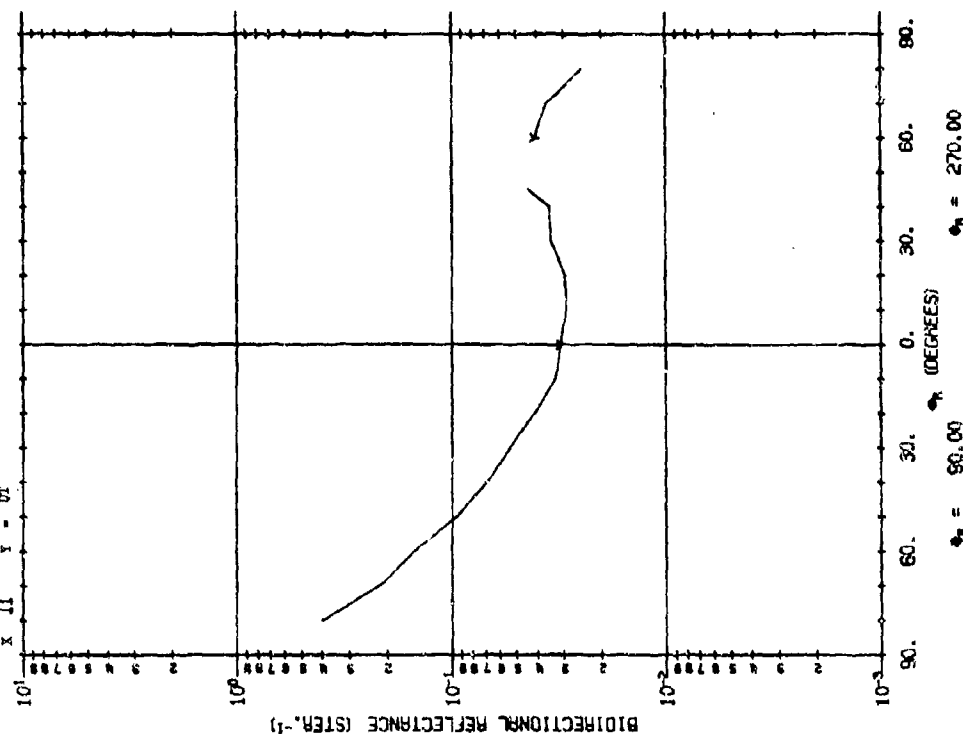
0 ||  $\theta_1 = 0.0$   
 + ||  $\phi_1 = 270.0$   
 Δ ||  $\lambda = 10.6$   
 x ||  $\tau = 07$



R01584 001

Creosote Treated Wood

0 ||  $\theta_1 = 50.0$   
 + ||  $\phi_1 = 270.0$   
 Δ ||  $\lambda = 10.6$   
 x ||  $\tau = 07$

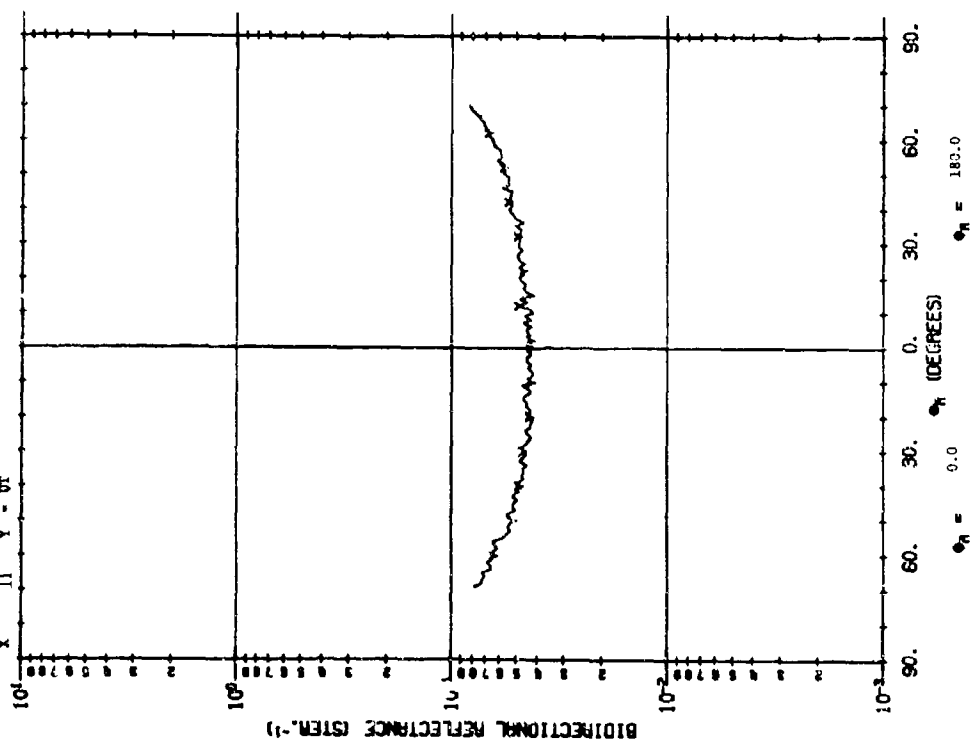


MISCELLANEOUS

A01921 101

Pressed Cork

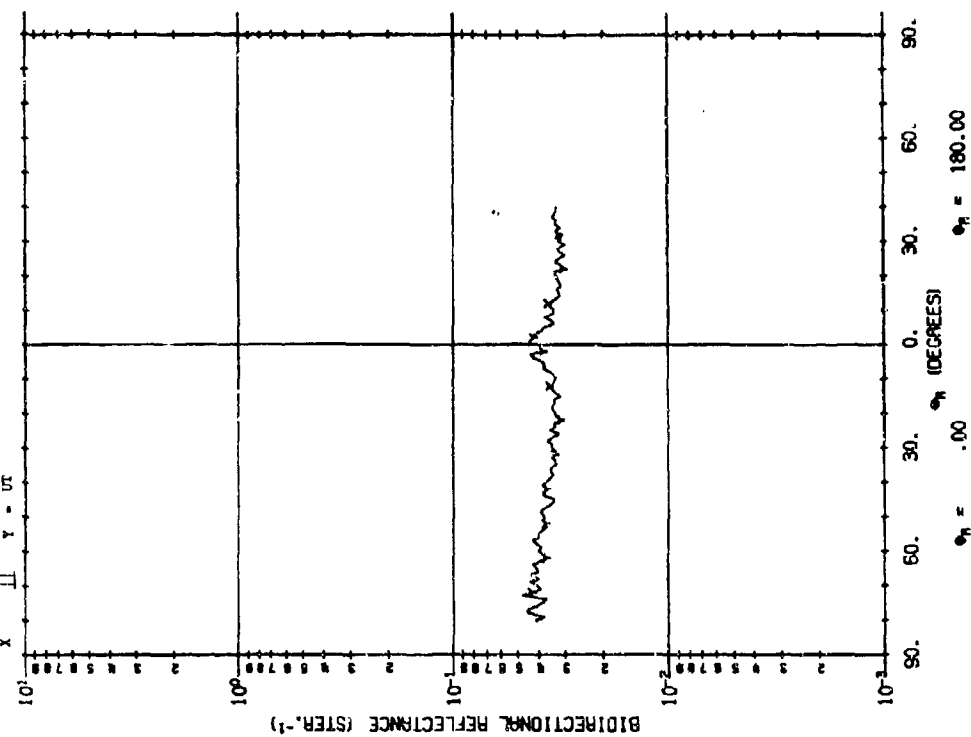
0 ||  $2\theta = 2.0$   
 + ||  $\phi_1 = \phi_c$   
 $\Delta$  ||  $\lambda = 10.6$   
 X ||  $Y = UT$



A01921 101

Pressed Cork

0 ||  $\phi_1 = 0.0$   
 + ||  $\phi_2 = 180.0$   
 $\Delta$  ||  $\lambda = 10.6$   
 X ||  $Y = UT$

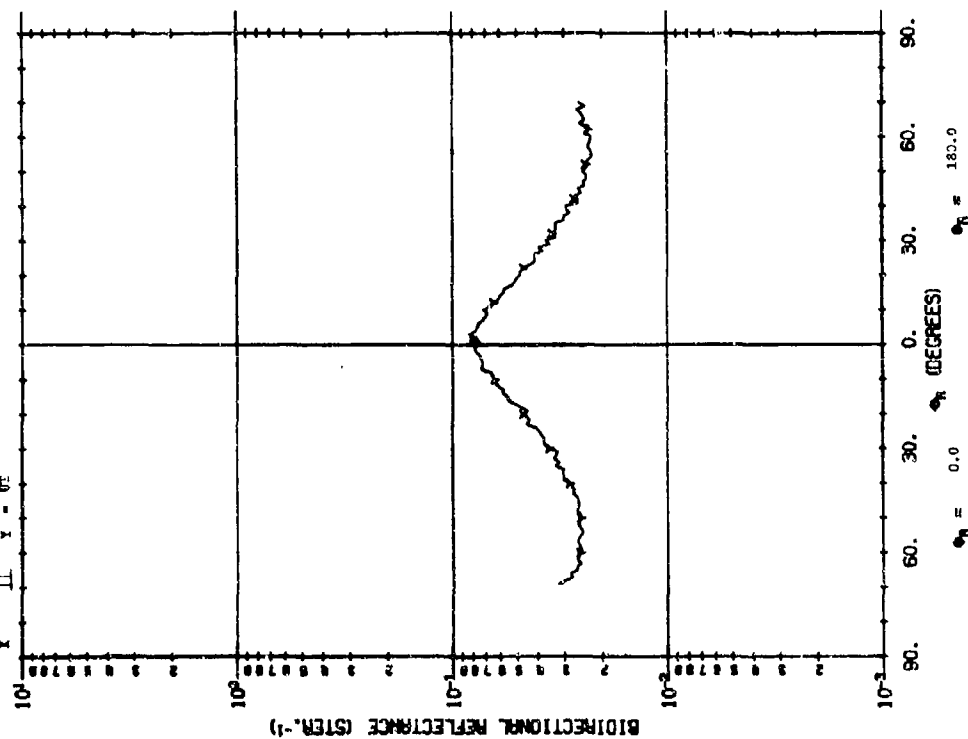




R01923 101

White Posterboard

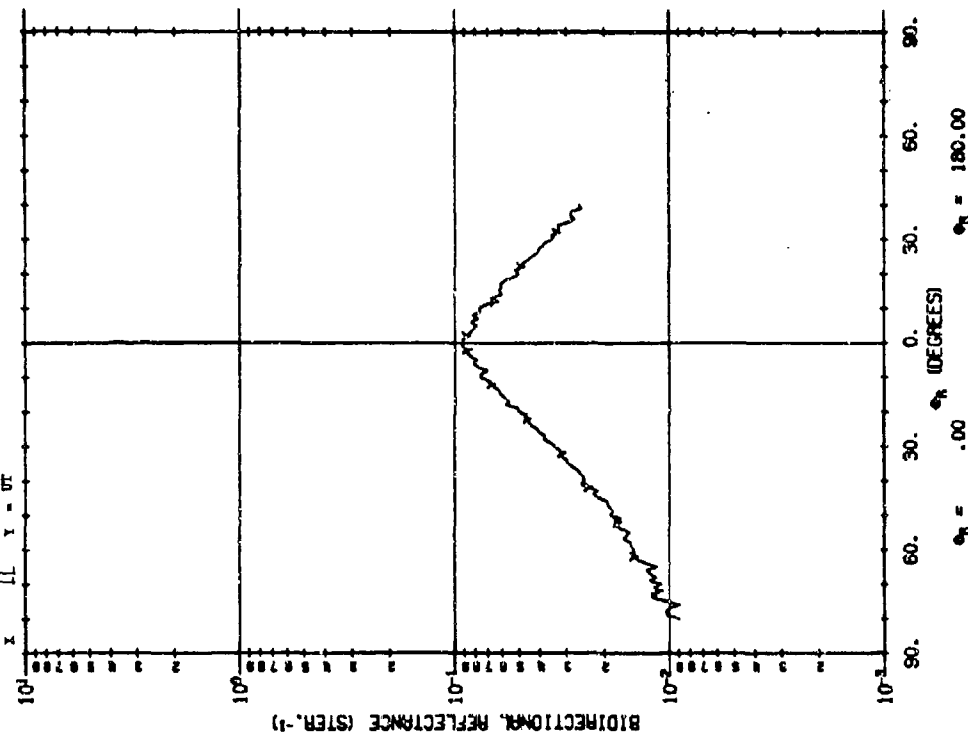
0 || 23 = 2.0  
+ || ||  $\phi_L = \phi_T$   
Δ || ||  $\lambda = 10.6$   
X || ||  $\gamma = 0^\circ$



R01923 101

White Posterboard

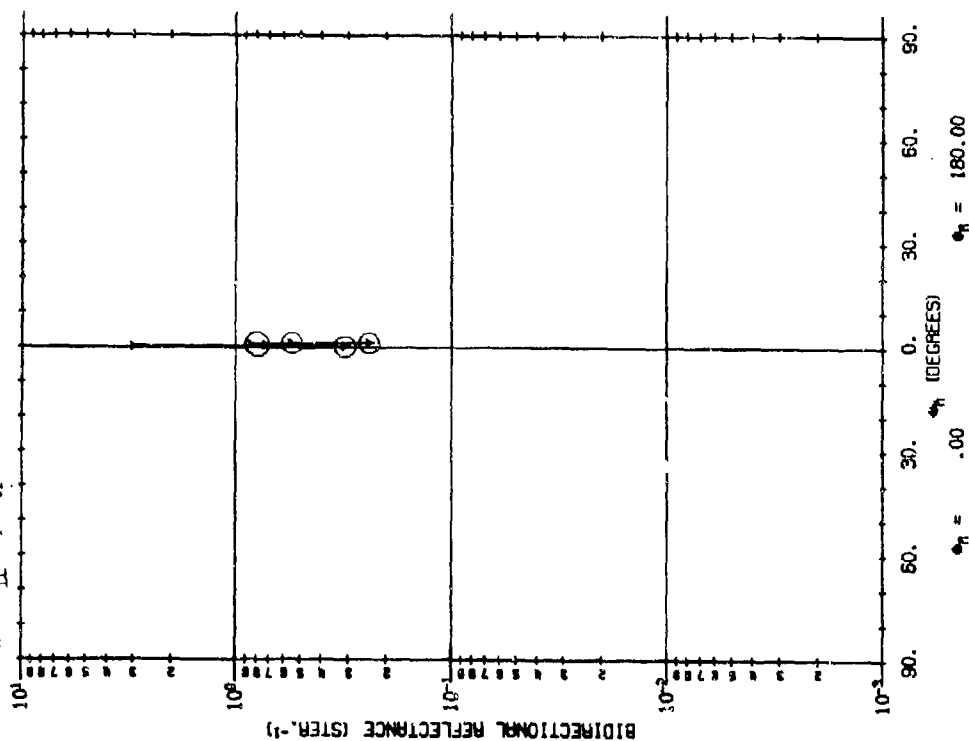
0 ||  $\phi_L = 0.0$   
+ || ||  $\phi_T = 180.0$   
Δ || ||  $\lambda = 10.6$   
X || ||  $\gamma = 0^\circ$



MISCELLANEOUS

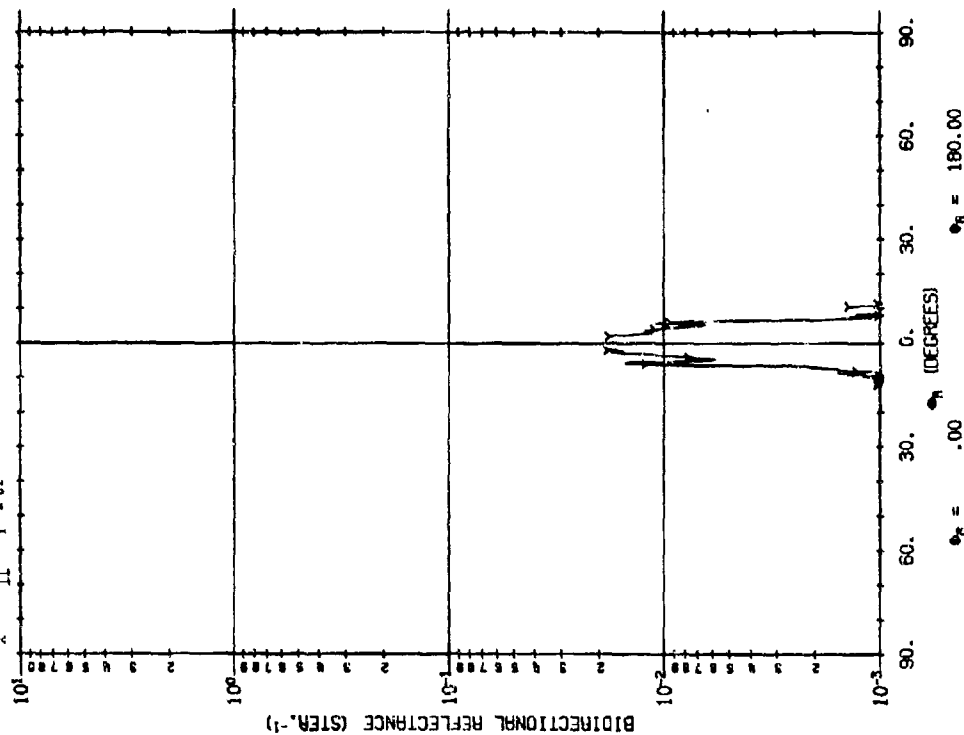
A01925 101  
 0 11 2 $\theta$  = 2.0  
 + 11  
 $\Delta$  11  $\phi_1 = \phi_r$   
 X 11  $\lambda = 10.6$   
 Y = VT

Acrylic Plexiglass



A01925 101  
 0 11  $\phi_1 = 0.0$   
 + 11  $\phi_r = 180.0$   
 $\Delta$  11  $\lambda = 10.6$   
 X Y = VT

Acrylic Plexiglass





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